

NASA Contractor Report 177982

**AERODYNAMIC CHARACTERISTICS
OF A PROPULSIVE WING/CANARD
CONCEPT AT STOL SPEEDS**

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CHARACTERISTICS OF A PROPULSIVE WING-CANARD
CONCEPT AT STOL SPEEDS Interim Report
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✓
V. R. Stewart

**Rockwell International Corporation
Columbus, Ohio 43216**

**Contract NAS1-17171
November 1985**



**National Aeronautics and
Space Administration**

**Langley Research Center
Hampton, Virginia 23665**

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ABSTRACT

A full span model of a wing/canard concept representing a fighter configuration has been tested at STOL conditions in the NASA Langley 4 by 7 Water Tunnel. The results of this test are presented, and comparisons are made to previous data of the same configuration tested as a semispan model. The potential of the propulsive wing/canard to develop very high lift coefficients was investigated with several nozzle spans (nozzle aspect ratios). Although longitudinal trim was not accomplished with the blowing distributions and configurations tested, the propulsive wing/canard appears to offer an approach to managing the large negative pitching moments associated with trailing edge flap blowing. Also presented are data showing the effects of large flap deflections and relative wing/canard positions. Presented in the appendix to the report are limited lateral-directional and ground effects data, as well as wing downwash measurements.

TABLE OF CONTENTS

<u>SECTION</u>	<u>TITLE</u>	<u>PAGE</u>
	ABSTRACT	11
	TABLE OF CONTENTS	111
	LIST OF FIGURES	1v
	LIST OF TABLES	v
	SYMBOLS	vi
1.0	INTRODUCTION	1
2.0	MODEL AND TEST PROCEDURE	2
	2.1 Model Description	2
	2.2 Model Instrumentation	10
	2.3 Model - Data Reduction	10
	2.4 Installation and Test Procedure	12
3.0	SUMMARY OF TEST RESULTS	14
	3.1 Effect of Nozzle Span	14
	3.2 Canard Effects	19
	3.3 Semi/Full Span Comparison	21
4.0	CONCLUSIONS	22
5.0	REFERENCES	24
	APPENDIX A - PRESENTATION OF BASIC TEST DATA	A-1

LIST OF FIGURES

<u>FIGURE NO.</u>	<u>TITLE</u>	<u>PAGE</u>
1	Model Sketch, Surface Locations	3
2	Model Sketch (Dimensions)	4
3	Schematic of Sting, Balance, and Air Supply	8
4	Model Air Supply Diagram	9
5	Surface Pressure Tap Locations	11
6	Full Span Model in LaRC 4 x 7 Meter Wind Tunnel Facility	13
7	Effect of Blowing Span on Total Lift Coefficient, Canard Off, $\alpha = 0$ Degrees	14
8	Effect of Blowing Span on Total Lift Coefficient, Canard Off, $\alpha = 8$ Degrees	15
9	Effect of Blowing Span on the Thrust Removed Lift Coefficient, Canard Off, $\alpha = 0$ Degrees	15
10	Effect of Blowing Span on the Thrust Removed Lift Coefficient, Canard Off, $\alpha = 8$ Degrees . .	16
11	Effect of Blowing Span on the Total Drag Coefficient, Canard Off, $\alpha = 0$ Degrees	17
12	Effect of Blowing Span on the Thrust Removed Drag Coefficient, Canard Off, $\alpha = 0$ Degrees . . .	17
13	Effect of Blowing Span on the Total Pitching Moment Coefficient, Canard Off, $\alpha = 0$ Degrees . .	18
14	Effect of Blowing Span on the Thrust Removed Pitching Moment Coefficient, Canard Off, $\alpha = 0$ Degrees	18
15	Effect of the Canard on the Pitching Moment Coefficient, $\alpha = 0$ Degrees	19
16	Effect of the Canard on the Pitching Moment Coefficient, $\alpha = 8$ Degrees	20
17	Effect of Canard Position on Total Lift Coefficient	21

LIST OF FIGURES (Concluded)

<u>FIGURE NO.</u>	<u>TITLE</u>	<u>PAGE</u>
18	Comparison of Semispan and Full Span Test Results, Wing/Canard/Body, $C_{\mu} = 0$, $\delta_F = 0$. .	23
19	Comparison of Semispan and Full Span Test Results, Wing/Body, $\delta_F = 15$ Degrees	23

LIST OF TABLES

<u>TABLE NO.</u>	<u>TITLE</u>	<u>PAGE</u>
1	Model Geometry	5
2	Airfoil Coordinates	6
3	Configuration Definition	12

SYMBOLS

	A	~	Aspect Ratio	~ b^2/S
	AF	~	Aft Force - balance	
	b	~	Span	
	b_{exposed}	~	Exposed Span	
	b_f	~	Flap Span	
BH/B	b_j	~	Jet Span/Exposed Span	
	BP	~	Butt Plane (B.P. = 0 at wing root)	
	$\bar{c}$	~	Mean Aerodynamic Chord	
CD	C_D	~	Drag Coefficient	~ $\frac{\text{Drag}}{qS}$
CDTR	$C_{D_{TR}}$	~	Thrust Removed Drag Coefficient	
CL	C_L	~	Lift Coefficient	~ $\frac{\text{Lift}}{qS}$
CLTR	$C_{L_{TR}}$	~	Thrust Removed Lift Coefficient	
CM	C_M	~	Pitching Moment Coefficient	~ $\frac{\text{Pitching Moment}}{qS \bar{c}}$
CMTR	$C_{M_{TR}}$	~	Thrust Removed Pitching Moment Coefficient	
	C_p	~	Pressure Coefficient	
CMU	C_μ	~	Blowing Coefficient	~ $\frac{\dot{m} V_j}{qS}$
CN	C_n	~	Yawing Moment Coefficient	
CROLL	C_ℓ	~	Rolling Moment Coefficient	
CY	C_y	~	Side Force Coefficient	
	FRL	~	Fuselage Reference Line	
	H	~	Height of FRL above Ground	
	K_b	~	Span Correlation Factor	

SYMBOLS (Concluded)

	M	~	Mach Number
	$\dot{m}$	~	Nozzle Mass Flow
	NF	~	Normal Force - Balance
	P_L	~	Local Static Pressure
	P_∞	~	Ambient Pressure
	q	~	Dynamic Pressure ~ $\frac{1}{2}\rho V^2$
	S	~	Reference Area
V_∞	V	~	Freestream Velocity
	V_j	~	Jet Velocity
	Y	~	Spanwise Measurement
	α	~	Angle of Attack of Fuselage
	ρ	~	Density of Air
DELC	δ_C	~	Canard Deflection
DELF	δ_F	~	Flap Deflection
	ϵ	~	Downwash Angle

Subscripts

c	~	Canard
N	~	Nozzle
w	~	Wing
TR	~	Thrust Removed

1.0 INTRODUCTION

Attainment of very short ground roll distances (approximately 400 feet) for takeoff and landing requires that operation at flight speeds of approximately 50 knots must be attainable. In today's fighter design, high thrust to weight ratios are required for maneuvering and high speed flight. If a concept can be developed which can utilize these thrust levels to augment the aerodynamic lift, then it may be possible to operate at these speeds.

One such concept involves the use of all or a large percentage of the engine exhaust ducted over the flap of the lifting surfaces. The blown flap or propulsive wing has been recognized as a method of producing large circulation lift coefficients. However, these large induced circulation lift coefficients, as well as the deflected thrust vector, react well aft on the wing and produce sizable nose-down pitching moments. The addition of a propulsive canard offers a possible conceptual design relief for these sizable trim requirements. The displacement of a portion of the thrust forward, as well as the induced circulation lift on the canard, tend to balance the moment due to the aft loading on the wing.

An earlier program done on this propulsive wing/canard configuration was primarily a cruise and maneuvering investigation. During that study (ref. 1), it was demonstrated that the concept would provide an improved maneuvering lift/drag (L/D) at transonic speeds. Also, the earlier study indicated quite large circulation lift coefficients at relatively low flap deflections. The study was done with a semispan model and tests were conducted in the Ames 14 foot Transonic Tunnel and in the Rockwell 7 by 10 foot low speed tunnel. Flap deflections in these tests were limited to a maximum of 15 degrees. The major configuration variable investigated was the effect of wing/canard relative locations. Analysis of that data showed that the best position for the low flap deflection ($\delta_f \leq 15$ degrees) and for all speeds ($M = 0.1$ to 0.9) was with the canard high relative to the wing. These test results were discussed in References 1 through 3.

The investigation of the propulsive wing/canard concept has continued with additional tests and analysis. The data have been extended to the higher flap deflections and into ground effects as required for STOL operation, see Reference 4.

This report covers this test phase of the propulsive wing/canard concept investigation in STOL conditions in the NASA Langley 4 by 7 Meter Tunnel. The major variables investigated were:

- (1) blown flap span
- (2) canard/wing relative location, and
- (3) flap deflection with large blowing coefficients.

2.0 MODEL AND TEST PROCEDURE

2.1 Model Description

The model is a full span wing/canard configuration. Both wing and canard have blown trailing edge flaps which can be deflected from zero to 60 degrees. The nozzle slots are at the flap hinge line (the 80 percent local chord position) and are perpendicular to the fuselage centerline. Figures 1 and 2 are model sketches presenting dimensional data. Table 1 presents a tabulation of the model geometry. The canard can be placed in one of three positions on the fuselage, and the wing can be placed in one of two positions on the fuselage, as shown in Figure 1. Figure 1 also shows the location of the downwash probe mounted one mean aerodynamic chord behind the wing.

The span of the nozzle slot on the wing was also variable. Provisions were made for the nozzle to blow either full span, half span, or a quarter span of the flap while maintaining approximately the same nozzle exit area. The nozzle was also always on the inboard portion of the wing. The canard nozzle was similarly configured except that only full span or half span configurations could be tested. When flap deflections were tested, the flap was deflected as a full span flap regardless of the extent of nozzle span. Wing and canard airfoil coordinates are tabulated in Table 2.

Air for the blowing slots is introduced to the model through a pressure reducer valve to the main fuselage plenum (see Figure 3). From the main fuselage plenum, air is ducted to four smaller plenums in the fuselage, one each for two canards and two wings.

Figure 3 also shows the balance installation and the manner in which air is supplied across the balance. The wings and canards plug into the fuselage plenums, allowing the air to flow to the wing or canard high pressure plenums where the flow is stagnated and ducted through pressure drop supply ducts to the low pressure plenums which supply the nozzle slots. The air supply system provided nearly uniform jet exit velocity with span. Figure 4 is a sketch showing the model air supply from the LaRC supply pipe to the nozzle exits. Flow split is adjustable to each of the four blowing surfaces by use of valves located on the main fuselage plenum. High pressure air brought onto the model in this manner results in balance constants which are determined by calibration with the air pipe in place and by a pressure tare which is a function of model internal geometry. These calibrations and tares are a part of the standard, NASA provided, data reduction capability.

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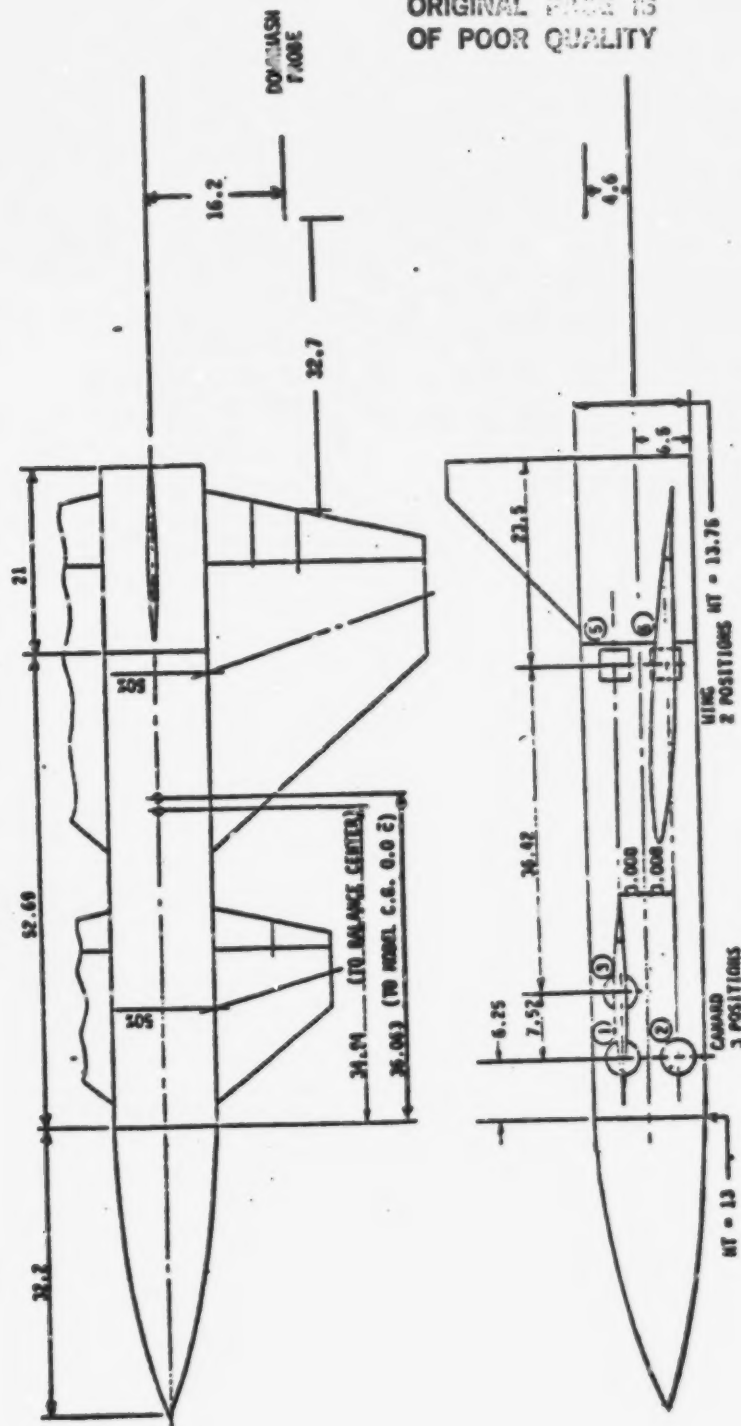


Figure 1. Model Sketch, Surface Locations

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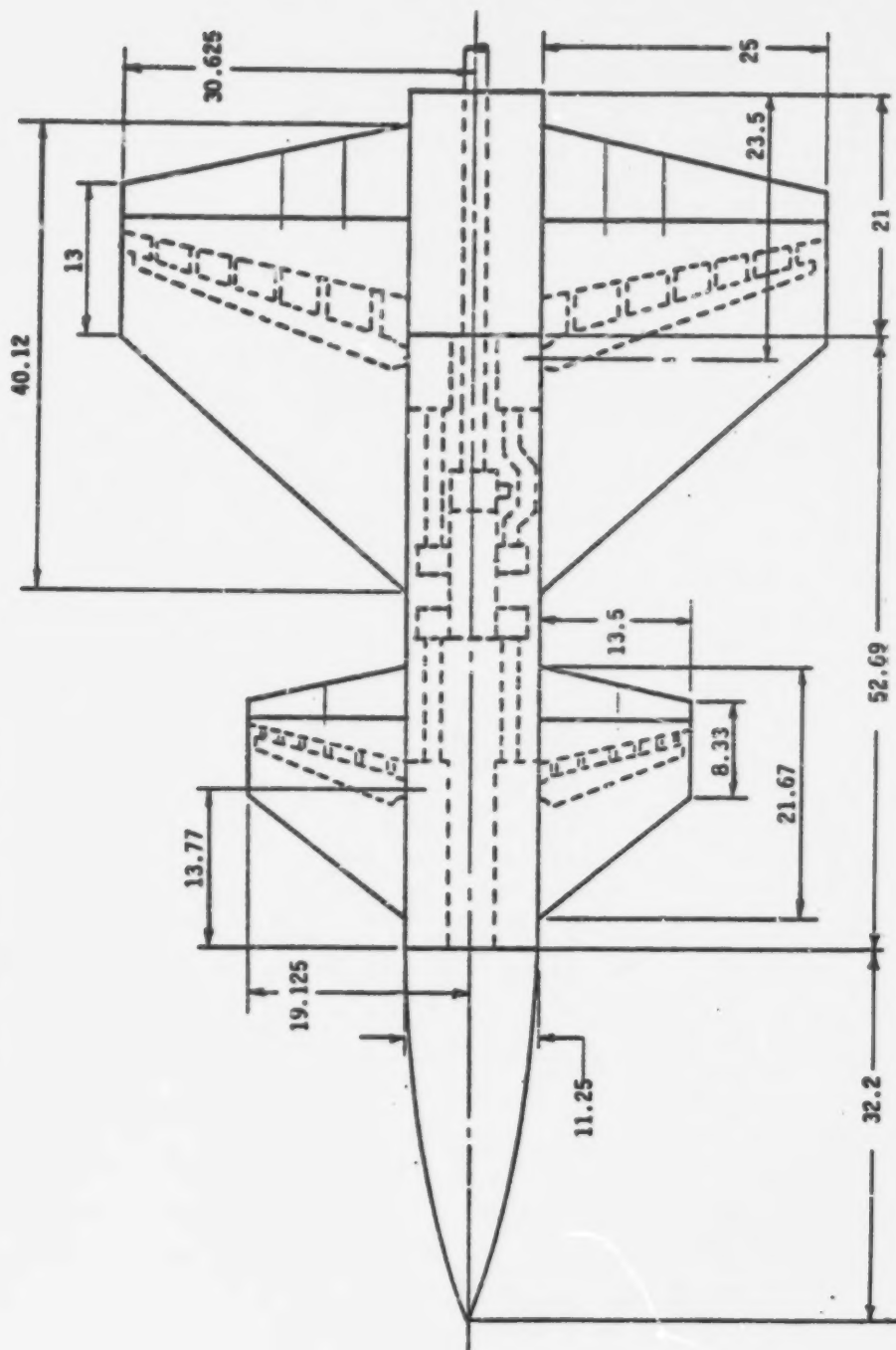


Figure 2. Model Sketch (Dimensions)

TABLE 1. - MODEL GEOMETRY

	WING	CAVARD	BODY	TAIL
TIP CHORD	13 IN	8.33 IN	-	4.25 IN
ROOT CHORD EXPOSED	40.12 IN	21.67 IN	-	19.50 IN
ROOT CHORD TOTAL (BP 0)	46.21 IN	27.23 IN	-	-
TAIL HEIGHT	-	-	-	15.20 IN
SPAN TOTAL	61.25 IN	38.25 IN	-	-
AREA EXPOSED	9.222 FT ²	2.812 FT ²	-	1.25 FT ²
AREA TOTAL	12.591 FT ²	3.334 FT ²	-	-
ASPECT RATIO EXPOSED	-	1.90	-	2.56
ASPECT RATIO TOTAL	2.069	3.047	-	-
BODY LENGTH	-	-	105.89 IN	-
BODY WIDTH	-	-	11.25 IN	-
MINIMUM BODY HEIGHT	-	-	13.00 IN	-
MAXIMUM BODY HEIGHT	-	-	13.75 IN	-
MAC EXPOSED	28.97 IN	16.0 IN	-	-
MAC TOTAL	32.71 IN	19.45 IN	-	-
SHEEP	41 DEG	38.33 DEG	-	45 DEG

TABLE 2. - BASIC AIRFOIL COORDINATES (NO NOZZLE)

X/C	WING				CANARD			
	NO DROOP		DROOP		NO DROOP		DROOP	
	Z/C UPPER	Z/C LOWER	Z/C UPPER	Z/C LOWER	Z/C UPPER	Z/C LOWER	Z/C UPPER	Z/C LOWER
0	0	0	-.035	-.035	0	0	-.025	-.025
.002	.0046	-.0044	-.0299	-.0395	.0046	-.0044	-.0195	-.0295
.005	.0068	-.00605	-.0263	-.04095	.0068	-.00605	-.0154	-.0311
.01	.0093	-.0077	-.0217	-.0411	.0093	-.0077	-.01035	-.0308
.02	.0126	-.0100	-.0150	-.0398	.0126	-.0100	-.003	-.029
.03	.0153	-.0120	-.0097	-.0383	.0153	-.0120	.0024	-.0278
.04	.0175	-.0133	-.0051	-.0370	.0175	-.0133	.007	-.0266
.06	.0212	-.0157	.0034	-.0346	.0212	-.0157	.0142	-.0249
.08	.0242	-.0176	.0107	-.0324	.0242	-.0176	.01955	-.0235
.10	.0264	-.0192	.0165	-.0303	.0264	-.0192	.0235	-.0226
.125	.0287	-.0208	.02235	-.0279	.0287	-.0208	.0273	-.0220
.15	.0305	-.0222	.0267	-.0258	.0305	-.0222	.030	-.0224
.20	.0329	-.0241	.0321	-.0246	.0329	-.0241	.0329	-.0241
.25	.0342	-.0254	.0342	-.0254	.0342	-.0254	.0342	-.0254
.30	.0350	-.0256	.0350	-.0256	.0350	-.0256	.0350	-.0256
.35	.03548	-.02545	.03548	-.02545	.0354	-.02545	.0354	-.02545
.40	.0357	-.0249	.0357	-.0249	.0357	-.0249	.0357	-.0249
.45	.03575	-.0241	.03575	-.0241	.0358	-.0241	.0358	-.0241
.50	.03565	-.0230	.03565	-.0230	.0358	-.0230	.0358	-.0230

TABLE 2. - BASIC AIRFOIL COORDINATES (NO NOZZLE) (Concluded)

X/C	WING				CANARD			
	NO DROOP		DROOP		NO DROOP		DROOP	
	Z/C UPPER	Z/C LOWER	Z/C UPPER	Z/C LOWER	Z/C UPPER	Z/C LOWER	Z/C UPPER	Z/C LOWER
.55	.03535	-.02175	.03535	-.02175	.0358	-.02175	.0358	-.02175
.60	.03488	-.01945	.03488	-.01945	.0356	-.01945	.0356	-.01945
.65	.0342	-.0165	.0342	-.0165	.03535	-.0165	.03535	-.0165
.70	.0332	-.0126	.0332	-.0126	.0348	-.0126	.0348	-.0126
.75	.03165	-.0081	.03165	-.0081	.0340	-.0081	.0340	-.0081
.80	.029	-.0028	.0290	-.0028	.0325	-.0028	.0325	-.0028
.85	.02325	+.002	.02325	+.002	.02325	+.002	.02325	+.002
.90	.0173	+.003	.0173	+.003	.0176	+.003	.0176	+.003
.95	.00935	+.0008	.00935	+.0008	.0112	+.0008	.0112	+.0008
1.00	0	-.004	0	-.004	.004	-.004	.004	-.004

FLAP {

L.E. RADIUS = .012

WING ROOT INCIDENCE +4.0°

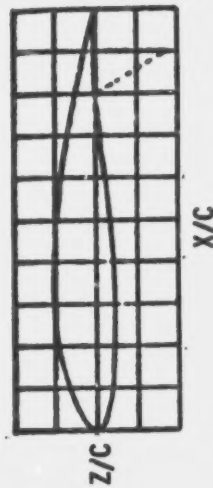
WING TIP INCIDENCE -1.0°

TWIST ALONG X/C = 0.80

Z ~ VERTICAL DISTANCE

C ~ CHORD ~ IN.

Z/C



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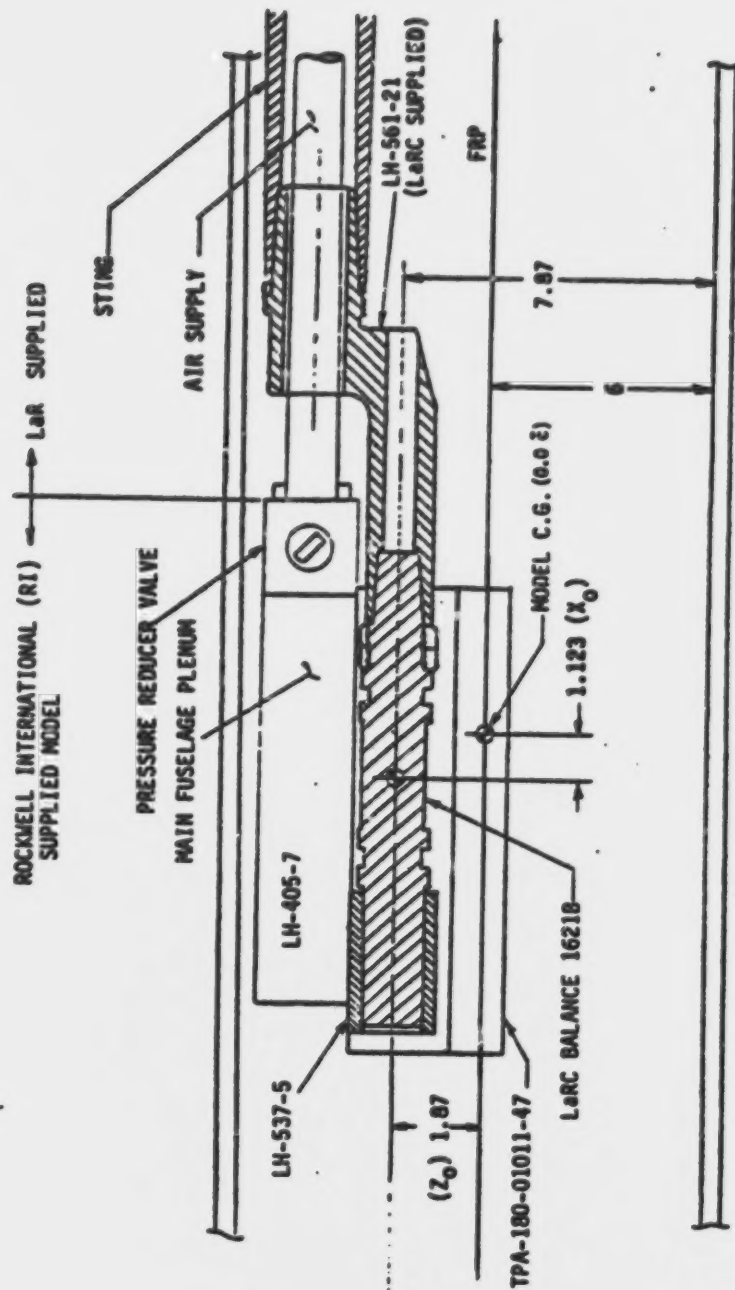


Figure 3. Schematic of Sting, Balance, and Air Supply

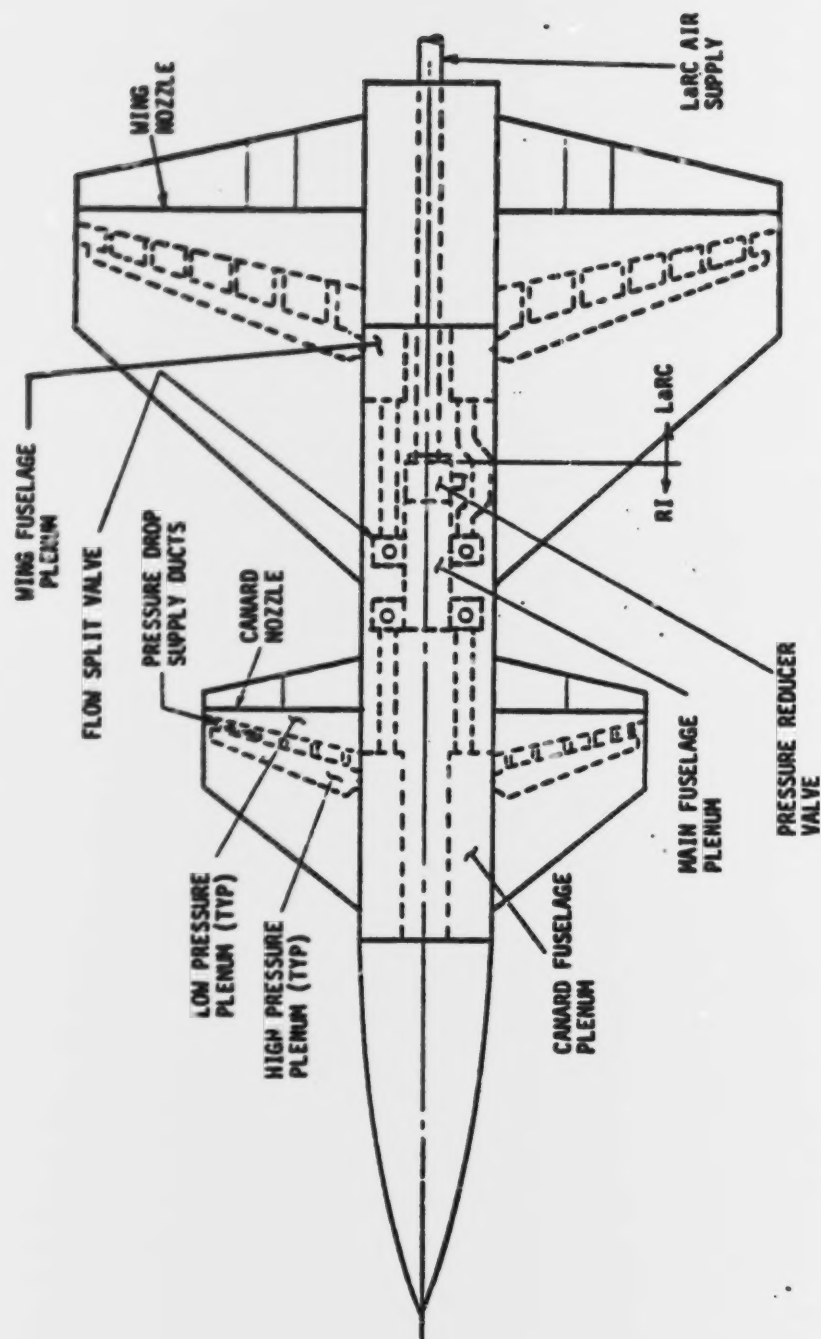


Figure 4. Model Air Supply Diagram

2.2 Model Instrumentation

The model and test instrumentation consisted of the following:

1. six-component internal balance
2. wing surface static pressure ports
3. canard surface static pressure ports
4. fuselage surface static pressure ports
5. internal flow pressure sensors
6. airflow measuring and calibrating instrumentation (NASA supplied)
7. calibrated downwash probe (NASA supplied)

Surface pressure instrumentation consisted of a total of 229 surface taps with 151 located on the left hand wing, 56 located on the left hand canard, and 22 located at 3 inches left of the plane of symmetry on the fuselage upper and lower surfaces. These were all monitored with a standard scani-valve system. Figure 5 shows the location of the wing and canard pressure taps by butt plane and local chord. The locations of the fuselage pressures along the fuselage length are presented with the tabulated pressure data in Appendix A.

The downwash probe was a five-hole directional probe mounted approximately one chord length aft of wing trailing edge (see Figure 1). The calibration of the probe provided local angle of attack relative to model FRL. These angles of attack have been converted to downwash angle and are presented in Appendix A.

2.3 Model - Data Reduction

The force data have been reduced to standard six component force and moment coefficient about the stability axis by standard data reduction equations. The blowing coefficient C_u is obtained by expanding the measured mass flow to the fully expanded, isentropic, velocity and normalizing on freestream dynamic pressure and the total wing area.

$$C_u = \frac{\dot{m} V_1}{qS}$$

The thrust removed coefficients are obtained by adjusting the balance raw data output by the static thrust tares and then applying normal corrections to the adjusted data, i.e.:

$$NF_{TR} = NF_{uncorrected} - NF_{static\ thrust}$$

$$AF_{TR} = AF_{uncorrected} - AF_{static\ thrust}$$

etc.

This procedure required that a thrust tare be taken each time a configuration change involving the thrust nozzle system was made.

WIND STATE, DIRECTION AND VELOCITY									
Obs'd	%	L		U		L		U	
		Dir	Spd	Dir	Spd	Dir	Spd	Dir	Spd
0	2.6								
5	10								
10	10								
15	20								
20	30								
25	40								
30	50								
35	60								
40	70.6								
45	78.6								
50	79.6								
55	80.6								
60	81.6								
65	82								
70	86								
75	87								
80	88								
85	93								
90	96								
95	100								

[illegible]

11

Surface pressure distributions were reduced to pressure coefficient by the normal data reduction equations.

$$C_p = \frac{\Delta P}{q} = \frac{P_L - P_\infty}{q}$$

Test data are presented in Appendix A. The force data are plotted, and selected pressure data and downwash angle measurements are tabulated. Table 3 defines the configurations for which data are presented.

TABLE 3. CONFIGURATION DEFINITION

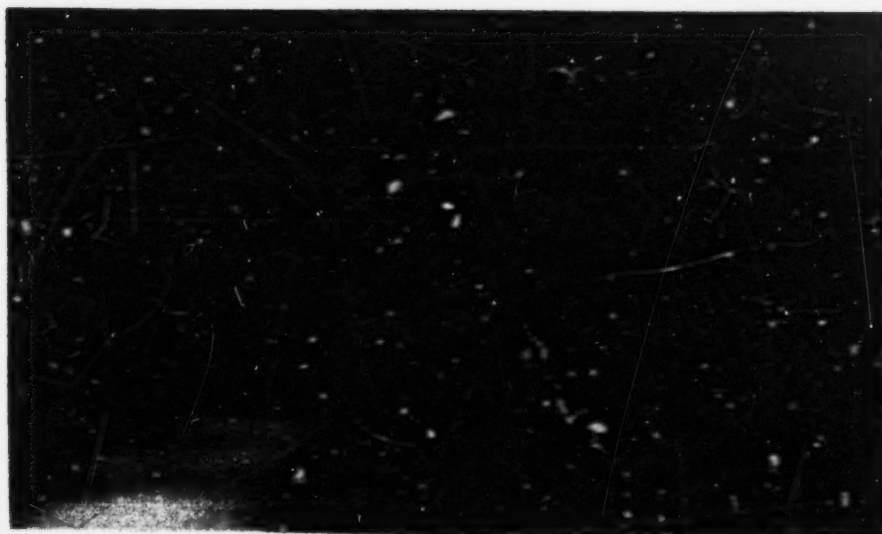
SYMBOL	DEFINITION	CANARD POSITION	WING POSITION
B OR BV	BODY, VERTICAL	OFF	OFF
BC1V	BODY, CANARD, VERTICAL	1	OFF
BC1W6V	BODY, CANARD, WING, VERTICAL	1	6
BC2W6V	BODY, CANARD, WING, VERTICAL	2	6
BC2W5V	BODY, CANARD, WING, VERTICAL	2	5
BC3W6V	BODY, CANARD, WING, VERTICAL	3	6
BW6V	BODY, WING, VERTICAL	OFF	6

2.4 Installation and Test Procedure

The model is shown installed in the test section of the NASA-Langley 4 x 7 meter tunnel in Figure 6. High pressure air for jet simulation was supplied to the model through an air line in the model support sting, and supplied to each nozzle as described in Section 2.1. The nozzle pressure ratio was maintained at 1.7 or greater, and blowing coefficient was controlled by varying tunnel dynamic pressure. The nozzles were calibrated with the tunnel off, and this static thrust was utilized to obtain the thrust removed coefficients.

The configurations which were tested included: (1) flap deflections of 0, 15, and 45 degrees, (2) blowing spans of 1/4, 1/2, and full span on the wing and 1/2 and full span on the canard, (3) relative wing/canard placement. Blowing coefficients were varied from 0 to 4.0. These configurations were tested both in and out of ground effect. Basic data were obtained through a pitch range of -4 to 20 degrees angle of attack. Selected configurations were tested through a range of yaw angles of +8 to -8 degrees. Where ground effects were investigated, the model was tested at heights from approximately $h/c = 0.4$ to free air. The sideslip and

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(a) Front View



(b) 3/4 Side View

Figure 6. Full Span Model in LaRC 4 x 7 Meter
Wind Tunnel Facility

height data were obtained at an angle of attack near zero degrees. Downwash angle was measured behind the wing for most of the configurations. Figure 1 shows the relative wing canard locations of the model, and Figure 5 presents the wing and canard pressure tap locations.

3.0 SUMMARY OF TEST RESULTS

A brief analysis of the effect of the blowing nozzle span and wing/canard positioning effects on longitudinal aerodynamic characteristics is presented. The lateral-directional characteristics of the propulsive wing/canard obtained during the test are presented in Appendix A with the complete data. The effect of ground proximity is also presented in Appendix A, A177 to A-209. No unexpected ground effects were noted.

3.1 Effect of Nozzle Span

Nozzle span was varied from approximately 1/4 span to full span with a full span flap deflection of 45 degrees. The effects of nozzle span and blowing coefficient on lift coefficient and thrust removed lift coefficient are presented in Figures 7 through 10. Total C_L at angles of attack of zero and eight degrees are presented in Figures 7 and 8 with the corresponding thrust removed lift, $C_{L_{TR}}$, presented in Figures 9 and 10.

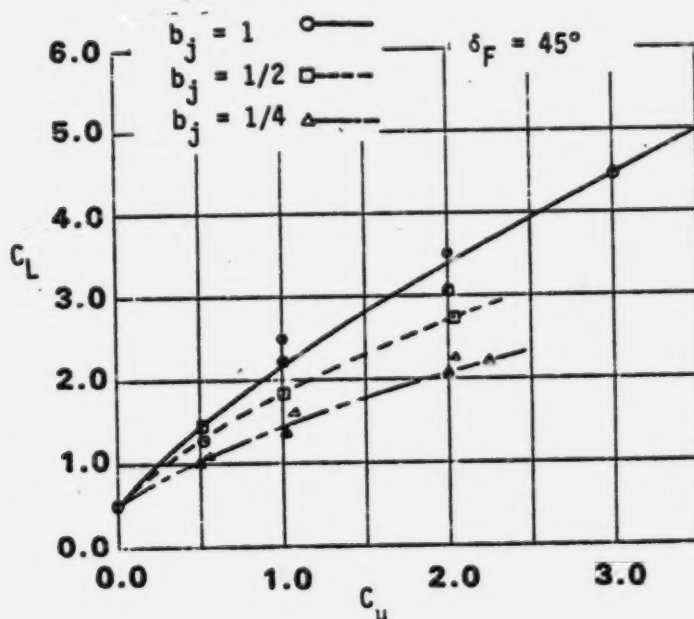


Figure 7. Effect of Blowing Span on Total Lift Coefficient, Canard Off, $\alpha = 0$ Degrees

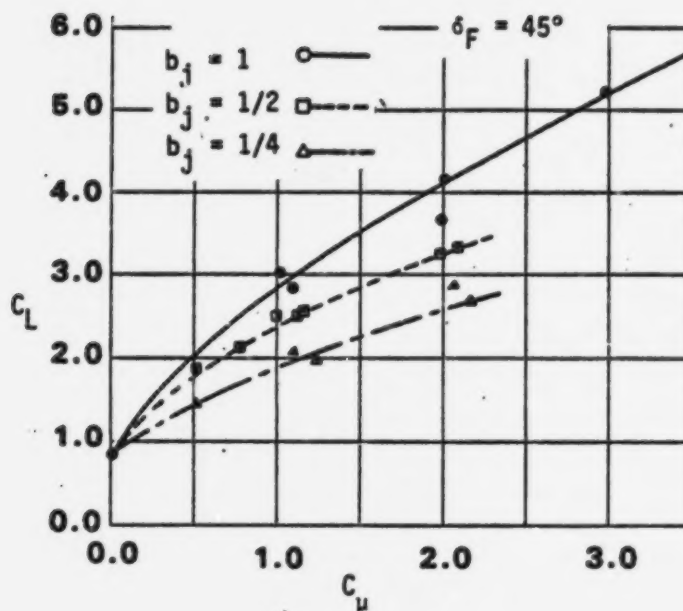


Figure 8. Effect of Blowing Span on Total Lift Coefficient, Canard Off, $\alpha = 8$ Degrees

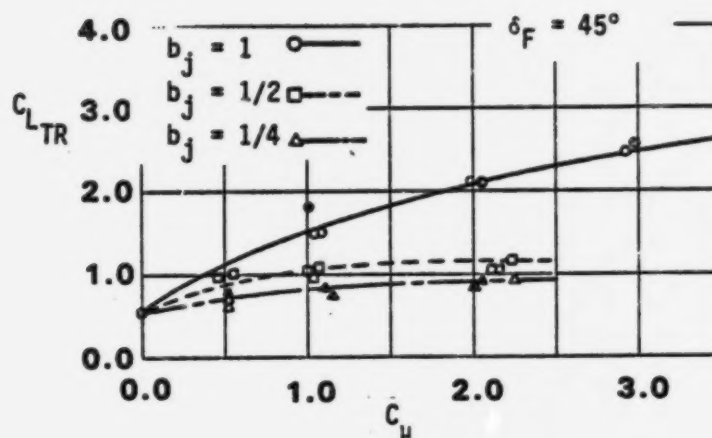


Figure 9. Effect of Blowing Span on the Thrust Removed Lift Coefficient, Canard Off, $\alpha = 0$ Degrees

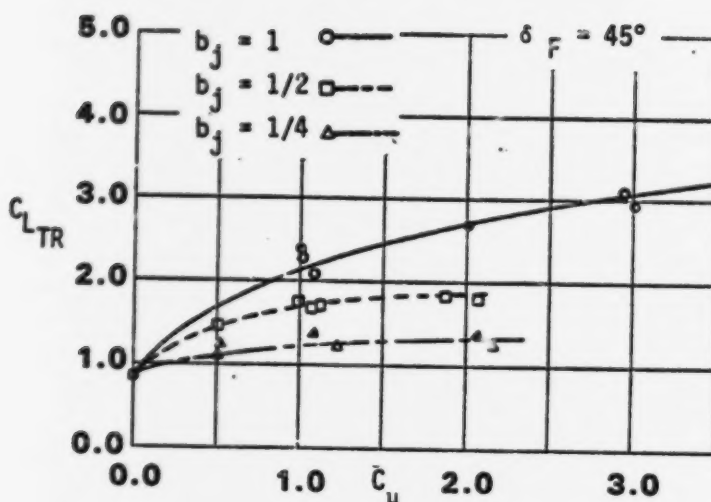


Figure 10. Effect of Blowing Span on the Thrust Removed Lift Coefficient, Canard Off, $\alpha = 8$ Degrees

These thrust removed lift coefficients are developed by removing the static thrust components from the total force measurements. The results of Figures 9 and 10 show that the full span flap is much superior in developing circulation lift. The full span configuration continues to show an increase in circulation to levels of C_u greater than three while the shorter spans appear to have attained their maximum level of circulation lift at a much lower C_u . These characteristics are indicative of the greater local blowing coefficient of the shorter nozzles compared to the longer, full span nozzle. The circulation lift increase with blowing is controlled by the local or section blowing coefficient. The jet flap theory accounts for the local C_u by the use of the affected wing area ratio, Reference 5.

The drag of the propulsive wing is presented in Figure 11 for the thrust included case and in Figure 12 with the thrust removed. The drag variation demonstrates the same characteristics as the lift. Large induced drag is indicated for the full span nozzle and less induced drag with the shorter span nozzles. This result is to be expected in view of the variation of lift coefficient discussed earlier.

Wing/body pitching moment coefficients presented in Figures 13 and 14 also show the same trend. The moments are about the leading edge of the mean aerodynamic chord; therefore, the vectored thrust inputs a significant negative moment. The thrust removed moment indicates that the aerodynamic load is acting at about the 70 percent chord of the wing. This is not unexpected for a blown flap with a chord of 20 percent of the wing chord.

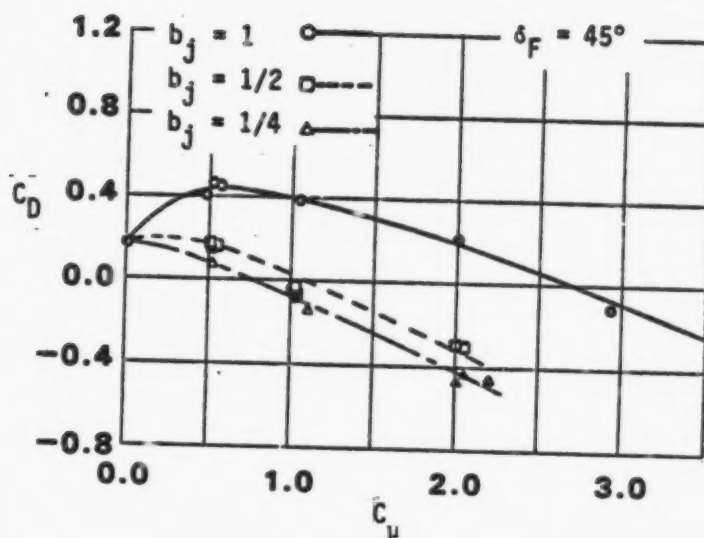


Figure 11. Effect of Blowing Span on the Total Drag Coefficient, Canard Off, $\alpha = 0$ Degrees

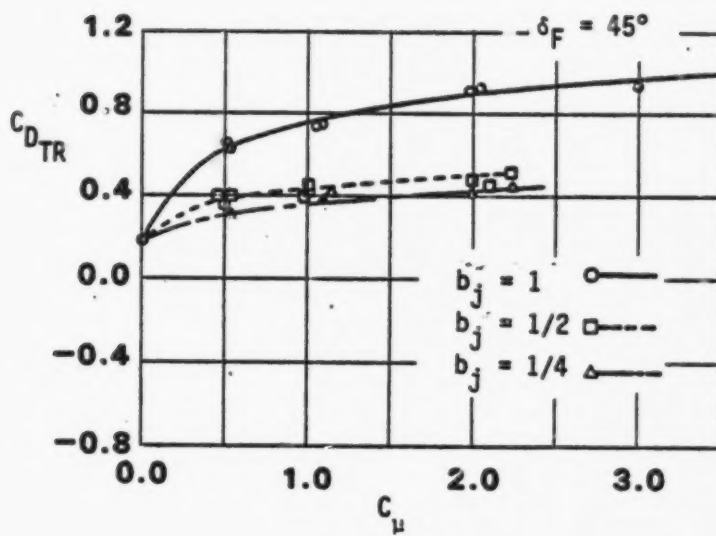


Figure 12. Effect of Blowing Span on the Thrust Removed Drag Coefficient, Canard Off, $\alpha = 0$ Degrees

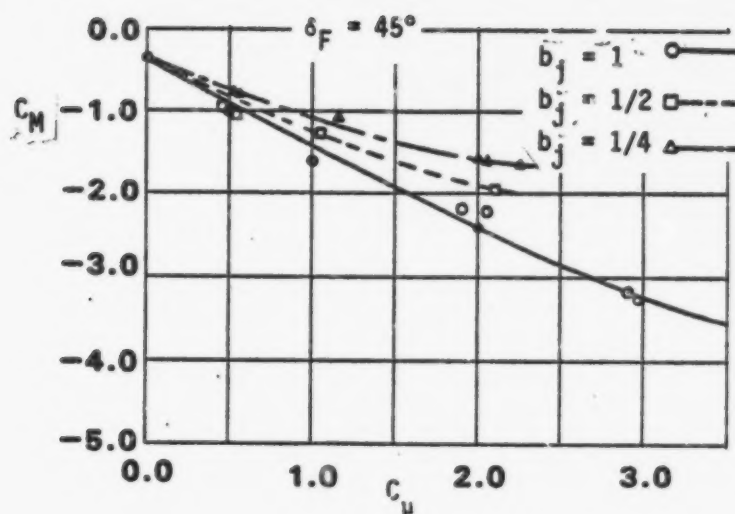


Figure 13. Effect of Blowing Span on the Total Pitching Moment Coefficient, Canard Off, $\alpha = 0$ Degrees

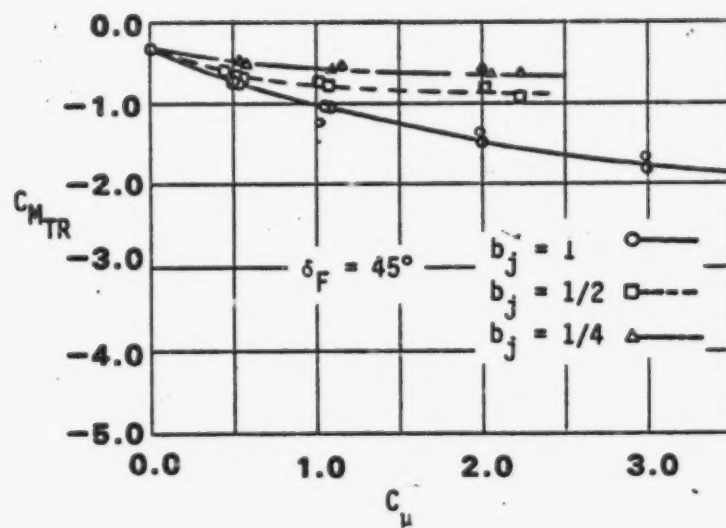


Figure 14. Effect of Blowing Span on the Thrust Removed Pitching Moment Coefficient, Canard Off, $\alpha = 0$ Degrees

3.2 Canard Effects

The negative pitching moments of the propulsive wing require a large force well forward of the center of gravity of the configuration to obtain trim. One means of accomplishing this is using a blown canard. Figure 15 presents the pitching moment coefficient at zero angle of attack with the canard installed in the high forward position and a blowing coefficient of 1/2 that of the wing. Figure 16 presents similar data at an angle of attack of eight degrees. It can be seen that a significant pitch-up moment is gained from the canard, even though it is not sufficient to trim at this center of gravity (CG) location. Increased canard flap deflection, canard incidence angle, or increased canard blowing rates are means of increasing the trim power of the canard. These variables will be addressed in future studies.

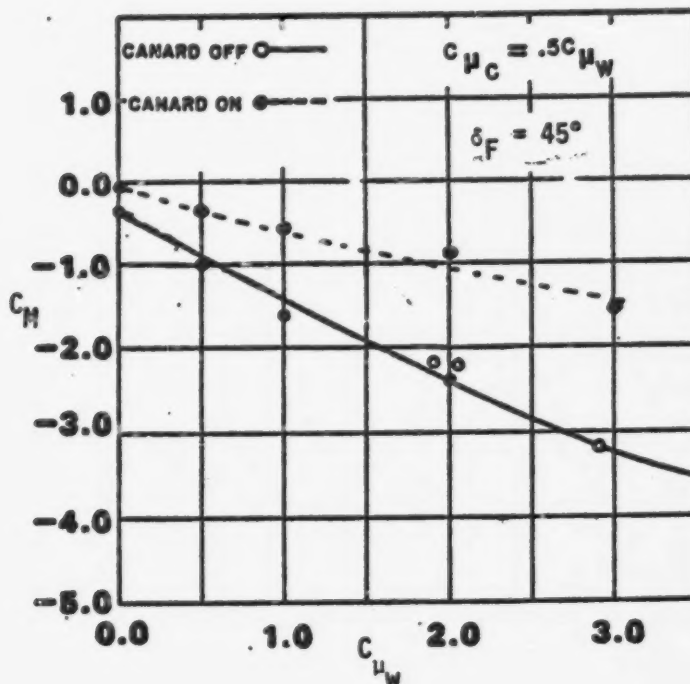


Figure 15. Effect of the Canard on the Pitching Moment Coefficient, $\alpha = 0$ Degrees

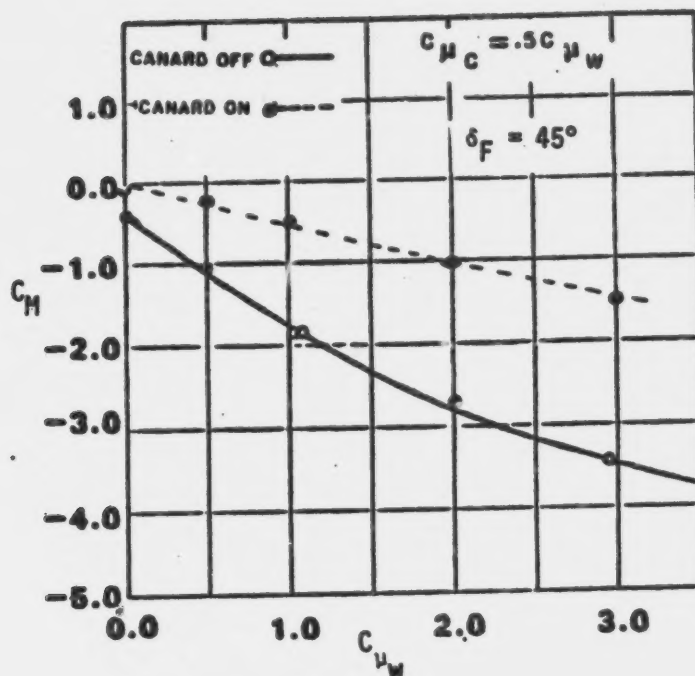


Figure 16. Effect of the Canard on the Pitching Moment Coefficient, $\alpha = 8$ Degrees

The relative position of the canard and the wing is also a very important consideration in the propulsive wing/canard concept. As is true in most design variables, there is no single position which is the so-called "best" for all conditions. Previous studies (Refs. 1, 2, and 3) showed that for deflections of 15 degrees and less, the high canard, low wing had the better characteristics. This held for blowing as well as for the non-blowing conditions. Early, unpublished, studies on a similar configuration indicated that at nozzle deflections of 60 degrees, the canard should be low relative to the wing. The results of a positioning variation on the current wing/canard model are presented in Figure 17. The flap deflection for this test was 45 degrees; however, with the upper surface contour aft of the nozzle included, the total jet turning angle was 60 degrees. The data show that for this configuration, the low canard, high wing, position 5,2, has the better lift characteristics for the blown, large deflection conditions.

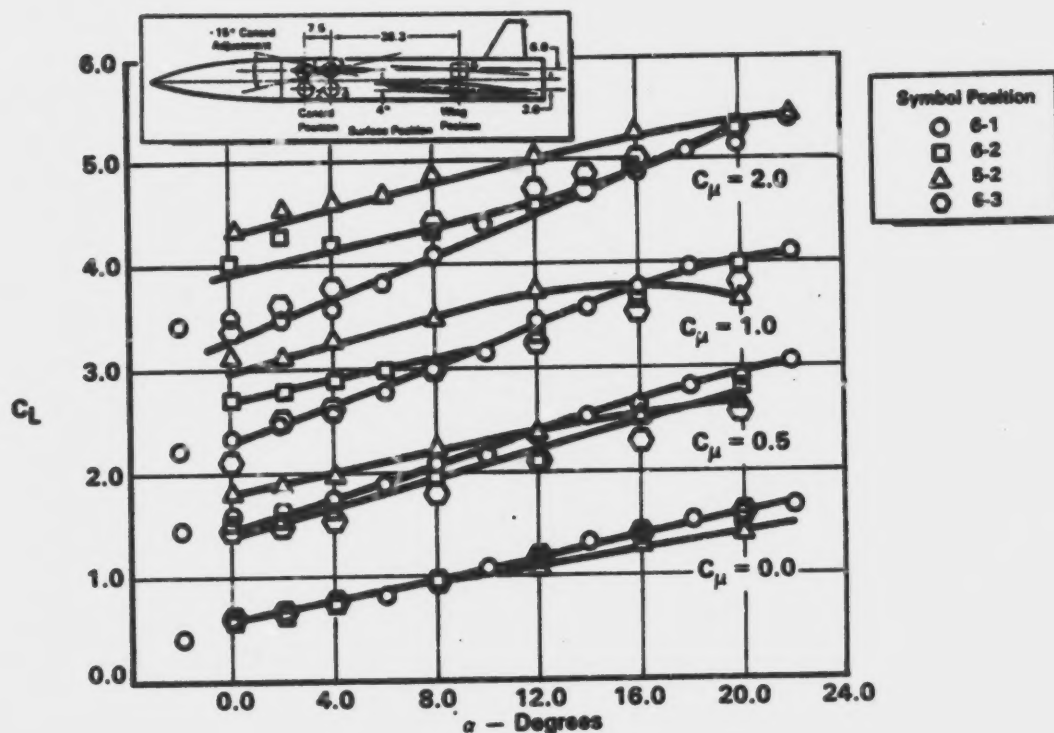


Figure 17. Effect of Canard Position on Total Lift Coefficient

The flight requirements of the STOL wing/canard airplane would dictate the compromises which would finally place the wing and canard in their positions. It is expected that the high speed requirements would prevail, and a propulsive wing/canard configuration would have a high canard with a low wing. Most operations would be at low flap deflections, 15 degrees or less, and the larger deflections would be used only for very short field operations, less than 400 feet.

3.3 Semi/Full Span Comparison

The propulsive wing/canard model has been tested in a semispan, as well as a full span configuration. However, the blowing distribution between the wing and canard was changed between the semi and full span configurations, so a comparison of the two configurations powered cannot be made. However, comparisons can be made for the wing alone at blowing coefficients of 0, 1.0, and 2.0 and for the wing/canard configuration with a blowing coefficient of zero.

The comparison of the full and semispan test results for the wing/canard configuration are presented in Figure 18 for the zero blowing case. Very good agreement is seen in most of the parameters. A difference is seen in the lift curve slope, but almost perfect agreement is seen in the drag coefficient. The pitching moment indicates a slightly greater stability for the semispan model. These small differences may have been the result of a change on the canard downwash on the wing.

The comparison of the wing/body is presented in Figure 19 for blowing coefficients of 0, 1.0, and 2.0. Near perfect agreement between the two models is shown in lift and in drag. Again, the semispan model indicates slightly greater stability.

4.0 CONCLUSIONS

The experimental STOL investigation of the propulsive wing/canard has been partially completed. The study, thus far, has shown these results.

The full span nozzle is more effective than the partial span nozzles in producing circulation lift.

The low canard, high wing positioning is preferred for large flap deflection and blowing; however, at other conditions, such as takeoff flaps, cruise, and transonic flight, the high canard is preferred. It is expected that these conditions will prevail, yielding a high canard, low wing configuration.

Very good agreement between full span and semispan model test results were obtained where exact conditions were duplicated.

An additional test of this concept will be conducted with a contoured fuselage. The major objectives with the revised fuselage lines will be to determine the lateral-directional characteristics, to investigate means to trim the wing pitching moments, and to investigate the effect of the moving ground board. Flow field measurements behind the canard will be made for comparison with and as an extension of the semispan model data bank.

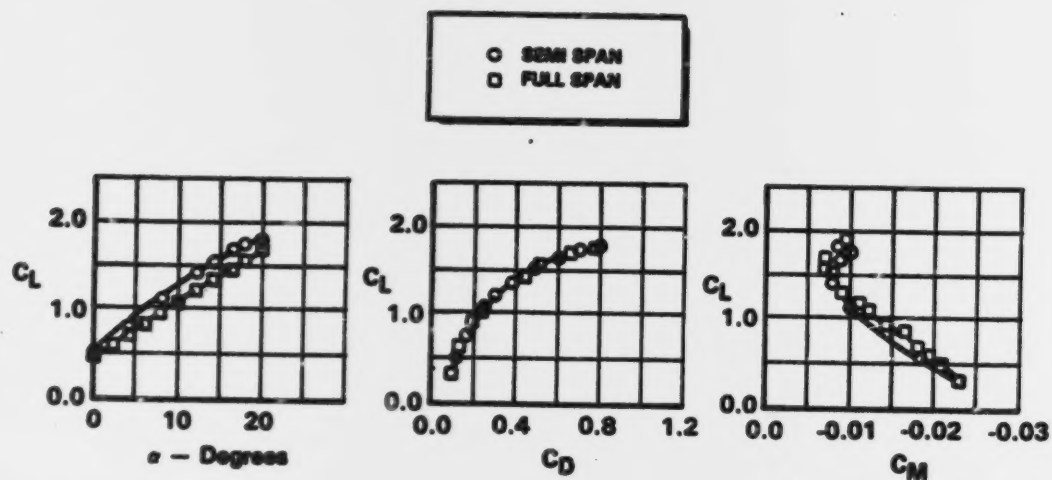


Figure 18. Comparison of Semispan and Full Span Test Results, Wing/Canard/Body, $C_{\mu} = 0$, $\delta_F = 0$

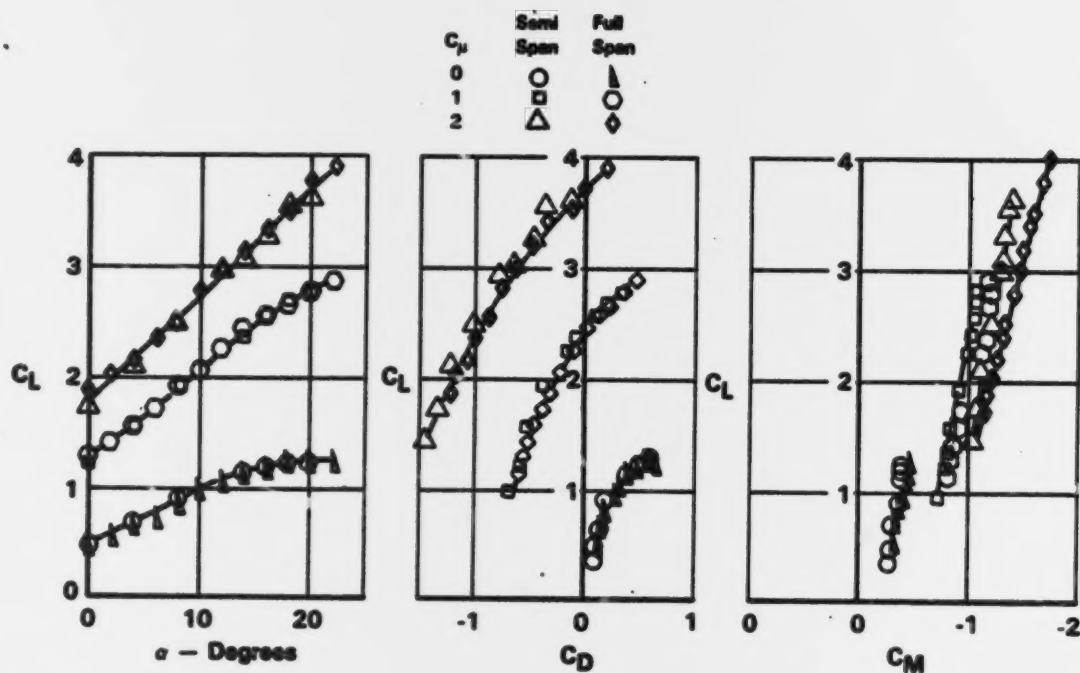


Figure 19. Comparison of Semispan and Full Span Test Results Wing/Body, $\delta_F = 15$ Degrees

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APPENDIX A

PRESENTATION OF BASIC TEST DATA

APPENDIX A

TABLE OF CONTENTS

<u>SECTION</u>	<u>TITLE</u>	<u>PAGE</u>
	TABLE OF CONTENTS	A-2
	LIST OF FIGURES	A-3
	LIST OF TABLES	A-6
A1.0	INTRODUCTION	A-9
A2.0	PLOTTED FORCE DATA	A-9
A3.0	TABULATED PRESSURE DATA	A-210
A4.0	TABULATED DOWNWASH DATA	A-360
A5.0	TABULATED RUN INDEX	A-376

LIST OF FIGURES

<u>FIGURE NO.</u>	<u>TITLE</u>	<u>PAGE</u>
	PITCH POLARS	
A1a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BC1W6V, DELF=0, BN/B=1	A-10
A2a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, DELF=0, BN/B=1	A-16
A3a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, DELF=15, BN/B=1	A-22
A4a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BC1W6V, DELF=15, BN/B=1	A-28
A5a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BC1W6V, DELF=45, BN/B=1	A-34
A6a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BC2W6V, DELF=45, BN/B=1	A-40
A7a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BC2W5V, DELF=45, BN/B=1	A-46
A8a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BC3W6V, DELF=45, BN/B=1	A-52
A9a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BC1W6V, DELF=45, BN/B=1, DELC=10 . .	A-58
A10a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BC1W6V, DELF=45, BN/B=1	A-64
A11a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, DELF=45, BN/B=1	A-70
A12a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BC1V, DELF=45, DELC=10, BN/B=1	A-76
A13a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BC1V, DELF=45, BN/B=1	A-82
A14a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BC1W6V, (BN/B)C=1, (BN/B)W=0.5, DELF=45	A-88

LIST OF FIGURES (Continued)

<u>FIGURE NO.</u>	<u>TITLE</u>	<u>PAGE</u>
A15a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, BN/B=0.5, DELF=45	A-94
A16a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BC1W6V, (BN/B)C=1, (BN/B)W=0.5, DELF=0	A-100
A17a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, BN/B=0.5, DELF=0	A-106
A18a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, BN/B=0.25, DELF=0	A-112
A19a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BC1W6V, (BN/B)C=1, (BN/B)W=0.25, DELF=0	A-118
A20a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, DELF=45, BN/B=.25	A-124
A21a-f	BASIC DATA EFFECT OF CMU CONFIG. BC1W6V, DELF=45, (BN/B)C=1, (BN/B)W=0.25	A-130
A22a-f	BASIC DATA EFFECT OF CMU CONFIG. BC1W6V DELF=45 (BN/B)C=0.5 (BN/B)W=0.25	A-136
A23a-f	BASIC DATA EFFECT OF CMU CONFIG. BC1V, DELF=45, (BN/B)C=0.5.	A-142
A24a-e	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, DELF=45, BN/B=?	A-148

YAW POLARS

A25a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, BN/B=1.0, DELF=45, $\alpha = 2$. .	A-153
A26a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, BN/B=0.5, DELF=45	A-159
A27a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, DELF=45, BN/B=.25	A-165

LIST OF FIGURES (Concluded)

<u>FIGURE NO.</u>	<u>TITLE</u>	<u>PAGE</u>
A28a-f	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, DELF=45, BN/B=1	A-171
	HEIGHT POLARS	
A29a-c	BASIC DATA EFFECT OF CMU CONFIGURATION BC1W6V, DELF=45, BN/B=1	A-177
A30a-c	BASIC DATA EFFECT OF CMU CONFIGURATION BC2W6V, DELF=45, BN/B=1	A-180
A31a-c	BASIC DATA EFFECT OF CMU CONFIGURATION BC2W5V, DELF=45, BN/B=1	A-183
A32a-c	BASIC DATA EFFECT OF CMU CONFIGURATION BC3W6V, DELF=45, BN/B=1	A-186
A33a-c	BASIC DATA EFFECT OF CMU CONFIGURATION BC1W6V, DELF=45, BN/B=1 DELC=10	A-189
A34a-c	BASIC DATA EFFECT OF CMU CONFIGURATION BC1W6V, DELF=45, BN/B=1, $\beta = 0.8, \alpha = 2$	A-192
A35a-c	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, DELF=45, BN/B=1, ...	A-195
A36a-c	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, DELF=45, BN/B=1, $\alpha = 4$	A-198
A37a-c	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, BN/B=0.5, DELF=45	A-201
A38a-c	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, BN/B=0.5, $\alpha = 8$ DELF=45	A-204
A39a-c	BASIC DATA EFFECT OF CMU CONFIGURATION BW6V, DELF=45, BN/B=1, $\beta = 0.8$	A-207

LIST OF TABLES

<u>TABLE NO.</u>	<u>TITLE</u>	<u>PAGE</u>
TABULATED SURFACE PRESSURES		
A1.	RUN 61, BW6V, DELF=0, CMU=1.0, (BN/B)=1	A-211
A2.	RUN 62, BW6V, DELF=0, CMU=2.0, (BN/B)=1	A-214
A3.	RUN 64, BW6V, DELF=15, CMU=0, (BN/B)=1	A-217
A4.	RUN 65, BW6V, DELF=15, CMU=0.5, (BN/B)=1	A-220
A5.	RUN 66, BW6V, DELF=15, CMU=1.0, (BN/B)=1	A-223
A6.	RUN 67, BW6V, DELF=15, CMU=2.0, (BN/B)=1	A-226
A7.	RUN 75, BC1W6V, DELF=45, CMU=0, (BN/B)=1	A-229
A8.	RUN 76, BC1W6V, DELF=45, CMU=0.5, (BN/B)=1	A-232
A9.	RUN 77, BC1W6V, DELF=45, CMU=1.0, (BN/B)=1	A-235
A10.	RUN 79, BC1W6V, DELF=45, CMU=2.0, (BN/B)=1	A-238
A11.	RUN 142, BW6V, DELF=45, CMU=0, (BN/B)=1	A-240
A12.	RUN 143, BW6V, DELF=45, CMU=0.5, (BN/B)=1	A-243
A13.	RUN 144, BW6V, DELF=45, CMU=1.0, (BN/B)=1	A-246
A14.	RUN 145, BW6V, DELF=45, CMU=2.0, (BN/B)=1	A-249
A15.	RUN 146, BW6V, DELF=45, CMU=3.0, (BN/B)=1	A-252
A16.	RUN 147, BW6V, DELF=45, CMU=4.0, (BN/B)=1	A-255
A17.	RUN 148, BW6V, DELF=45, CMU=2.0, (BN/B)=1	A-258
A18.	RUN 149, BW6V, DELF=45, CMU=1.0, (BN/B)=1	A-261
A19.	RUN 187, BW6V, DELF=45, CMU=0, (BN/B) _W =0.5	A-264
A20.	RUN 188, BW6V, DELF=45, CMU=0.5, (BN/B) _W =0.5	A-267
A21.	RUN 189, BW6V, DELF=45, CMU=1.0, (BN/B) _W =0.5	A-270
A22.	RUN 190, BW6V, DELF=45, CMU=2.0, (BN/B) _W =0.5	A-272

LIST OF TABLES (Continued)

<u>TABLE NO.</u>	<u>TITLE</u>	<u>PAGE</u>
TABULATED SURFACE PRESSURES		
A23.	RUN 216, BC1W6V, DELF=45, CMU=0, $(BN/B)_W=0.5$. .	A-275
A24.	RUN 217, BC1W6V, DELF=45, CMU=1.0, $(BN/B)_W=0.5$.	A-278
A25.	RUN 218, BC1W6V, DELF=45, CMU=2.0, $(BN/B)_W=0.5$.	A-281
A26.	RUN 240, BC1W6V, DELF=0, CMU=0, $(BN/B)_W=0.5$. . .	A-284
A27.	RUN 241, BC1W6V, DELF=0, CMU=0.5, $(BN/B)_W=0.5$. .	A-287
A28.	RUN 256, BW6V, DELF=0, CMU=0, $(BN/B)_W=0.5$	A-290
A29.	RUN 257, BW6V, DELF=0, CMU=0.5, $(BN/B)_W=0.5$. . .	A-294
A30.	RUN 258, BW6V, DELF=0, CMU=1.0, $(BN/B)_W=0.5$. . .	A-297
A31.	RUN 259, BW6V, DELF=0, CMU=2.0, $(BN/B)_W=0.5$. . .	A-300
A32.	RUN 262, BW6V, DELF=0, CMU=0, $(BN/B)_W=0.25$. . .	A-303
A33.	RUN 265, BW6V, DELF=0, CMU=0.5, $(BN/B)_W=0.25$. .	A-306
A34.	RUN 266, BW6V, DELF=0, CMU=1.0, $(BN/B)_W=0.25$. .	A-309
A35.	RUN 267, BW6V, DELF=0, CMU=2.0, $(BN/B)_W=0.25$. .	A-312
A36.	RUN 271, BC1W6V, DELF=0, CMU=0, $(BN/B)_W=0.25$. .	A-315
A37.	RUN 272, BC1W6V, DELF=0, CMU=0.5, $(BN/B)_W=0.25$.	A-318
A38.	RUN 273, BC1W6V, DELF=0, CMU=1.0, $(BN/B)_W=0.25$.	A-321
A39.	RUN 274, BC1W6V, DELF=0, CMU=2.0, $(BN/B)_W=0.25$.	A-324
A40.	RUN 277, BW6V, DELF=45, CMU=0, $(BN/B)_W=0.25$. .	A-327
A41.	RUN 280, BW6V, DELF=45, CMU=0.5, $(BN/B)_W=0.25$. .	A-330
A42.	RUN 281, BW6V, DELF=45, CMU=1.0, $(BN/B)_W=0.25$. .	A-333
A43.	RUN 282, BW6V, DELF=45, CMU=2.0, $(BN/B)_W=0.25$. .	A-336

LIST OF TABLES (Concluded)

<u>TABLE NO.</u>	<u>TITLE</u>	<u>PAGE</u>
TABULATED SURFACE PRESSURES		
A44.	RUN 289, BC1W6V, DELF=45, CMU=0, $(BN/B)_W=0.25$.	A-339
A45.	RUN 290, BC1W6V, DELF=45, CMU=0.5, $(BN/B)_W=0.25$	A-342
A46.	RUN 291, BC1W6V, DELF=45, CMU=1.0, $(BN/B)_W=0.25$	A-345
A47.	RUN 292, BC1W6V, DELF=45, CMU=2.0, $(BN/B)_W=0.25$	A-348
A48.	RUN 296, BC1W6V, DELF=45, CMU=0.5, $(BN/B)_W=0.25$, $(BN/B)_C=0.5$	A-351
A49.	RUN 297, BC1W6V, DELF=45, CMU=1.0, $(BN/B)_W=0.25$, $(BN/B)_C=0.5$	A-354
A50.	RUN 298, BC1W6V, DELF=45, CMU=2.0, $(BN/B)_W=0.25$, $(BN/B)_C=0.5$	A-357
A51.	TABULATED DOWNWASH DATA	A-361
A52.	RUN INDEX	A-377

A1.0 INTRODUCTION

The test data are presented in Appendix A. Some mechanical and internal airflow fouling difficulties were experienced during the test period. The air pipe fouling was, apparently, the result of a gradual failure of the air coil internal to the support sting. The air coil eventually ruptured (Run 247), and the sting was replaced with Air Sting #2 ("bent") for the remainder of the test. The mechanical foul appeared to be a combination of several circumstances including: (1) large nose-down moments with the wing alone configuration, (2) an excessively long sting-to-balance adapter coupled with (3) the normal balance flexibility. It is not known if the internal coil failure entered into the mechanical foul, although the initial signs of coil failure did occur prior to the mechanical foul. In any event, those force data runs where a foul can be detected are not presented. In certain cases, surface pressure data and downwash data runs are presented without force data results. These runs represent those for which repeat force runs were made without the pressure instrumentation operating. The surface pressure data and downwash data presented in Appendix A are correct in that the foul experienced did not affect these data. The corresponding force data in some runs may be in error due to the fouling. In these cases, the correct force data run to be used in analysis is noted on the tabulated data.

A2.0 PLOTTED FORCE DATA

The force and moment data have been plotted and are presented in Section A2.0. The data are presented in three categories. Figures A1 through A24 present the force and moment coefficients for the basic angle of attack variations. Figures A25 through A28 present these coefficients for sideslip variations. And, Figures A29 through A39 show the results of ground height variations. Data are presented for major variables of canard/wing positioning, flap deflection, and flap span. Each major variable is presented as a function of blowing coefficient.

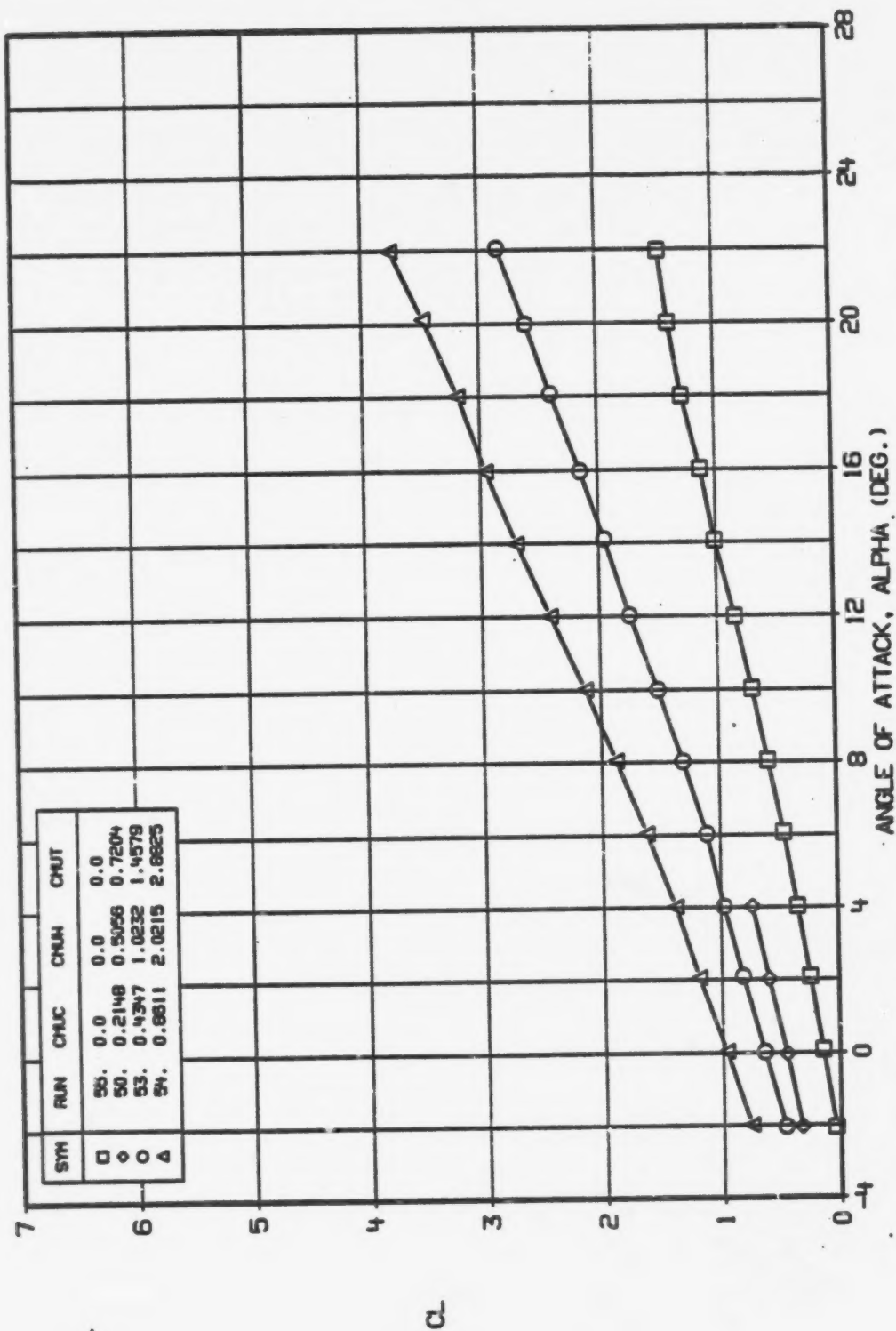


FIGURE A1a BASIC DATA EFFECT OF CMU
CONFIGURATION BC1W6V, DELF=0, BN/B=1

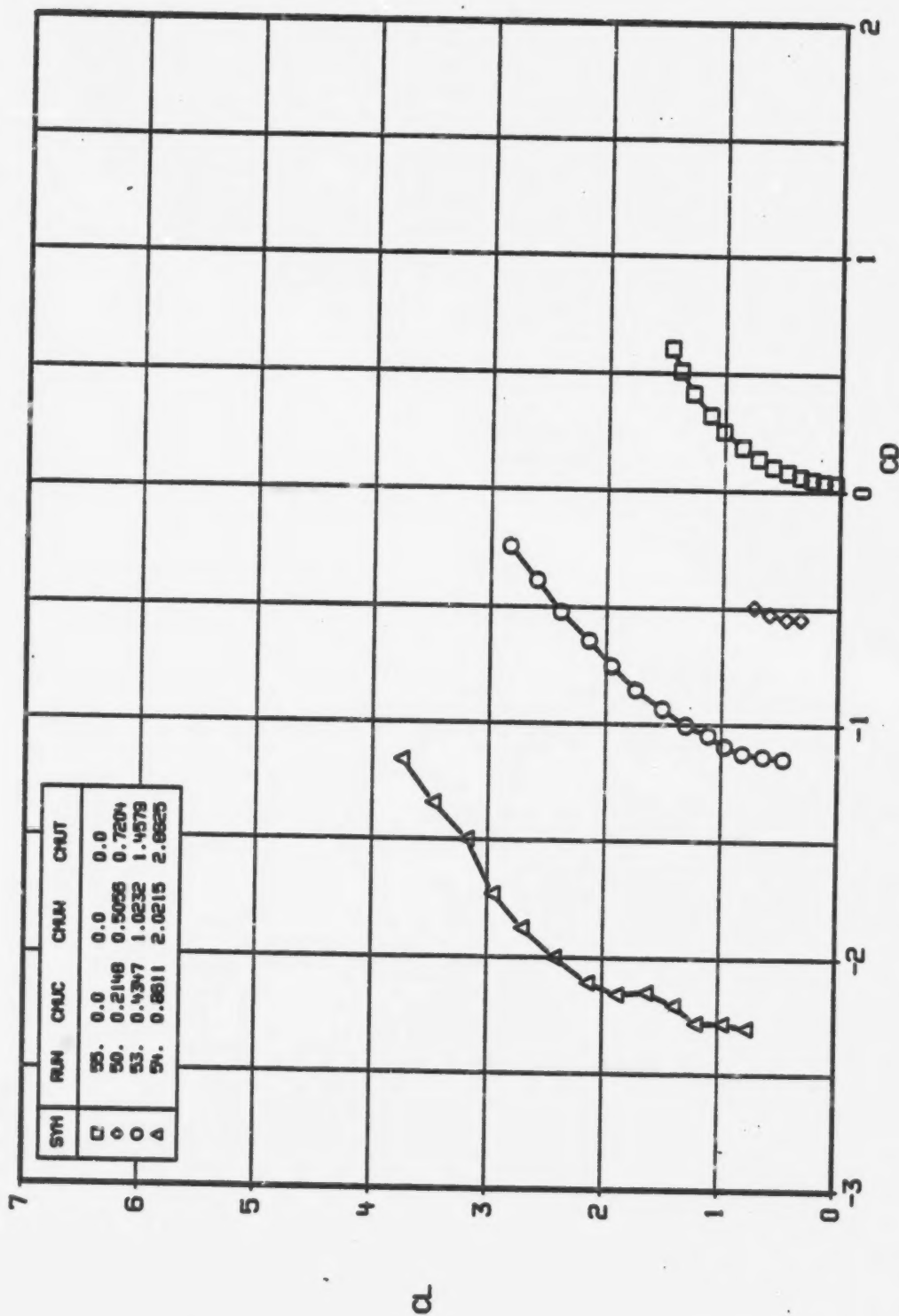


FIGURE A1b BASIC DATA EFFECT OF CMU
CONFIGURATION BC1W6V, DELF=0, BN/B=1

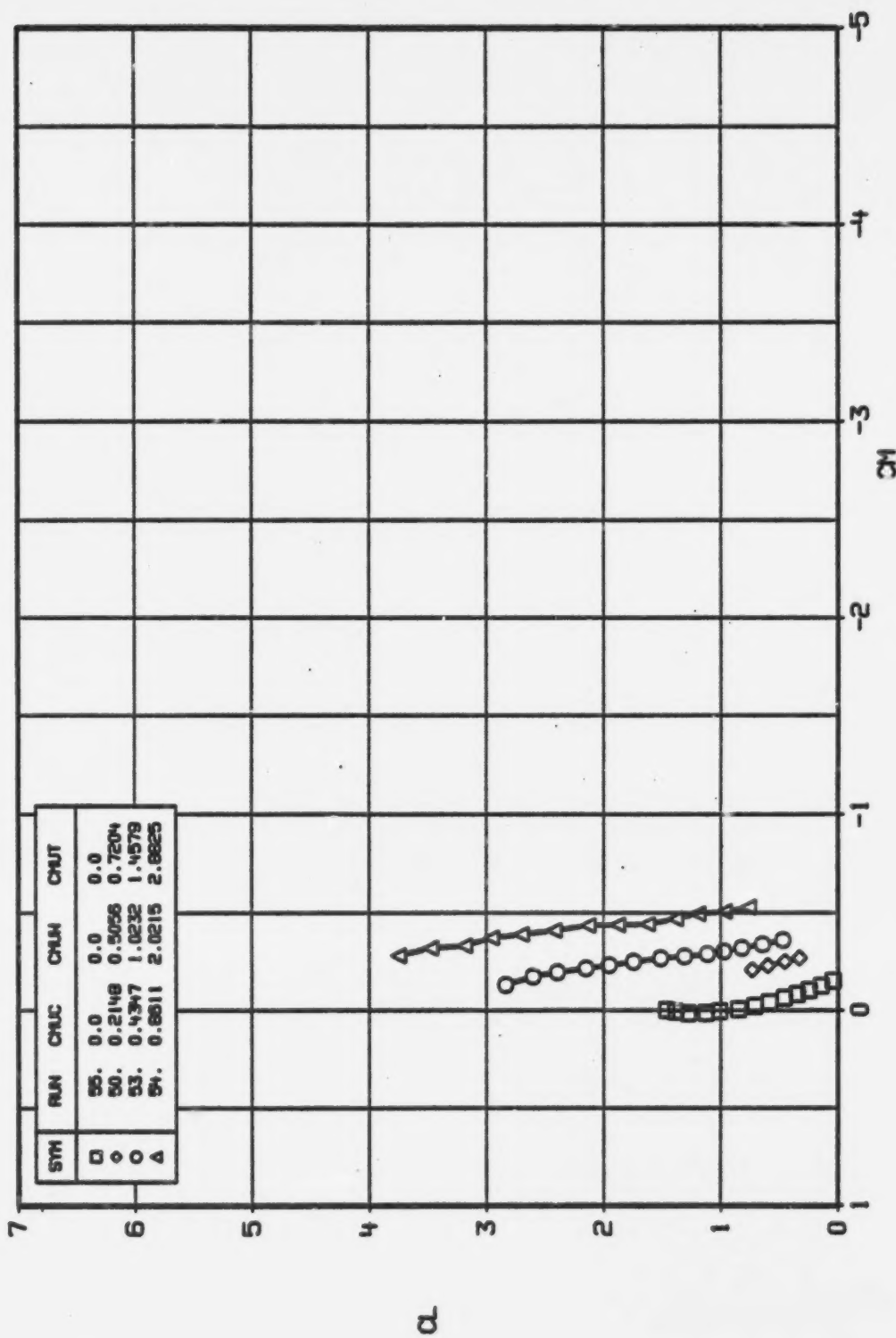


FIGURE A1c BASIC DATA EFFECT OF CMJ
CONFIGURATION BC146V, DELF=0, BN/B=1

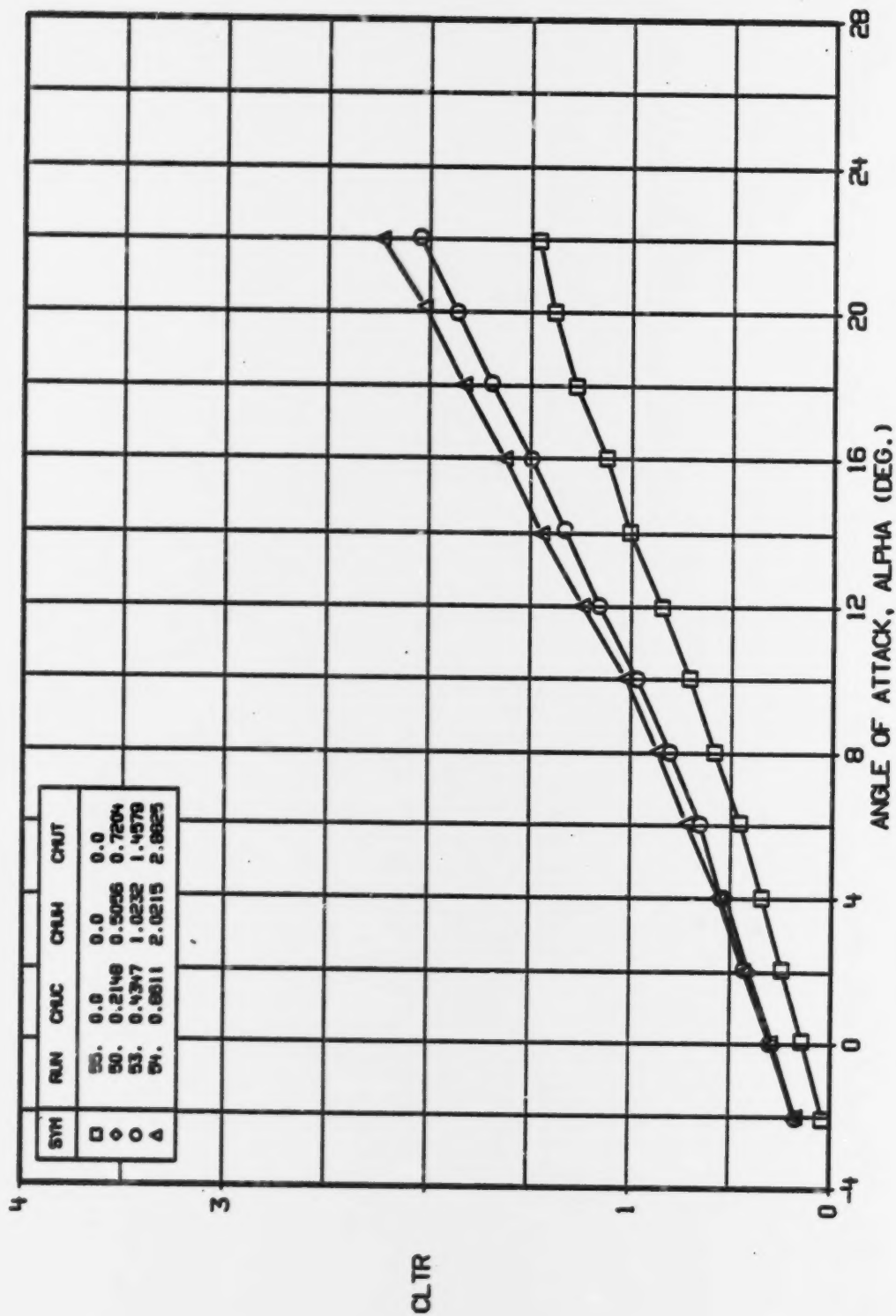


FIGURE A1d BASIC DATA EFFECT OF CMU
CONFIGURATION BC1W5V, DELF=0, BN/B=1

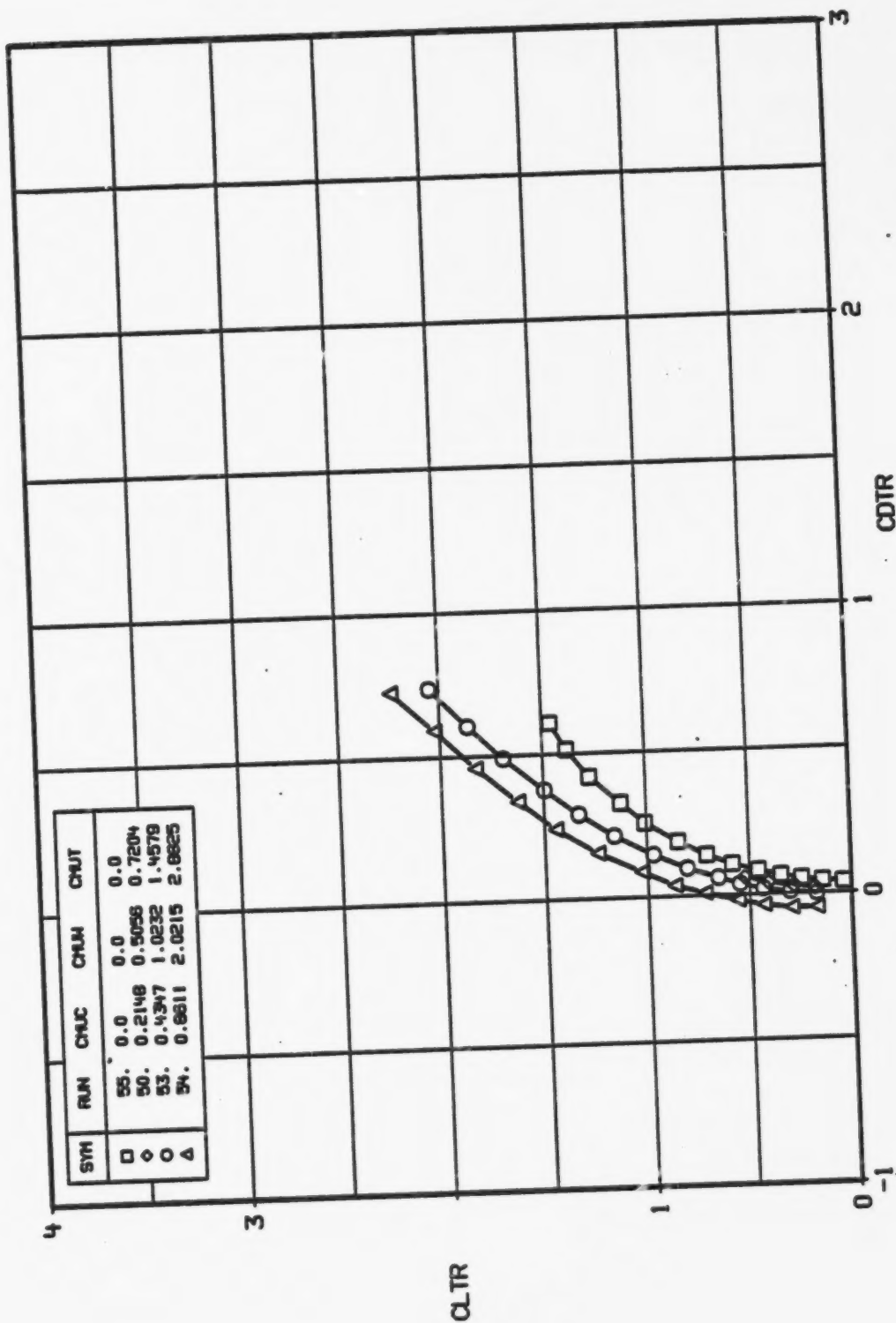


FIGURE A1e BASIC DATA EFFECT OF CMU
CONFIGURATION BC1MGV, DELF=0, BN/B=1

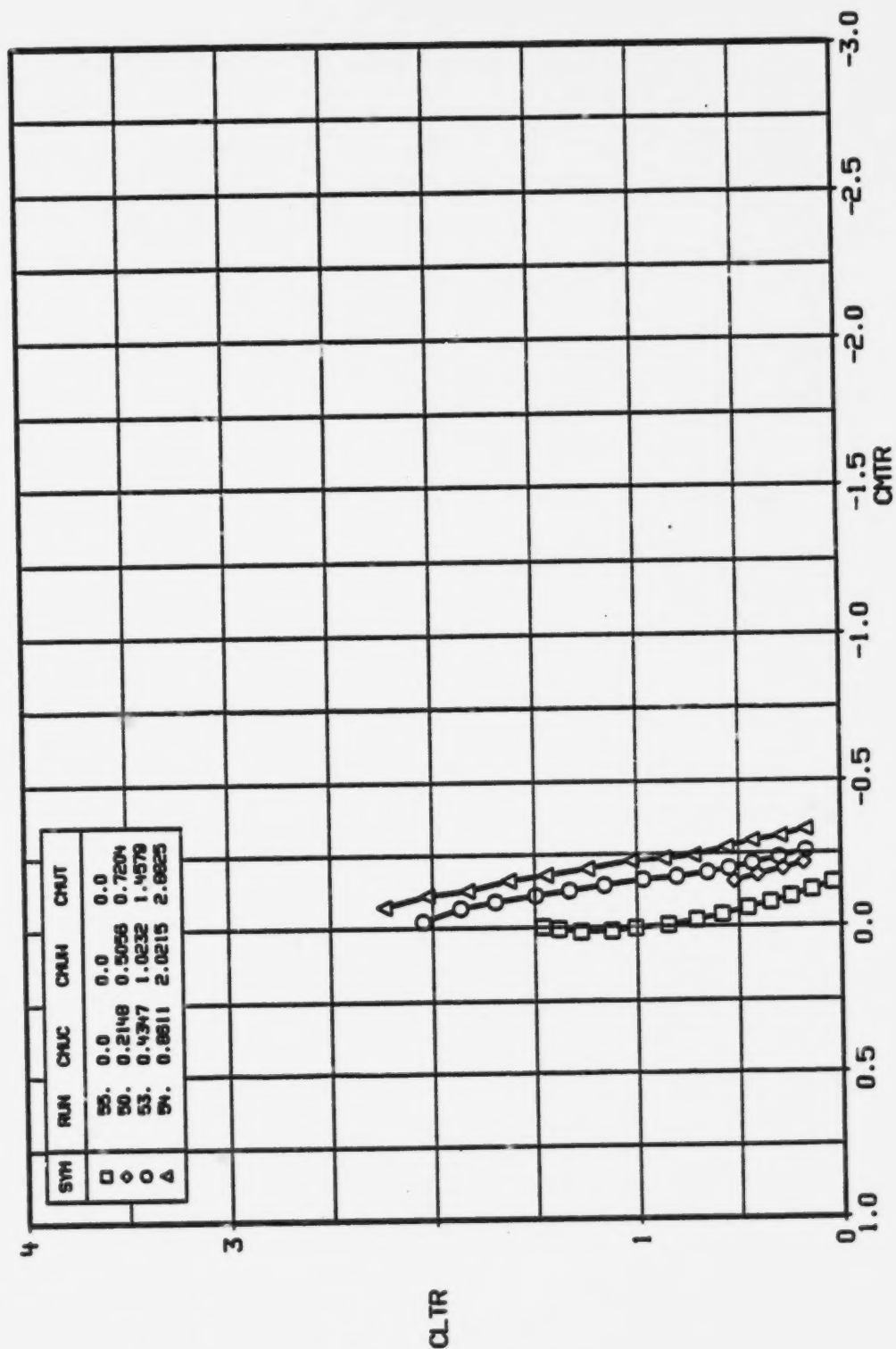


FIGURE A1f BASIC DATA EFFECT OF CMJ
CONFIGURATION BC146V, DELF=0, BN/B=1

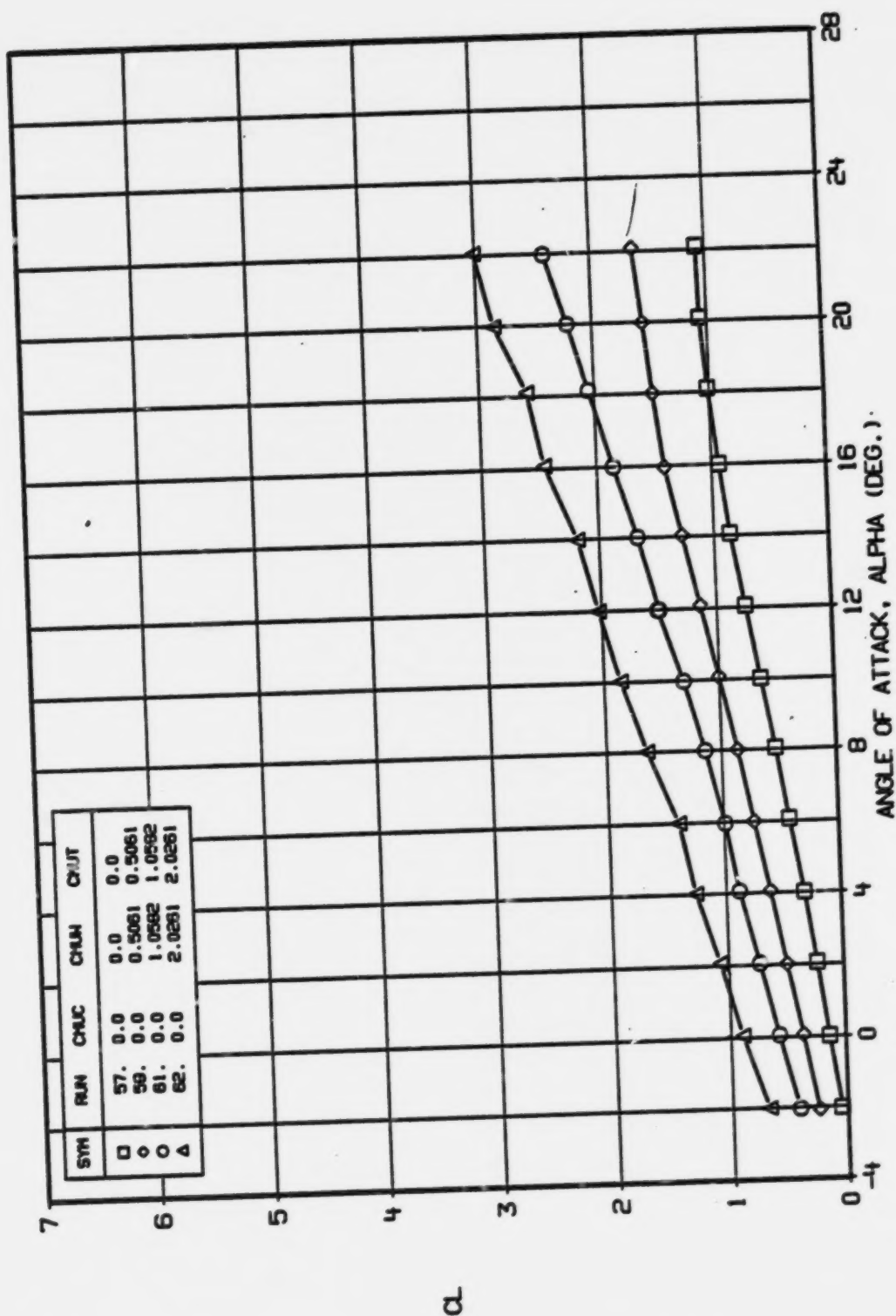


FIGURE A2a BASIC DATA EFFECT OF CMU
CONFIGURATION BM6V, DELF=0, BN/B=1

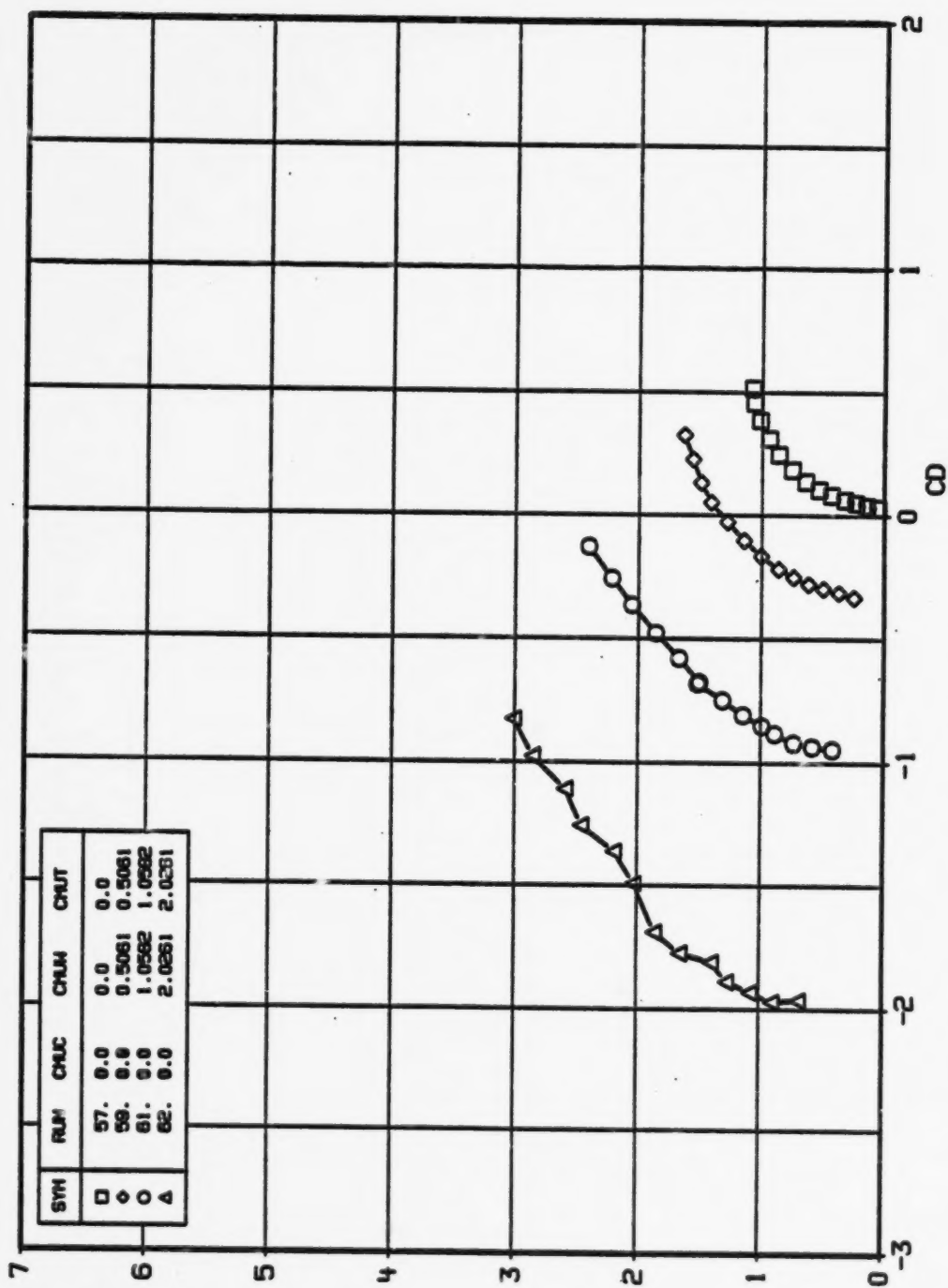


FIGURE A2b BASIC DATA EFFECT OF CMJ
CONFIGURATION B46V, DELF=0, BN/9=1

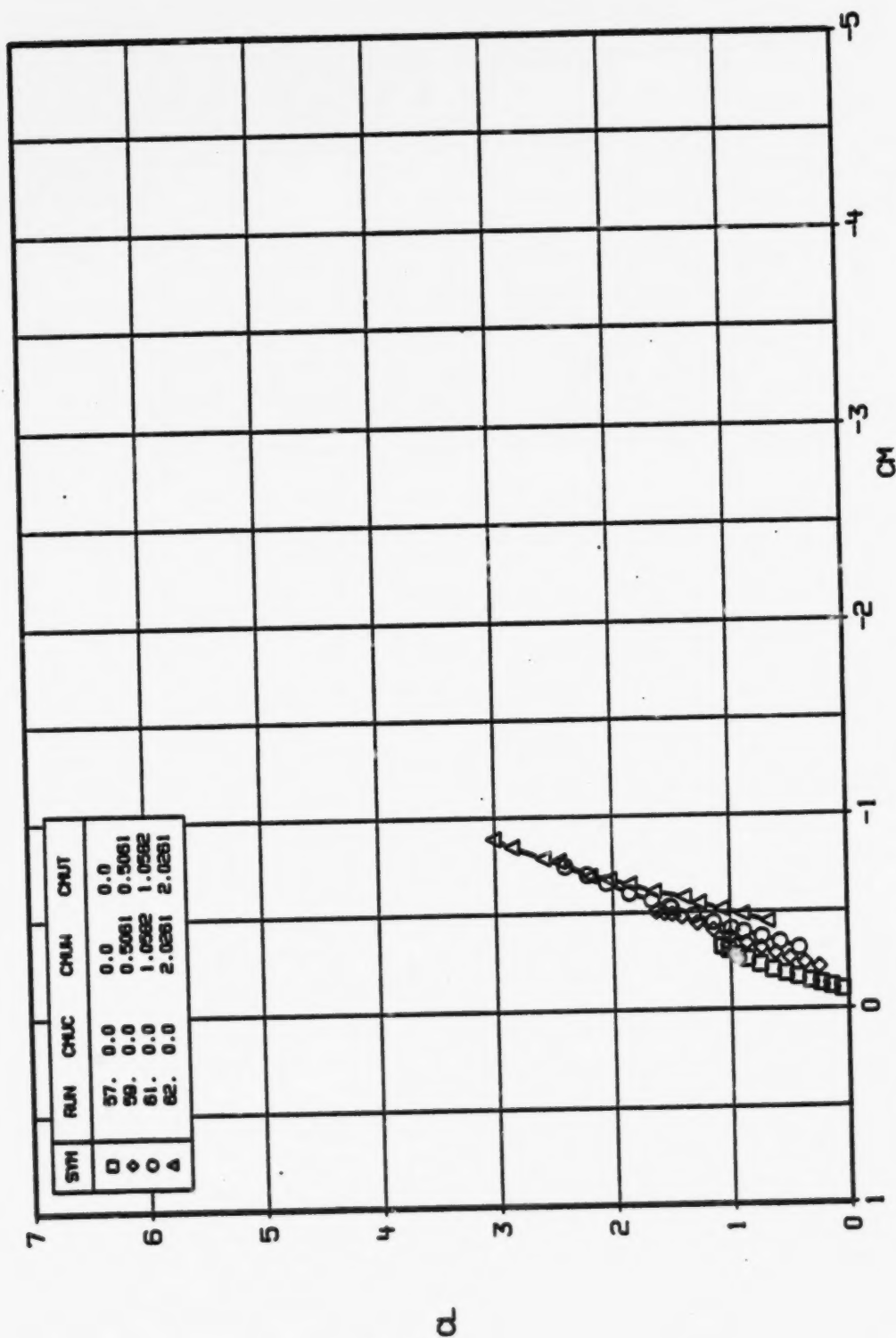


FIGURE A2c BASIC DATA EFFECT OF CMJ
CONFIGURATION B46V, DELF=0, BN/B=1

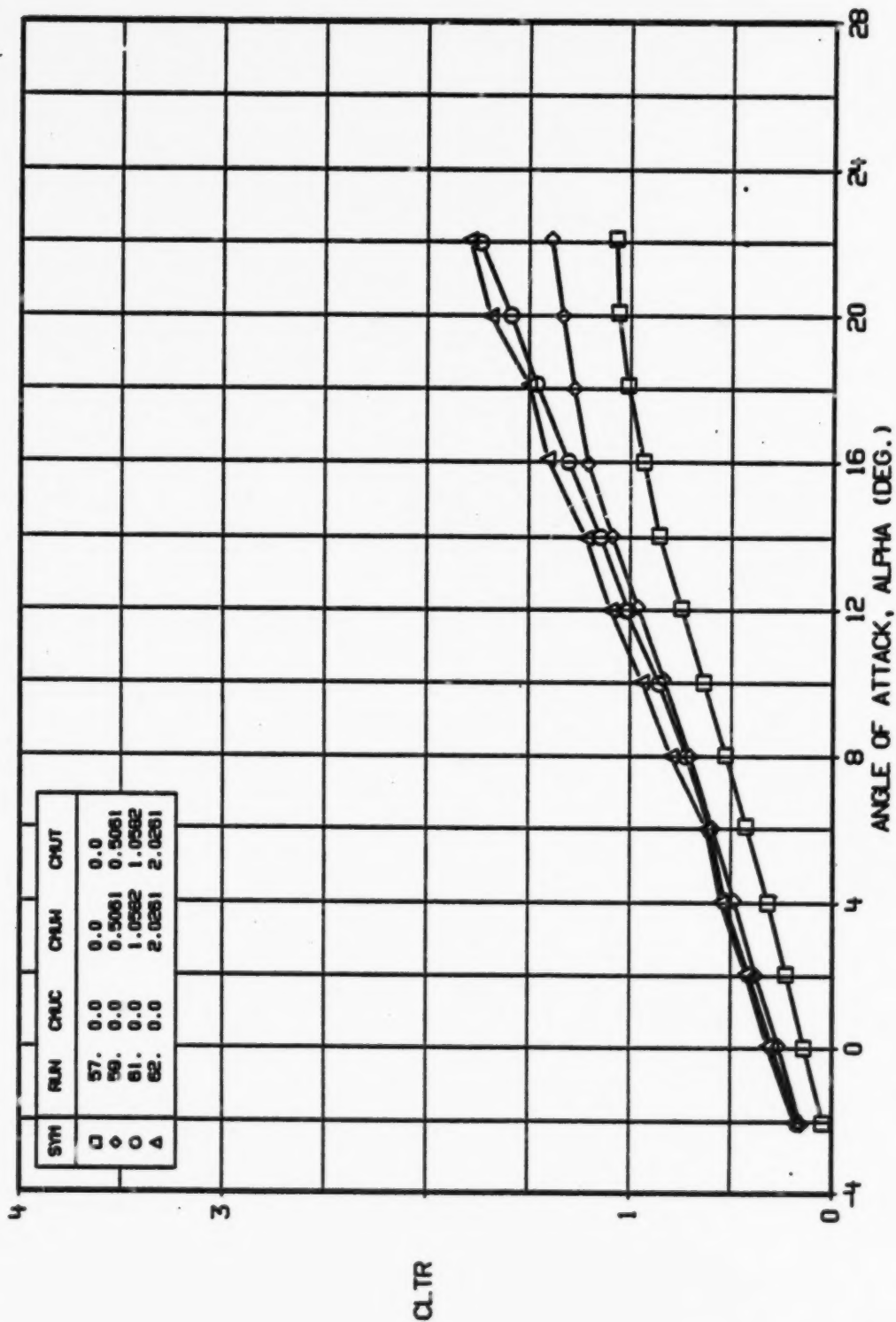


FIGURE A2d BASIC DATA EFFECT OF CHU
CONFIGURATION BMSV, DELF=0, BN/B=1

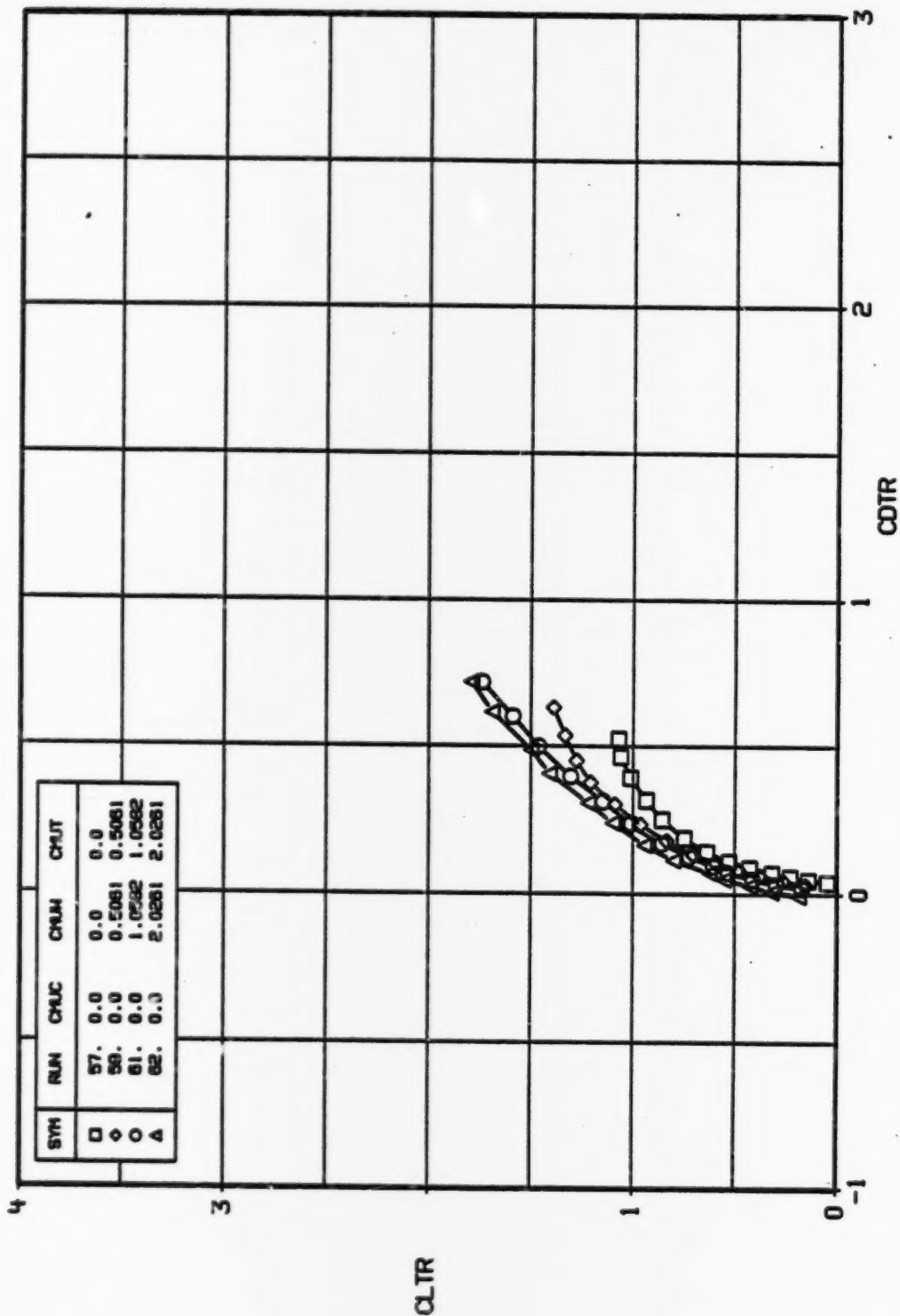


FIGURE A2e BASIC DATA EFFECT OF CMJ
CONFIGURATION B46V, DELF=0, BN/B=1

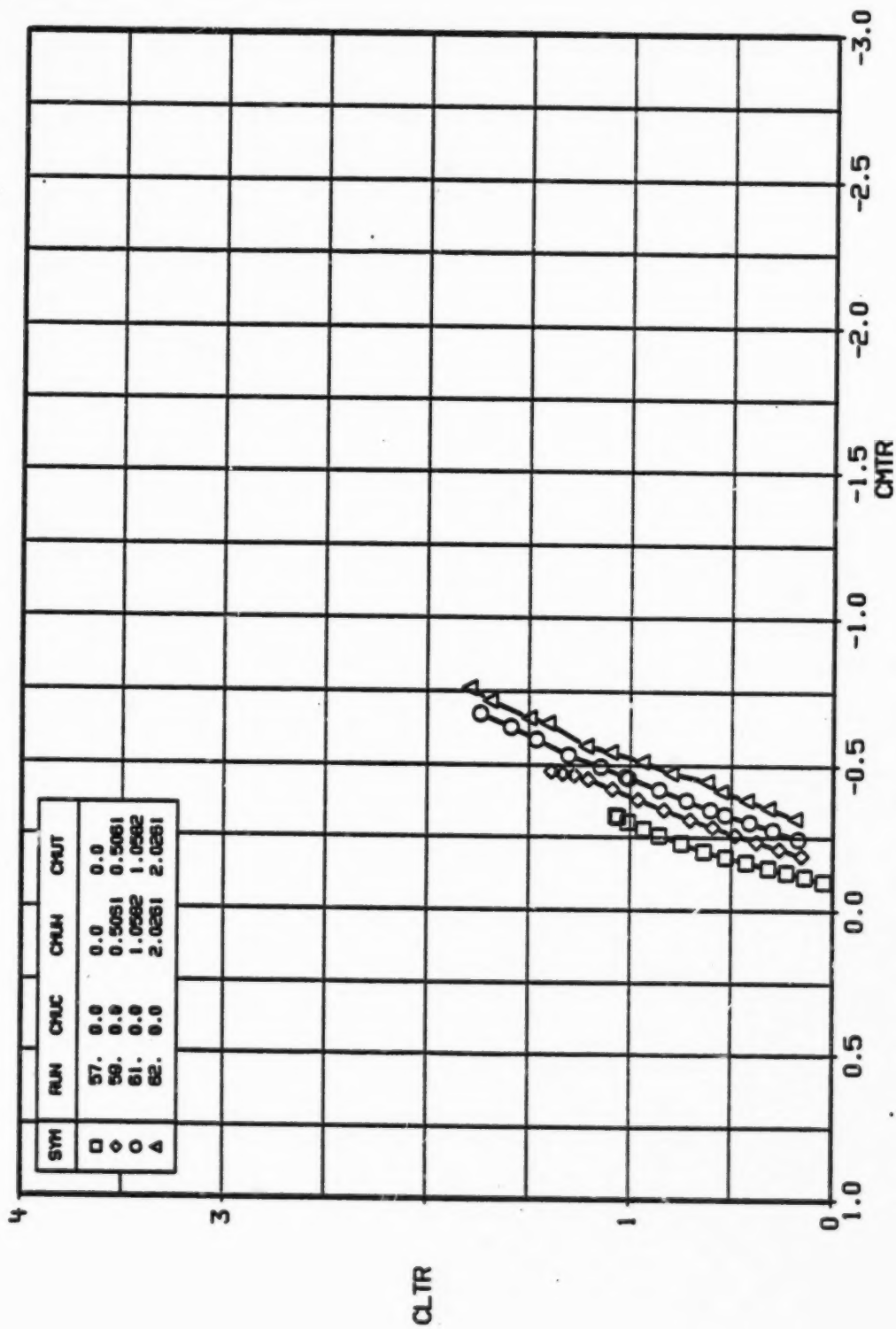


FIGURE A2f BASIC DATA EFFECT OF CMU
CONFIGURATION BMSV, DELF=0, BN/B=1

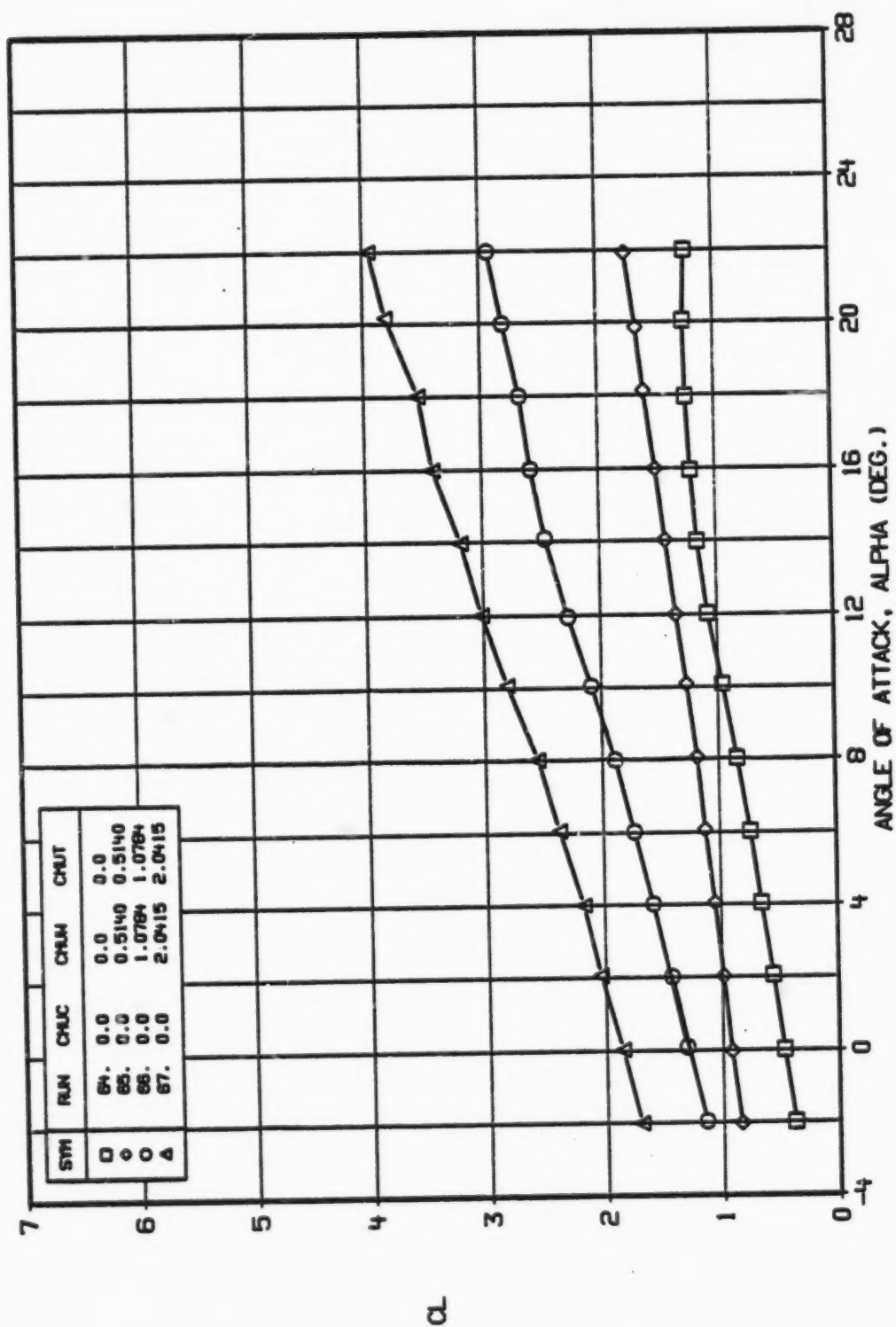


FIGURE A3a BASIC DATA EFFECT OF CMU
CONFIGURATION BN/V, DELF=15, BN/B=1

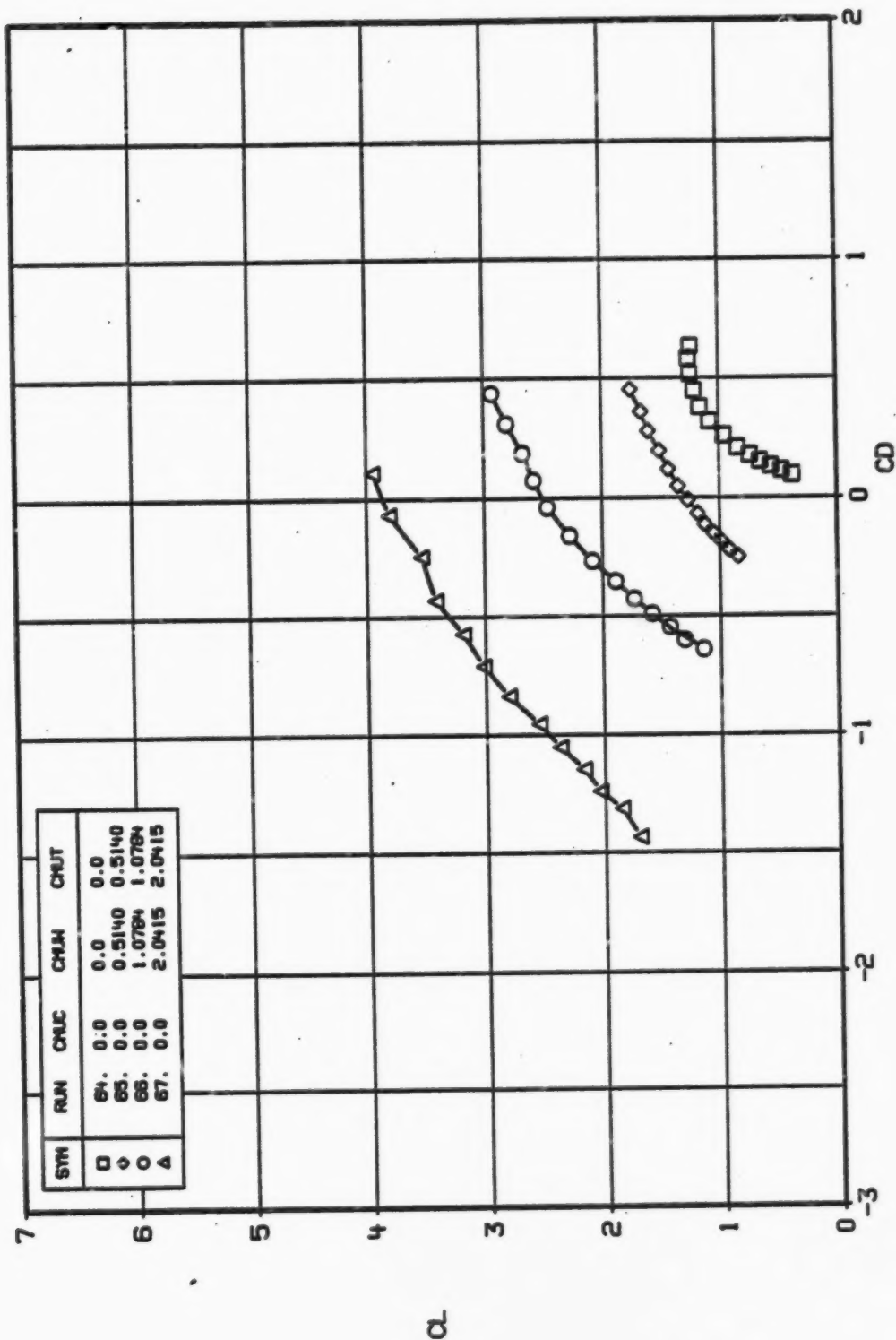


FIGURE A3b BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, DELF=15, BN/B=1

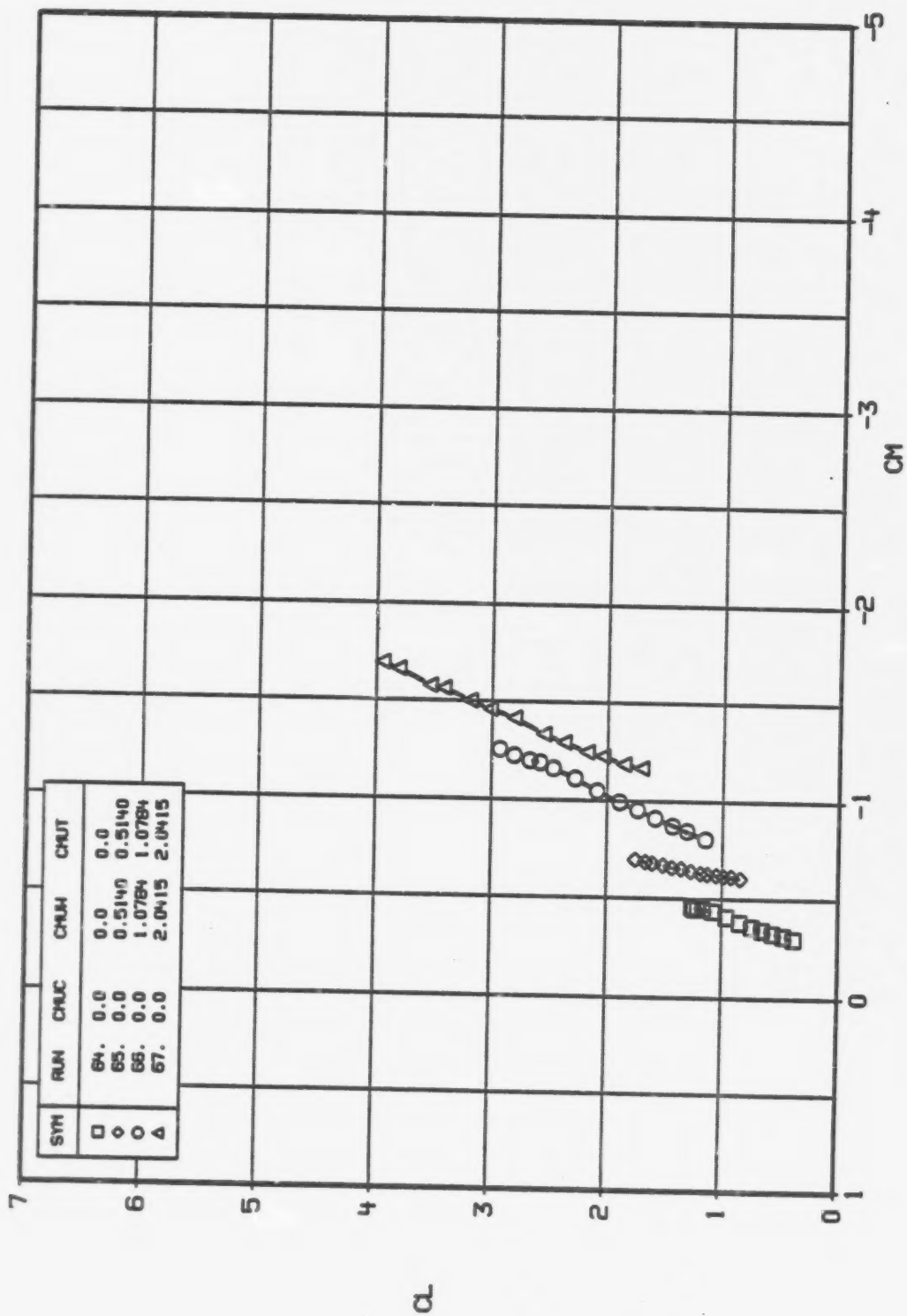


FIGURE A3c BASIC DATA EFFECT OF CMU
CONFIGURATION BMSV, DELF=15, BN/B=1

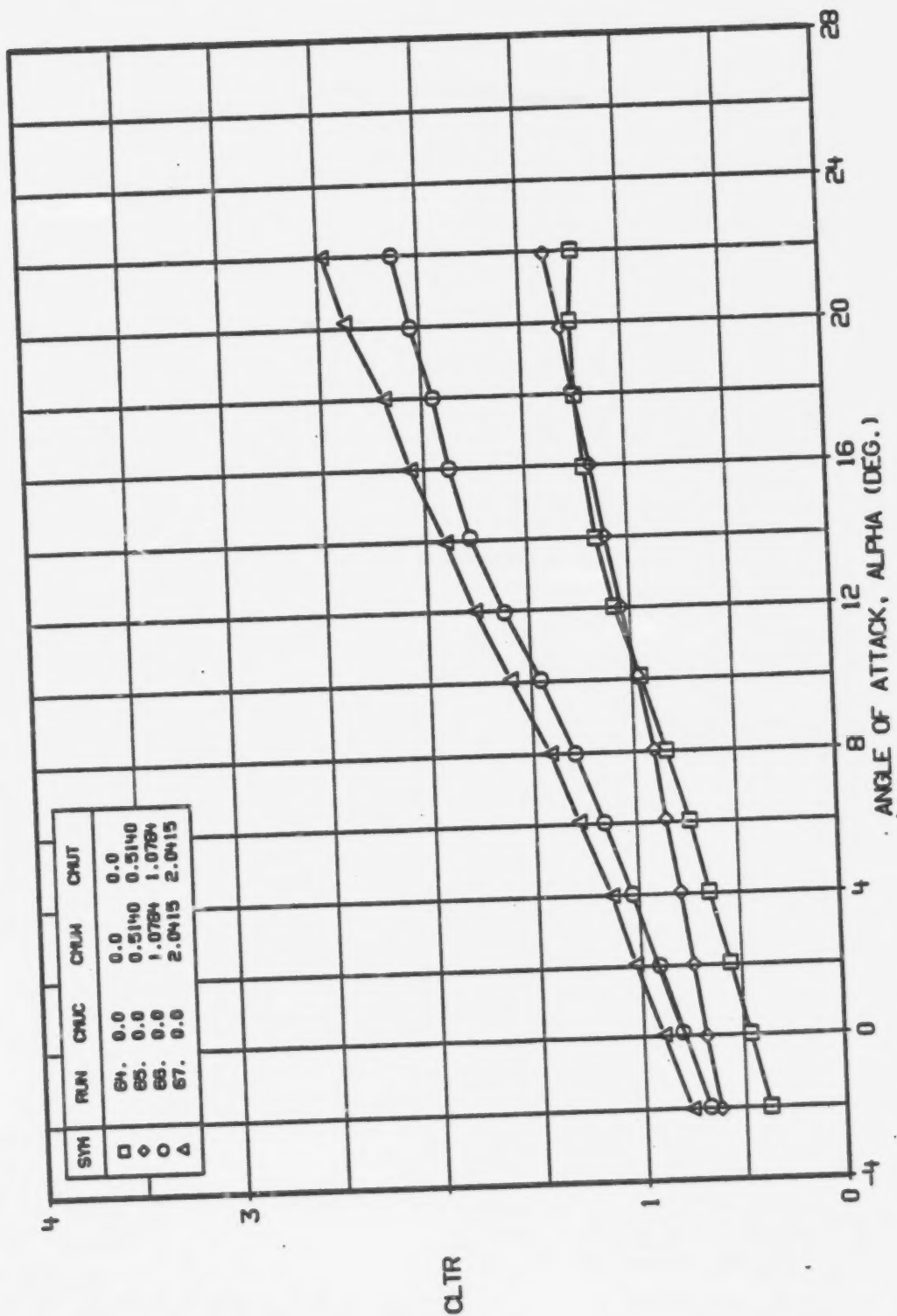


FIGURE A3d BASIC DATA EFFECT OF CMJ
CONFIGURATION BM6V, DELF=15, BN/B=1

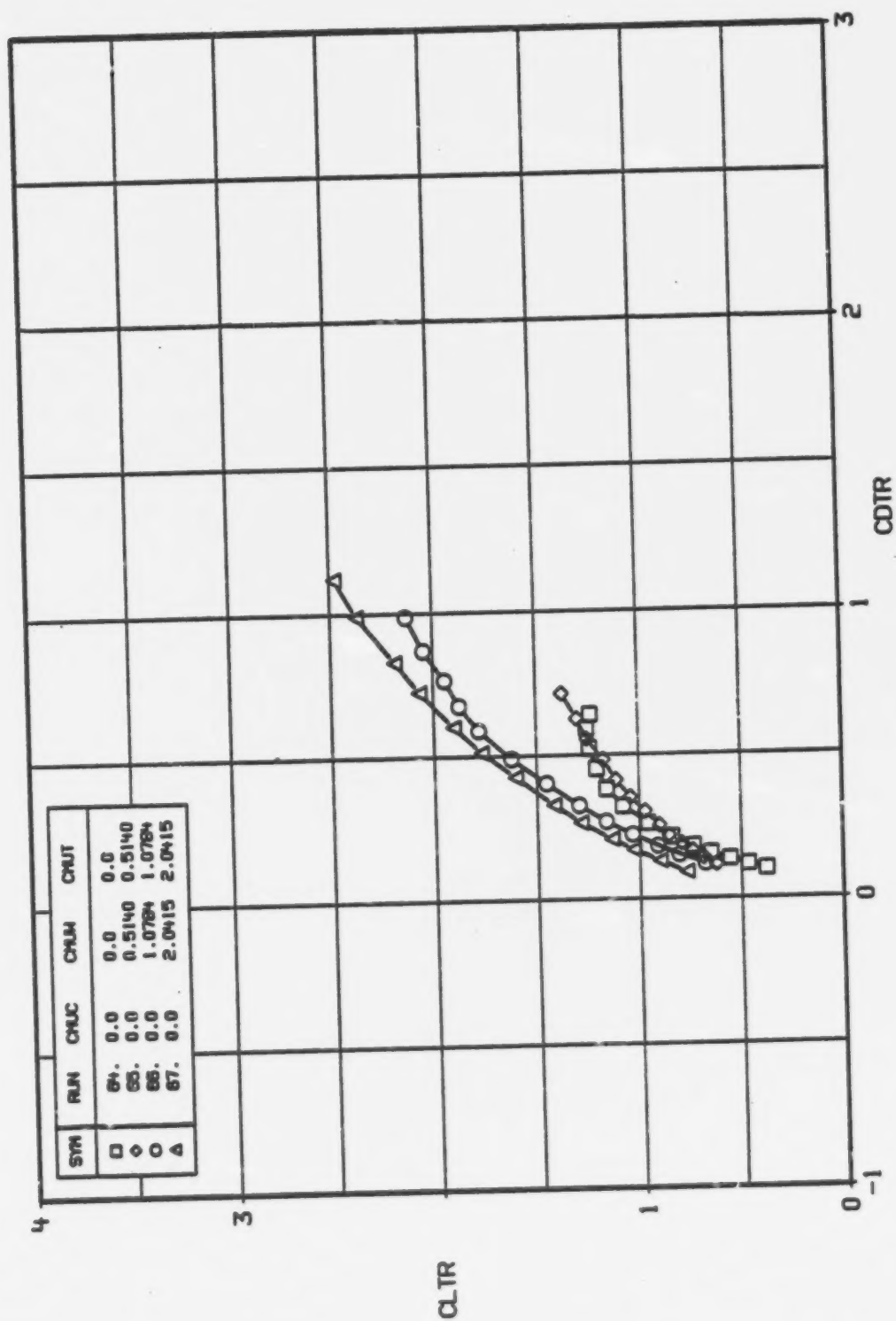


FIGURE A3e BASIC DATA EFFECT OF CMU
CONFIGURATION E46V, DELF=15, BN/B=1

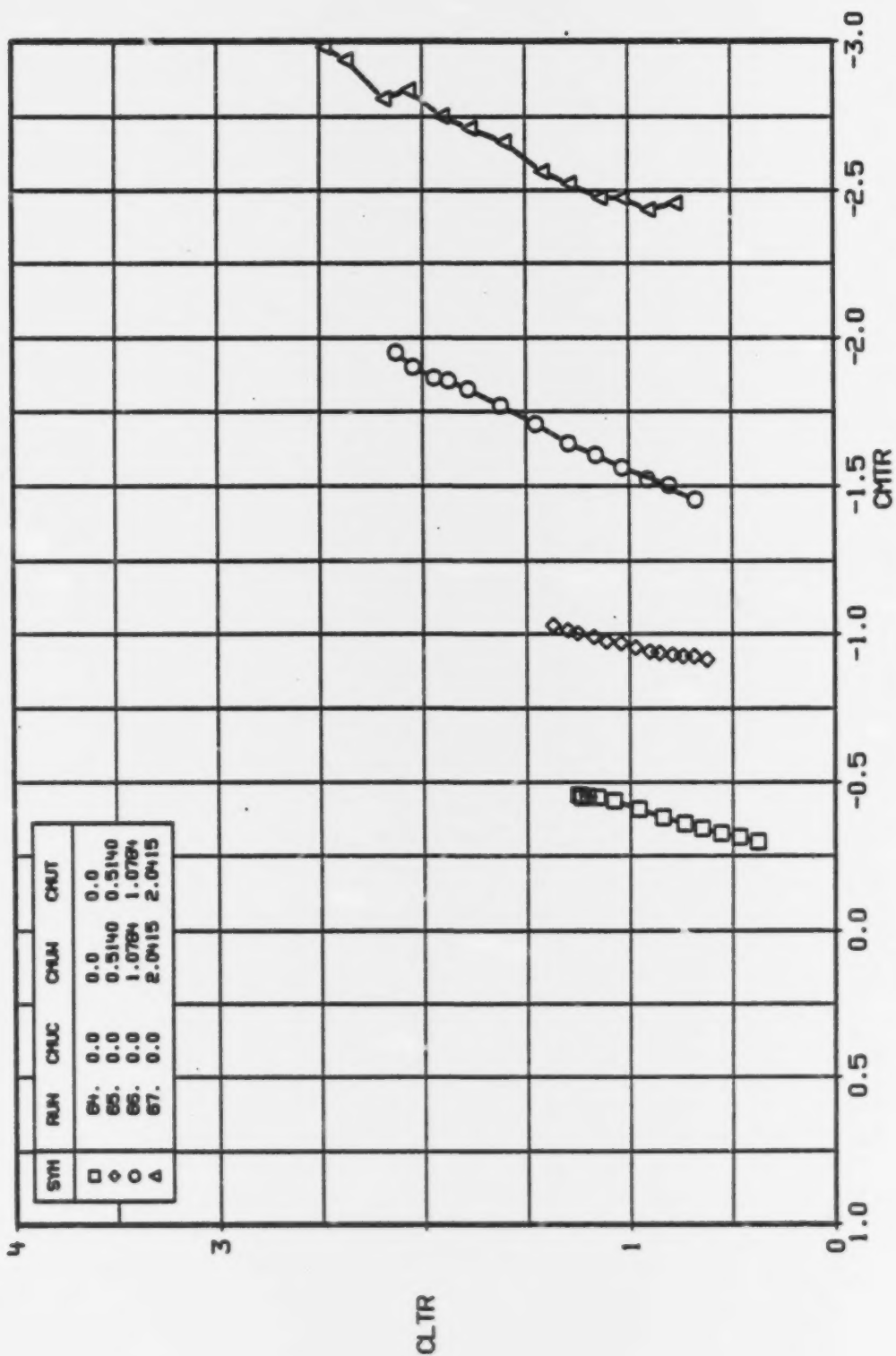


FIGURE A3f BASIC DATA EFFECT OF CHU
CONFIGURATION B46V, DELF=15, BN/B=1

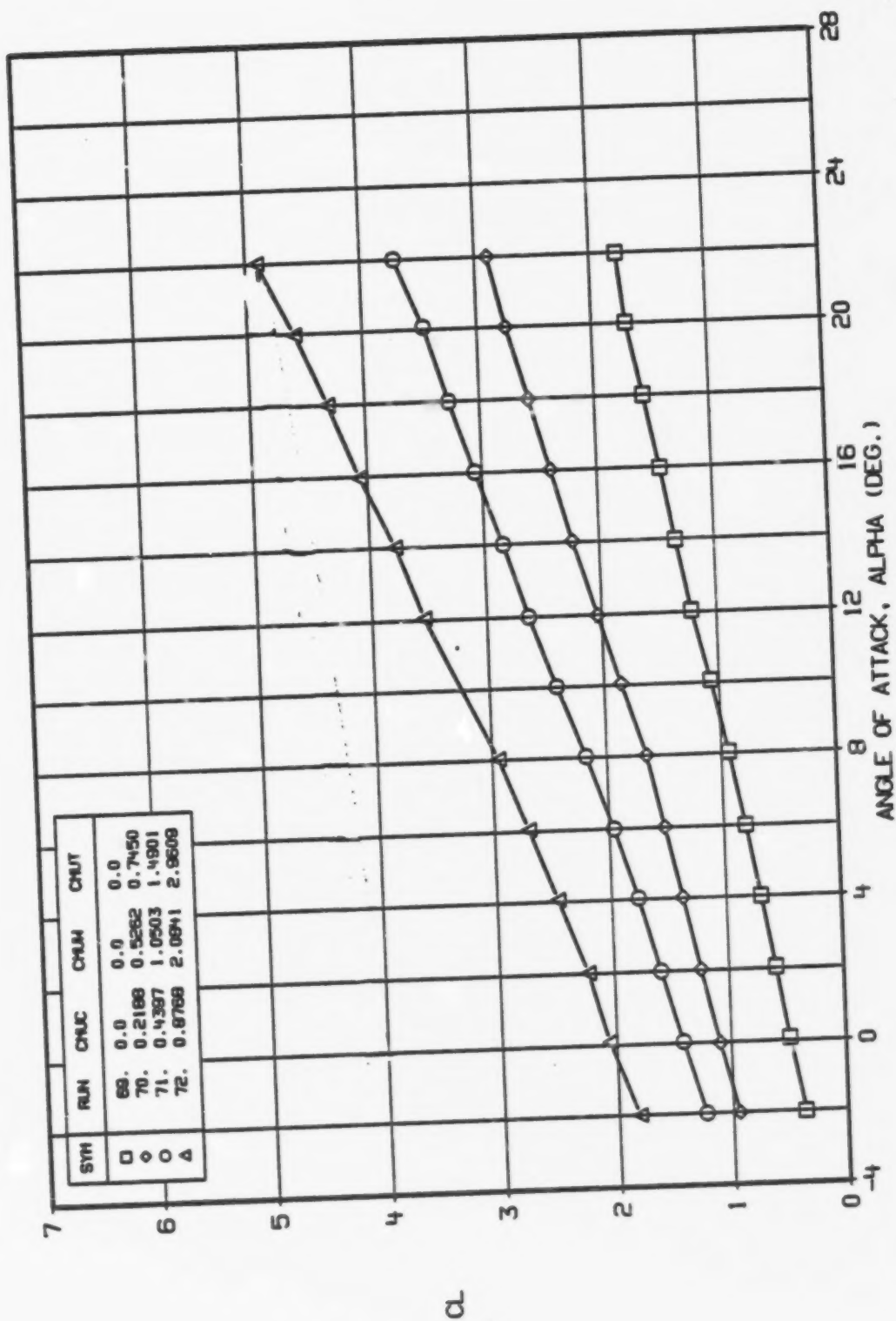


FIGURE A4a BASIC DATA EFFECT OF CMU
CONFIGURATION BC1W5V, DELF=15, BN/B=1

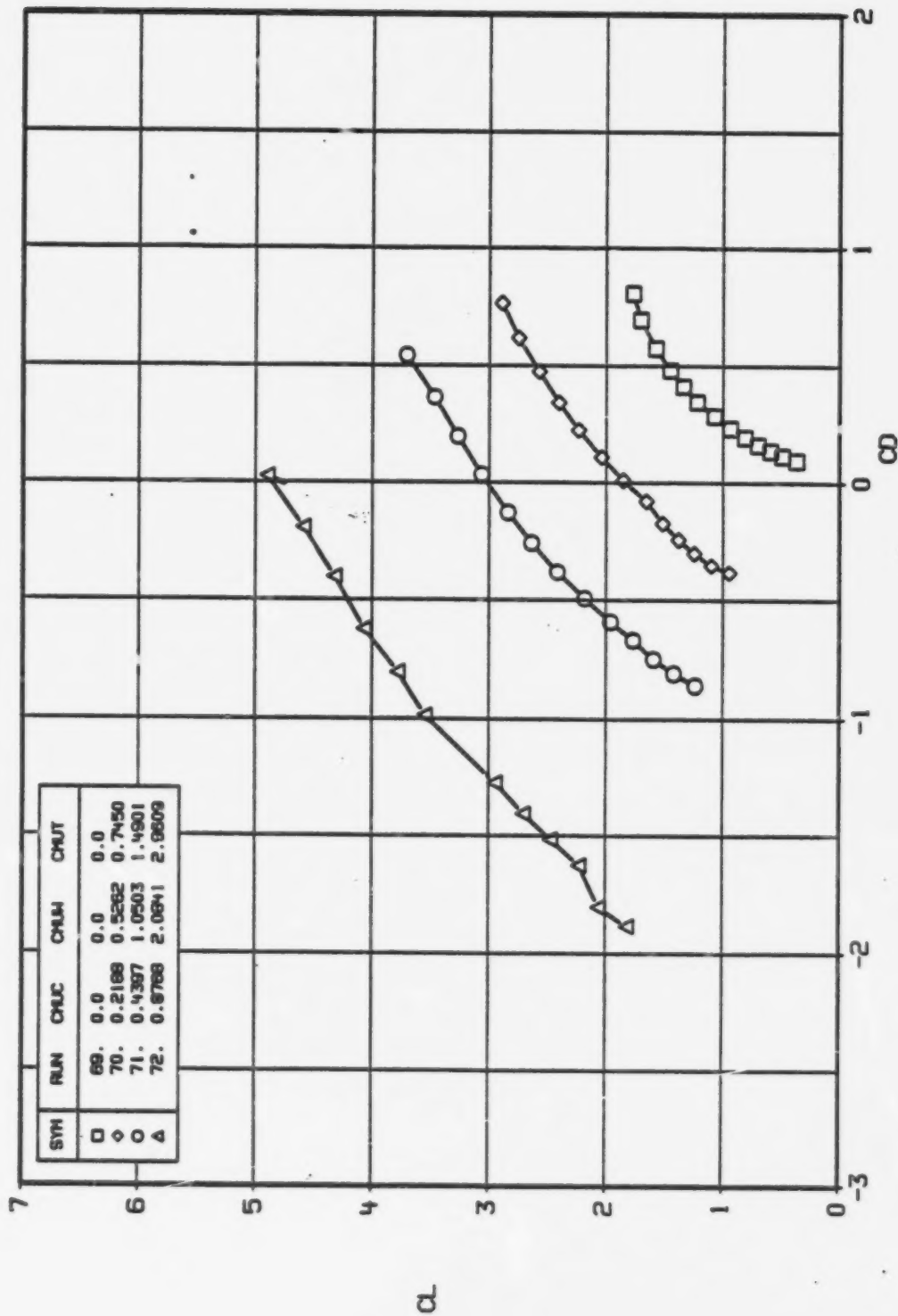


FIGURE A4b BASIC DATA EFFECT OF CMU
CONFIGURATION BC146V, DELF=15, BN/B=1

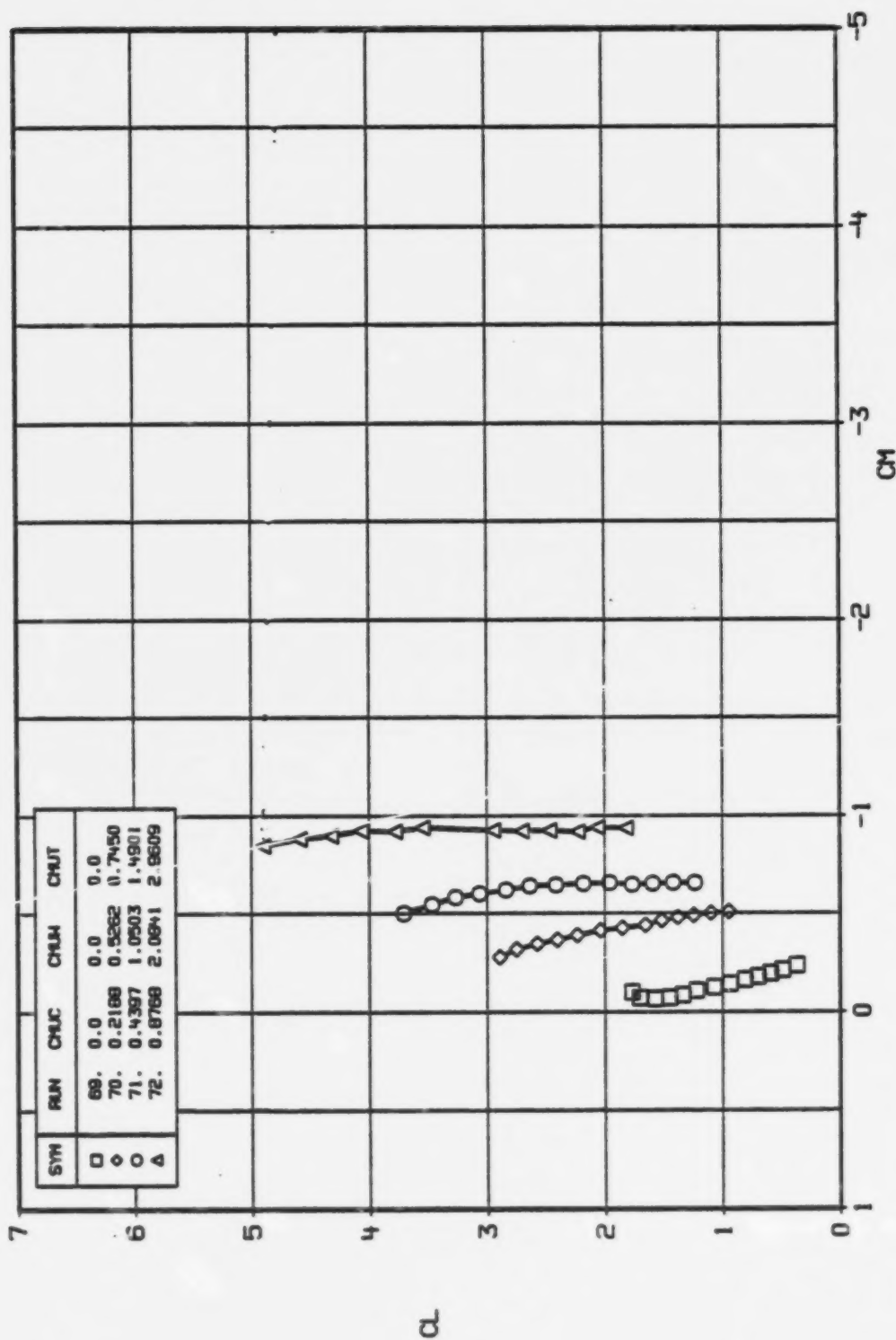


FIGURE A4c BASIC DATA EFFECT OF CMU
CONFIGURATION BC146V, DELF=15, BN/B=1

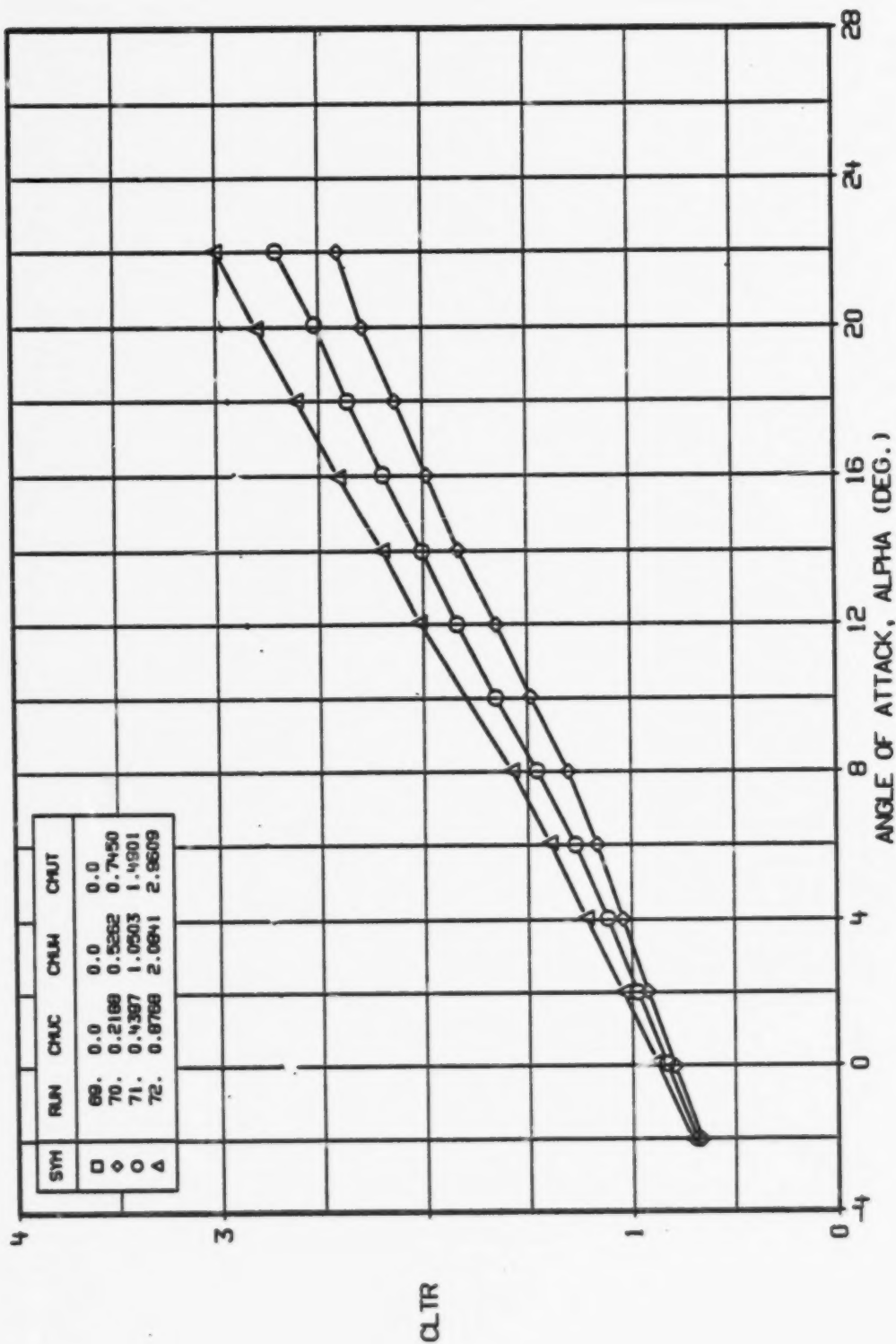


FIGURE A4d BASIC DATA EFFECT OF CMU
CONFIGURATION BC1W6V, DELF=15, BN/B=1

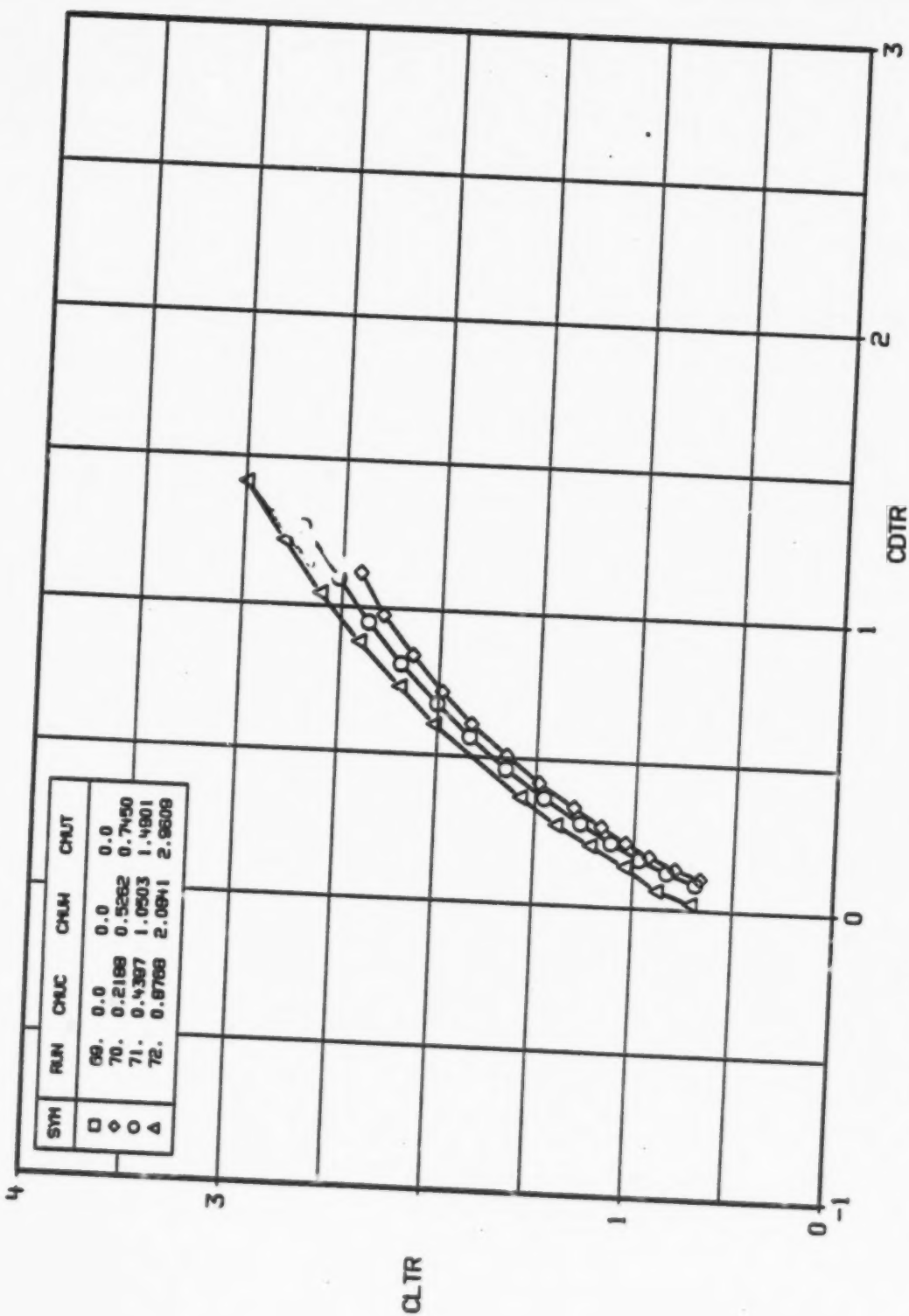


FIGURE A4e BASIC DATA EFFECT OF CHU
CONFIGURATION BC1H5V, DELF=15, BN/B=1

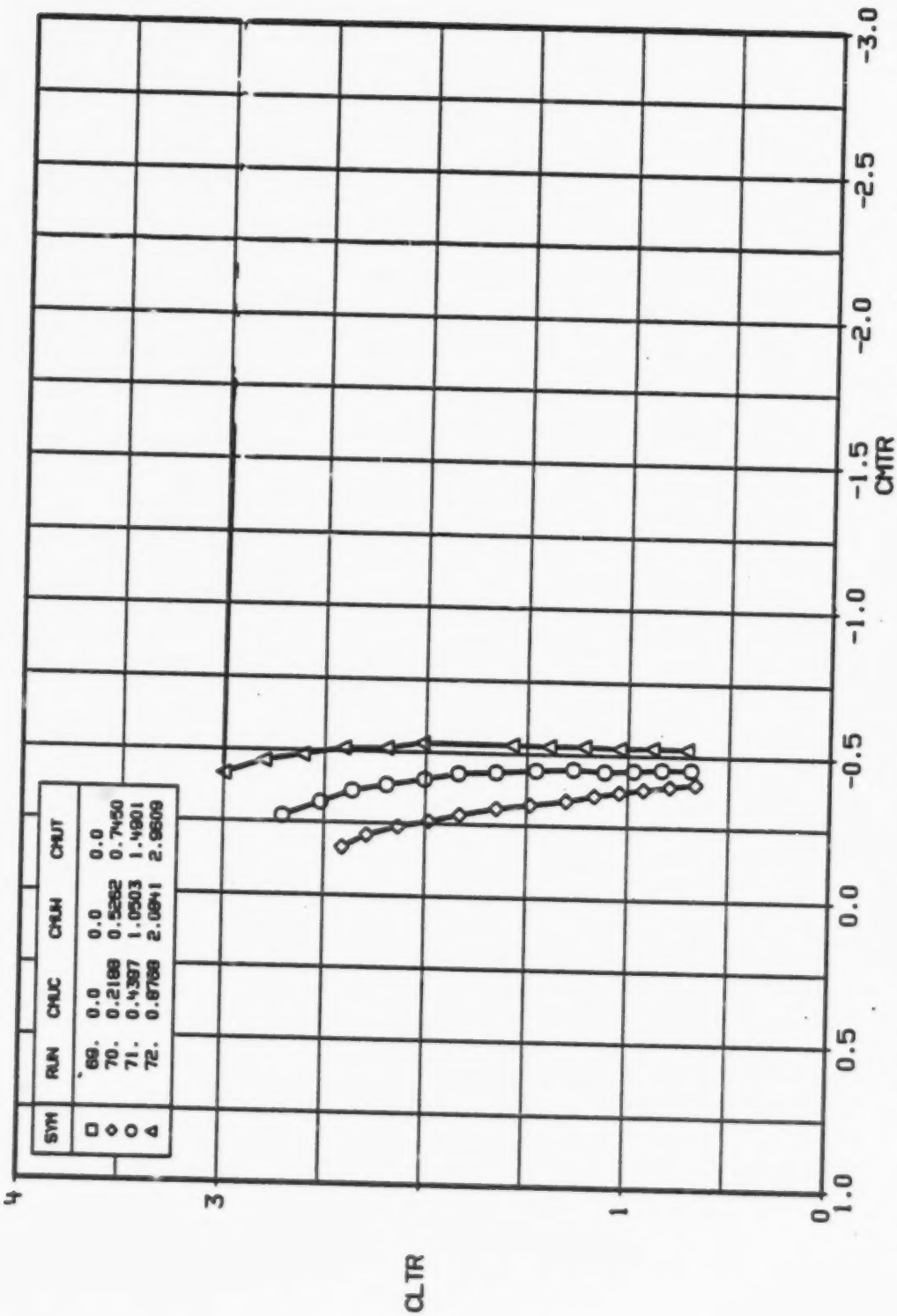


FIGURE A4f BASIC DATA EFFECT OF CMU
CONFIGURATION BC1W6V, DELF=15, BN/B=1

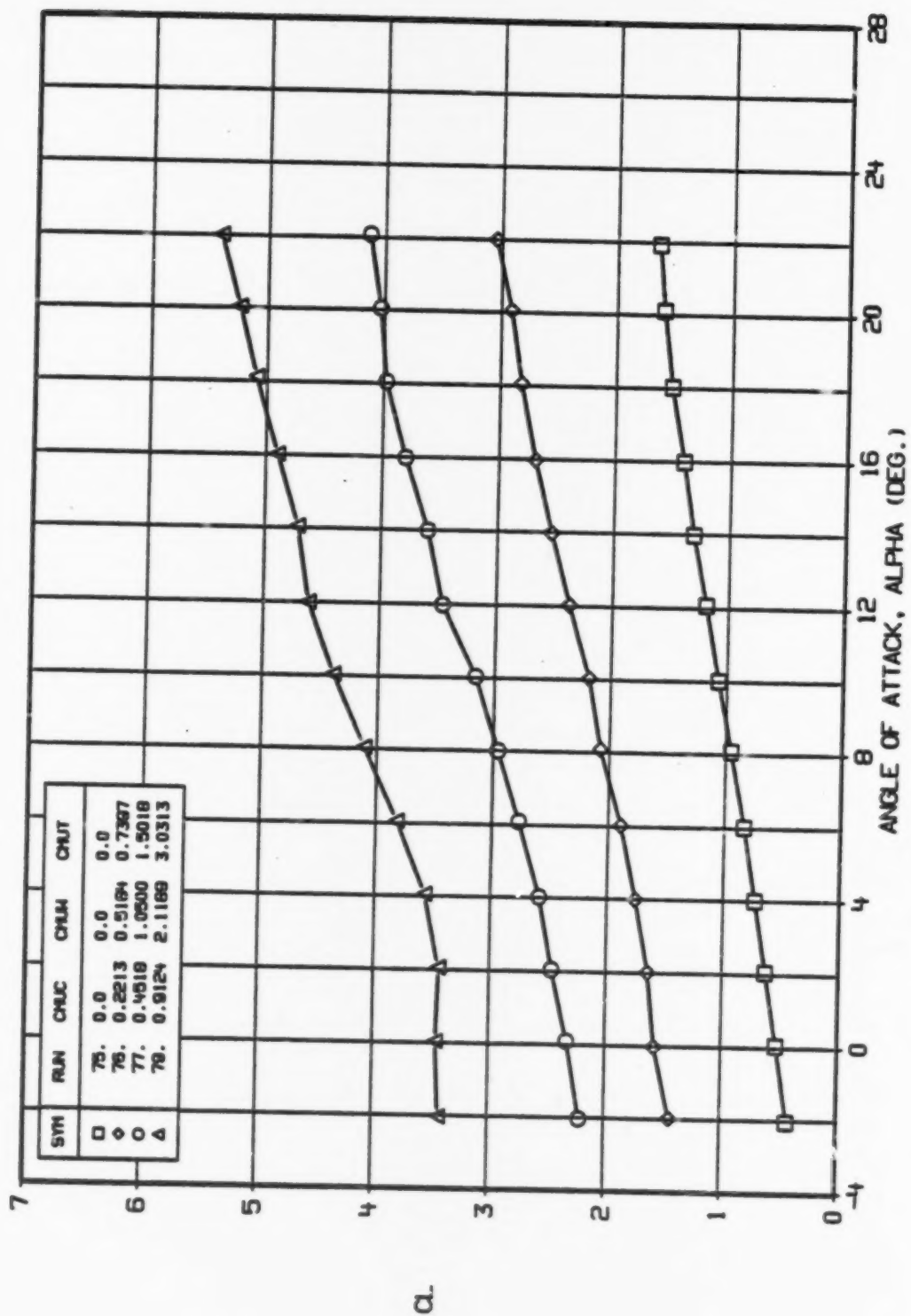


FIGURE A5a BASIC DATA EFFECT OF CHU
CONFIGURATION BC146V, DELF=45, BN/B=1

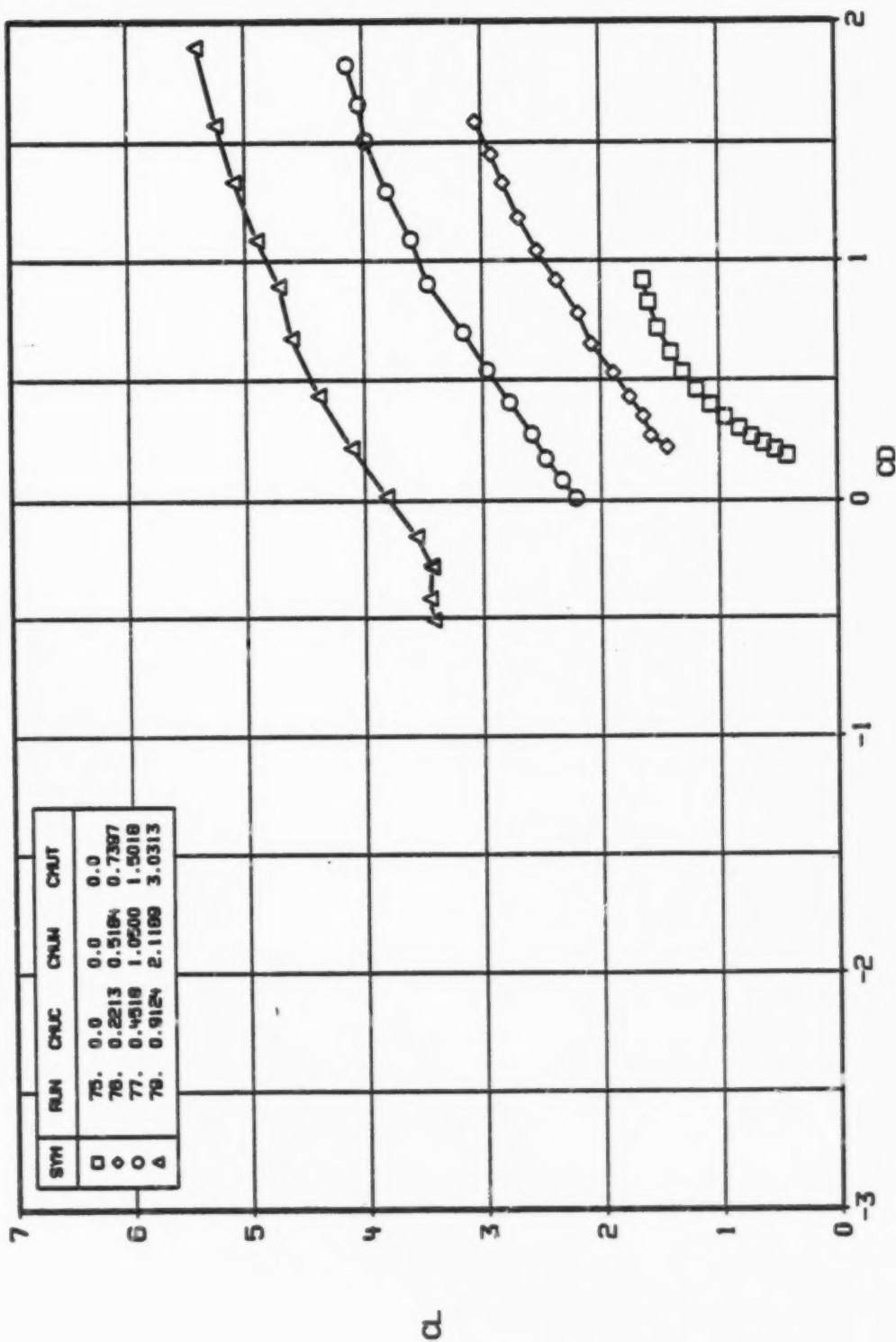


FIGURE A5b BASIC DATA EFFECT OF CMU
CONFIGURATION BC145V, DELF=45, BN/B=1

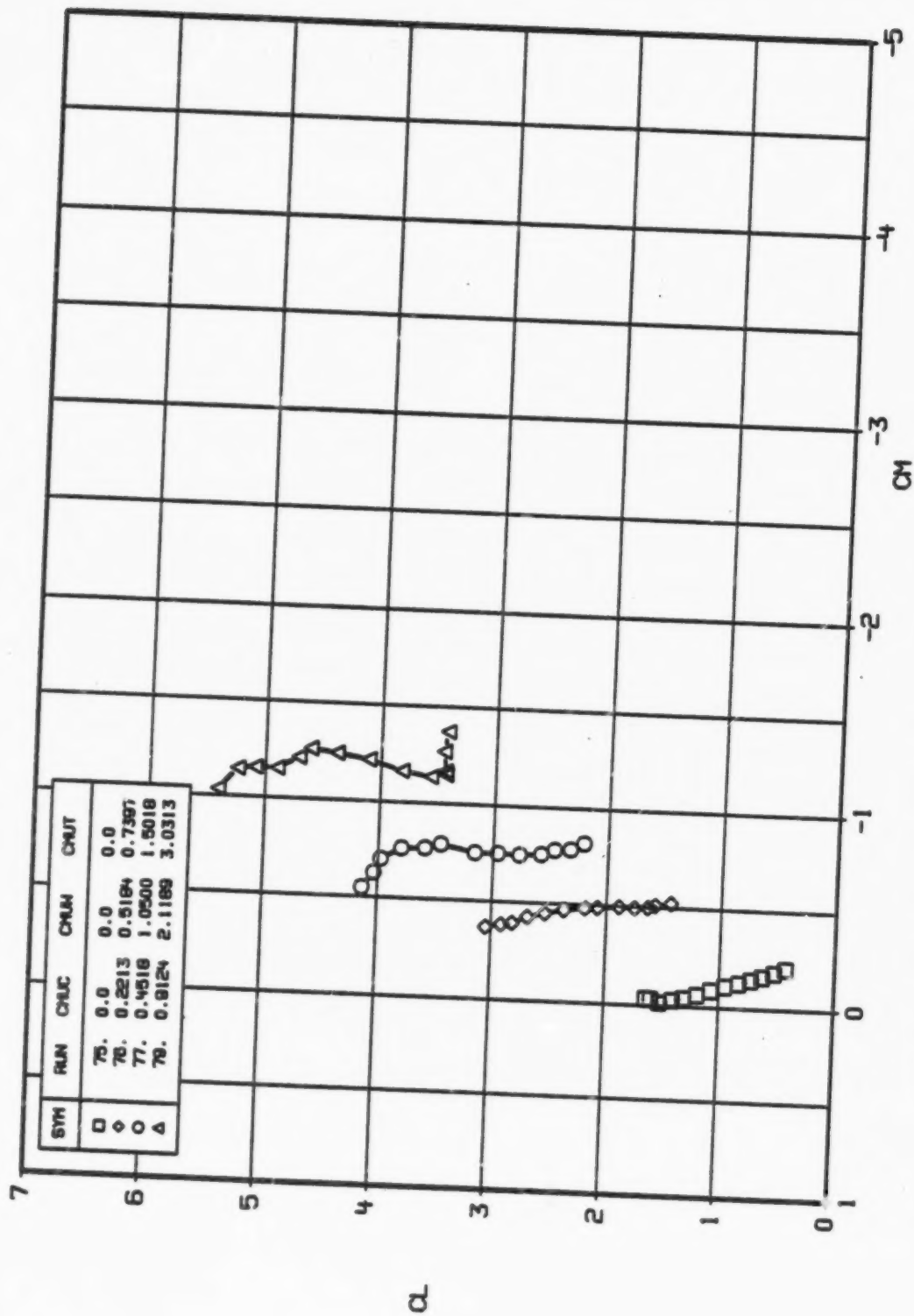


FIGURE A5c BASIC DATA EFFECT OF CMU
CONFIGURATION BC1WSV, DELF=45, BN/B=1

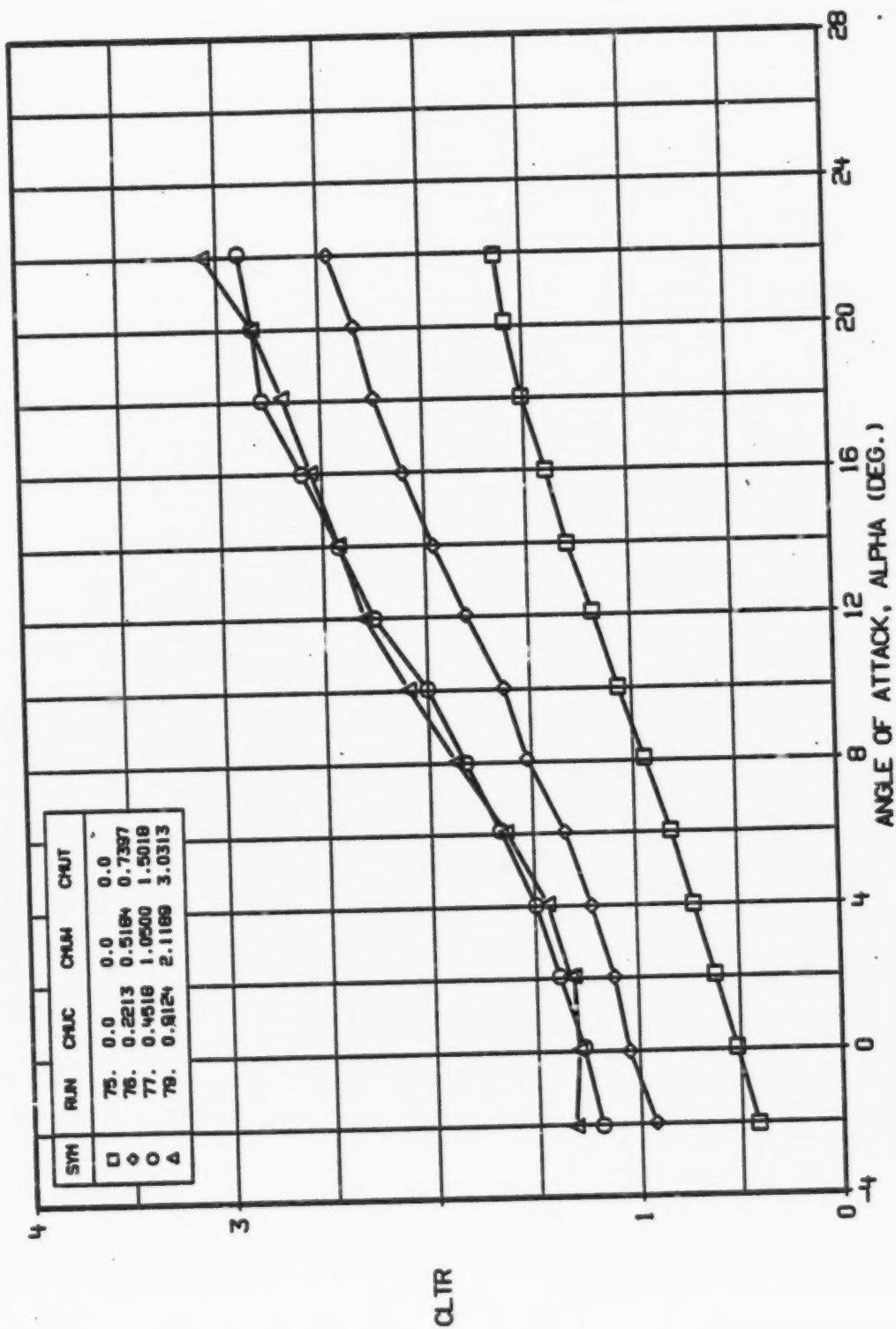


FIGURE A5d BASIC DATA EFFECT OF CMJ
CONFIGURATION BC1W5V, DELF=45, BN/B=1

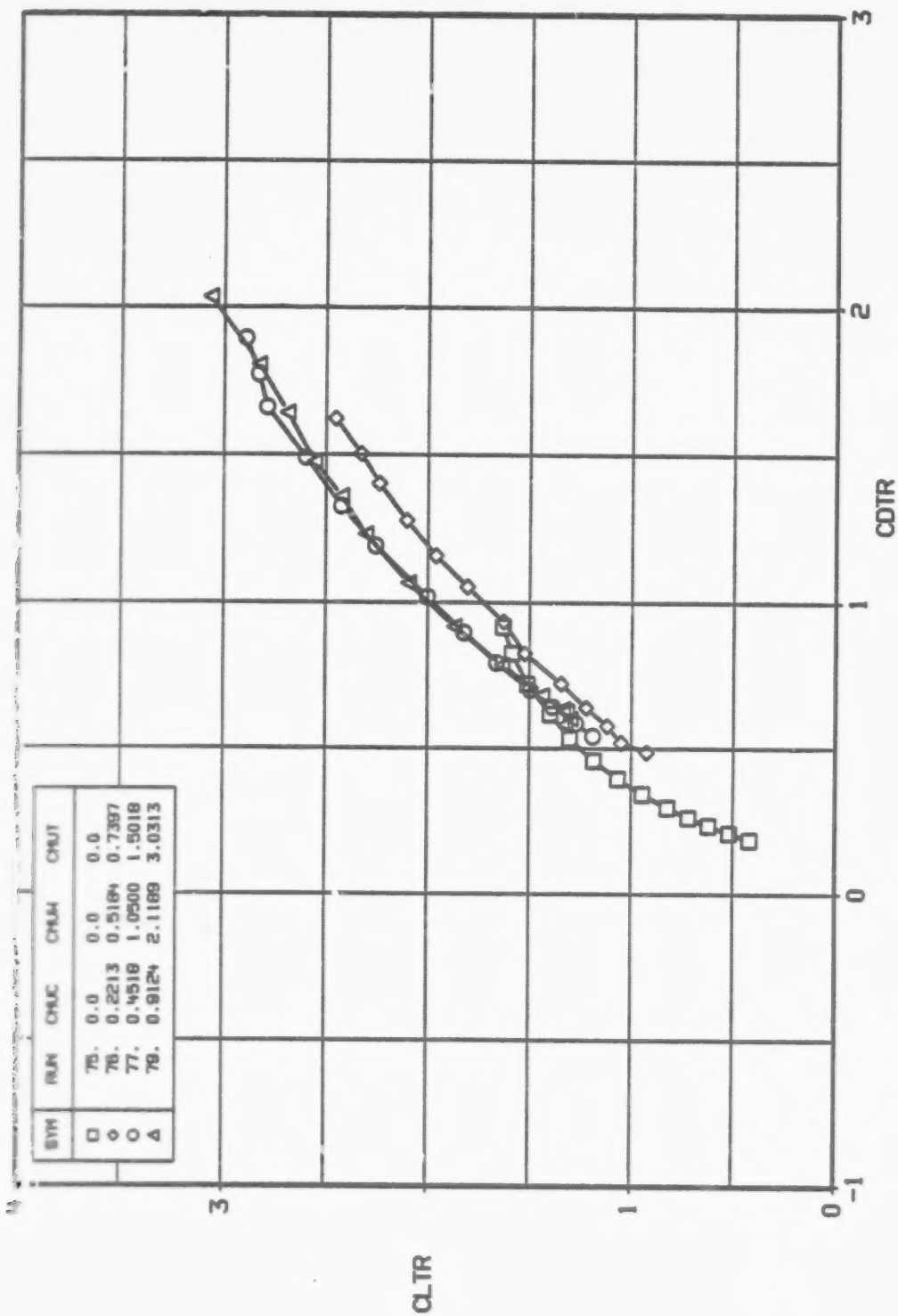


FIGURE A5e BASIC DATA EFFECT OF CMU
CONFIGURATION BC1W6V, DELF=45, BN/B=1

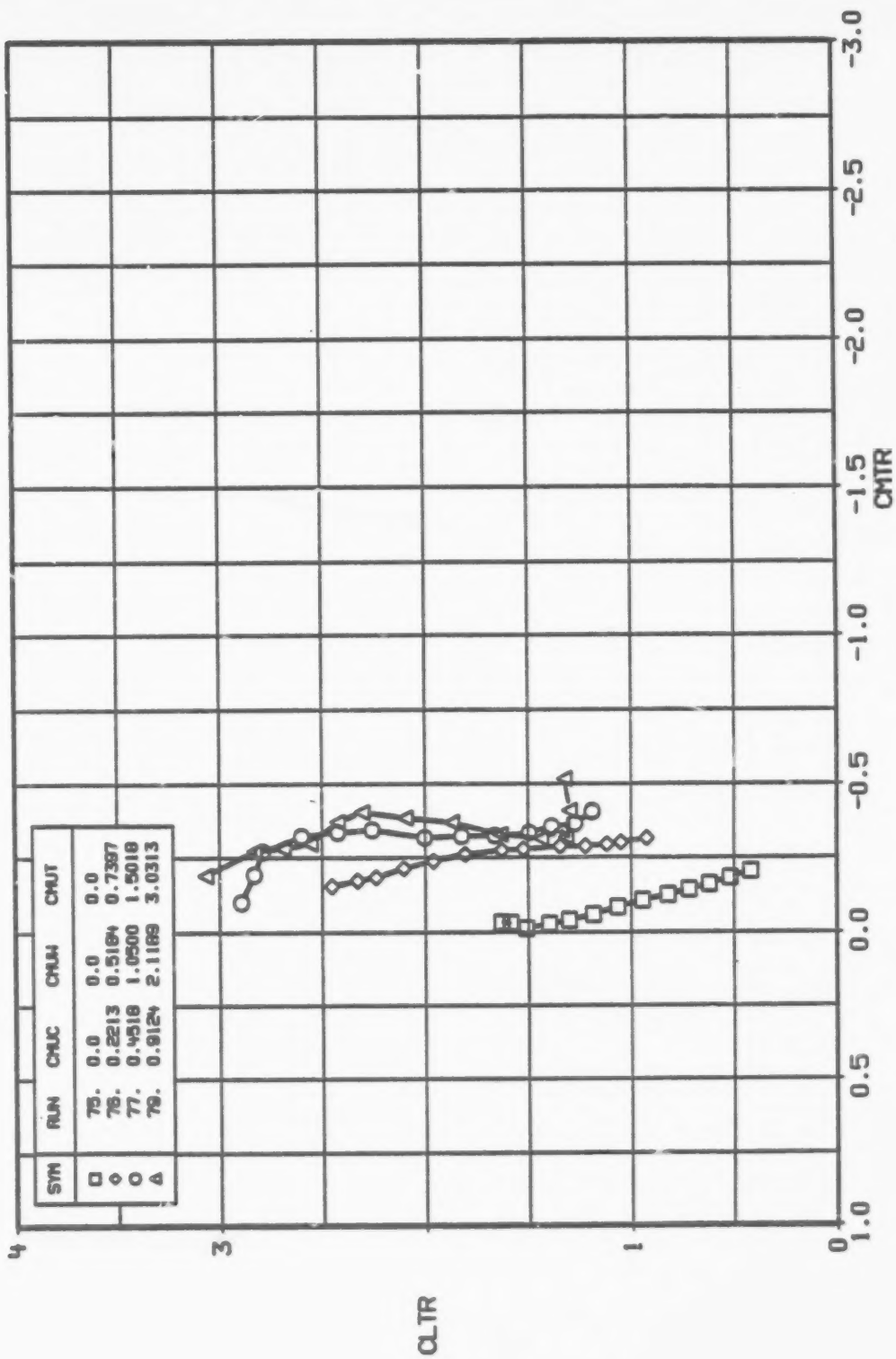


FIGURE A5f BASIC DATA EFFECT OF CHU
CONFIGURATION BC146V, DELF=45, BN/B=1

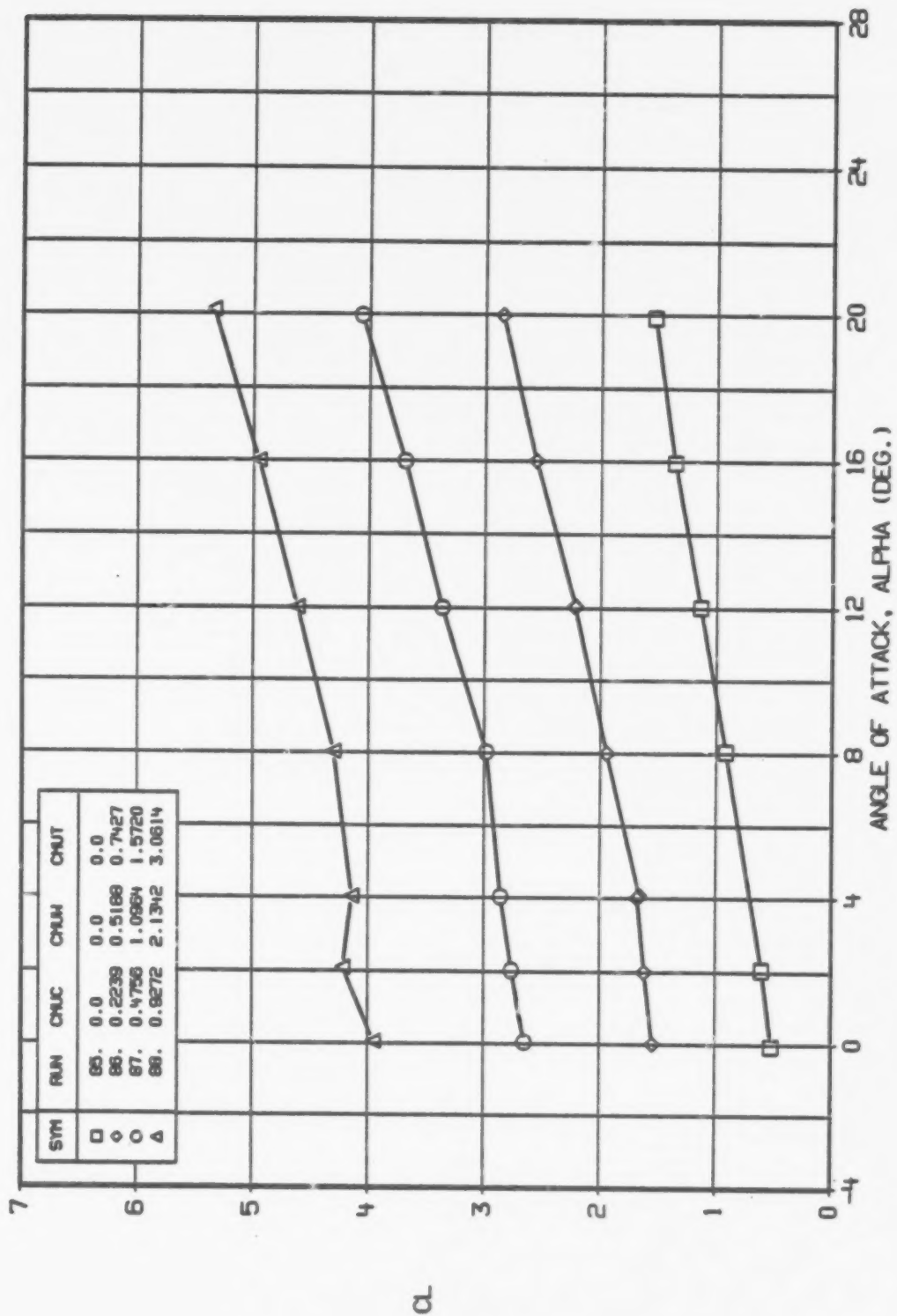


FIGURE A6a BASIC DATA EFFECT OF CMU
CONFIGURATION BC246V, DELF=45, BN/B=1

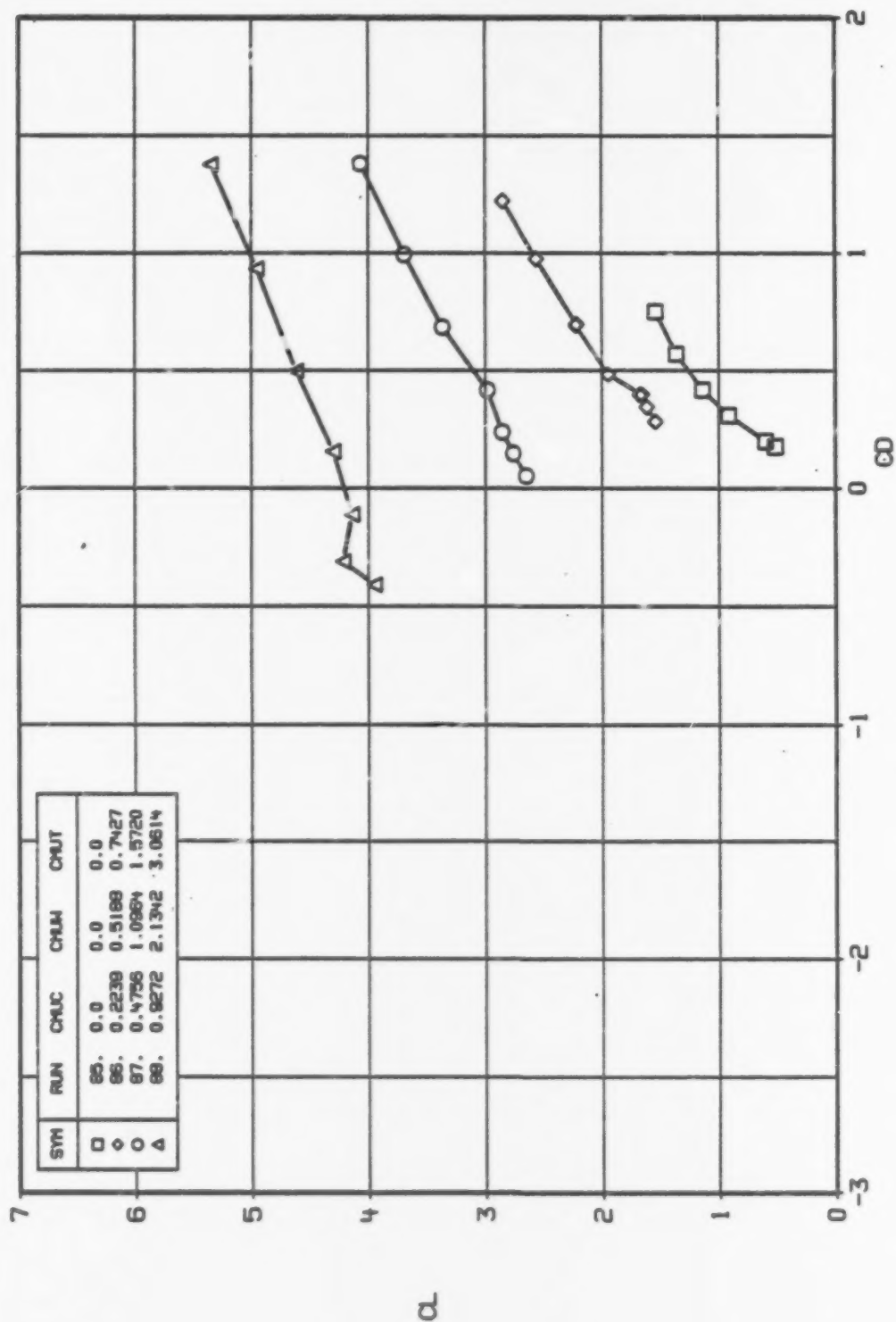


FIGURE A6b BASIC DATA EFFECT OF CMU
CONFIGURATION BC246V, DELF=45, BN/B=1

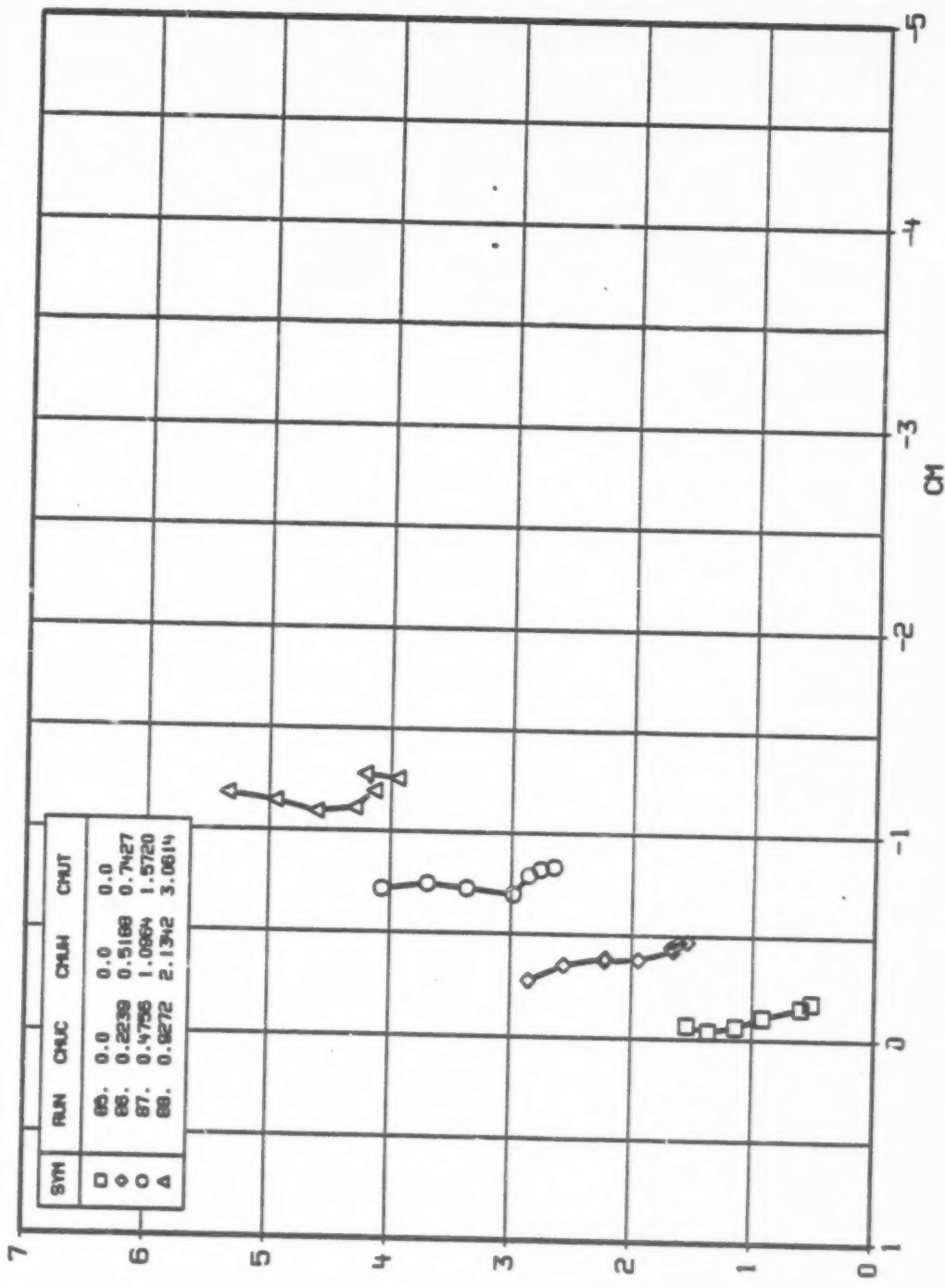


FIGURE A6c BASIC DATA EFFECT OF CMU
CONFIGURATION BC2MSV, DELF=45, BN/B=1

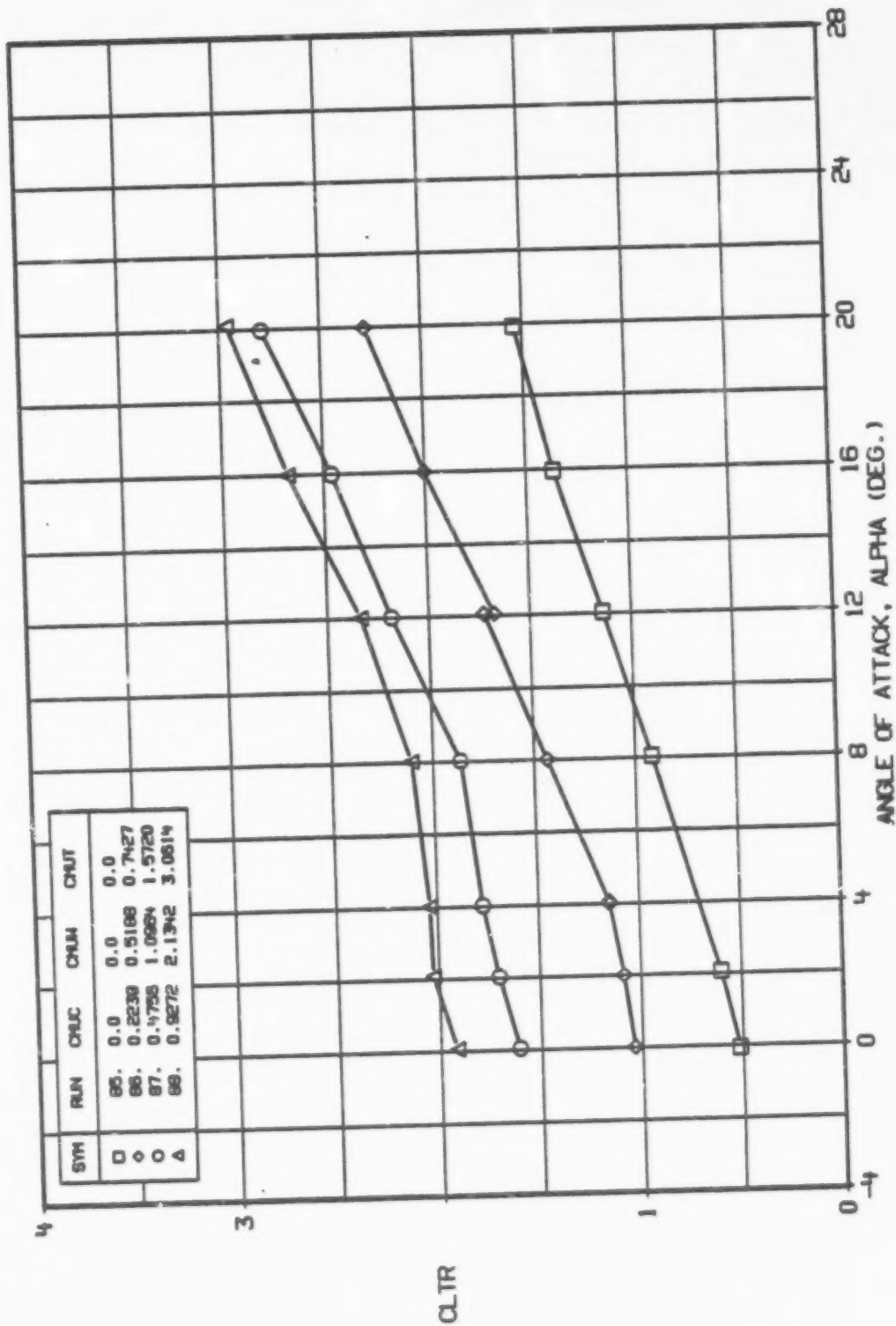


FIGURE A6d BASIC DATA EFFECT OF CHU
CONFIGURATION BC24EV, DELF=45, BN/B=1

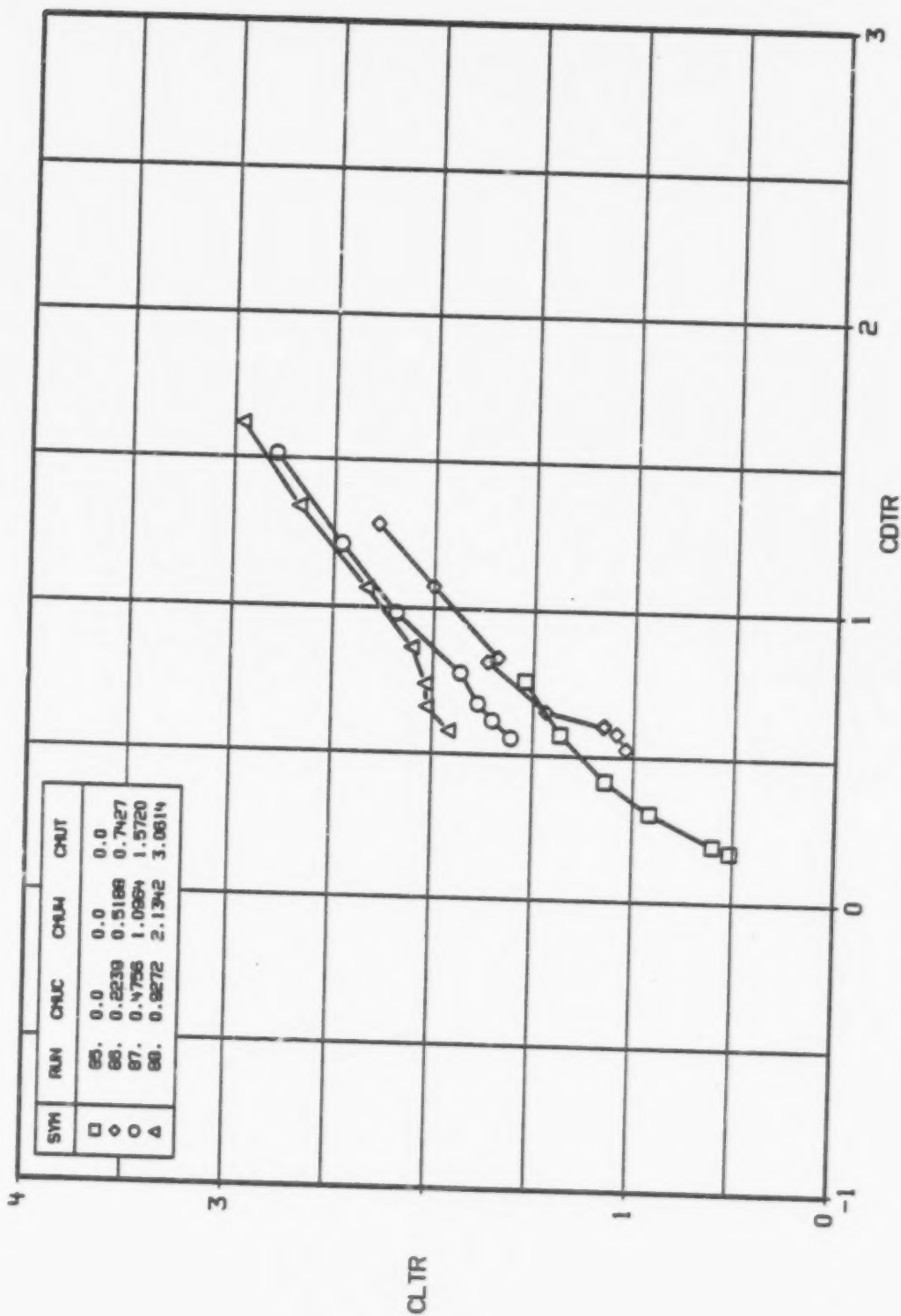


FIGURE A6e BASIC DATA EFFECT OF CHU
CONFIGURATION BC245V, DELF=45, BN/B=1

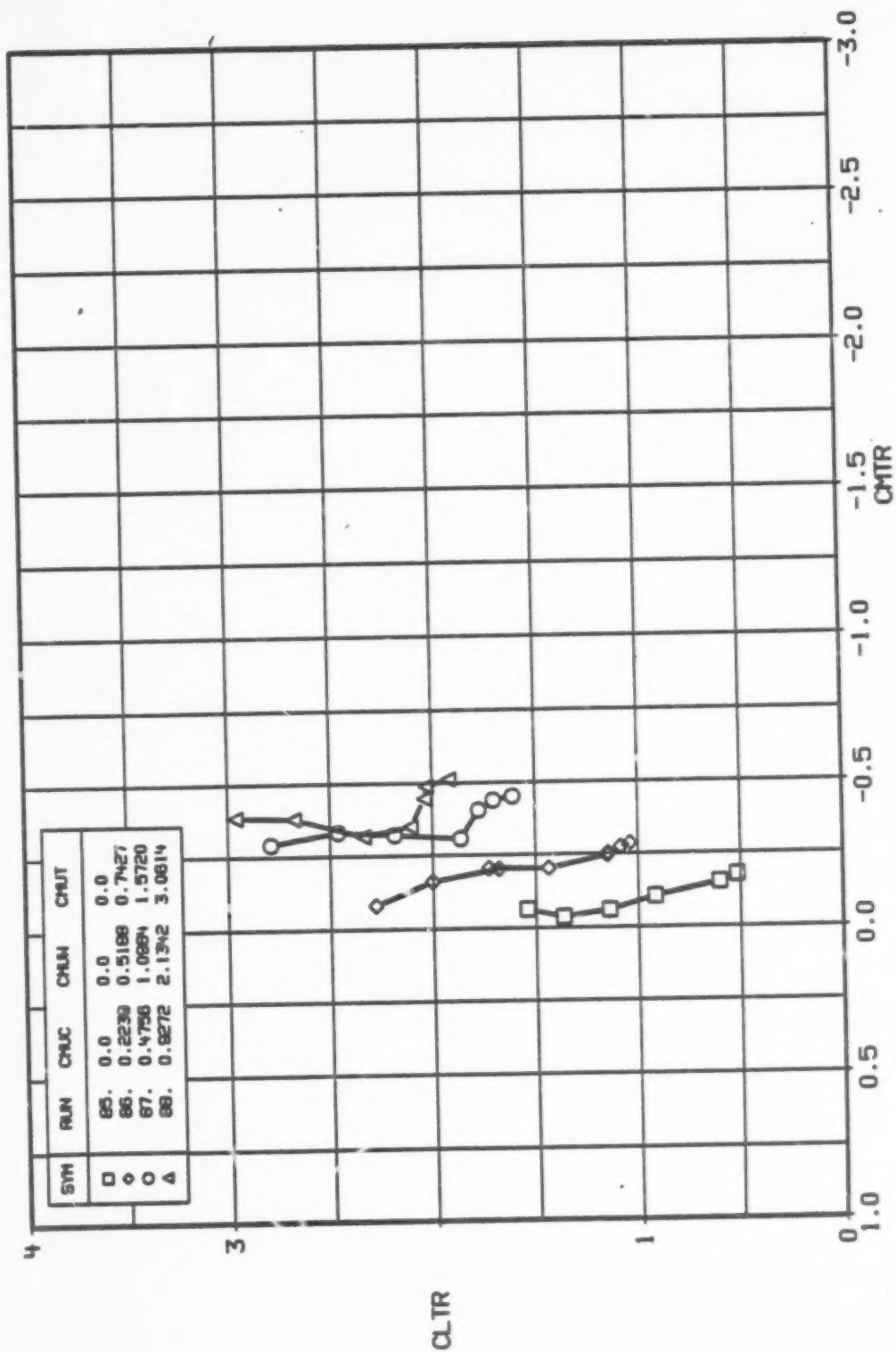


FIGURE A6f BASIC DATA EFFECT OF CHU
CONFIGURATION BC246V, DELF=45, BN/B=1

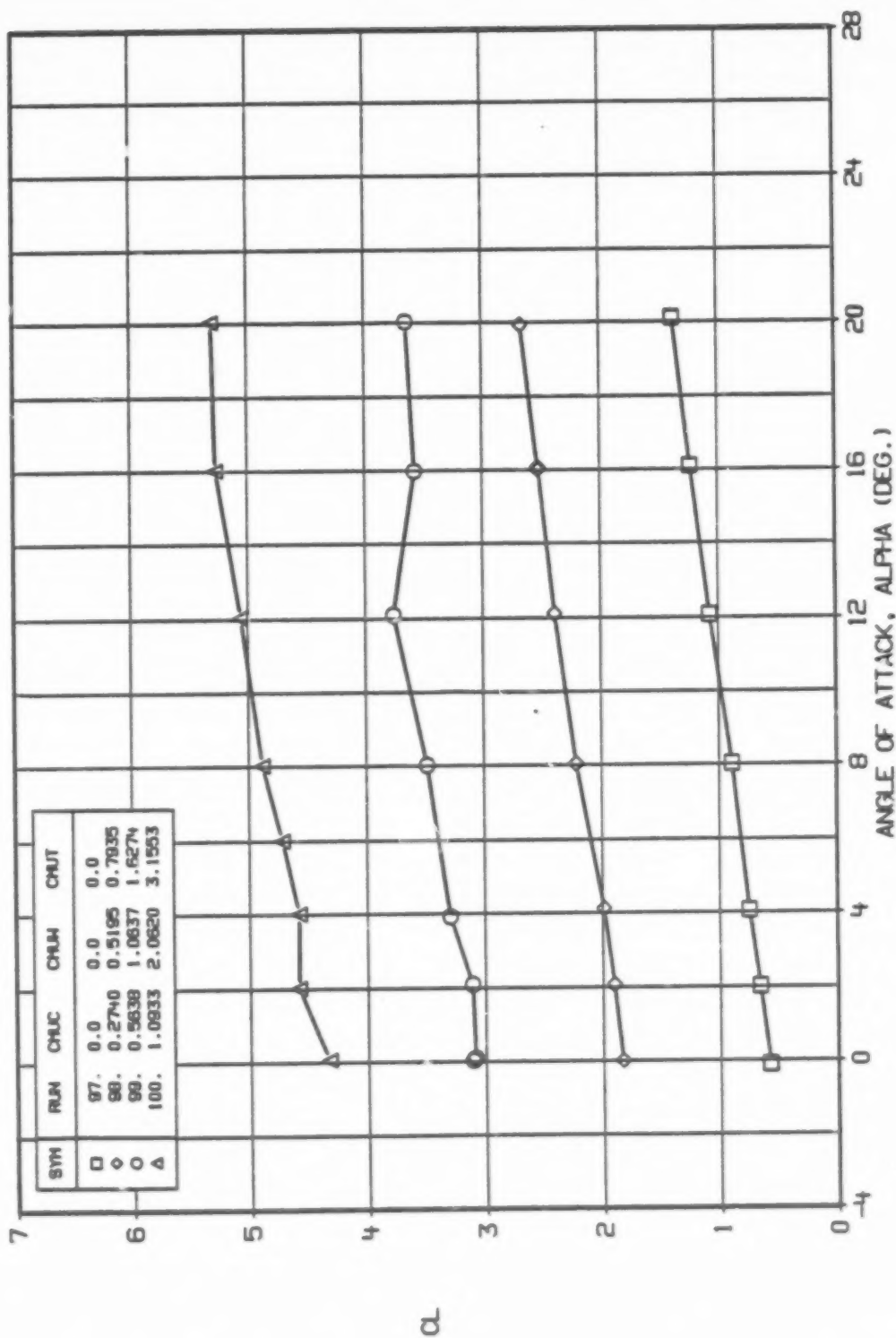


FIGURE A7a BASIC DATA EFFECT OF CMU
CONFIGURATION BC2W5V, DELF=45, BN/B=1

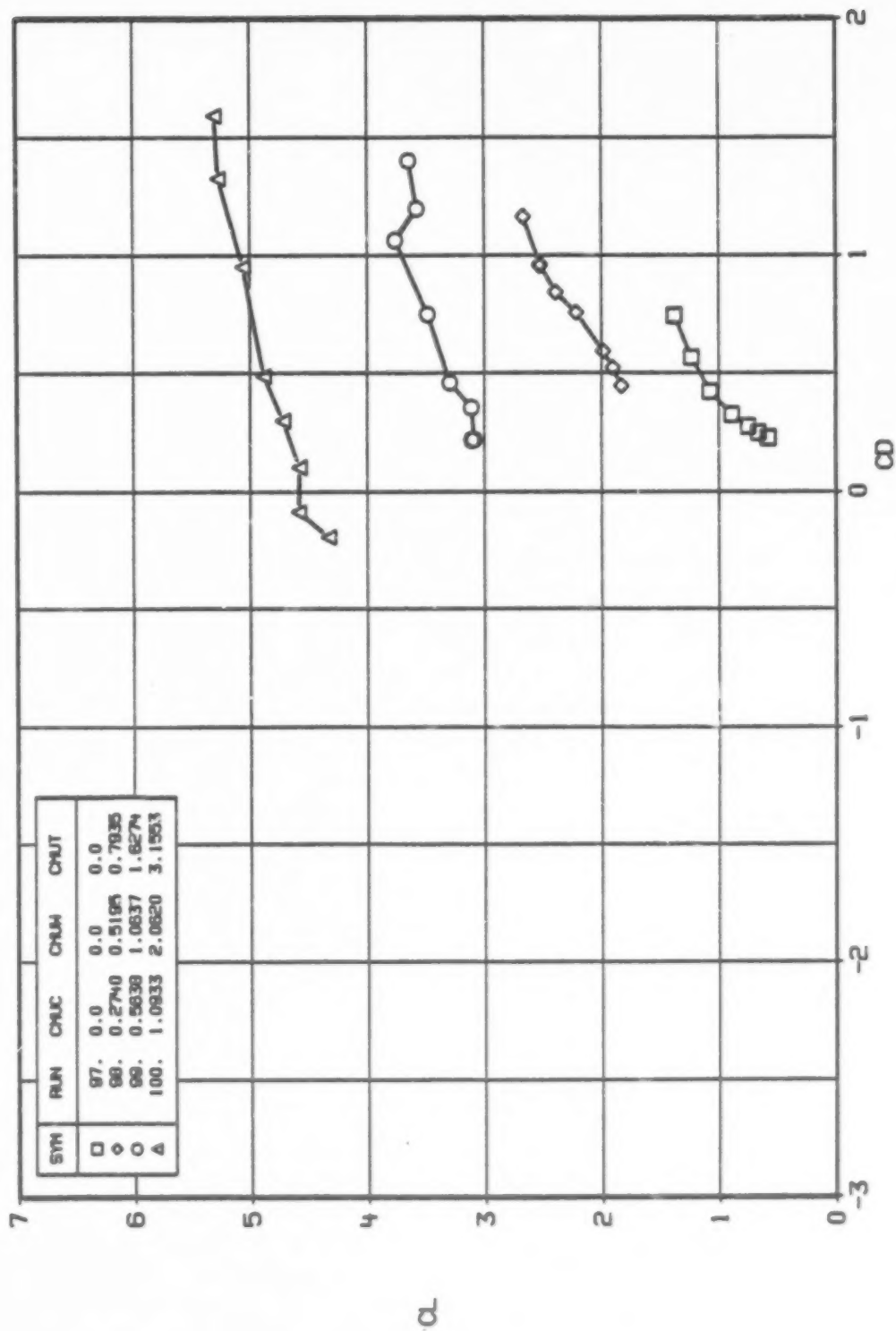


FIGURE A7b BASIC DATA EFFECT OF CHU
CONFIGURATION BC2W5V, DELF=45, BN/B=1

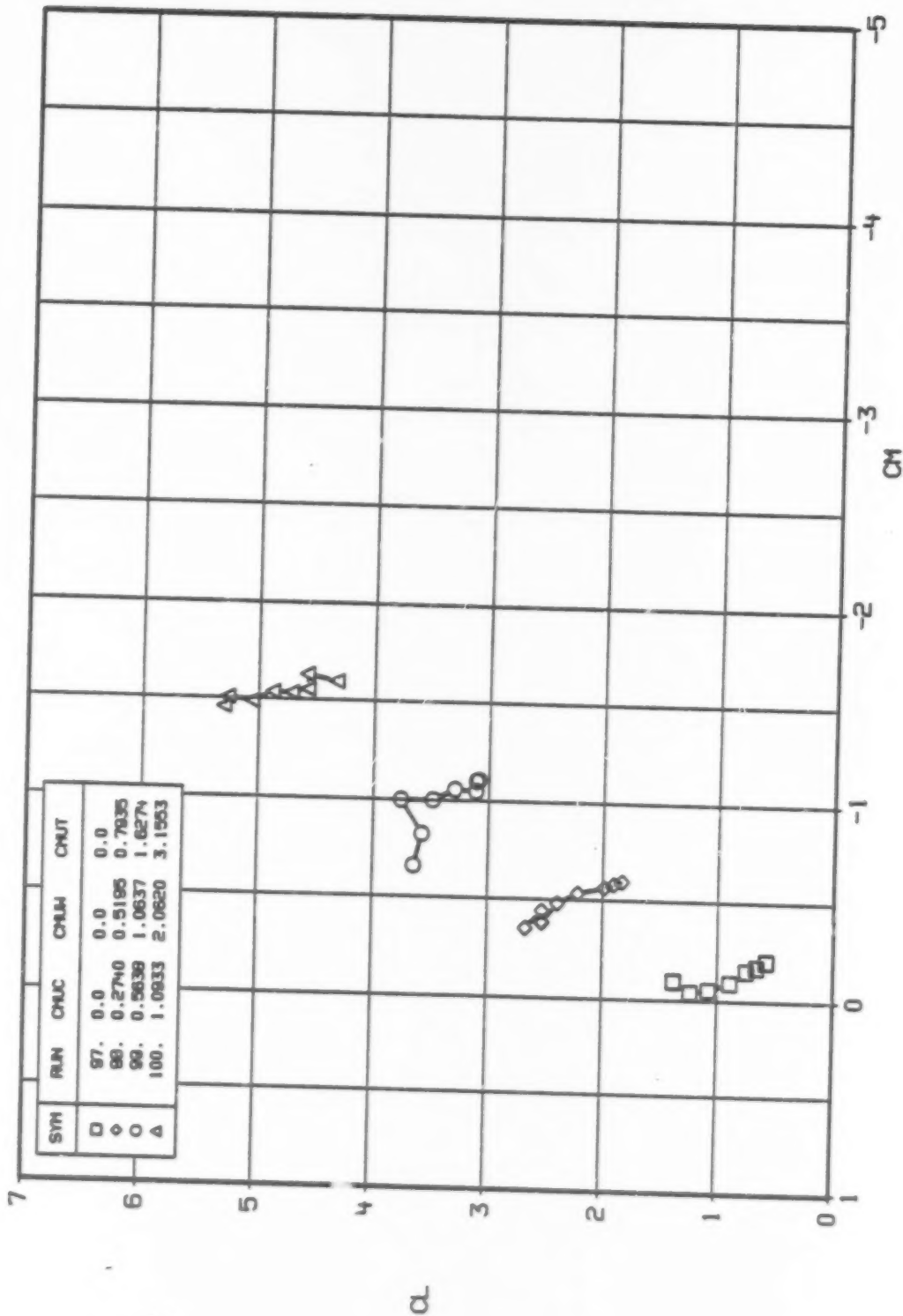


FIGURE A7c BASIC DATA EFFECT OF CMU
CONFIGURATION BC2W5V, DELF=45, BN/B=1

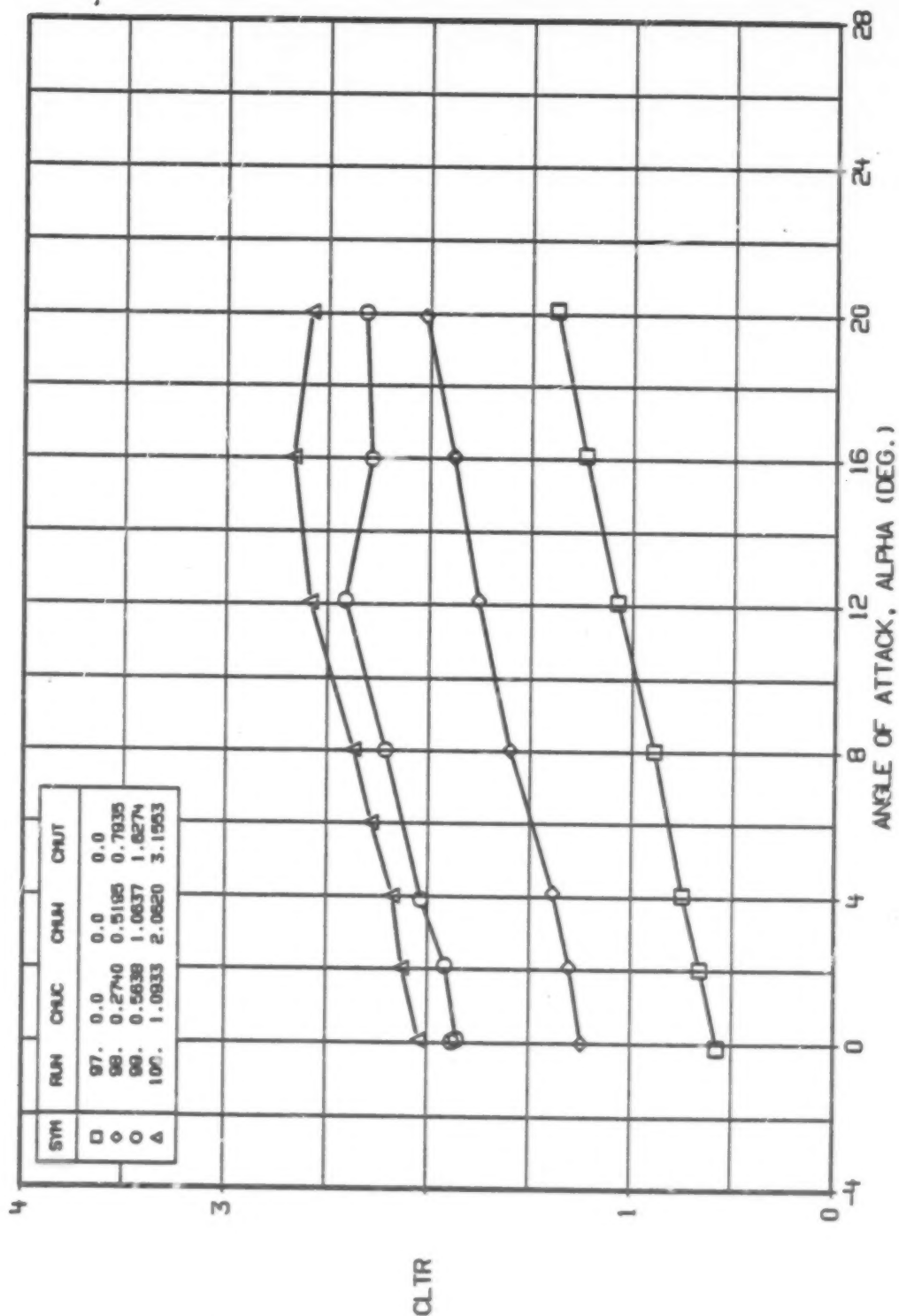


FIGURE A7d BASIC DATA EFFECT OF CMJ
CONFIGURATION BC2W5V, DELF=45, BN/B=1

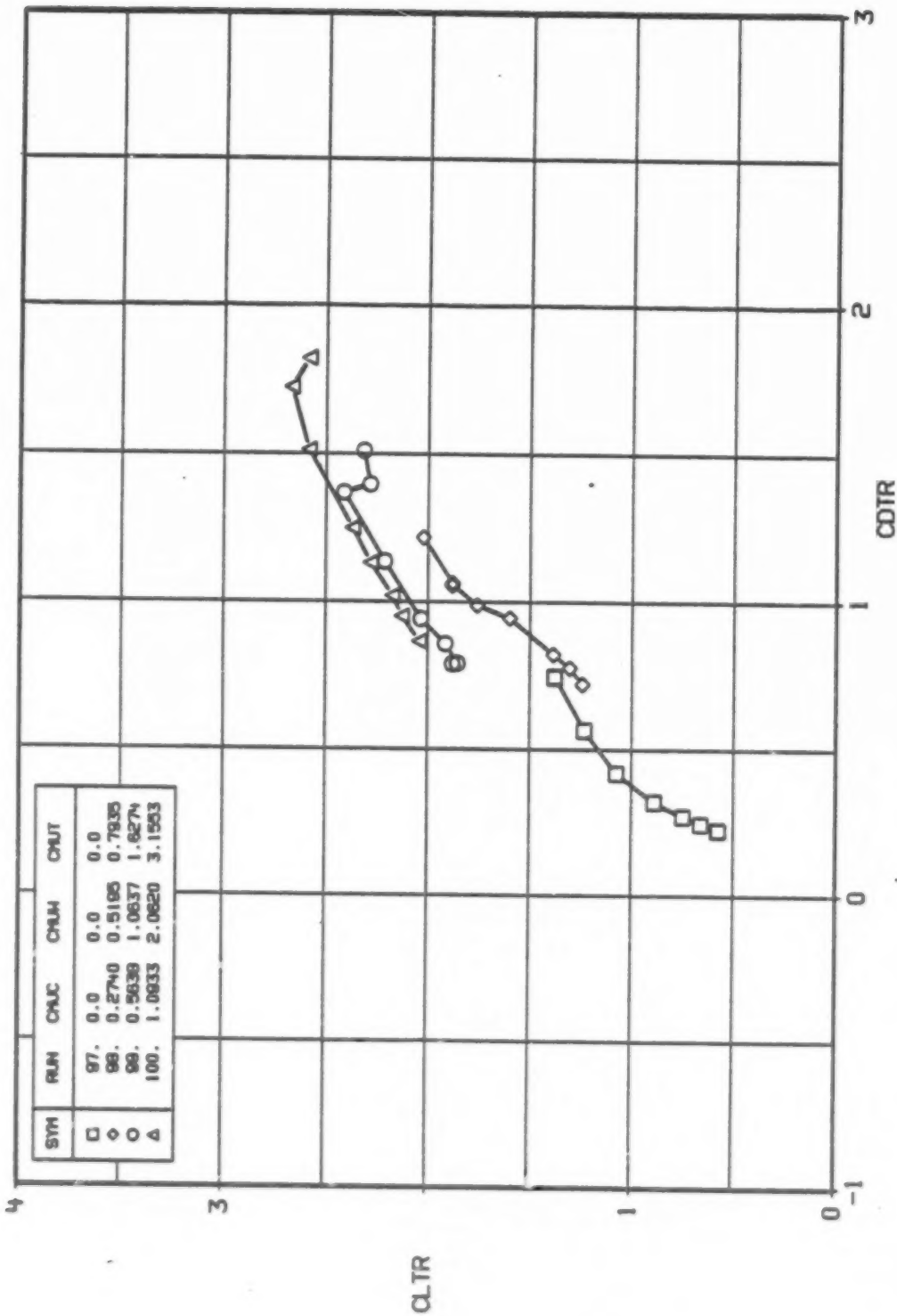


FIGURE A7e BASIC DATA EFFECT OF CMU
CONFIGURATION BC2M5V, DELF=45, BN/B=1

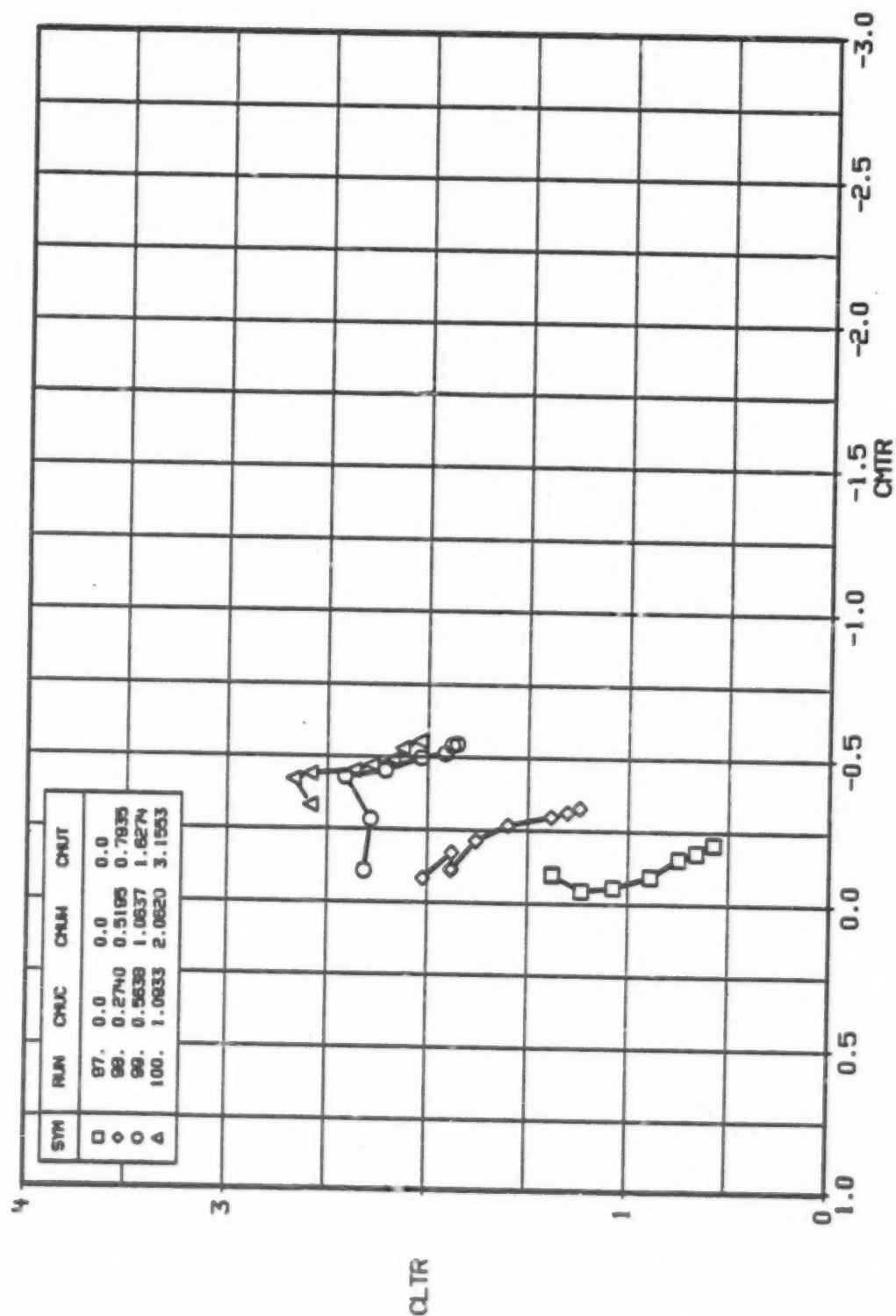


FIGURE A7f BASIC DATA EFFECT OF CMU
CONFIGURATION BC2W5V, DELF=45, BN/B=1

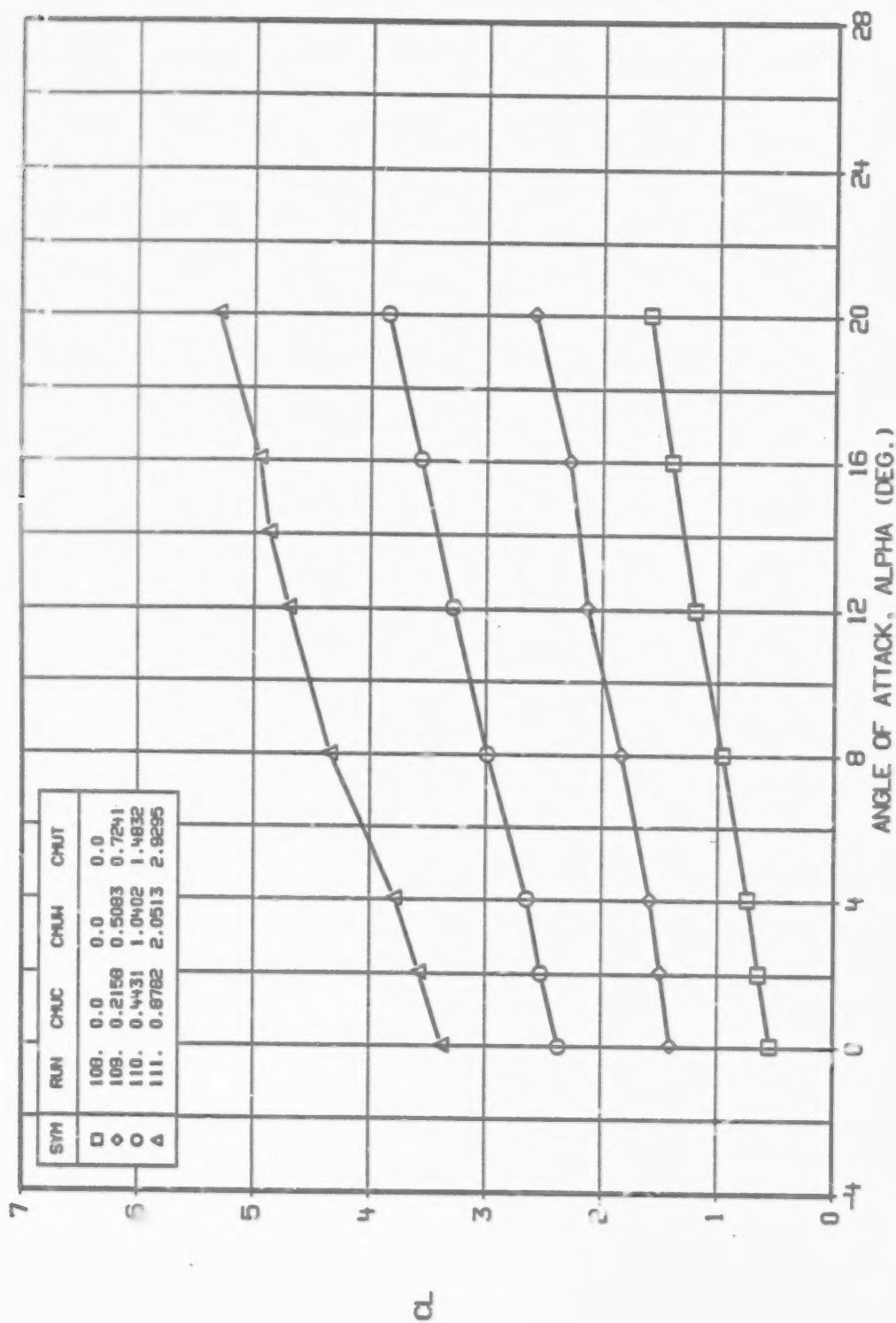


FIGURE A8a BASIC DATA EFFECT OF CMU
CONFIGURATION BC345V, DELF=45, BN/B=1

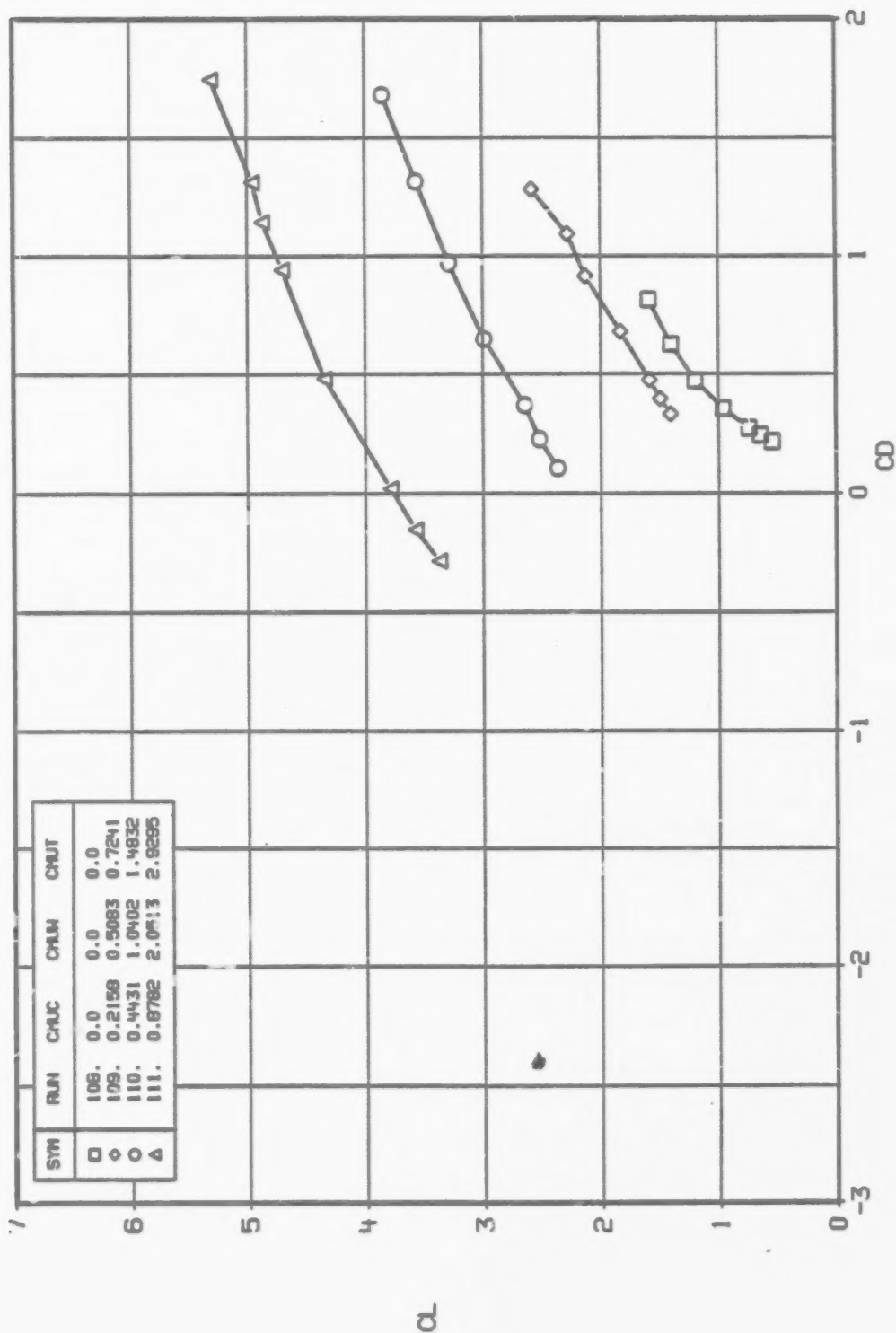


FIGURE A8b BASIC DATA EFFECT OF CMU
CONFIGURATION BC346V, DELF=45, BN/B=1

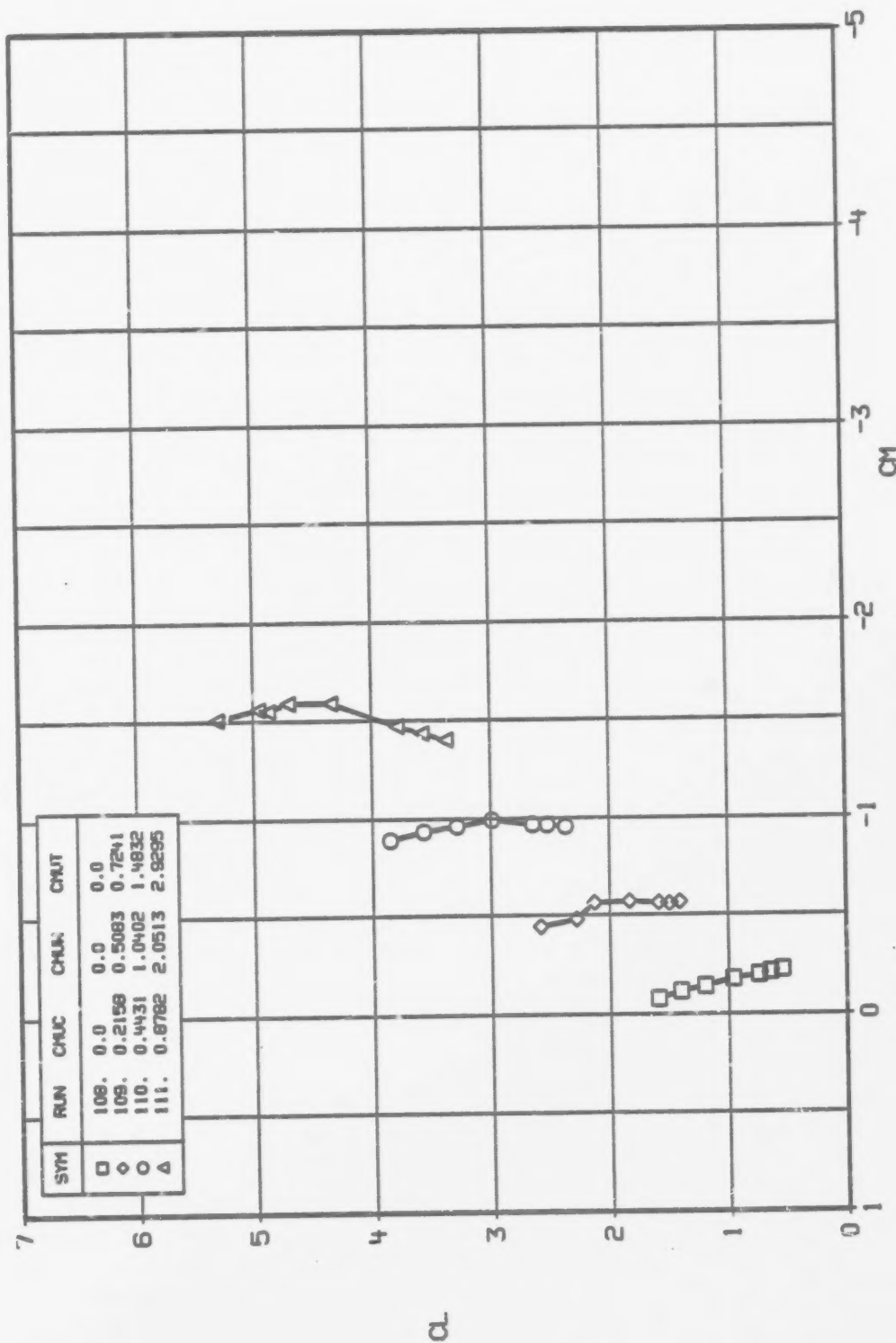


FIGURE A8c BASIC DATA EFFECT OF CMU
CONFIGURATION BC345V, DELF=45, BN/B=1

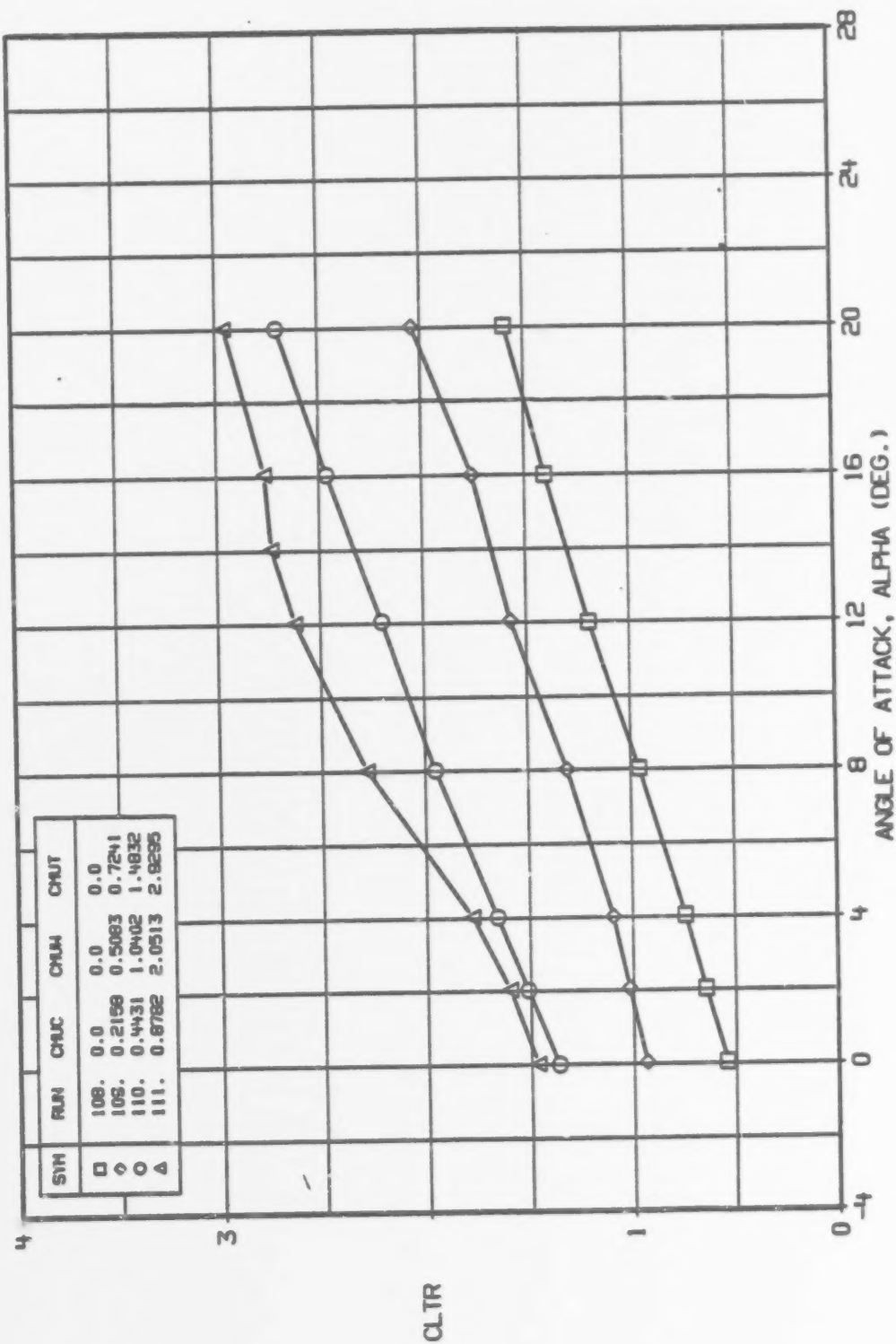


FIGURE A8d BASIC DATA EFFECT OF CMU
CONFIGURATION BC346V, DELF=45, BN/B=1

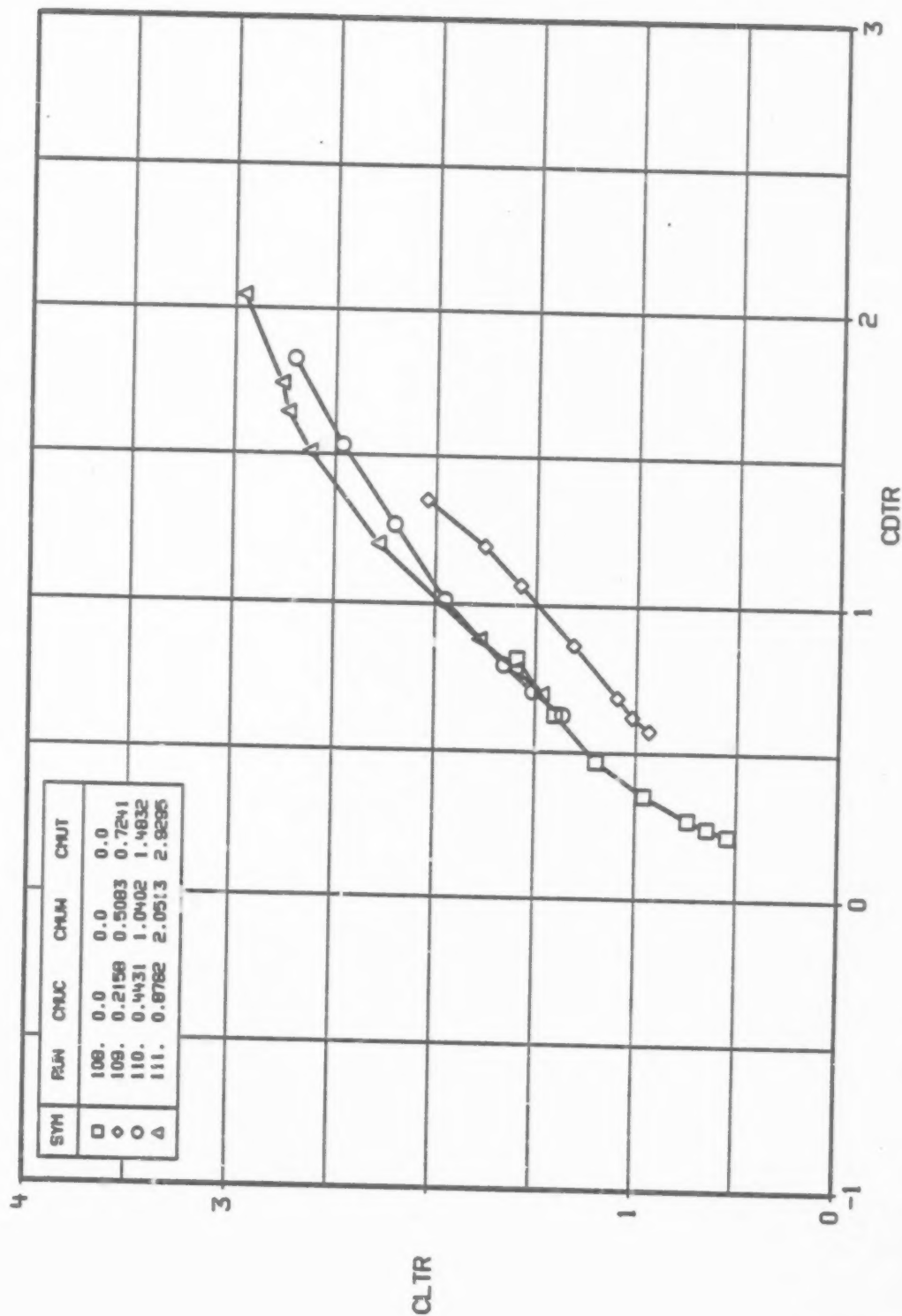


FIGURE A8e BASIC DATA EFFECT OF CMU
CONFIGURATION BC346V, DELF=45, BN/B=1

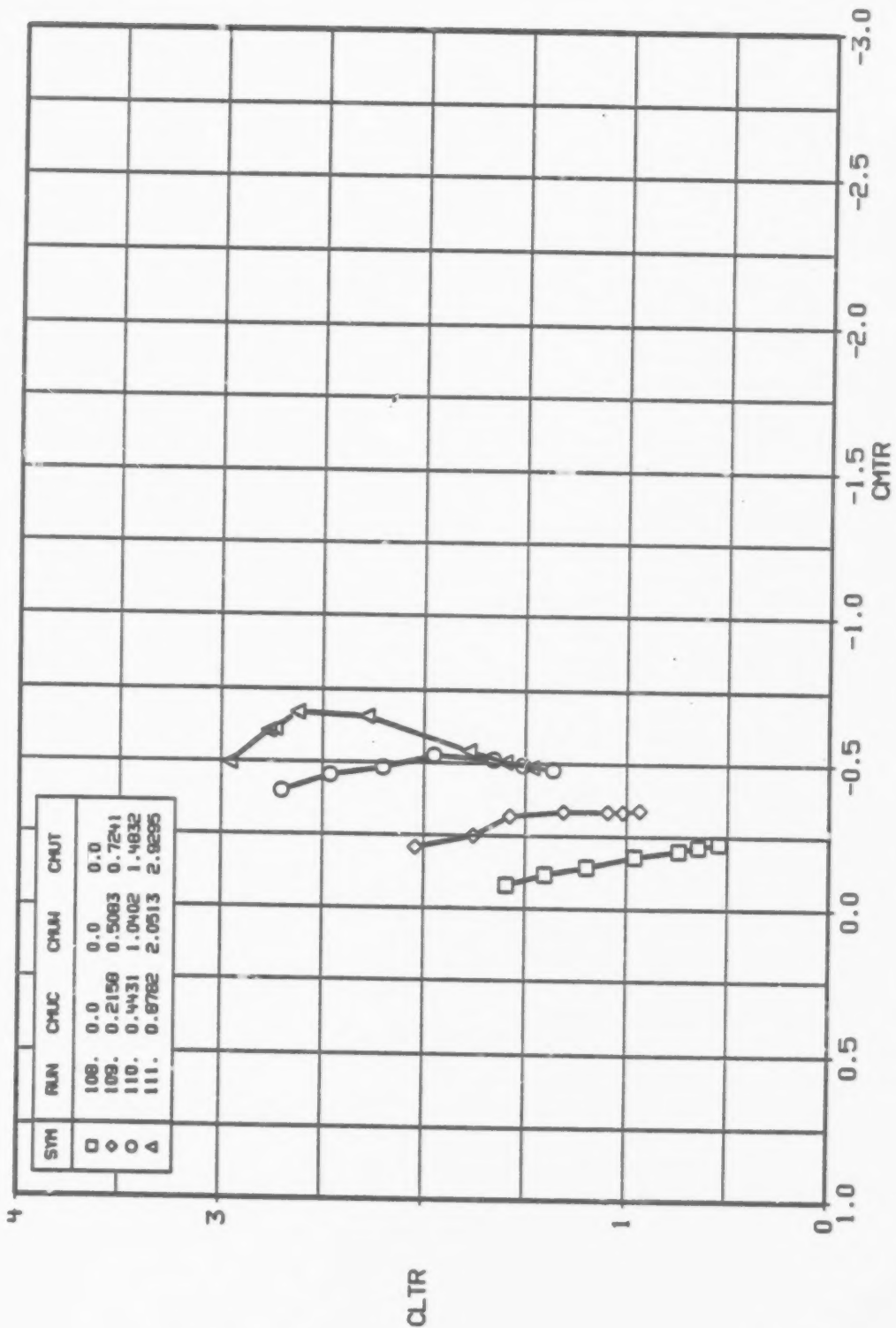


FIGURE A8f BASIC DATA EFFECT OF CMU
CONFIGURATION BC346V, DELF=45, BN/B=1

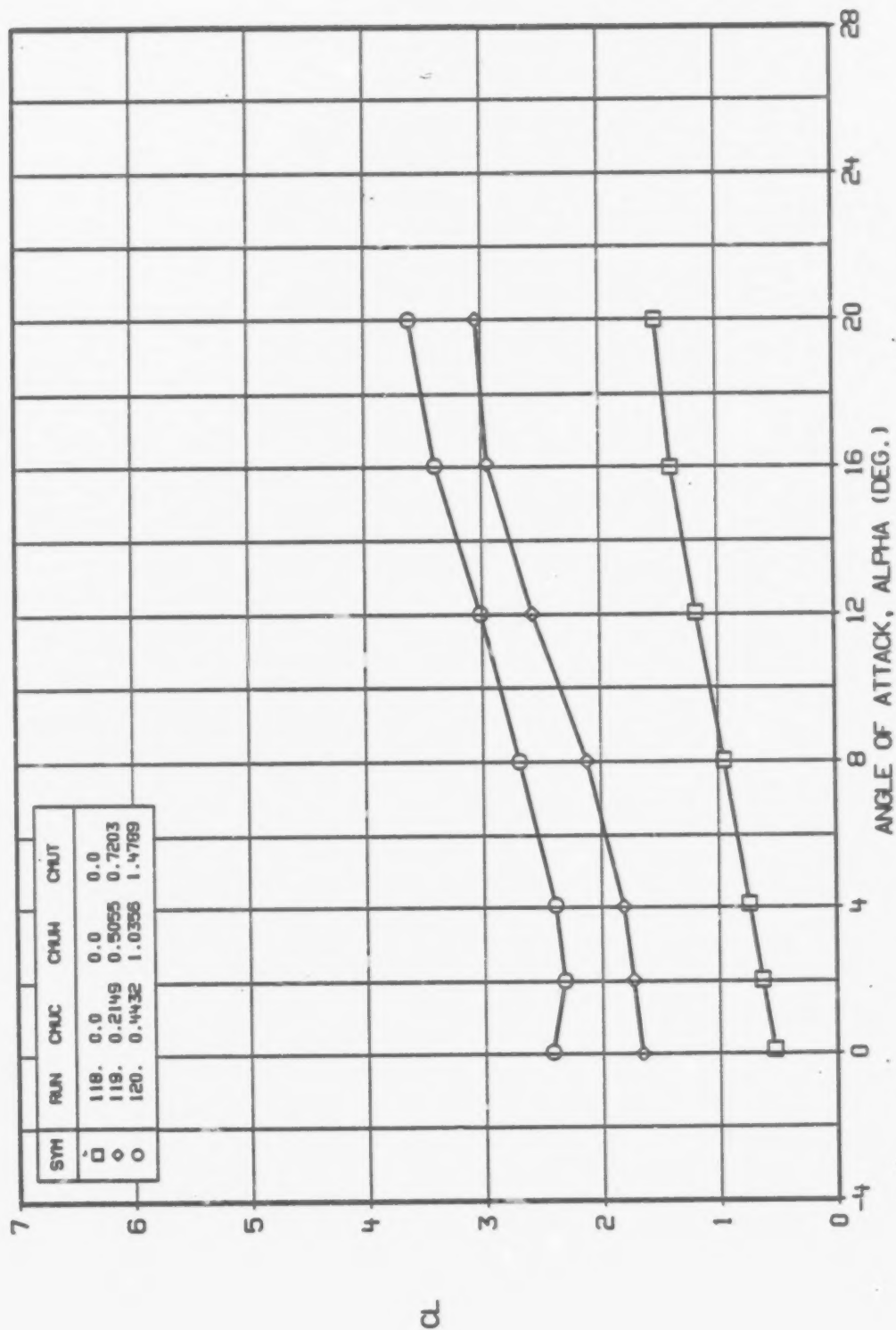


FIGURE A9a BASIC DATA EFFECT OF CMU
CONFIGURATION BC146V, DELF=45, BN/B=1, DELC=10

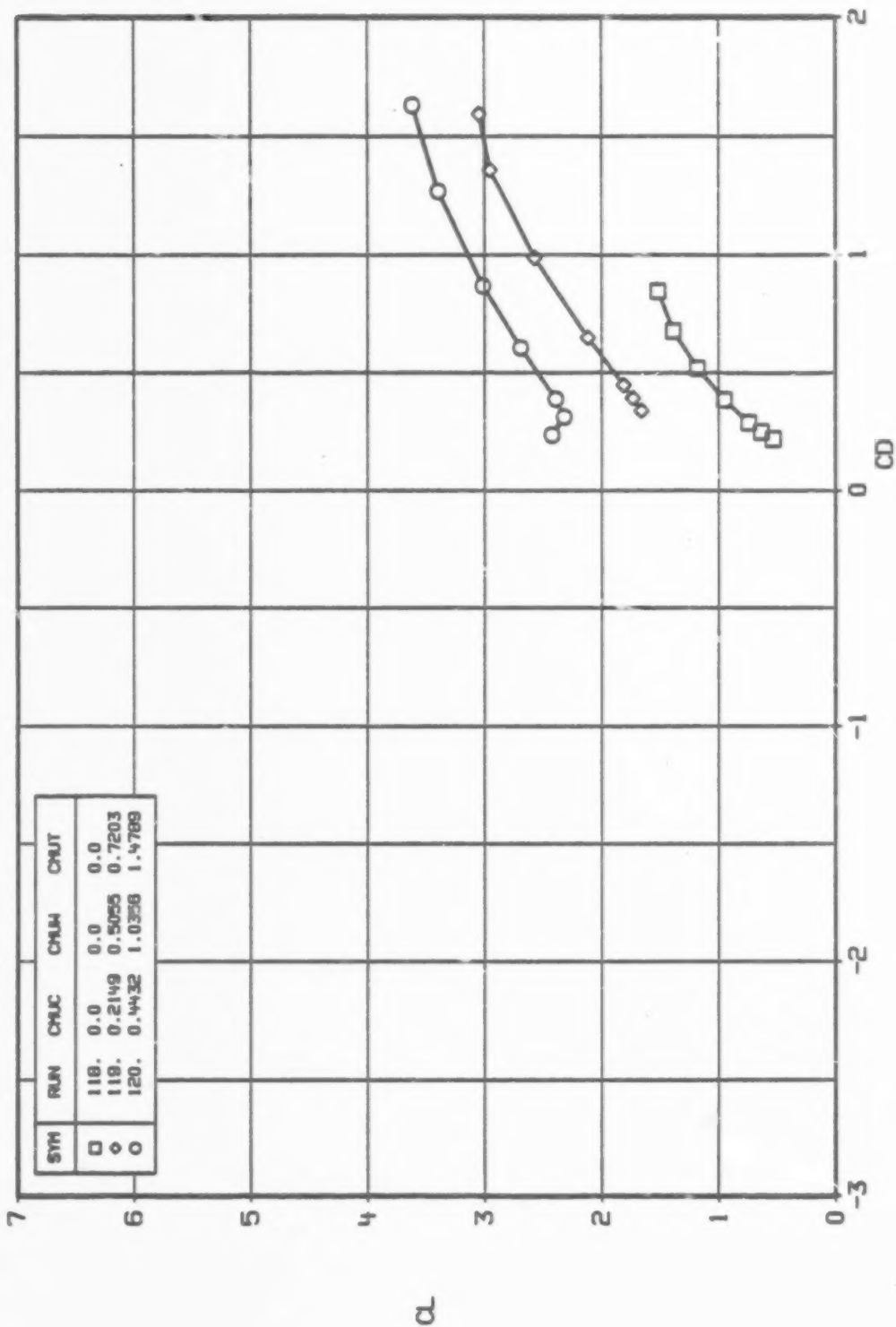


FIGURE A9b BASIC DATA EFFECT OF CMU
CONFIGURATION BC146V, DELF=45, BN/B=1, DELC=10

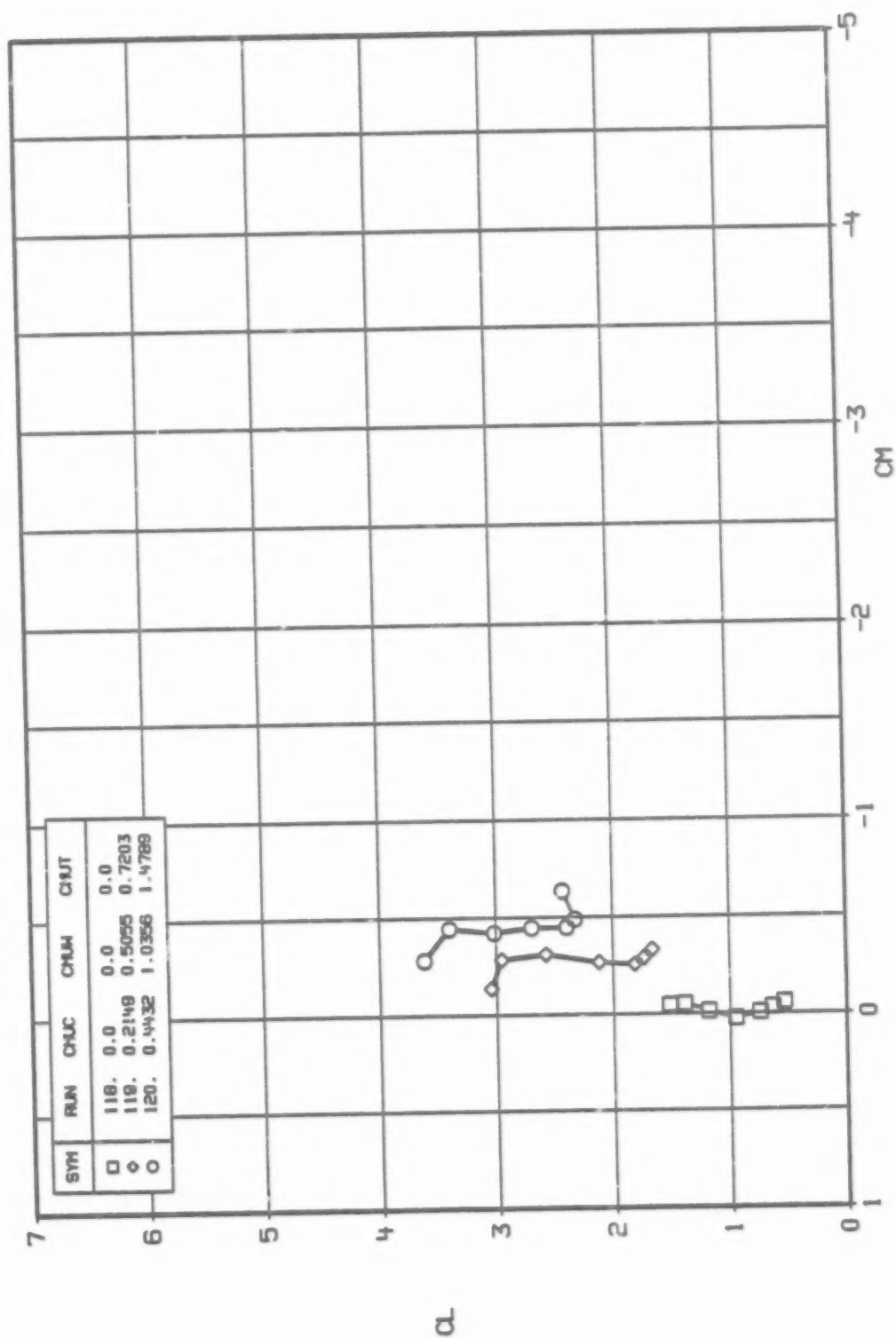


FIGURE A9c BASIC DATA EFFECT OF CMU
CONFIGURATION BC145V, DELF=45, BN/B=1, DELC=10

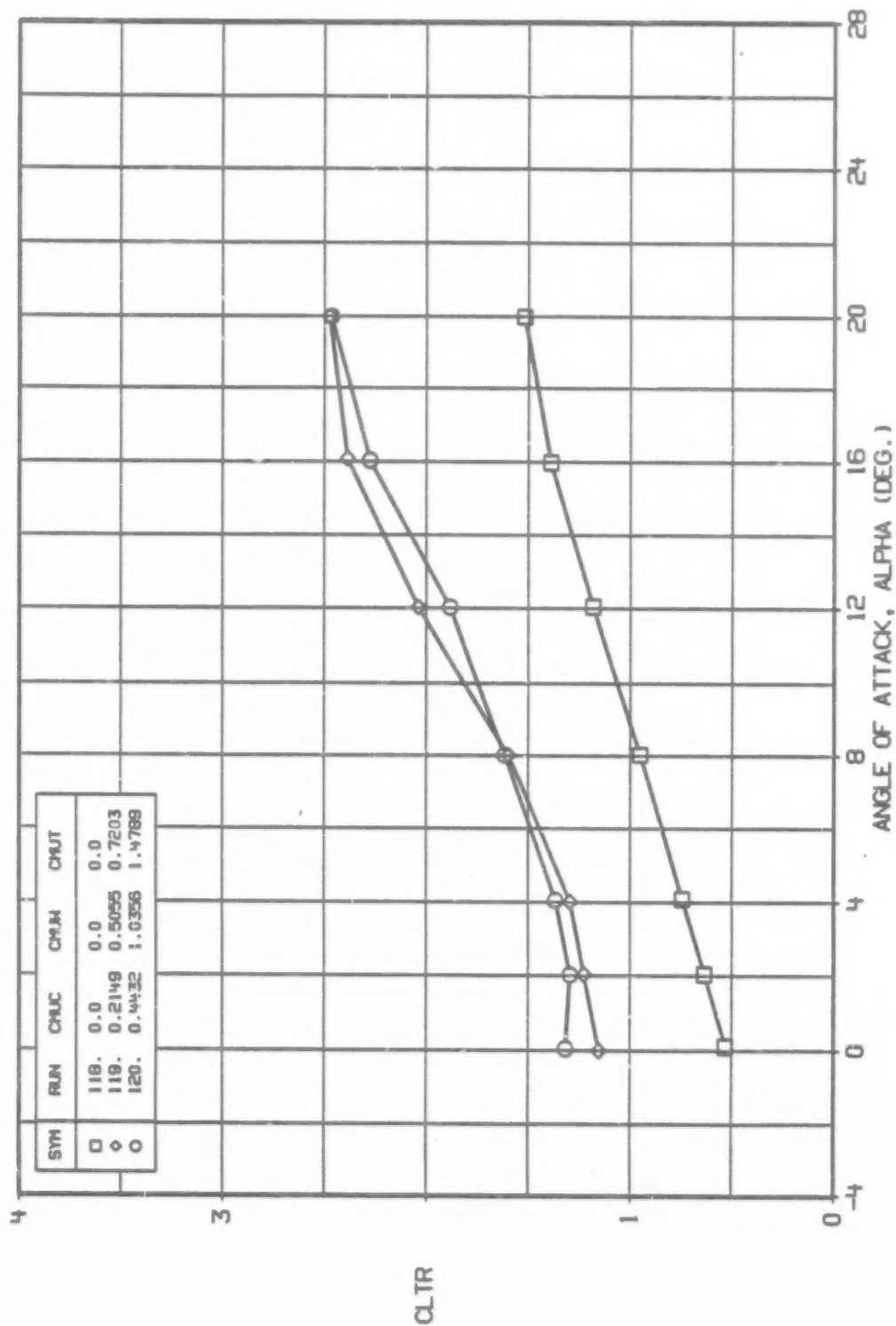


FIGURE A9d BASIC DATA EFFECT OF CMU
CONFIGURATION BC118V, DELF=45, BN/B=1, DELC=10

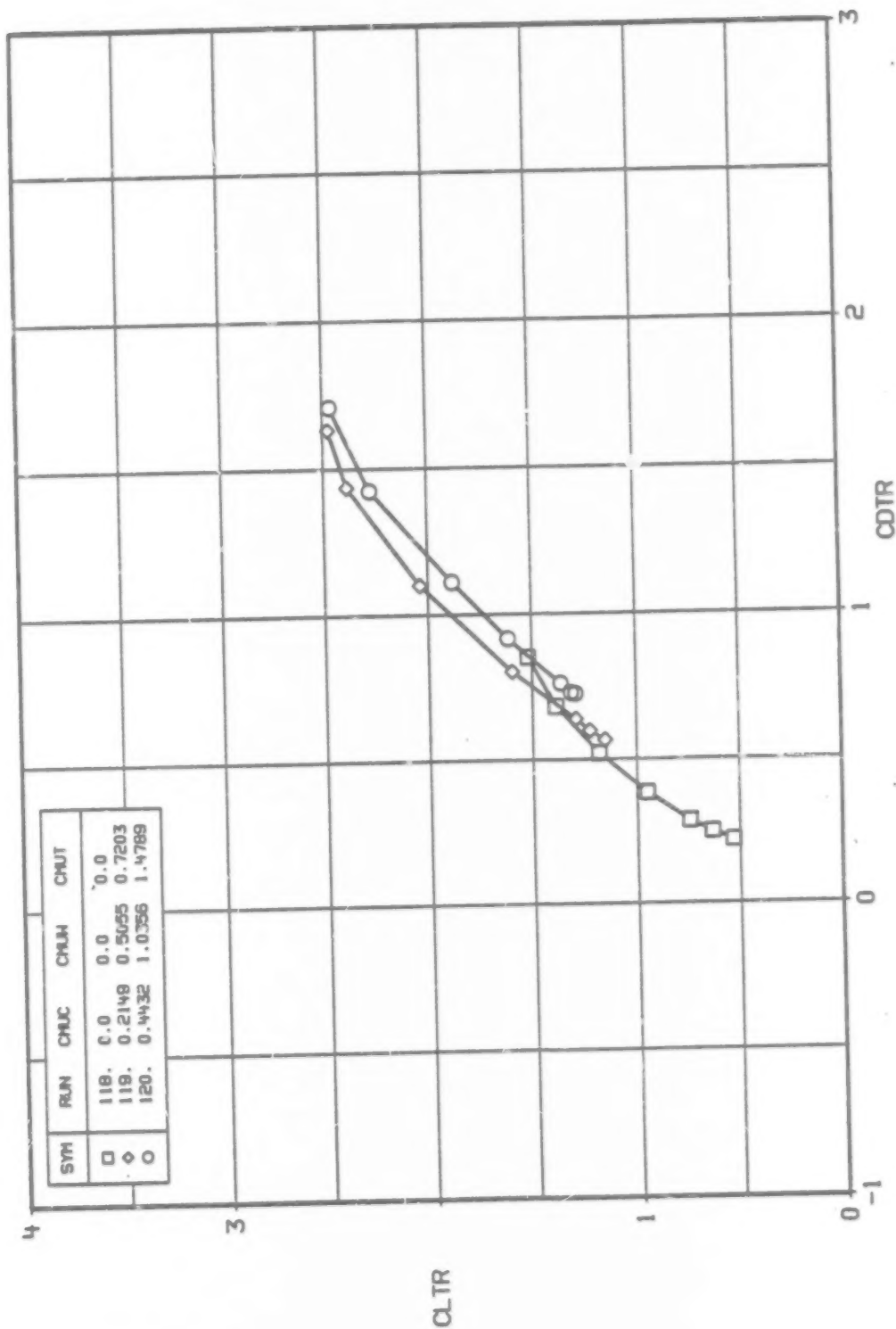


FIGURE A9e BASIC DATA EFFECT OF CMU
CONFIGURATION BC145V, DELF=45, BN/B=1, DELC=10

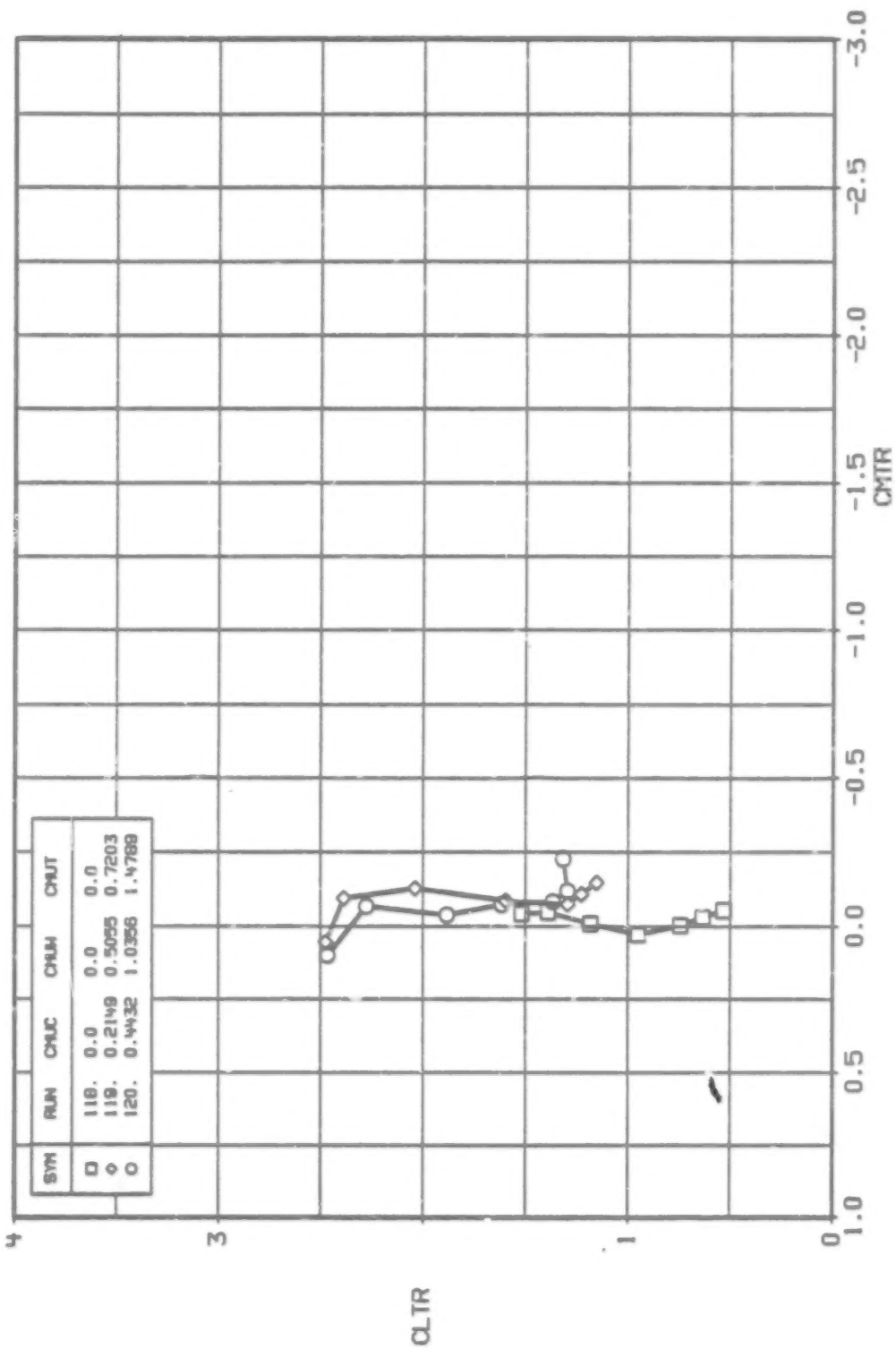


FIGURE A9f BASIC DATA EFFECT OF CMU
CONFIGURATION BC146V, DELF=45, BN/B=1, DELC=10

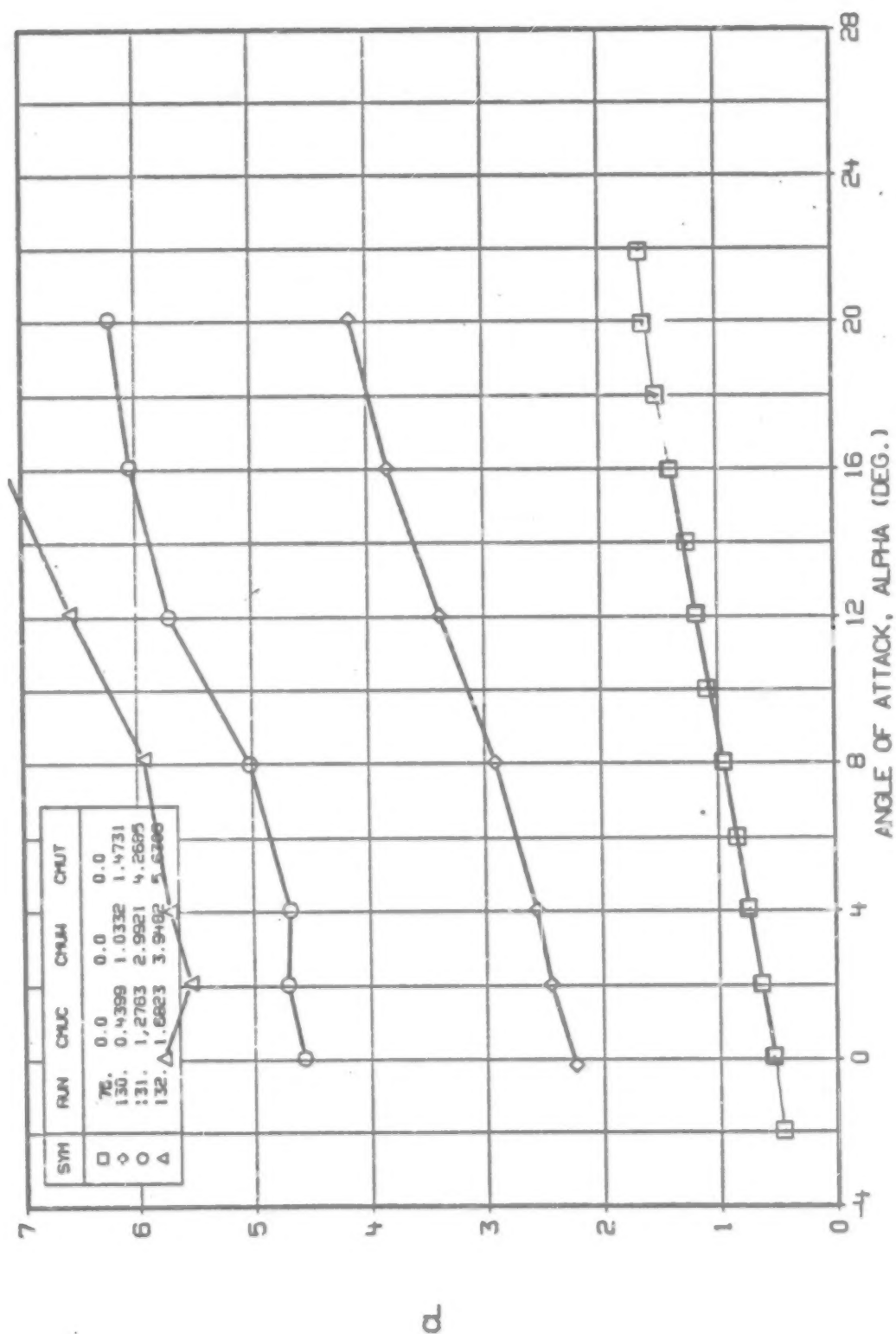


FIGURE A10a BASIC DATA EFFECT OF CMU
CONFIGURATION BC145V, DELF=45, BN/B=1

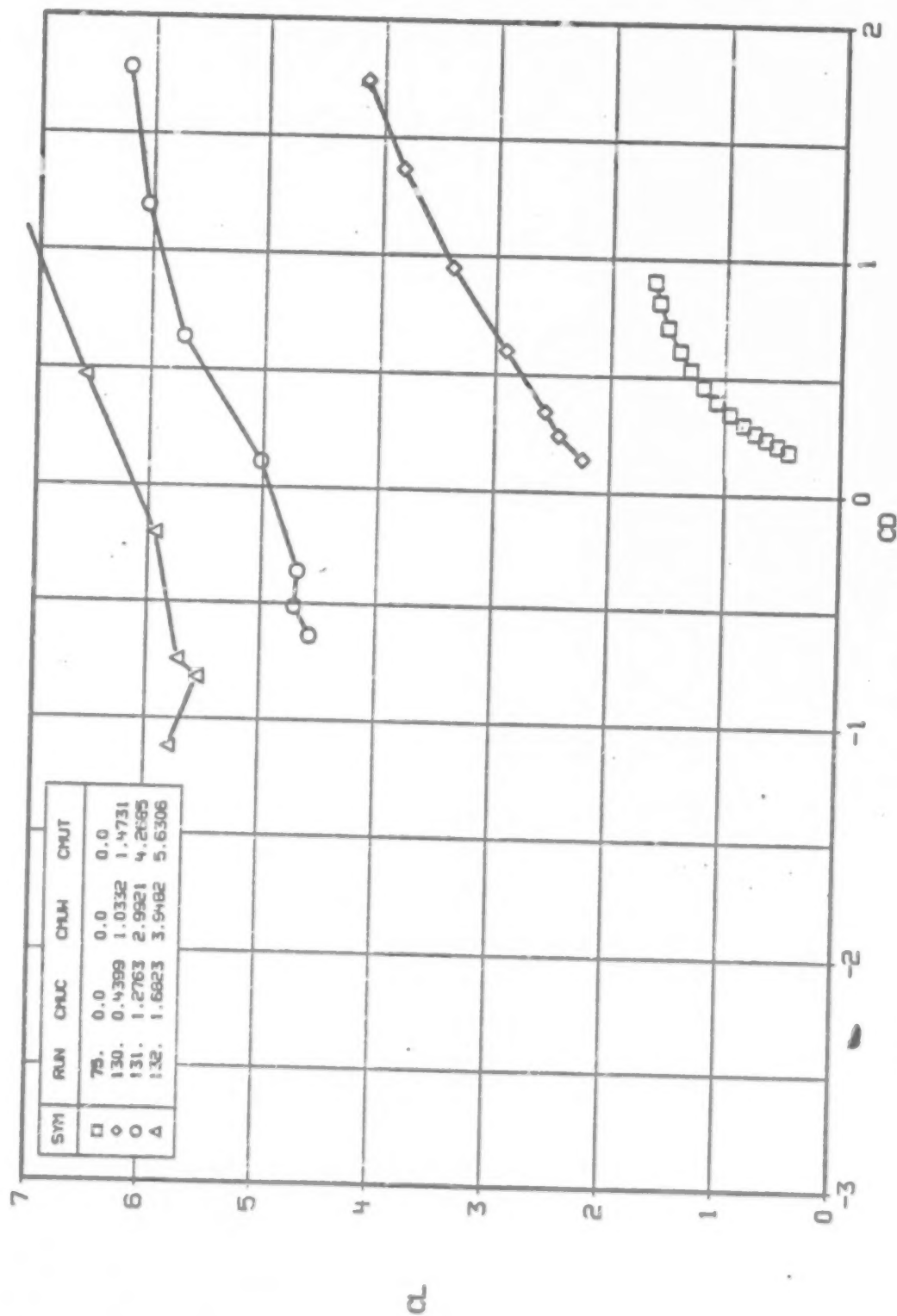


FIGURE A10b BASIC DATA EFFECT OF CMU
CONFIGURATION BC1W5V, DELF=45, BN/B=1

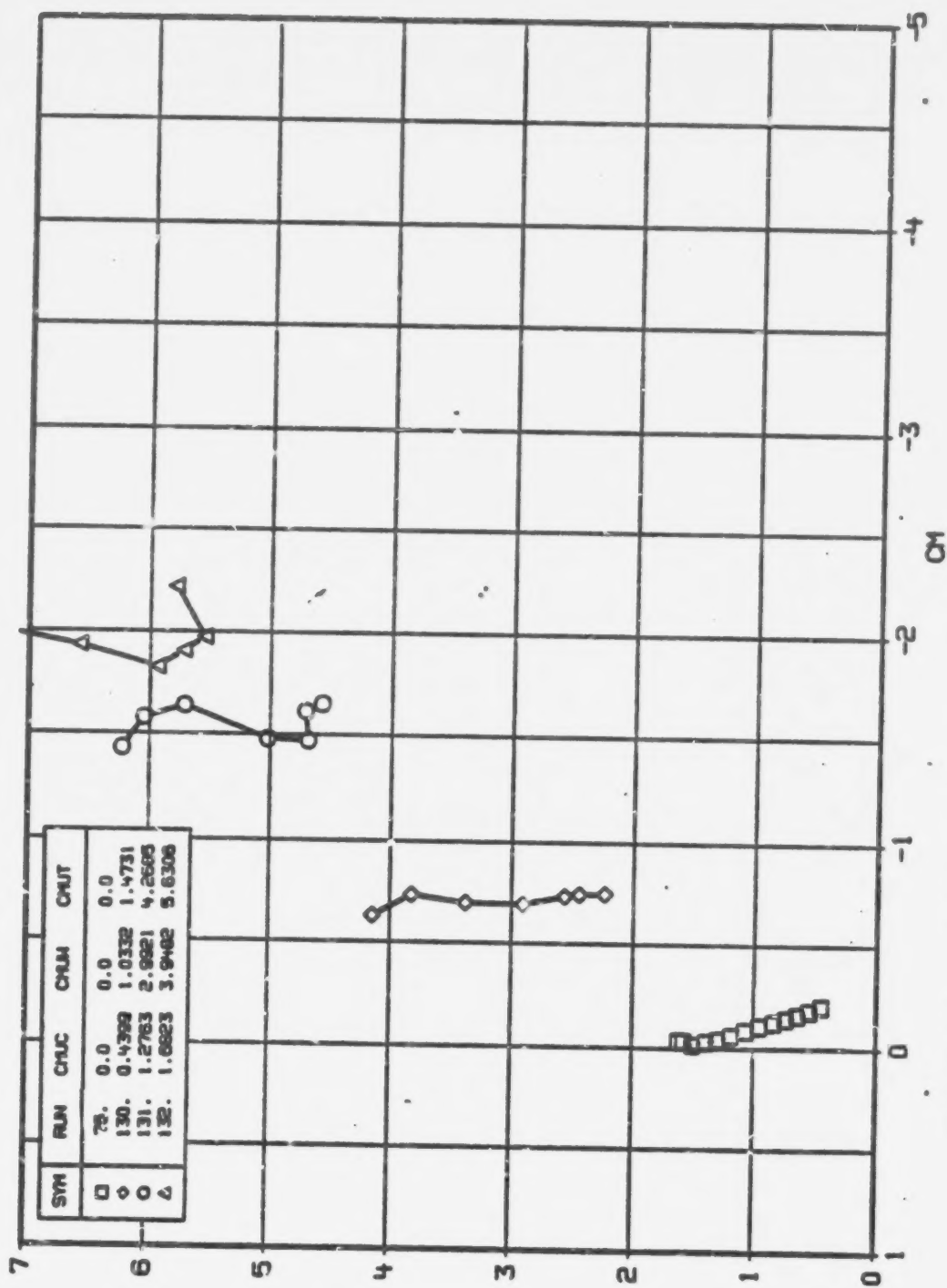


FIGURE A10c BASIC DATA EFFECT OF CHU
CONFIGURATION BC145V, DELF=45, BN/B=1

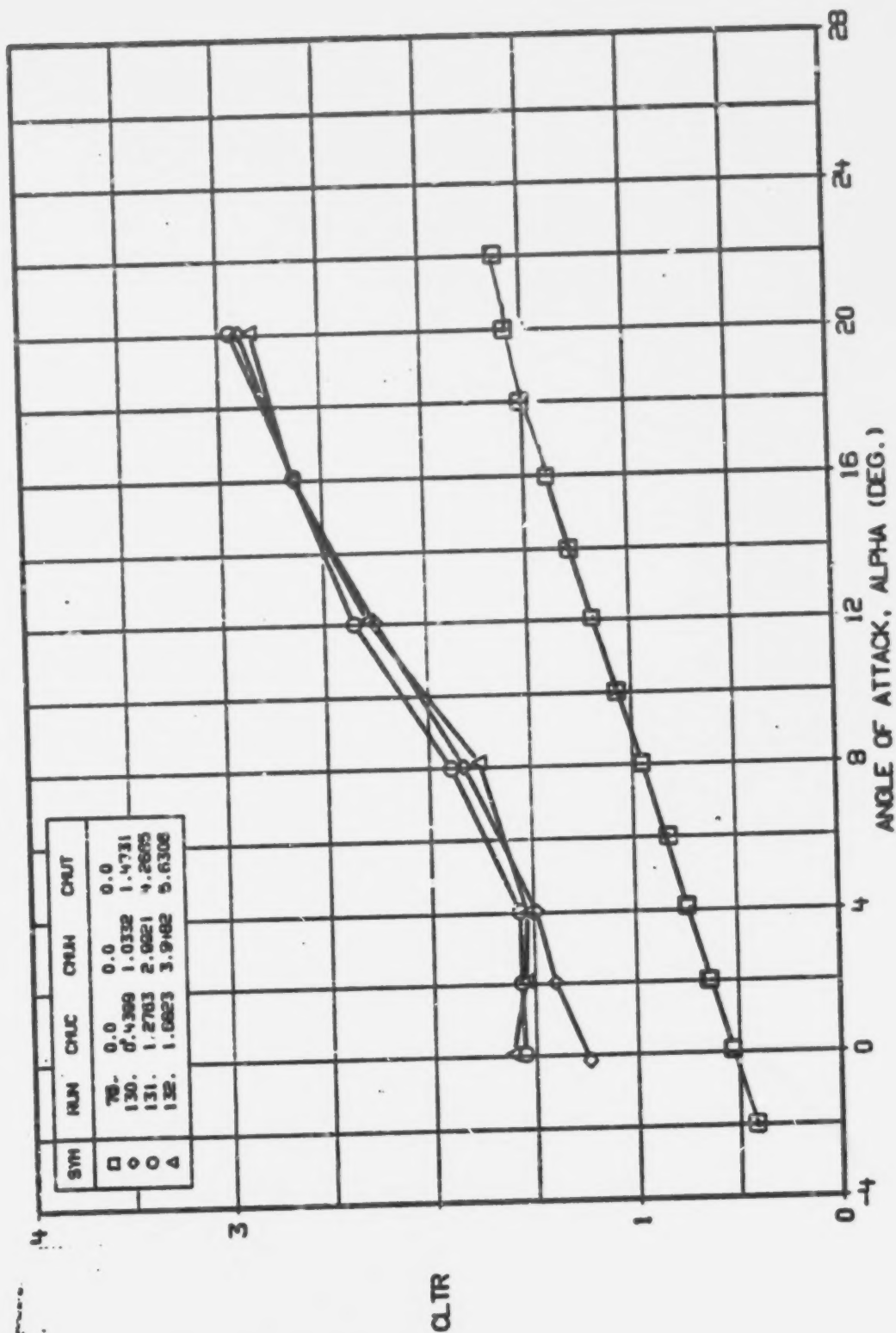


FIGURE A10d BASIC DATA EFFECT OF CHU
CONFIGURATION BC146V, DELF=45, BN/B=1

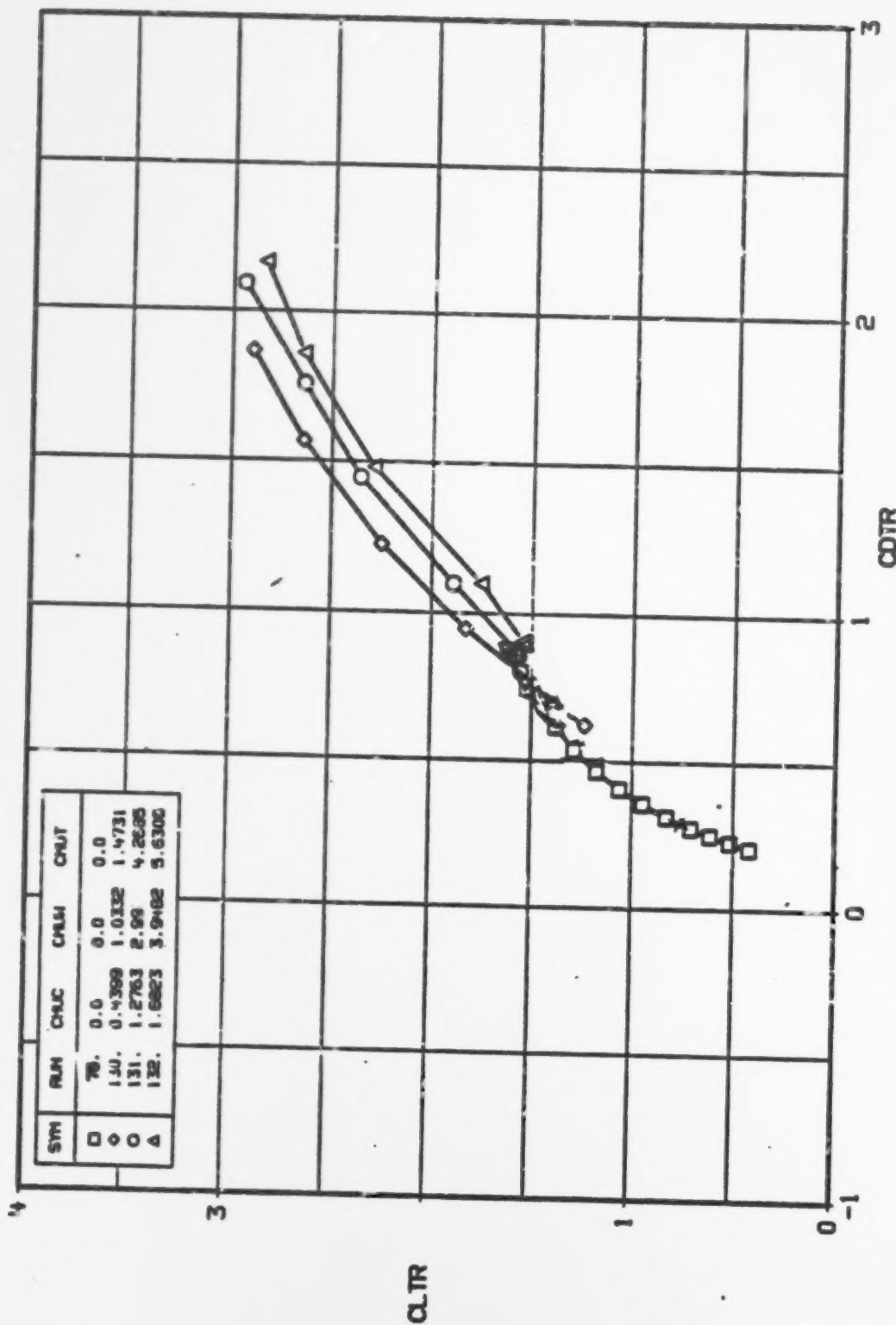


FIGURE A10e BASIC DATA EFFECT OF CHU
CONFIGURATION BC146V, DELF=45, BN/B=1

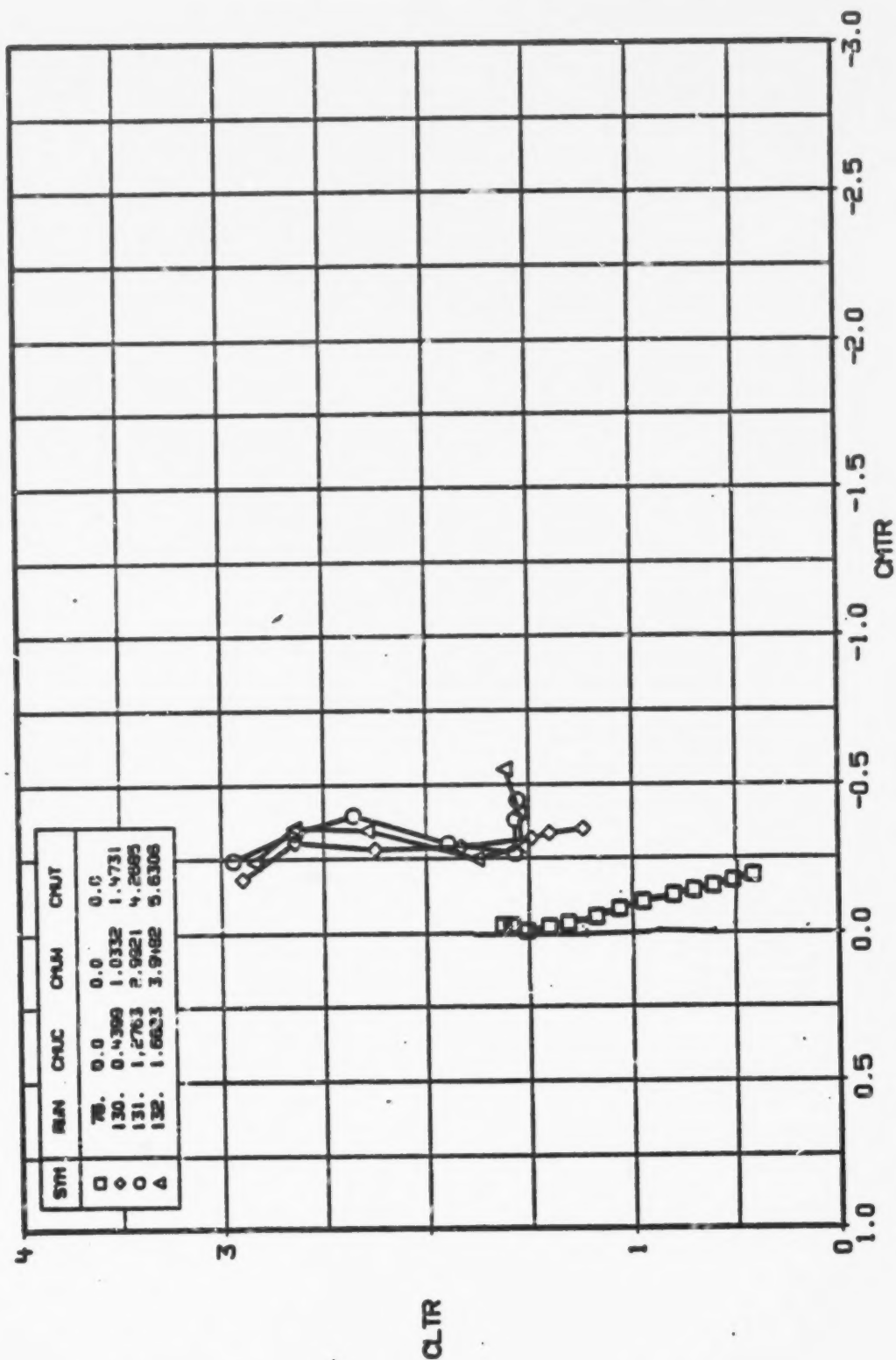


FIGURE A10f BASIC DATA EFFECT OF CMU
CONFIGURATION BC146V, DELF=45, BN/B=1

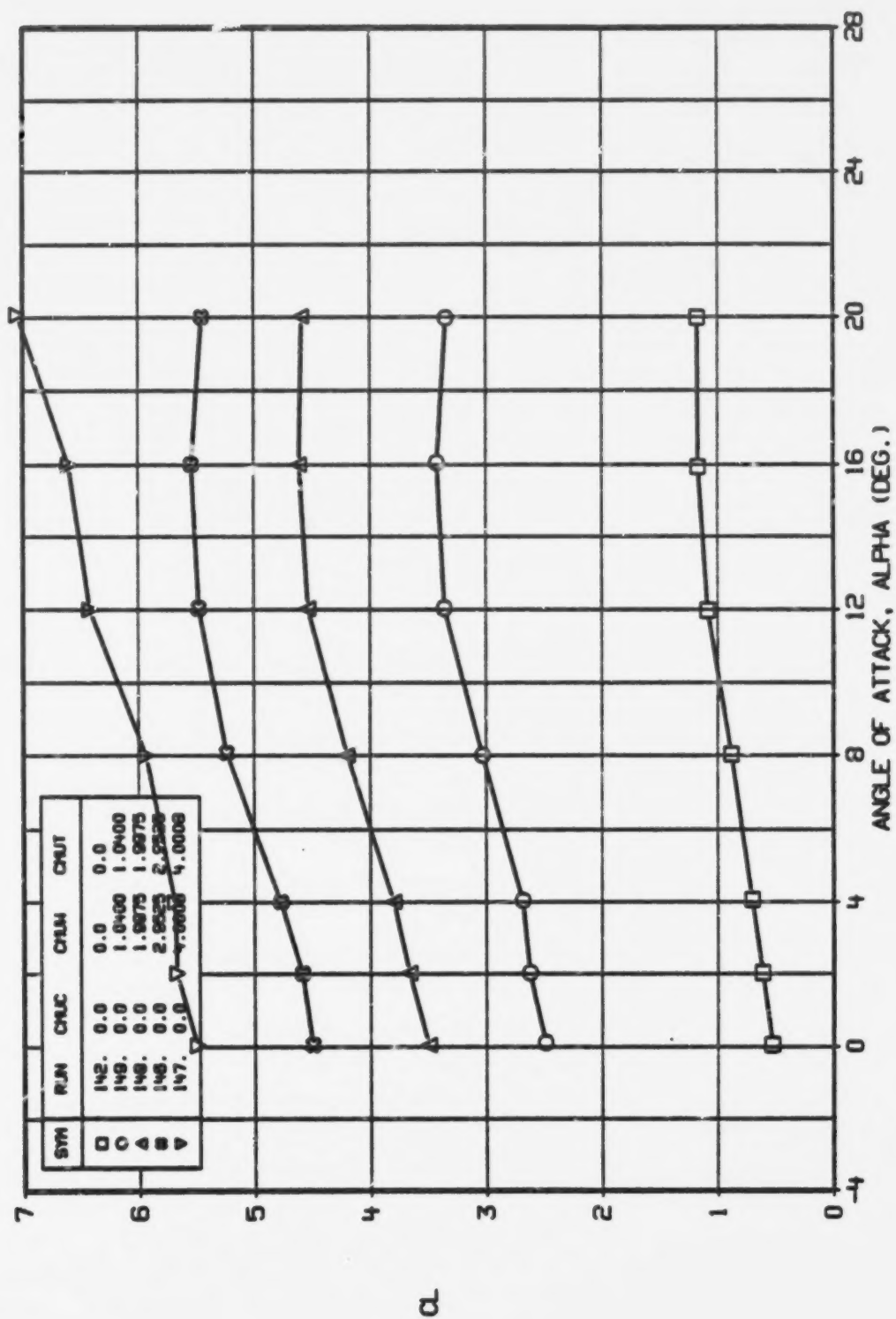


FIGURE A11a BASIC DATA EFFECT OF CMU
CONFIGURATION B45V, DELF=45, BN/B=1

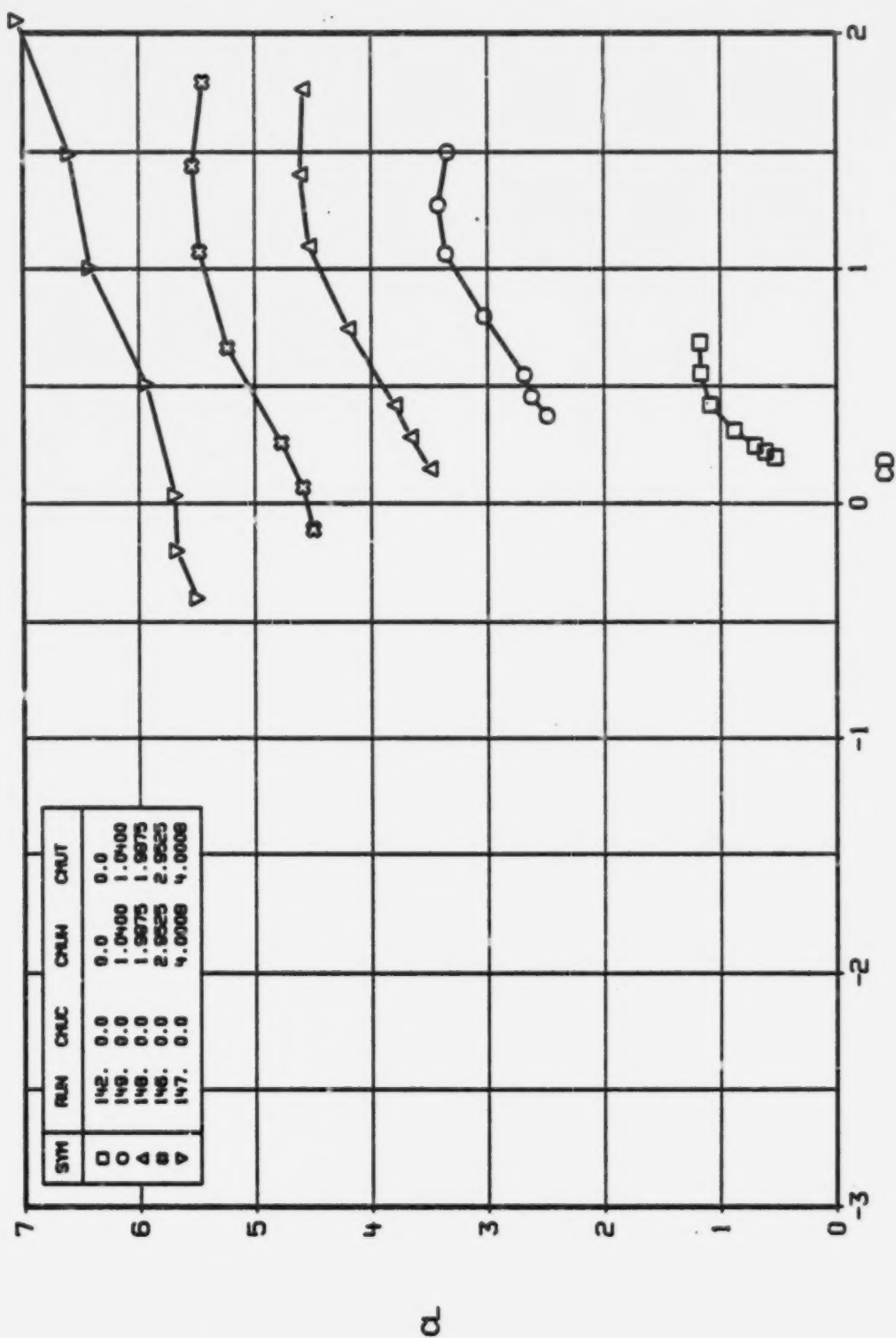


FIGURE A11b BASIC DATA EFFECT OF CHU
CONFIGURATION BM6V, DELF=45, BN/B=1

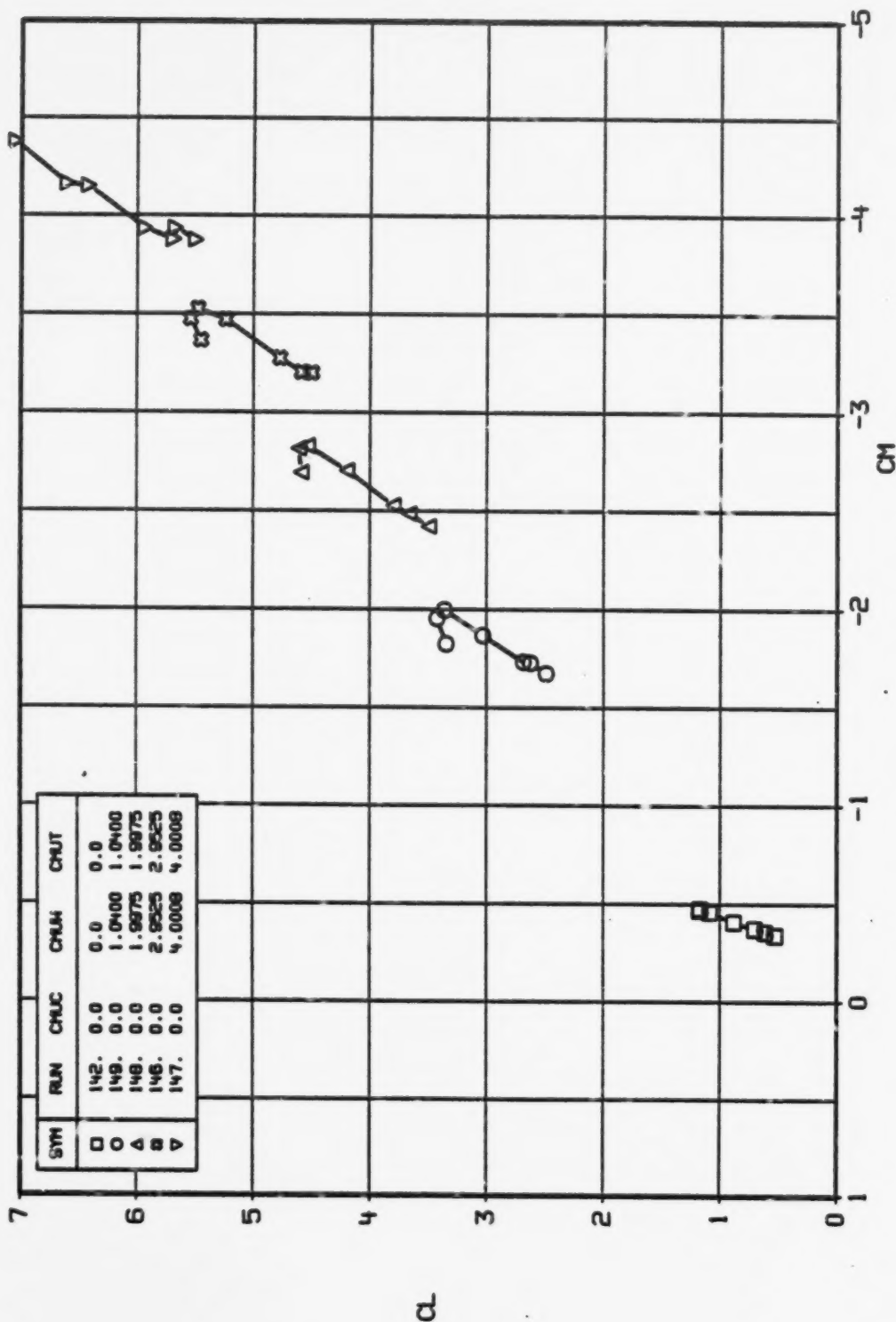


FIGURE A11c BASIC DATA EFFECT OF CMU
CONFIGURATION BM5V, DELF=45, BN/B=1

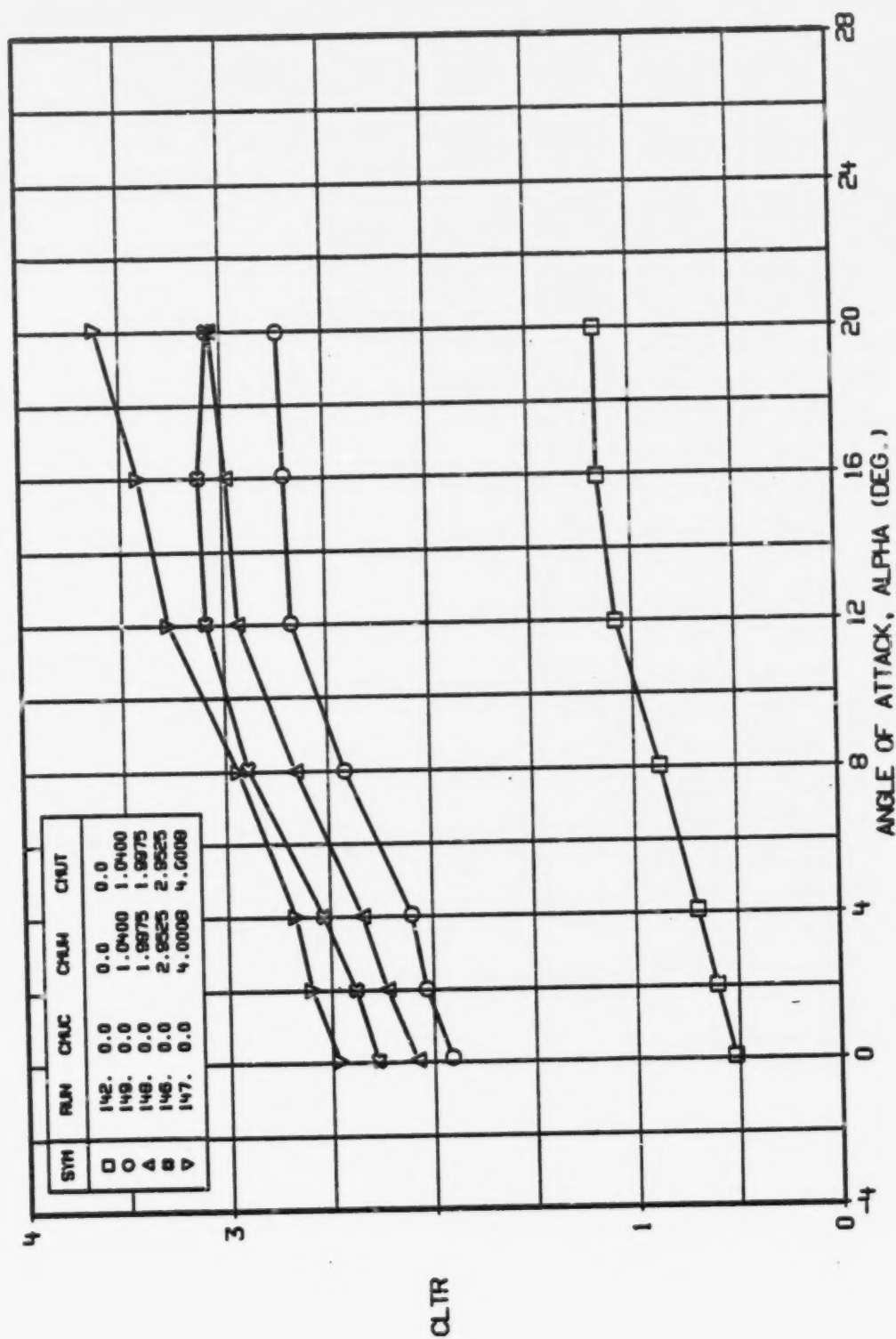


FIGURE A11d BASIC DATA EFFECT OF CHU
CONFIGURATION BW6V, DELF=45, BN/B=1

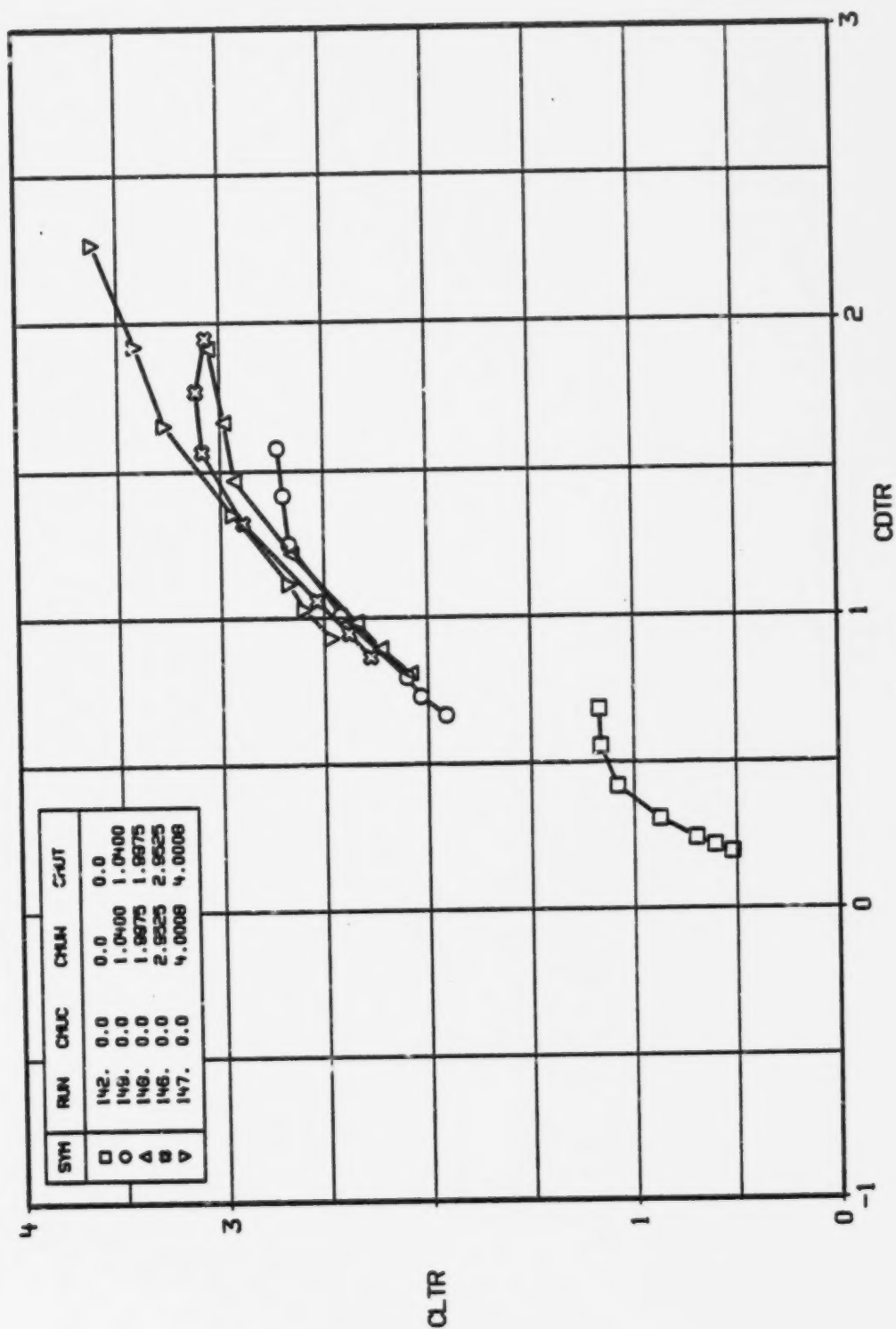


FIGURE A11e BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, DELF=45, BN/B=1

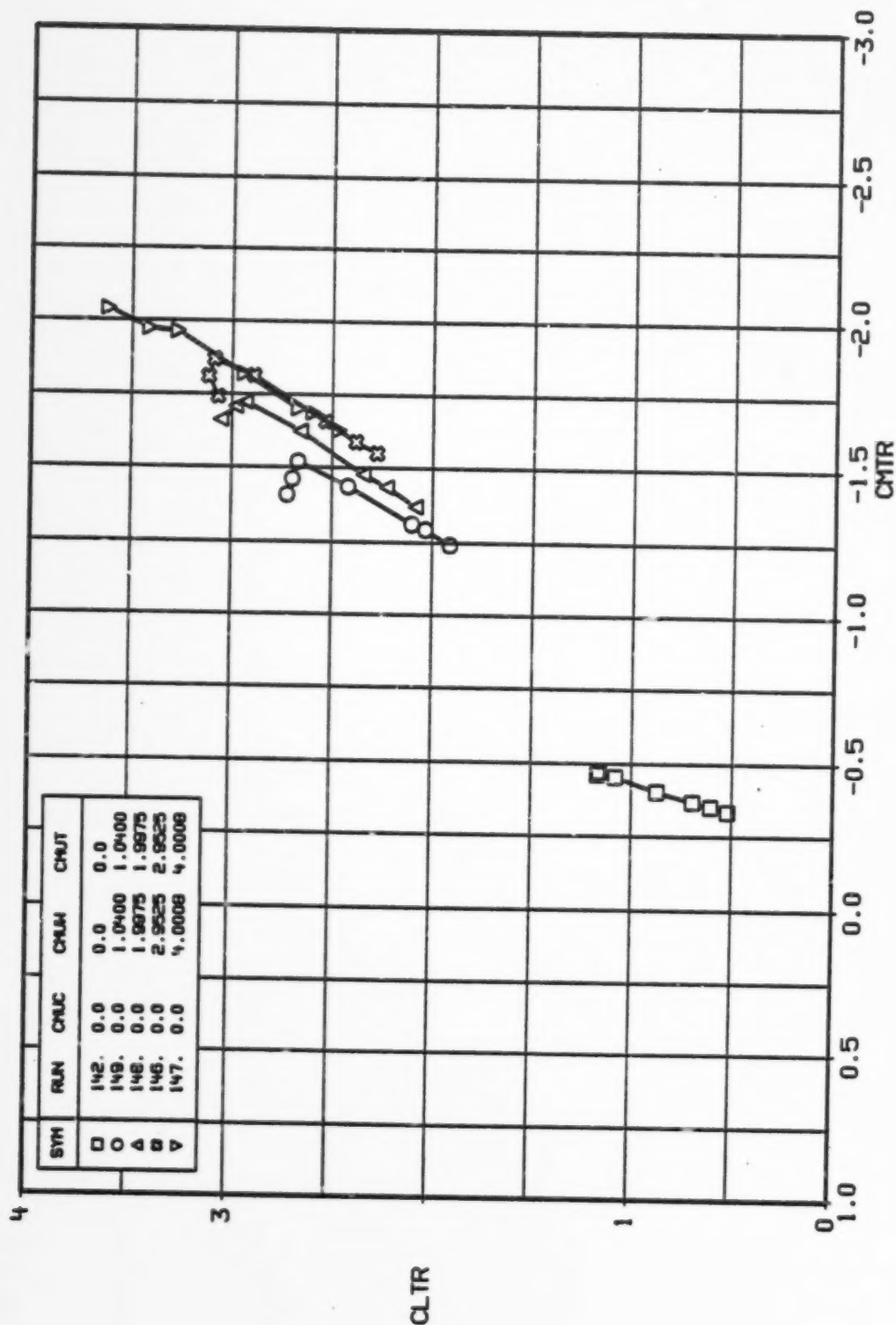


FIGURE A11f BASIC DATA EFFECT OF CMU
CONFIGURATION BMSV, DELF=45, BN/B=1

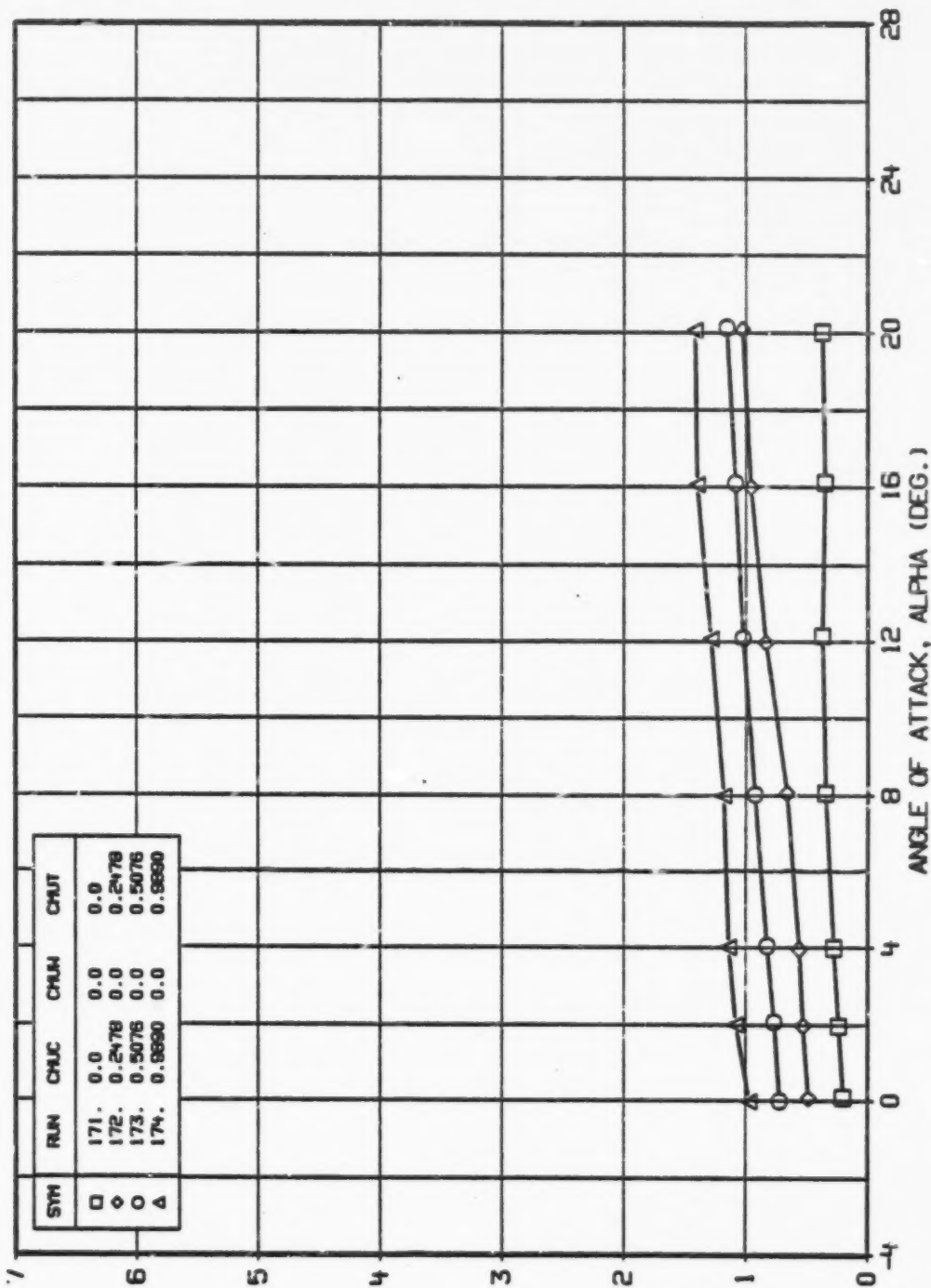


FIGURE A12a BASIC DATA EFFECT OF CHU
CONFIGURATION BCIV, DELF=45, DELC=10, BN/B=1

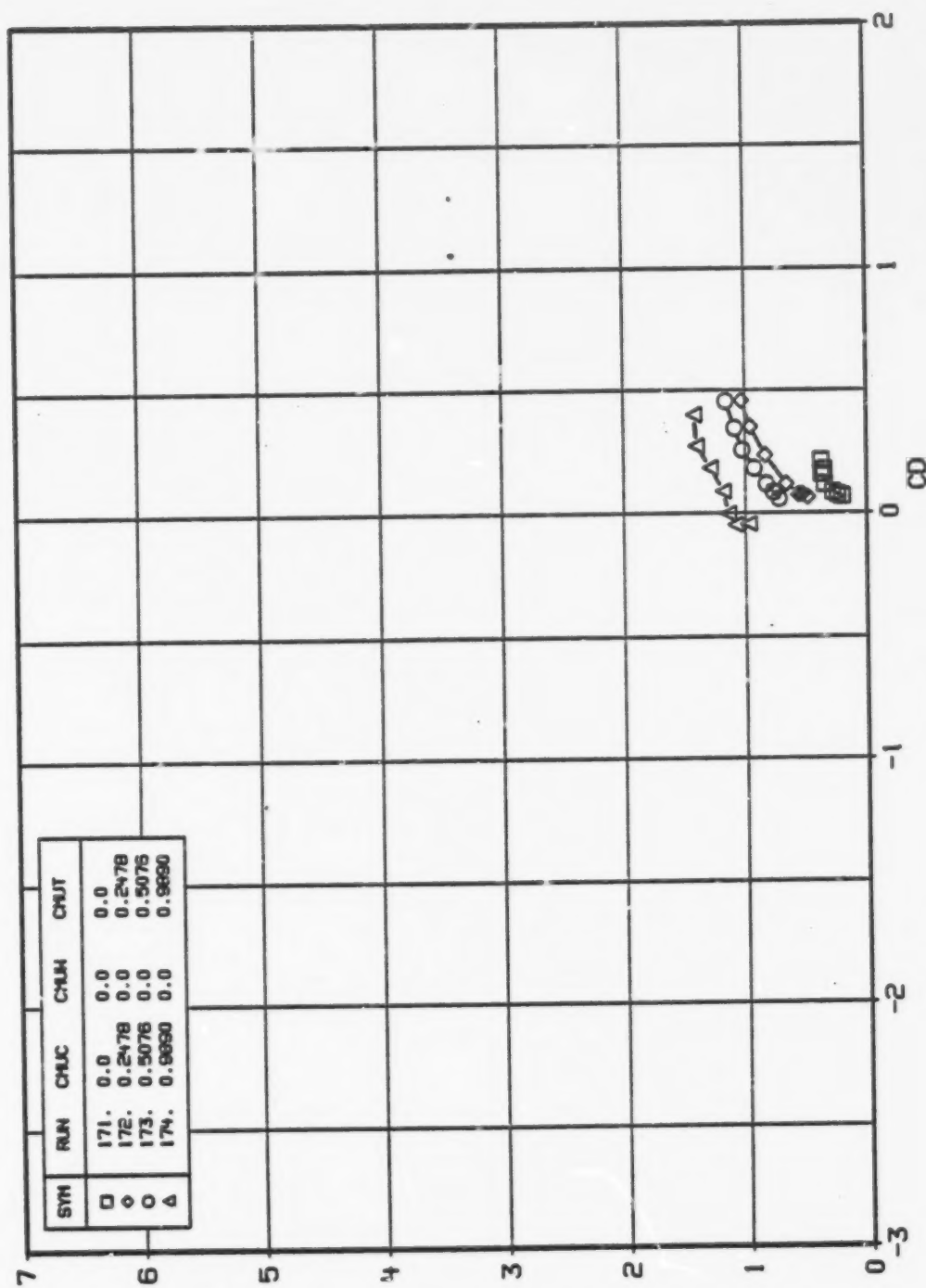


FIGURE A12b BASIC DATA EFFECT OF CMU
CONFIGURATION BCIV, DELF=45, DELC=10, BN/B=1

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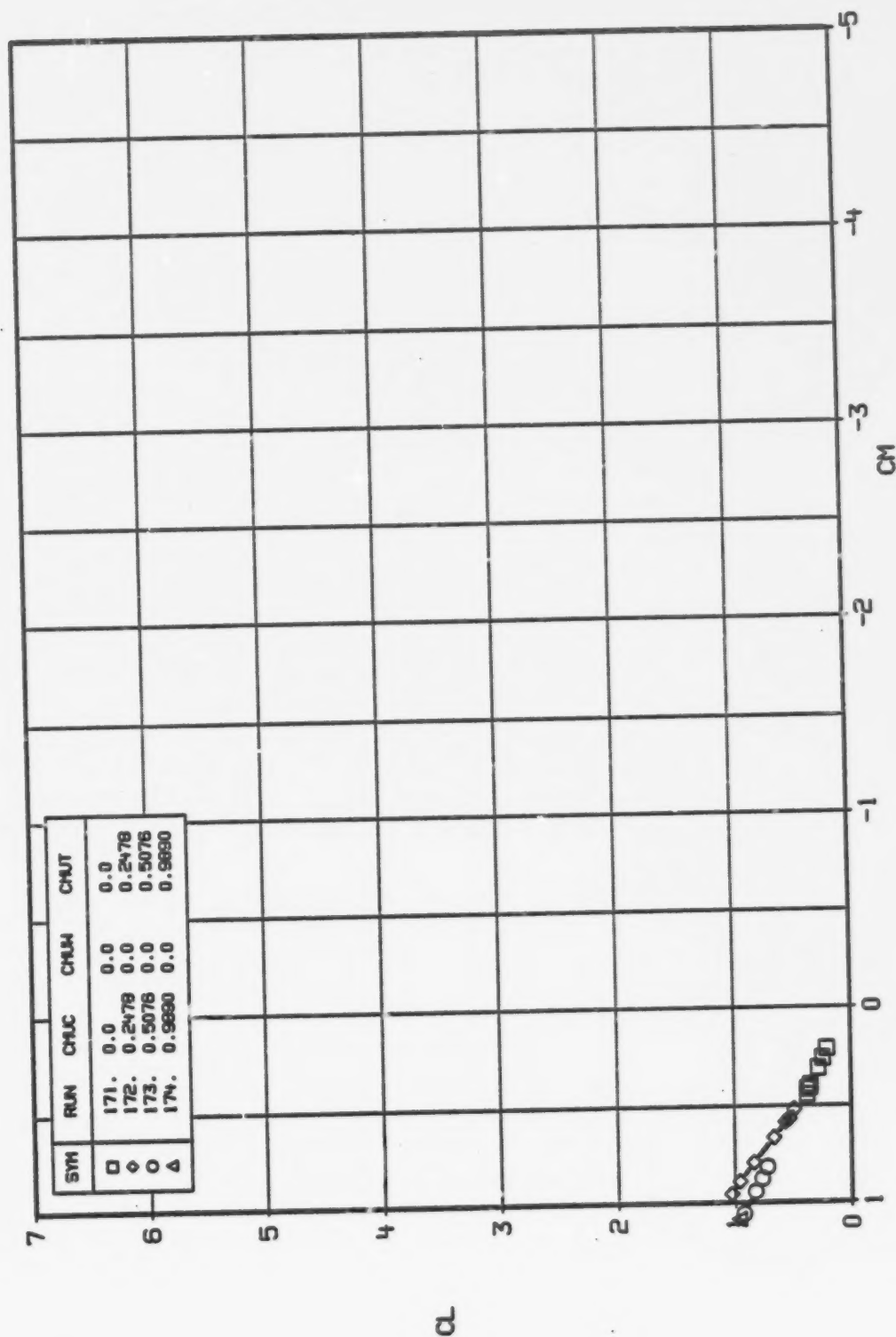


FIGURE A12C BASIC DATA EFFECT OF CMU
CONFIGURATION BCIV, DELF=45, DELC=10, BN/B=1

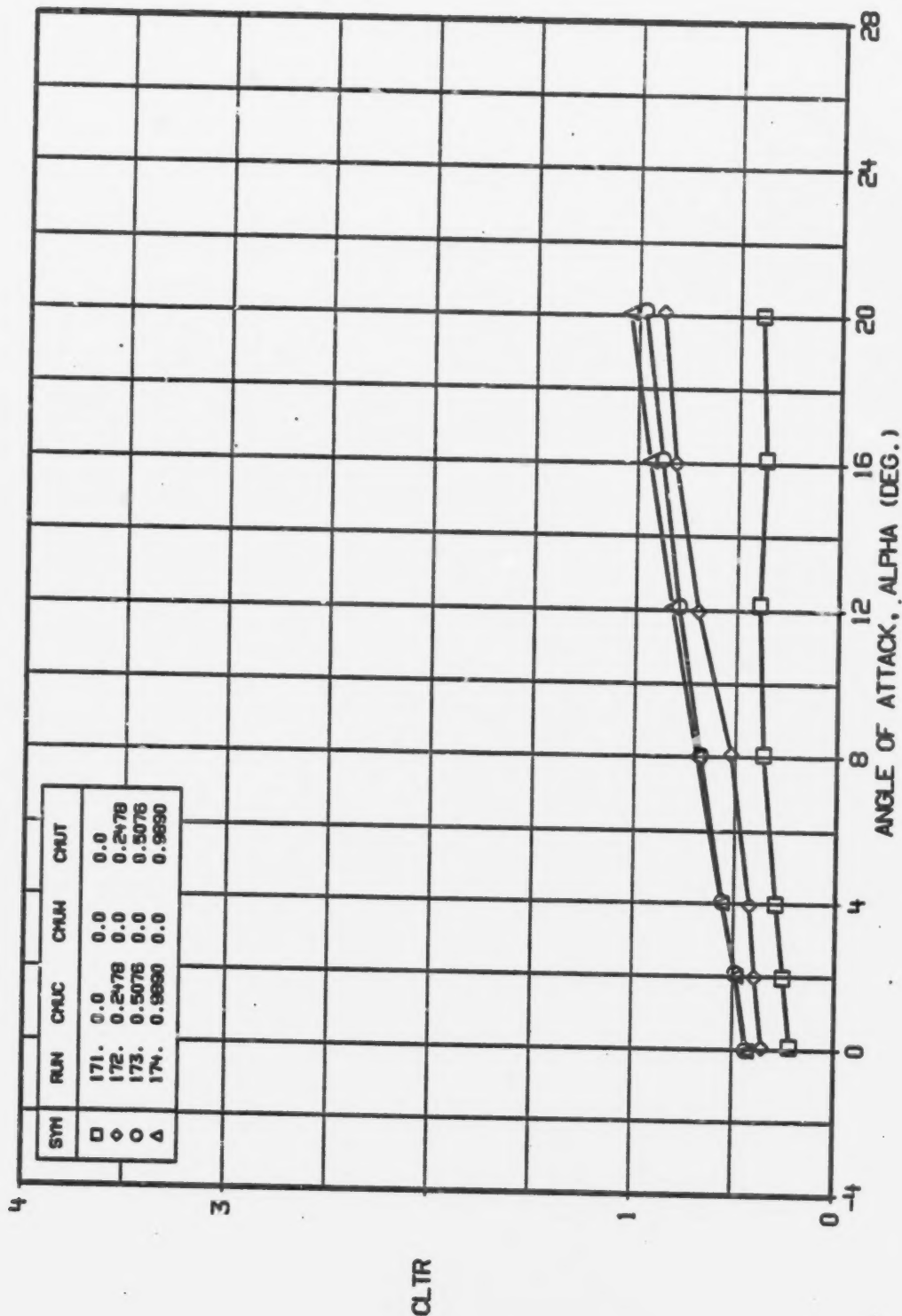


FIGURE A12d BASIC DATA EFFECT OF CMU
CONFIGURATION BCIV, DELF=45, DELC=10, BN/B=1

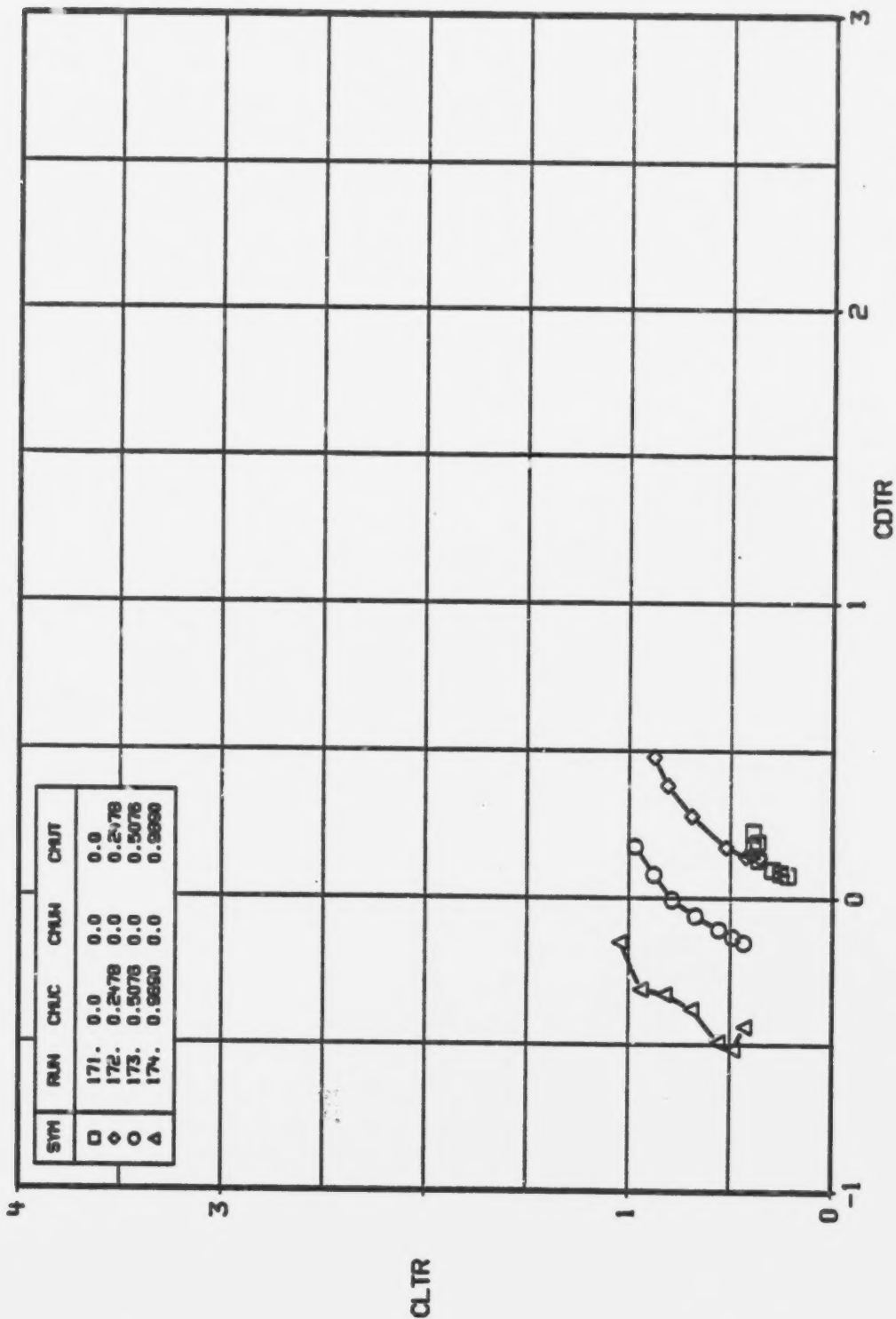


FIGURE A12e BASIC DATA EFFECT OF CMU
CONFIGURATION BCIV, DELF=45, DELC=10, EN/B=1

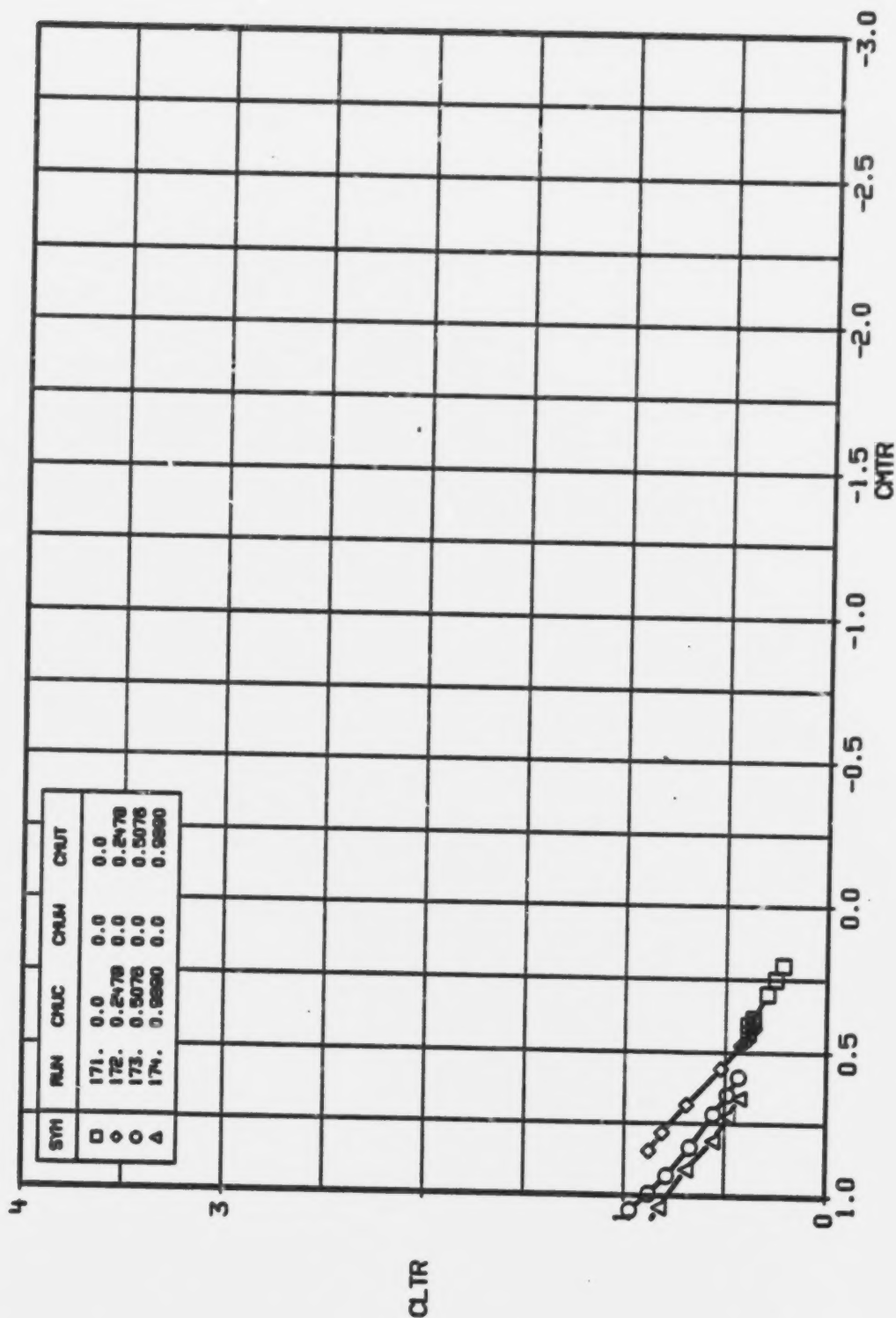


FIGURE A12f BASIC DATA EFFECT OF CMU
CONFIGURATION BCIV, DELF=45, DELC=10, BN/B=1

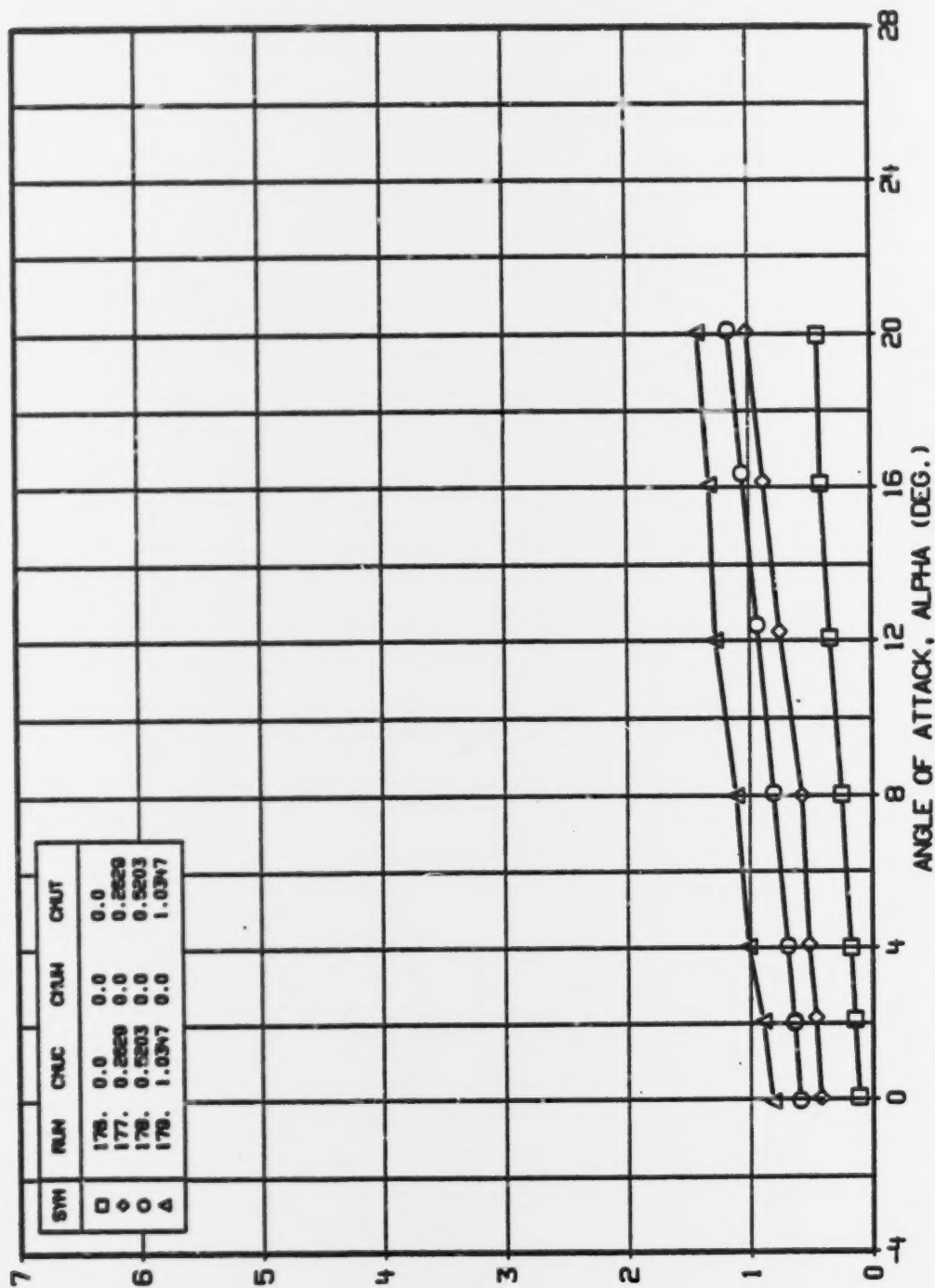


FIGURE A13a BASIC DATA EFFECT OF CMU
CONFIGURATION BCIV, DELF=45, BN/B=1

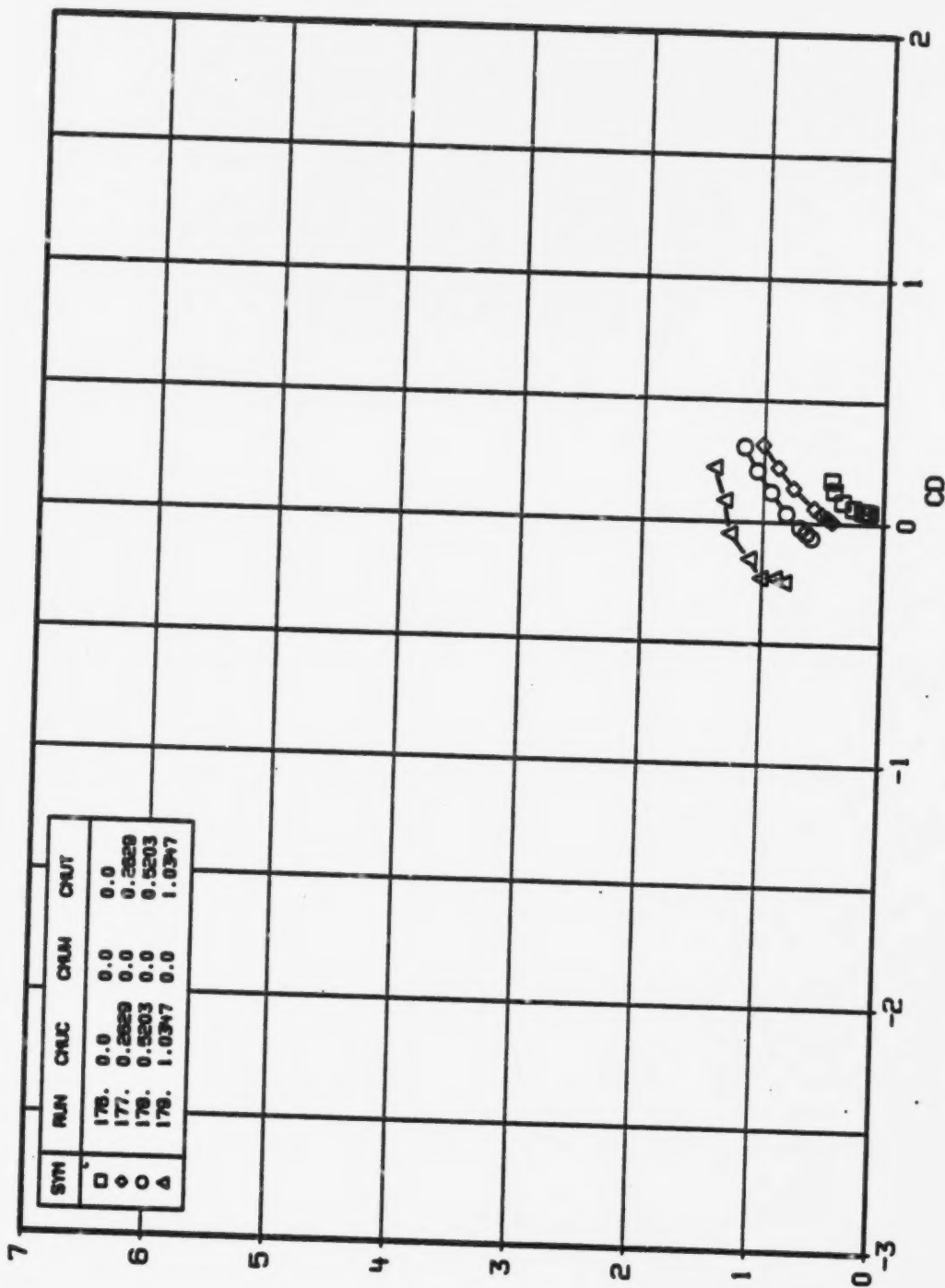


FIGURE A13b BASIC DATA EFFECT OF CHU
CONFIGURATION BCIV, DELF=45, BN/B=1

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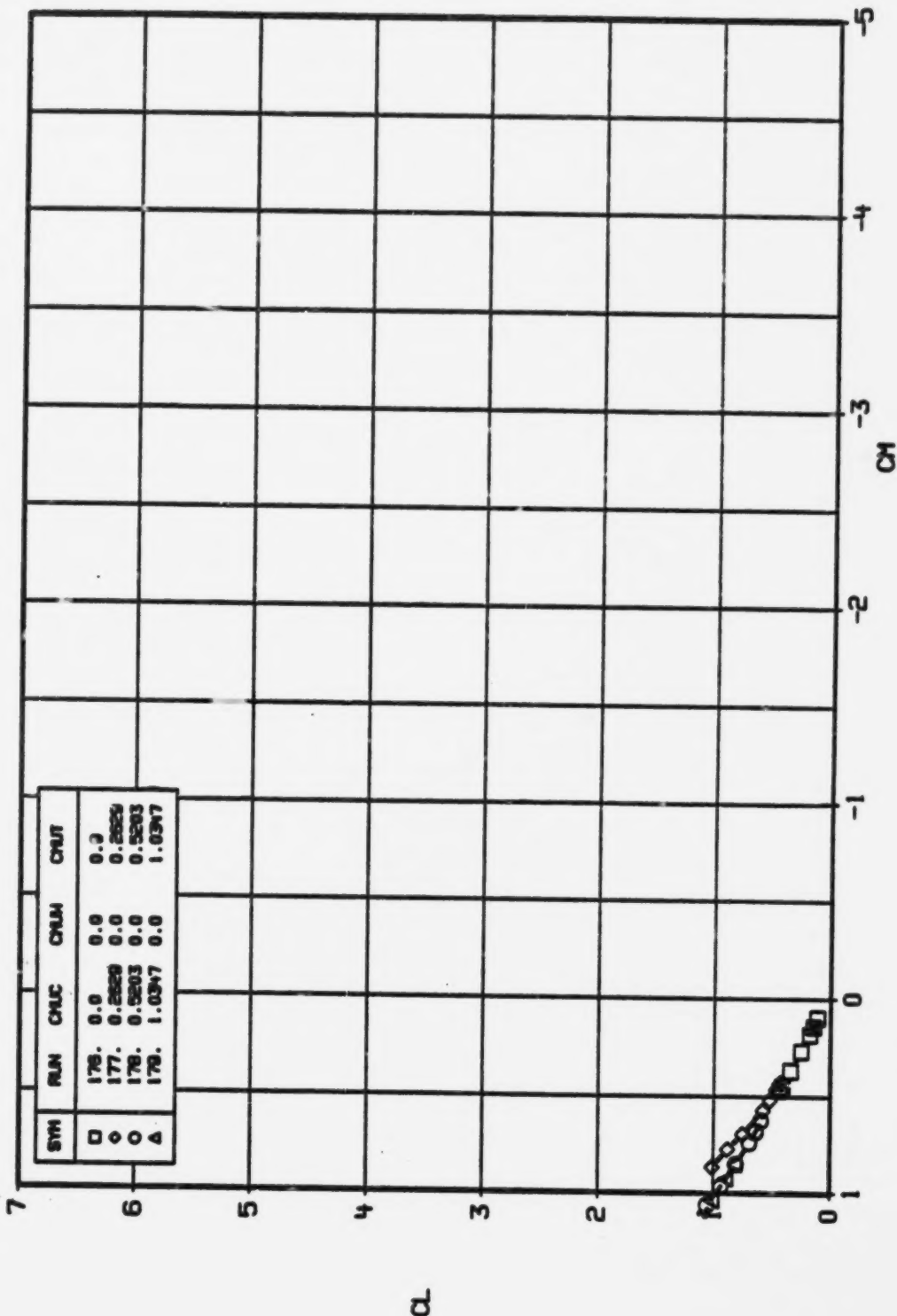


FIGURE A13c BASIC DATA EFFECT OF CHU
CONFIGURATION BCIV, DELF=45, BN/B=1

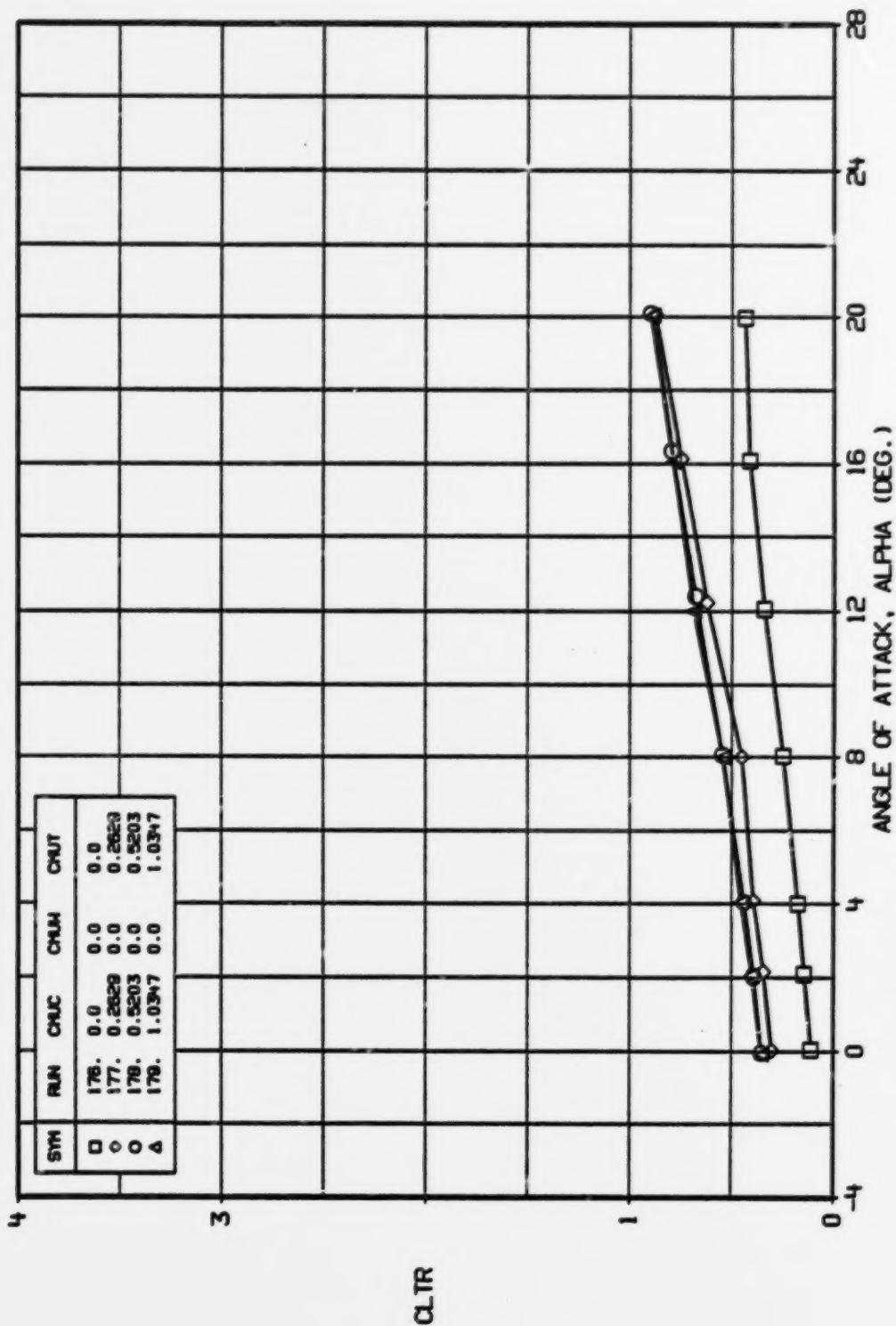


FIGURE A13d BASIC DATA EFFECT OF CMU
CONFIGURATION BCIV, DELF=45, BN/B=1

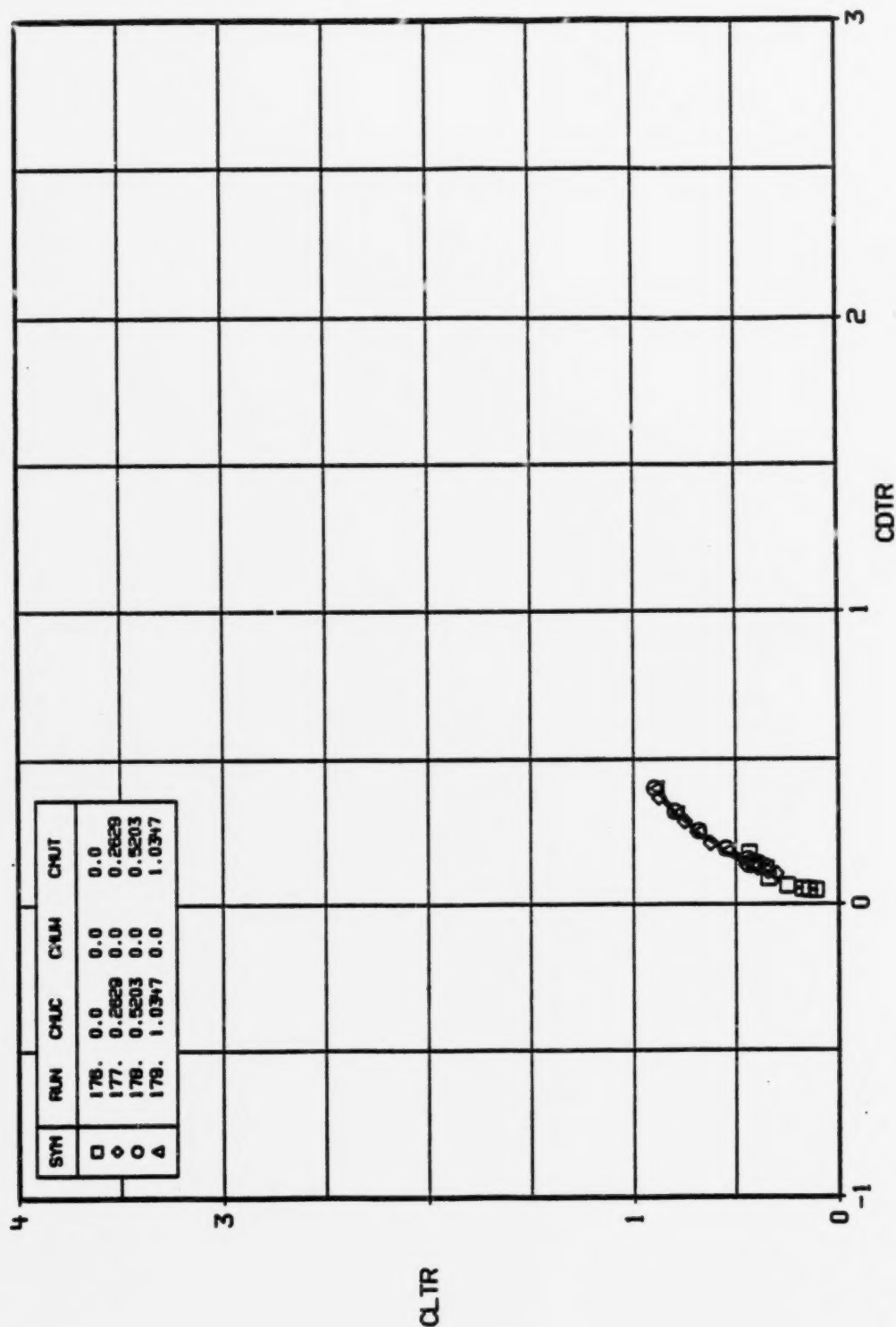


FIGURE A13e BASIC DATA EFFECT OF CMU
CONFIGURATION BC1V, DELF=45, BN/B=1

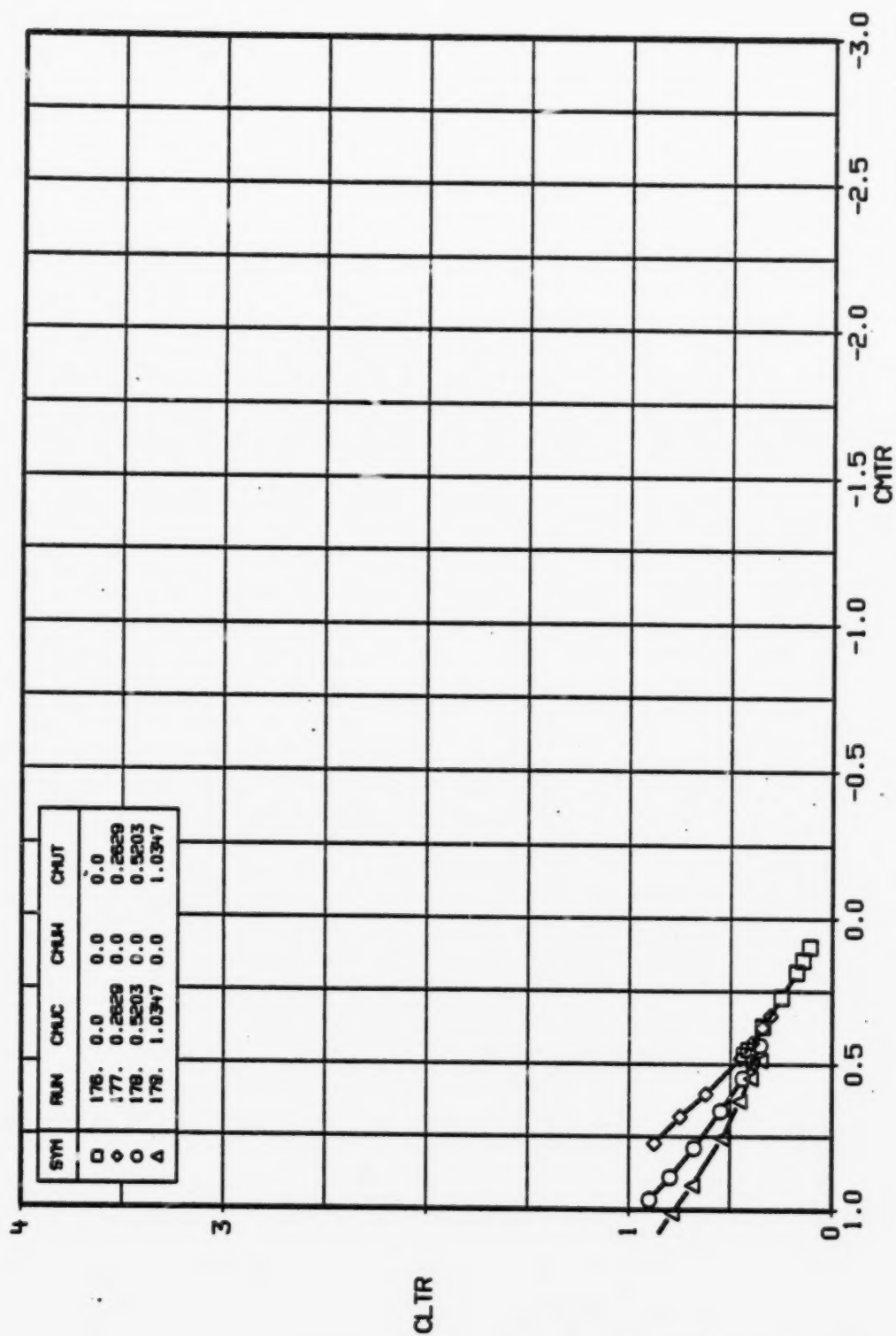


FIGURE A13F BASIC DATA EFFECT OF CMU
CONFIGURATION BC1V, DELF=45, BN/B=1

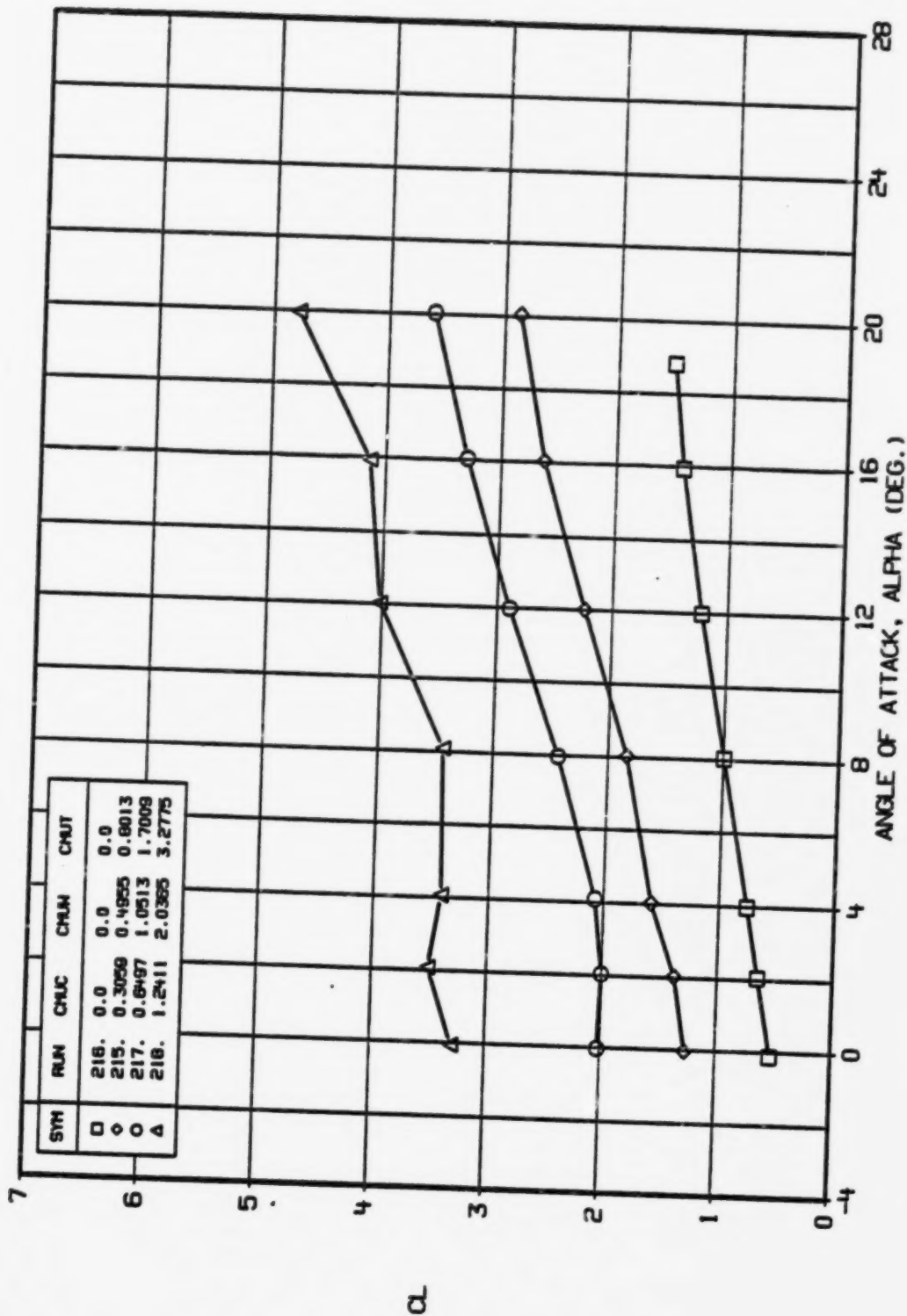


FIGURE A14a BASIC DATA EFFECT OF CHU
CONFIGURATION BC146V, (BN/B)C=1, (BN/B)W=0.5, DELF=45

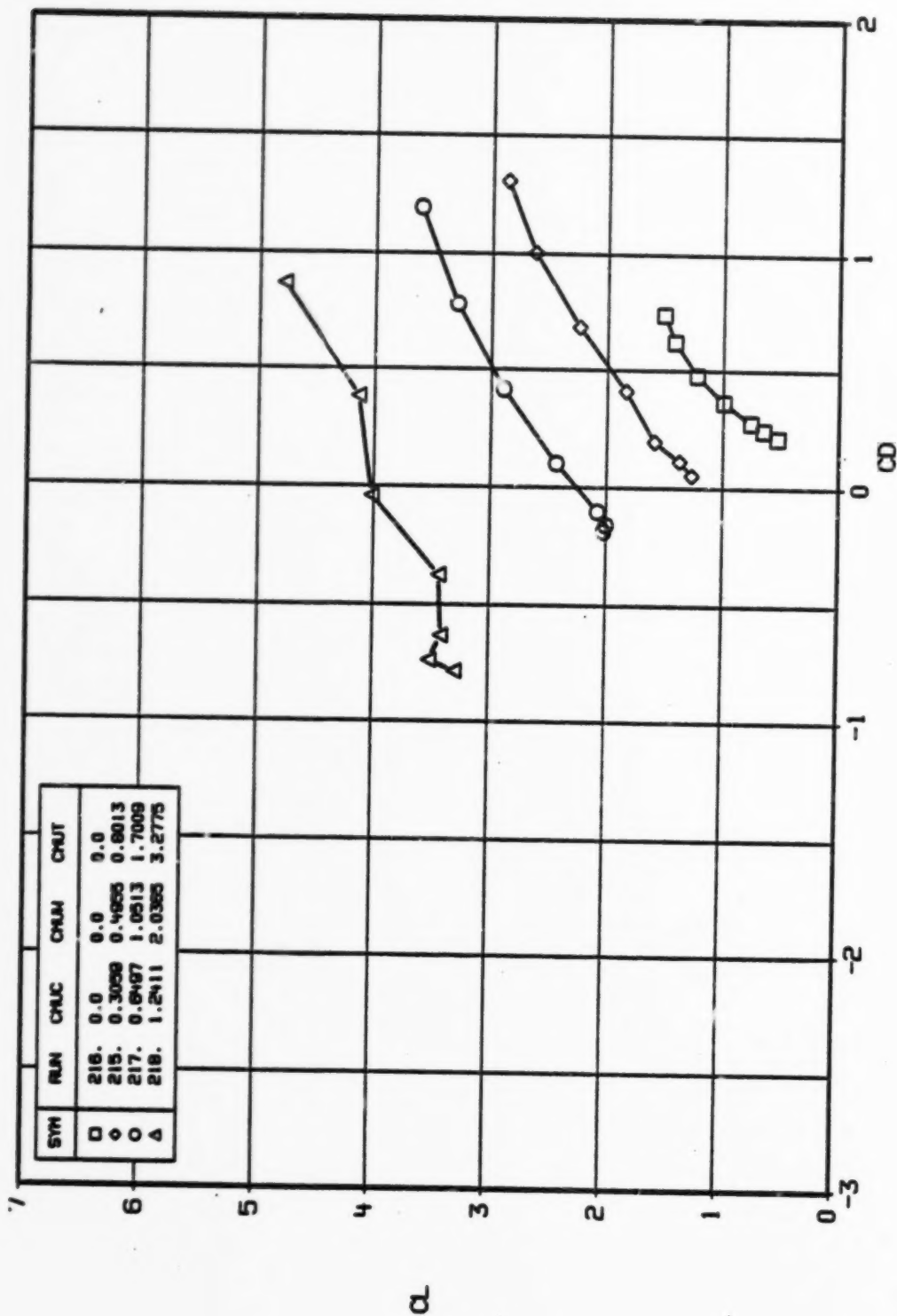


FIGURE A14b BASIC DATA EFFECT OF CHU
CONFIGURATION BC145V, (BN/BI)C=1, (BN/BI)W=0.5, DELF=45

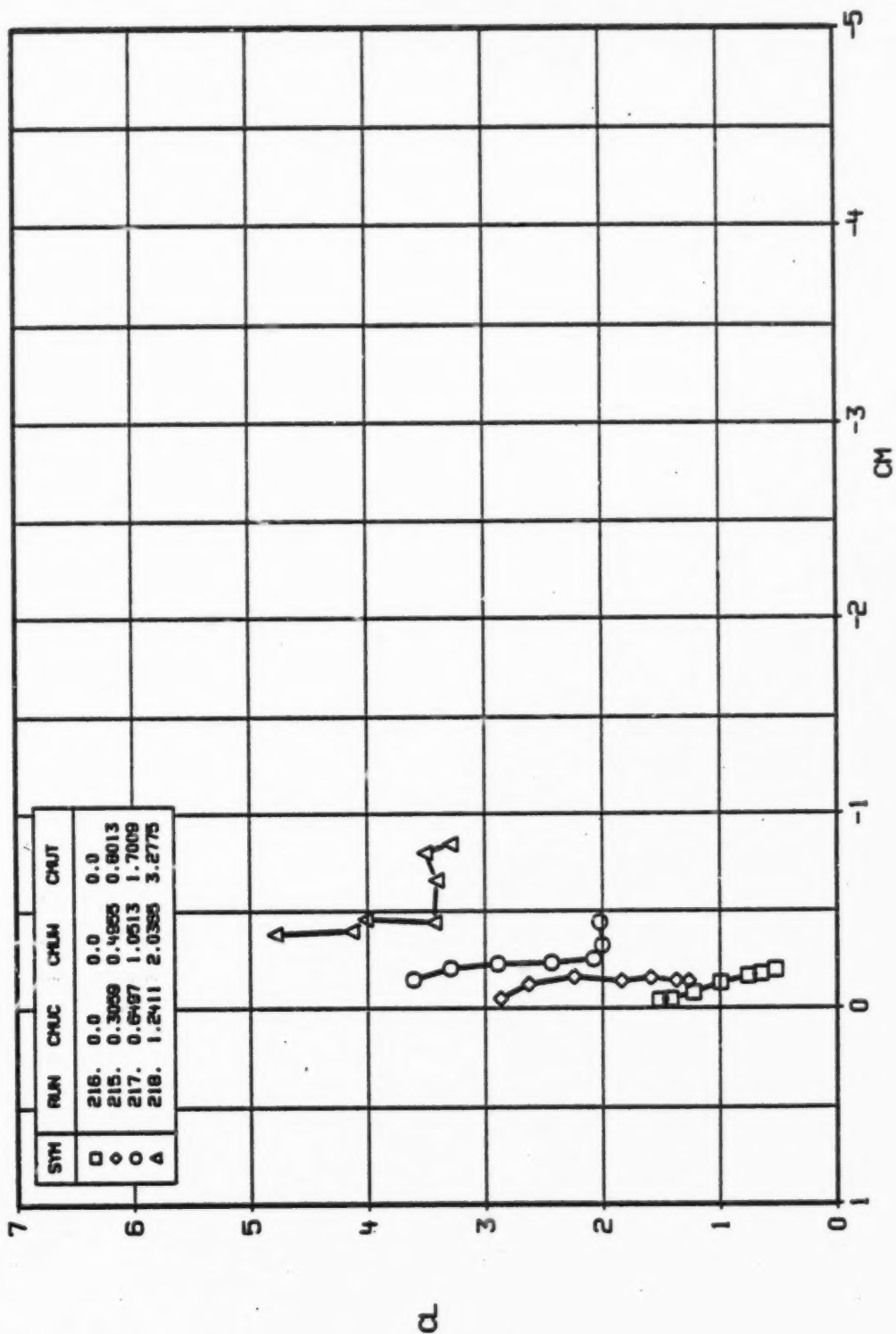


FIGURE A14c BASIC DATA EFFECT OF CMU
CONFIGURATION BC145V, (BN/B)C=1, (BN/B)W=0.5, DELF=45

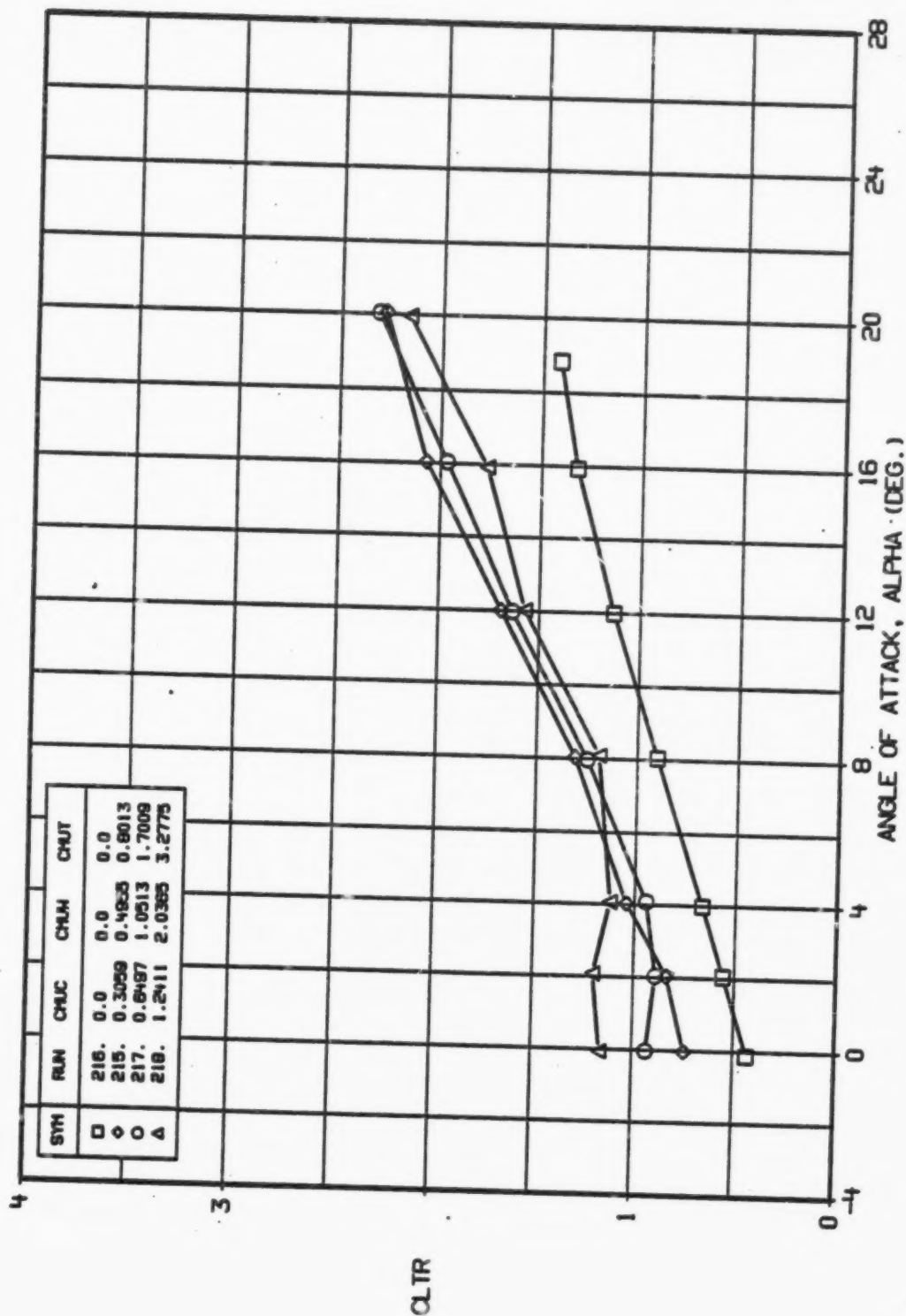


FIGURE A14d BASIC DATA EFFECT OF CMU
CONFIGURATION BC146V, (BN/B)C=1, (BN/B)W=0.5, DELF=45

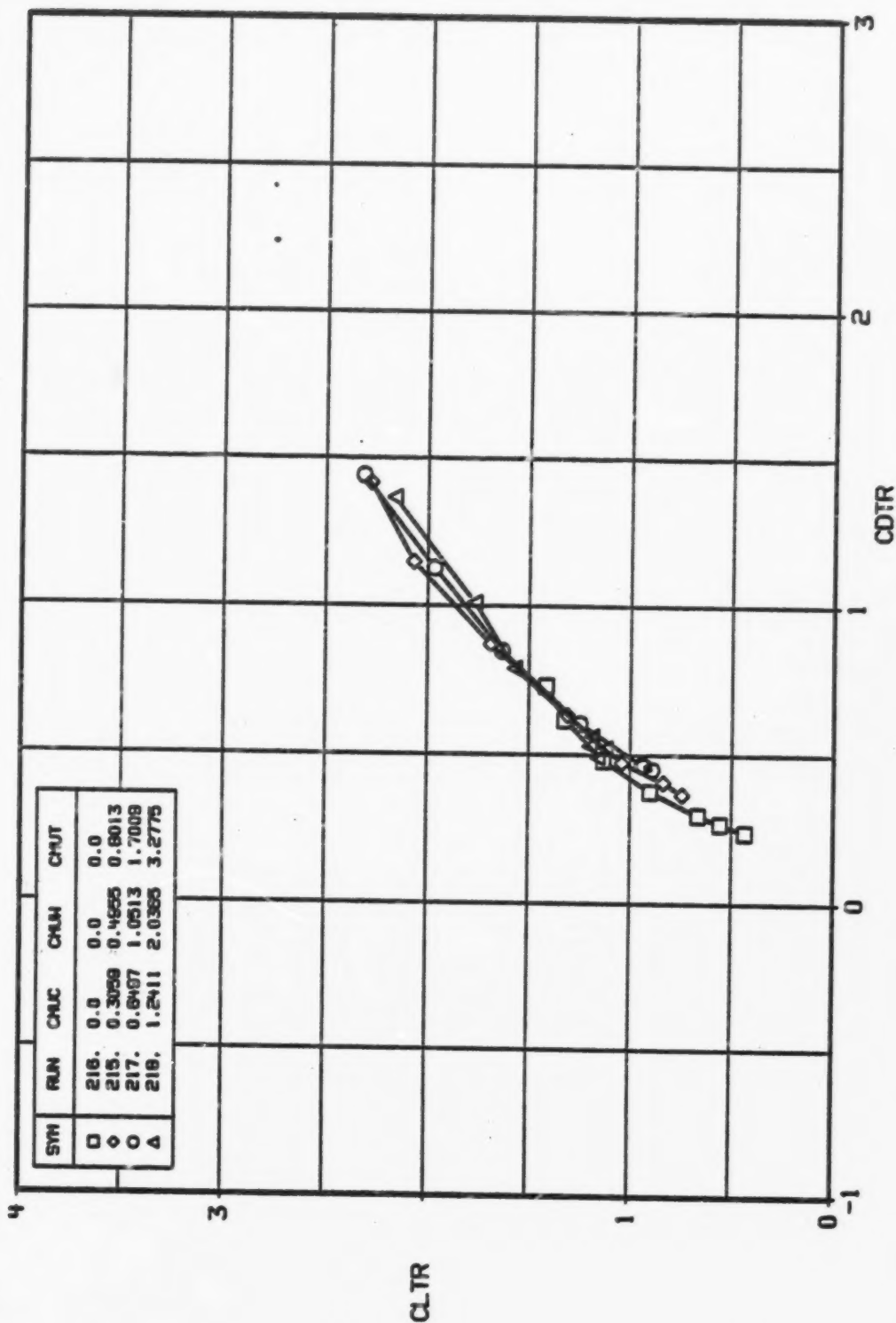


FIGURE A14e BASIC DATA EFFECT OF CHU
CONFIGURATION BC1WSV, (BN/BI)C=1, (BN/BI)W=0.5, DELF=45

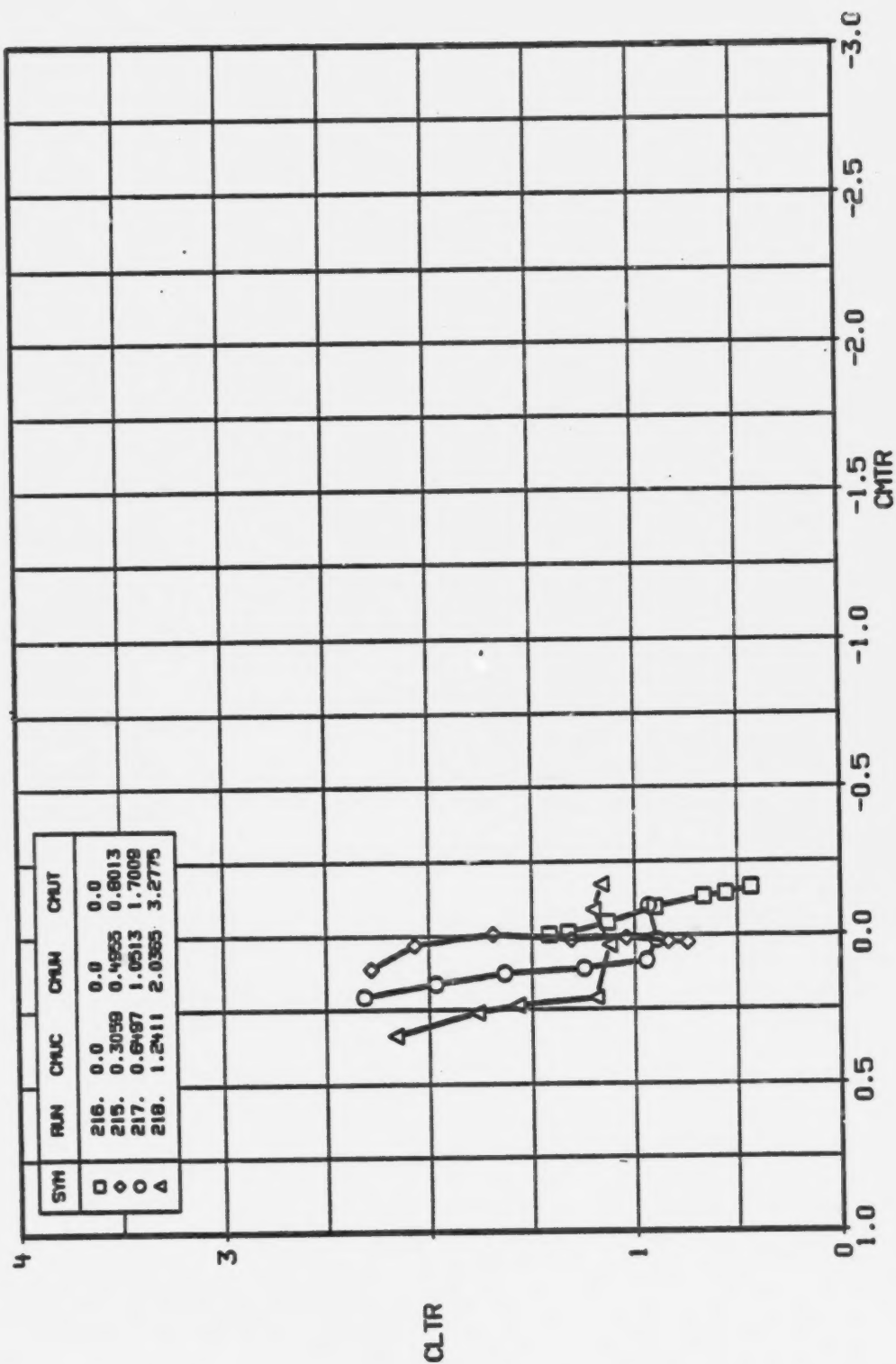


FIGURE A14f BASIC DATA EFFECT OF CMU
CONFIGURATION BC1W6V, (BN/B)C=1, (BN/B)W=0.5, DELF=45

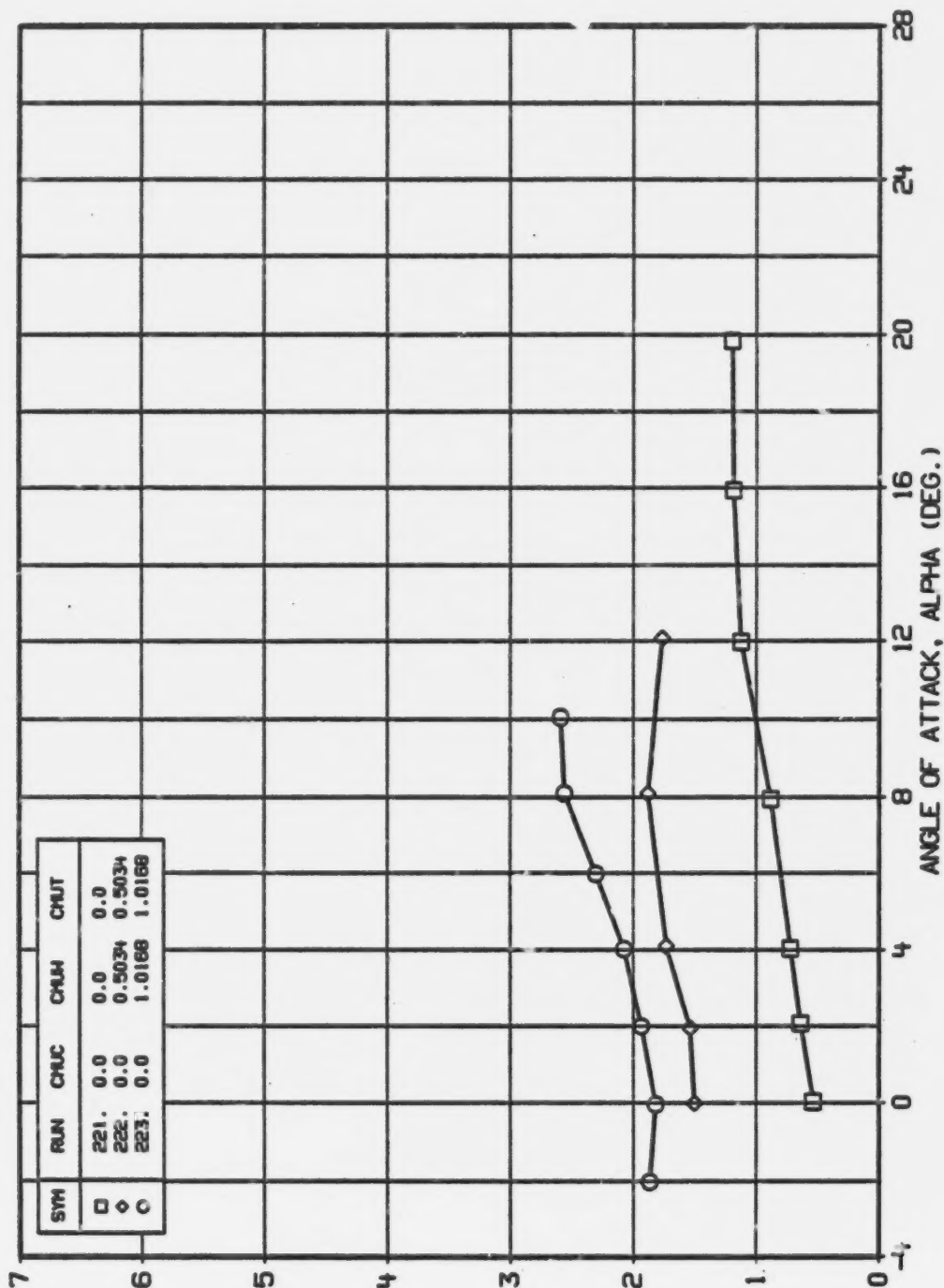


FIGURE A15a BASIC DATA EFFECT OF CMU
CONFIGURATION EM6V, EN/B=0.5, DELF=45

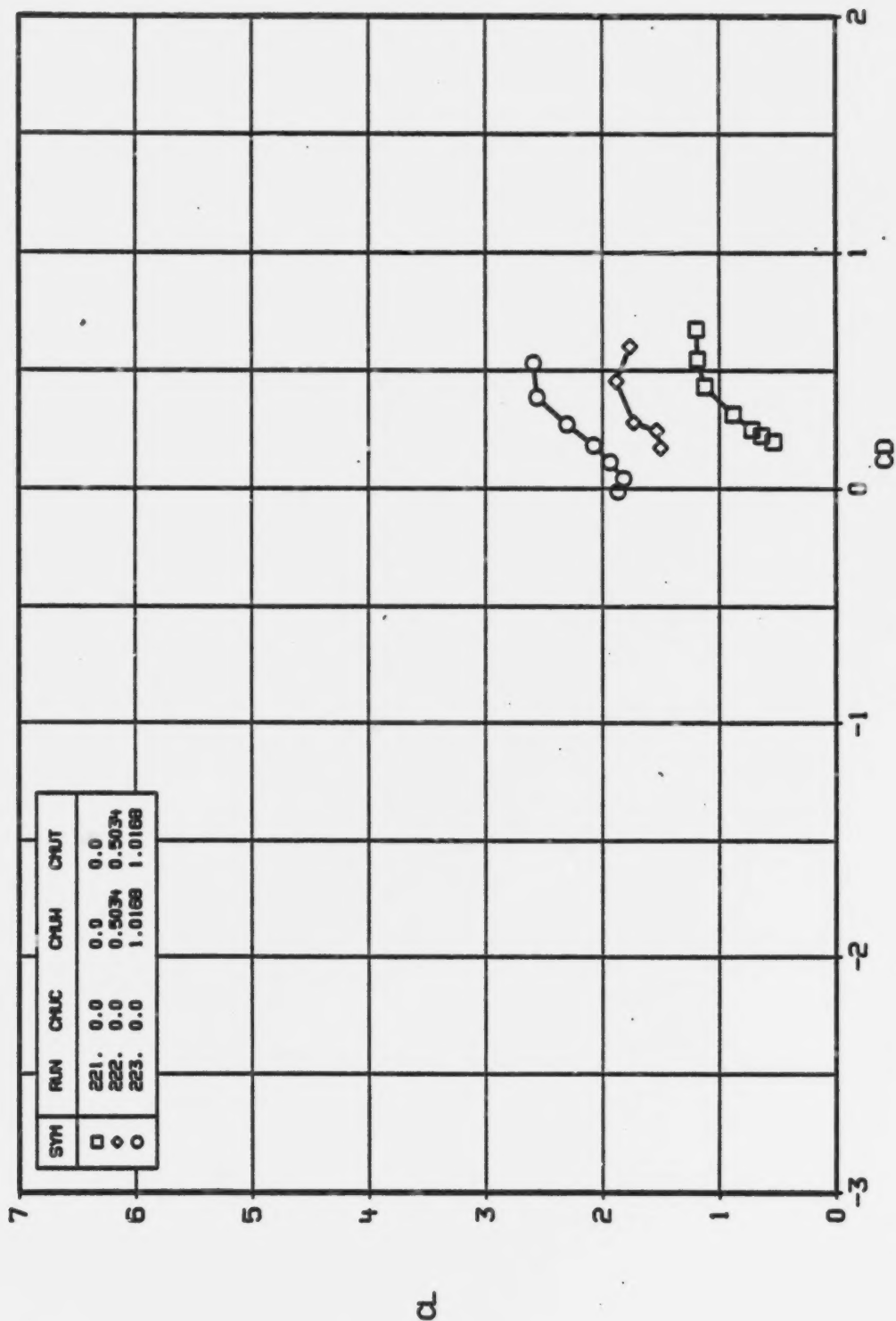


FIGURE A15b BASIC DATA EFFECT OF CMU
CONFIGURATION BAJV, EN/B=0.5, DELF=45

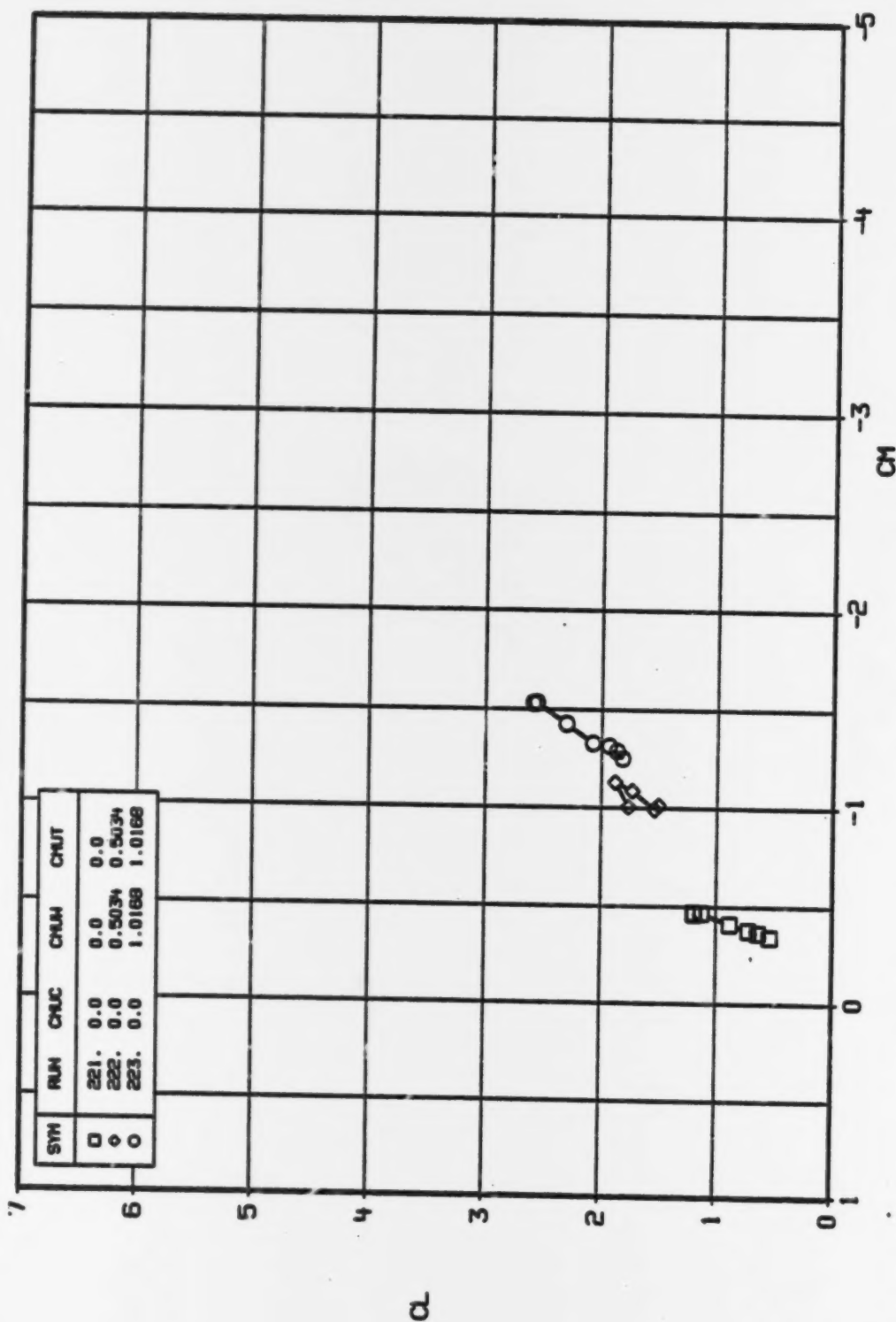


FIGURE A15c BASIC DATA EFFECT OF CMU
CONFIGURATION BMSV, BN/B=0.5, DELF=45

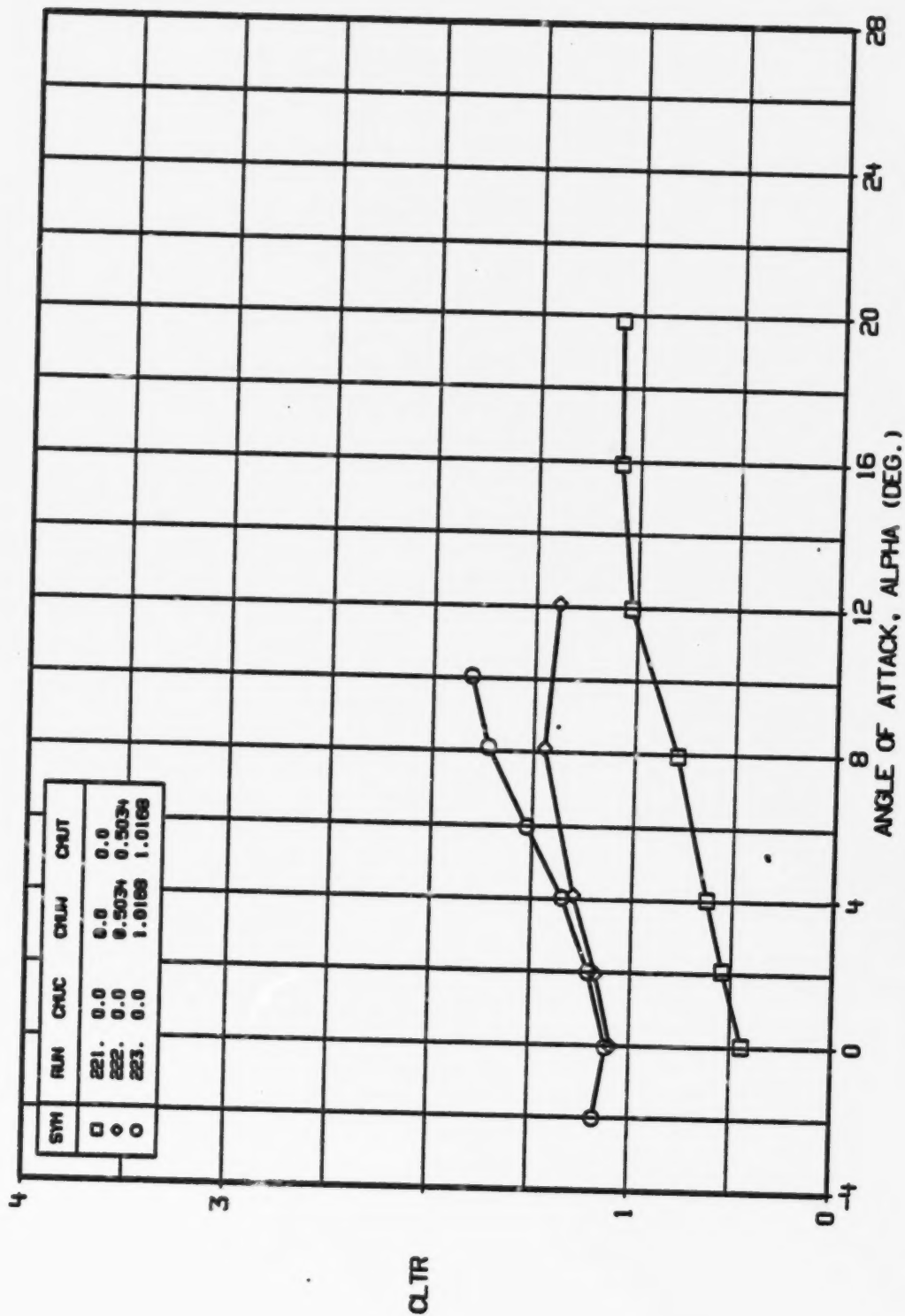


FIGURE A15d BASIC DATA EFFECT OF CMJ
CONFIGURATION B46V, BN/B=0.5, DELF=45

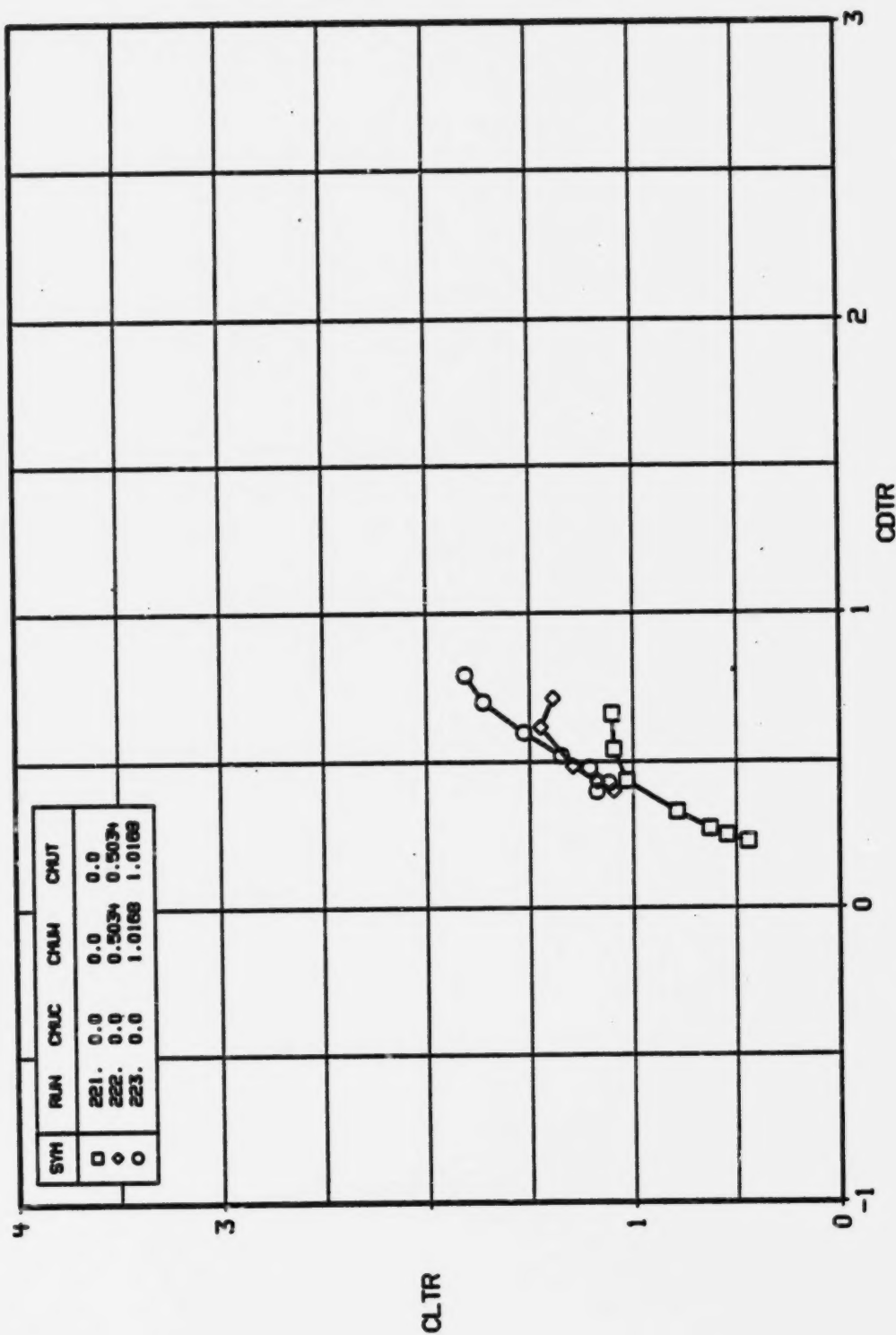


FIGURE A15e BASIC DATA EFFECT OF CHU
CONFIGURATION BMSV, BN/B=0.5, DELF=45

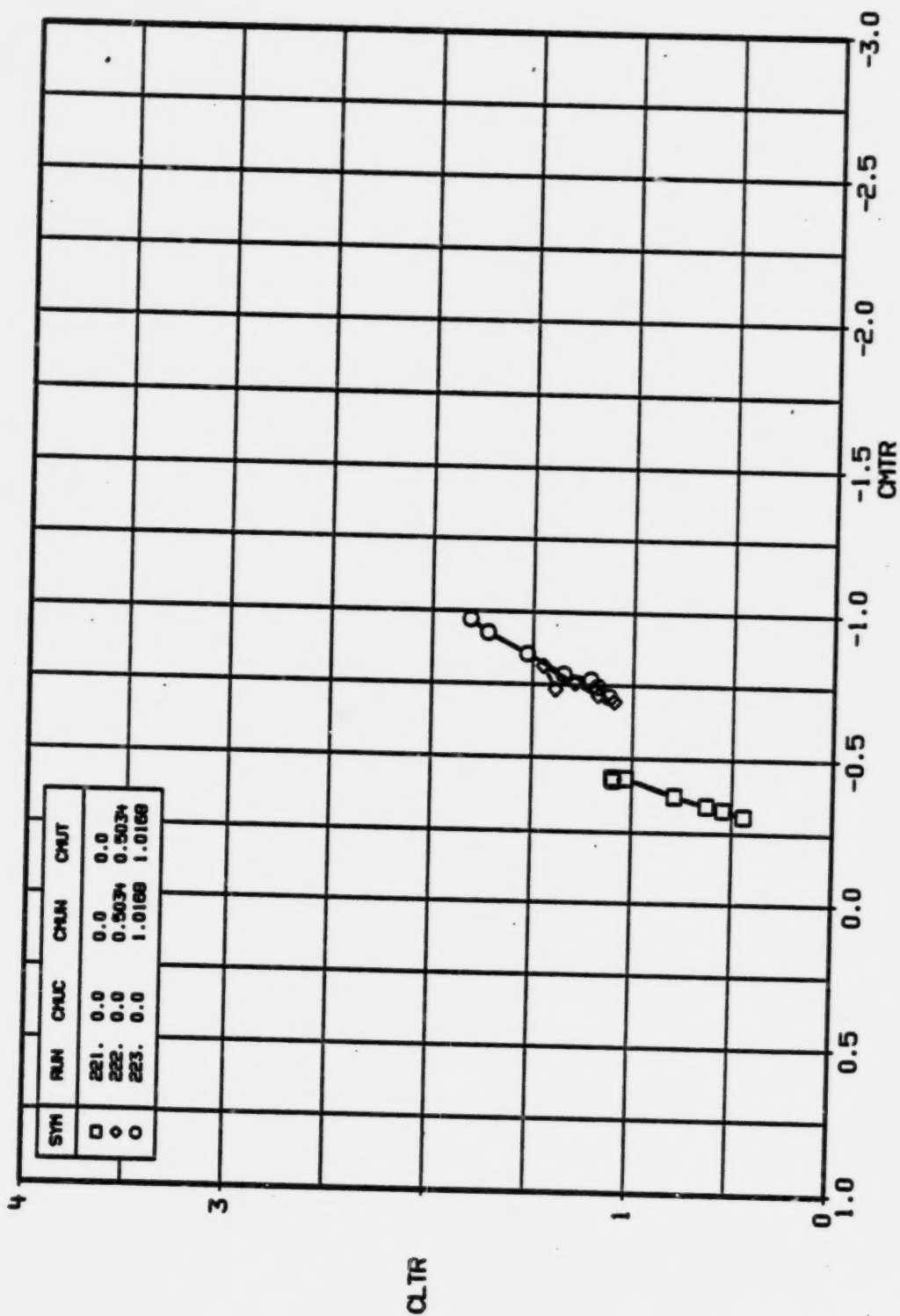


FIGURE A15f BASIC DATA EFFECT OF CMU
CONFIGURATION EN/BV, EN/B=0.5, DELF=45

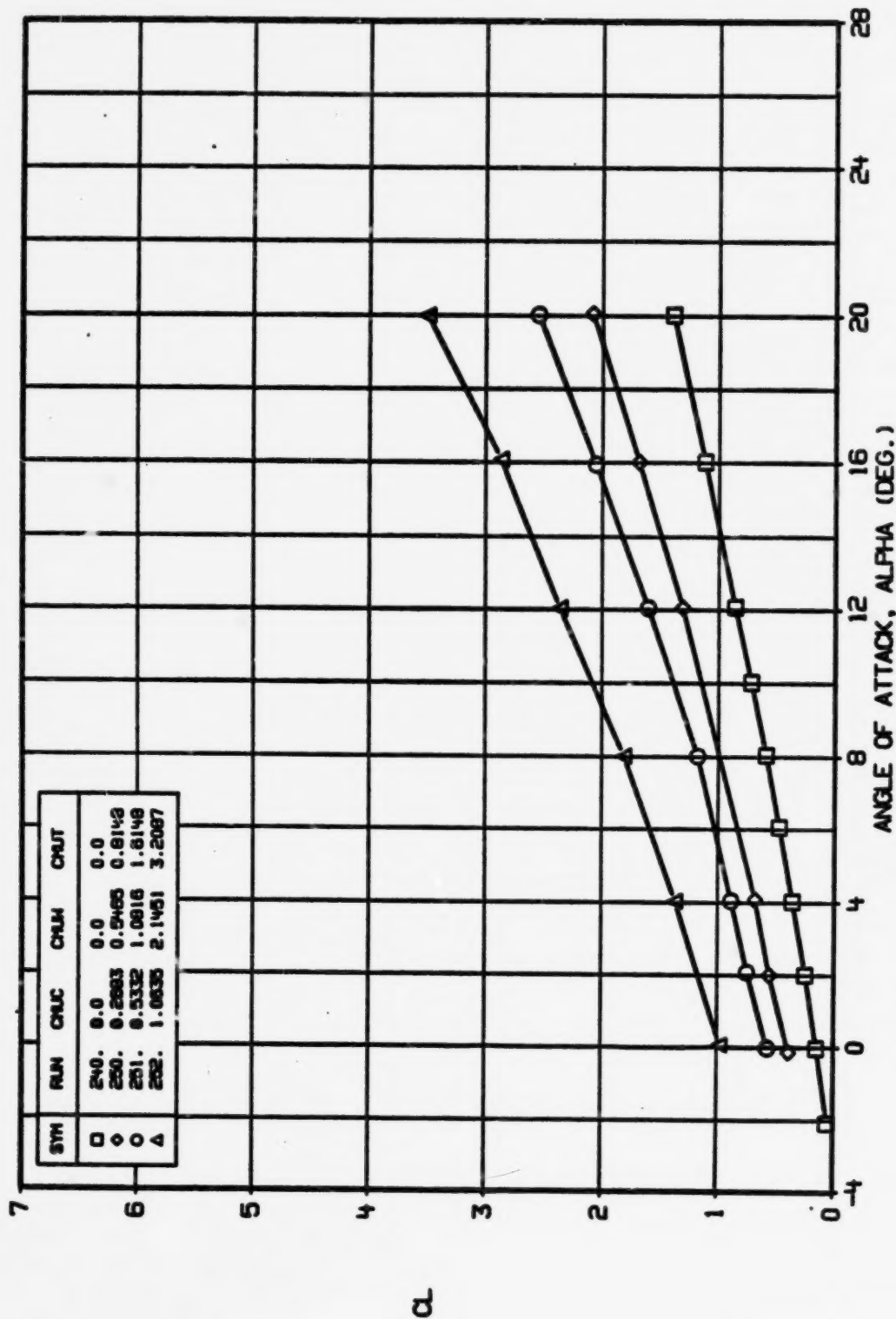


FIGURE A16a BASIC DATA EFFECT OF CMU
CONFIGURATION BC1M5V, (BN/B)C=1, (BN/B)H=0.5, DELF=0

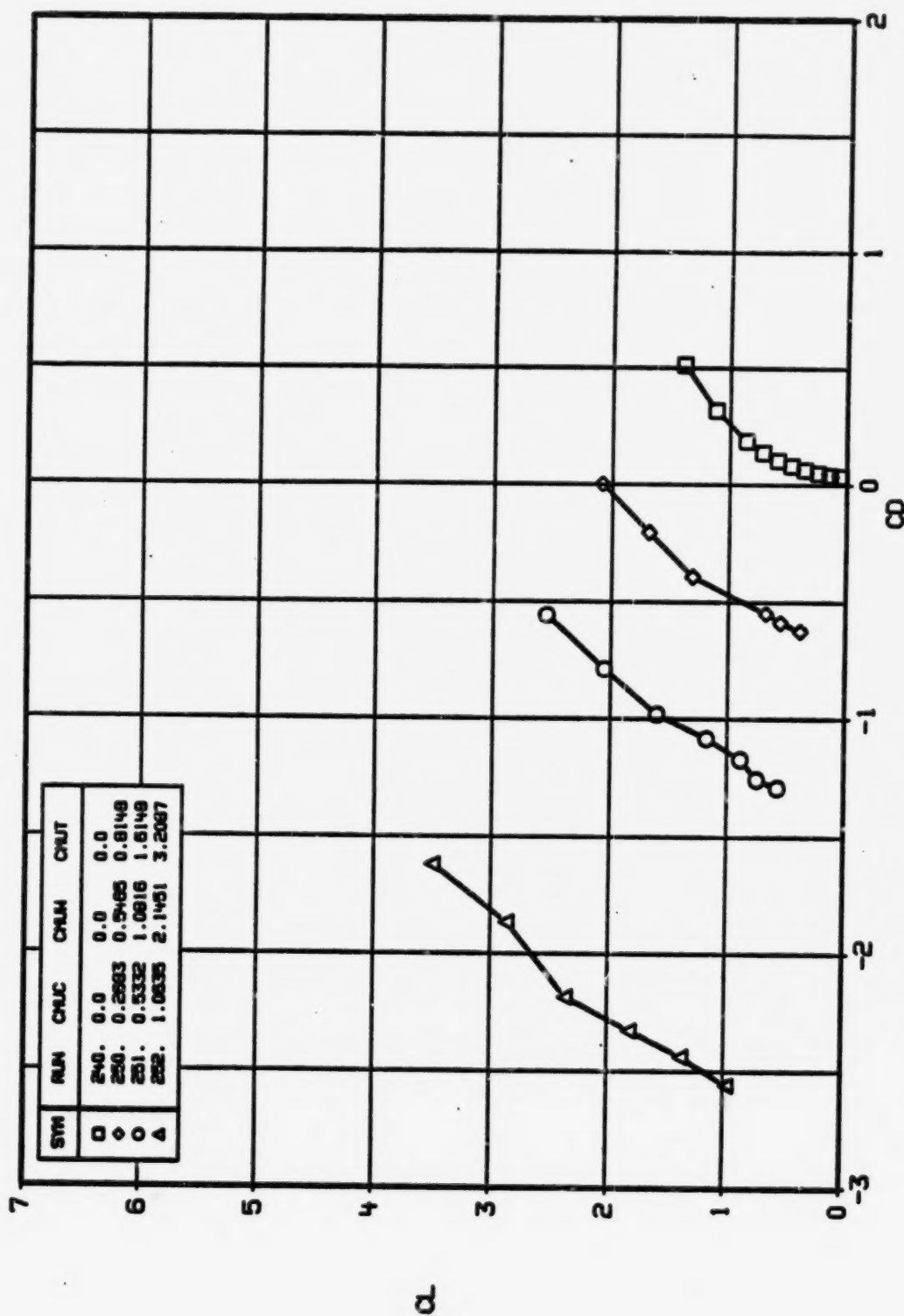


FIGURE A16b BASIC DATA EFFECT OF CHU
CONFIGURATION BC1HSV, (BN/B₁)C=1, (BN/B₂)W=0.5, DELF=0

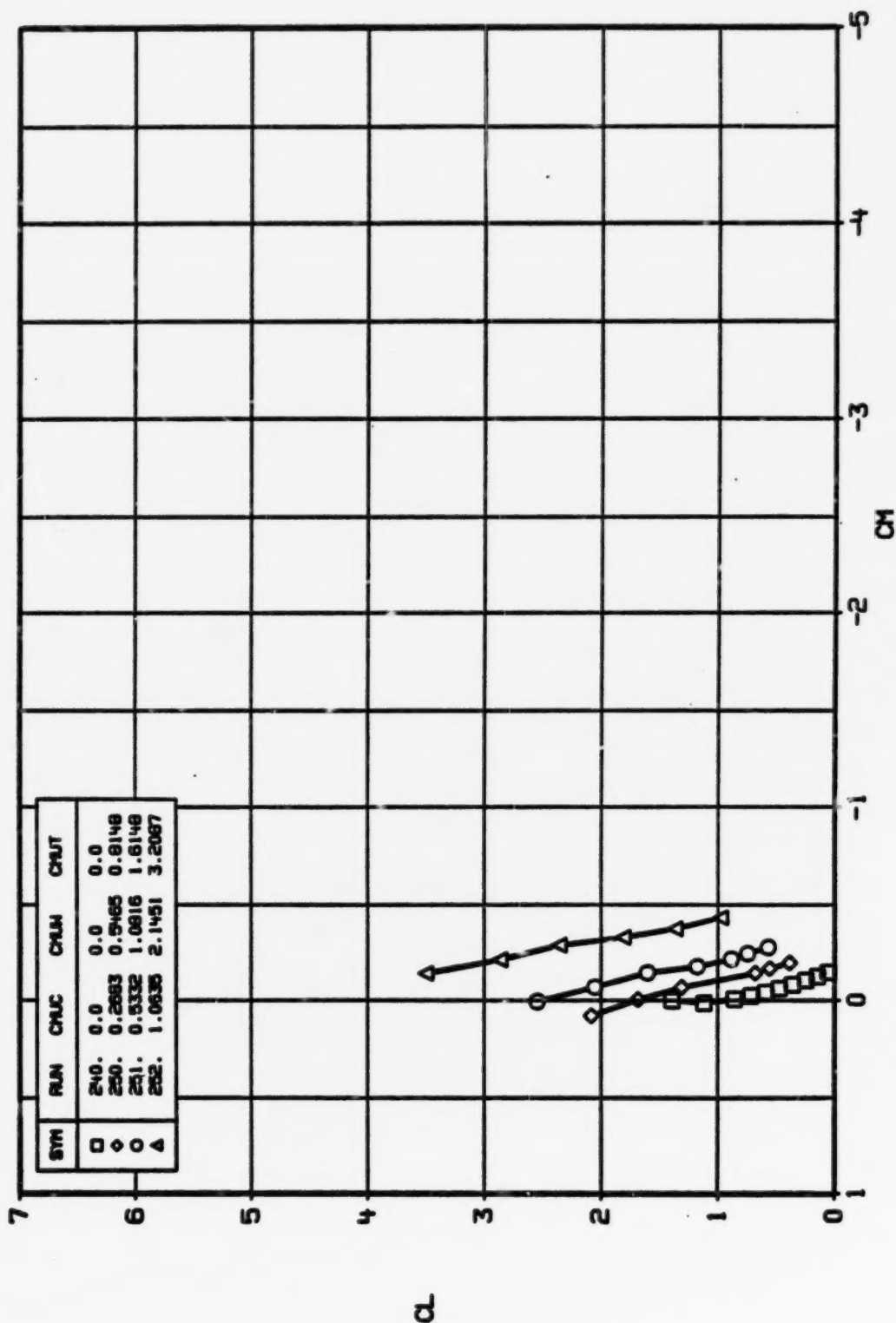


FIGURE A16c BASIC DATA EFFECT OF CHU
CONFIGURATION BC1WSV, (BN/B), C=1, (1BN/B)W=0.5, DELF=0

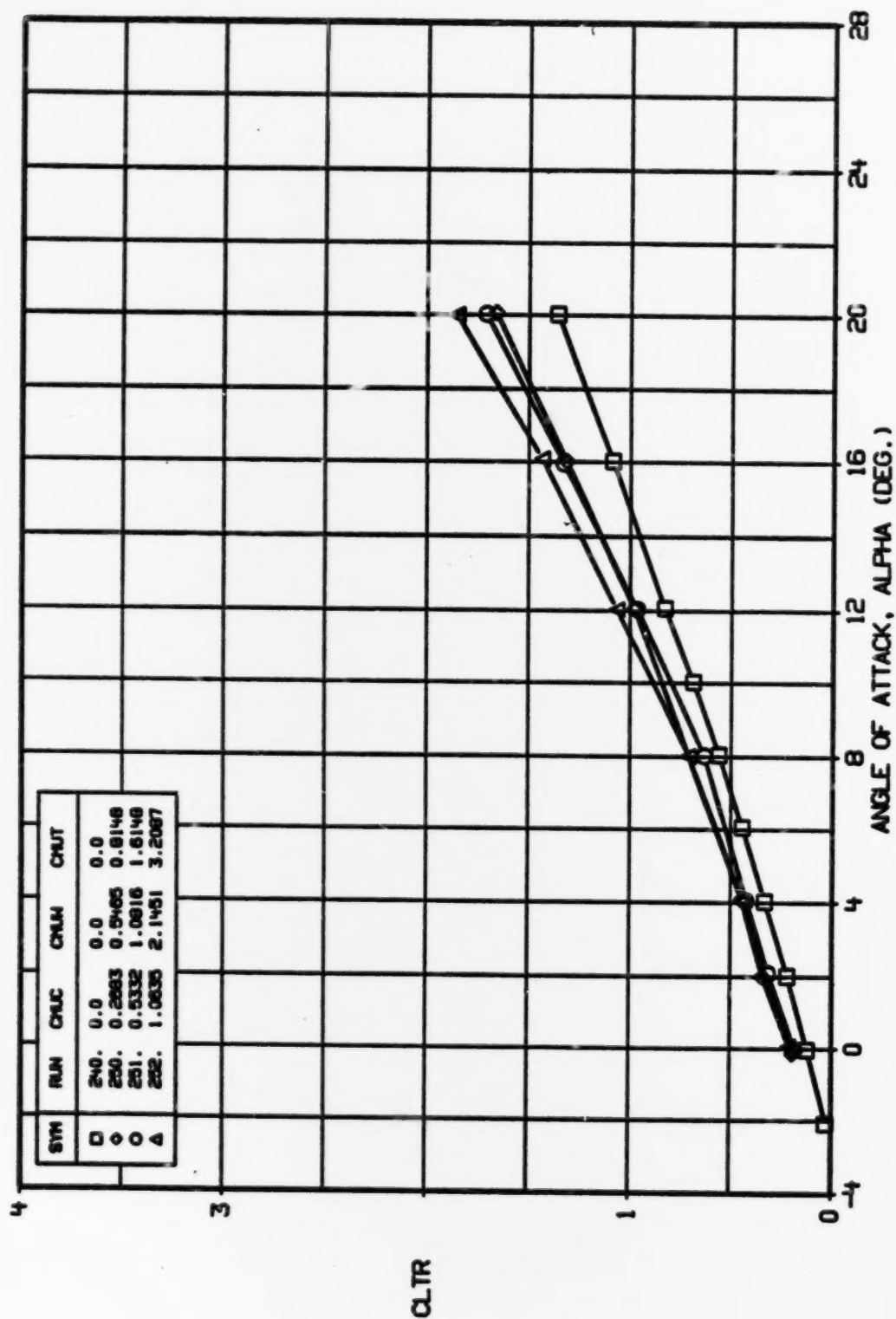


FIGURE A16d BASIC DATA EFFECT OF CHU
CONFIGURATION BC146V, $(18W/B)C=1$, $(8W/B)W=0.5$, $DEL F=0$

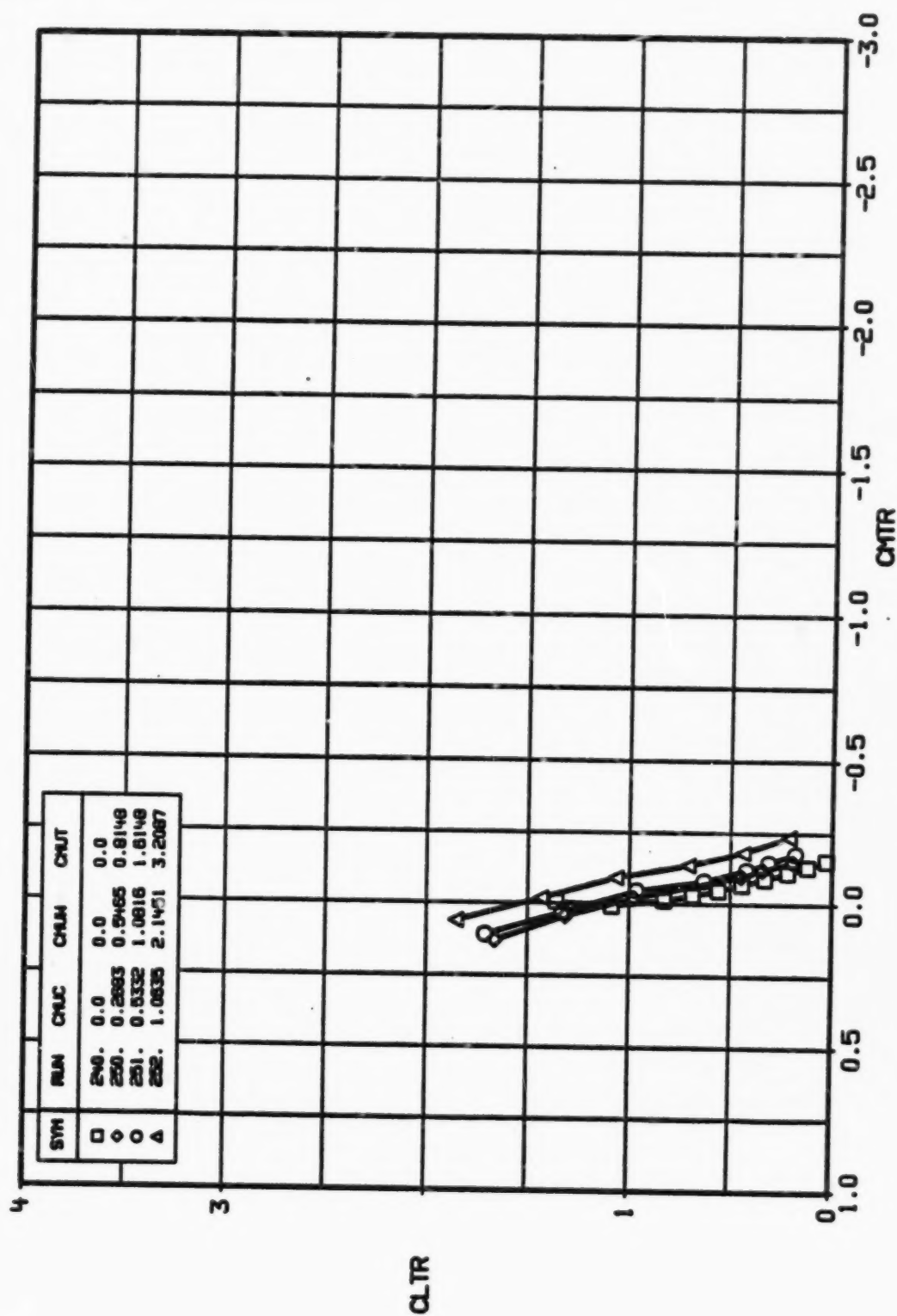


FIGURE A16e BASIC DATA EFFECT OF CMU
CONFIGURATION BC1WSV, (1BN/B)C=1, (8N/B)W=0.5, DELF=0

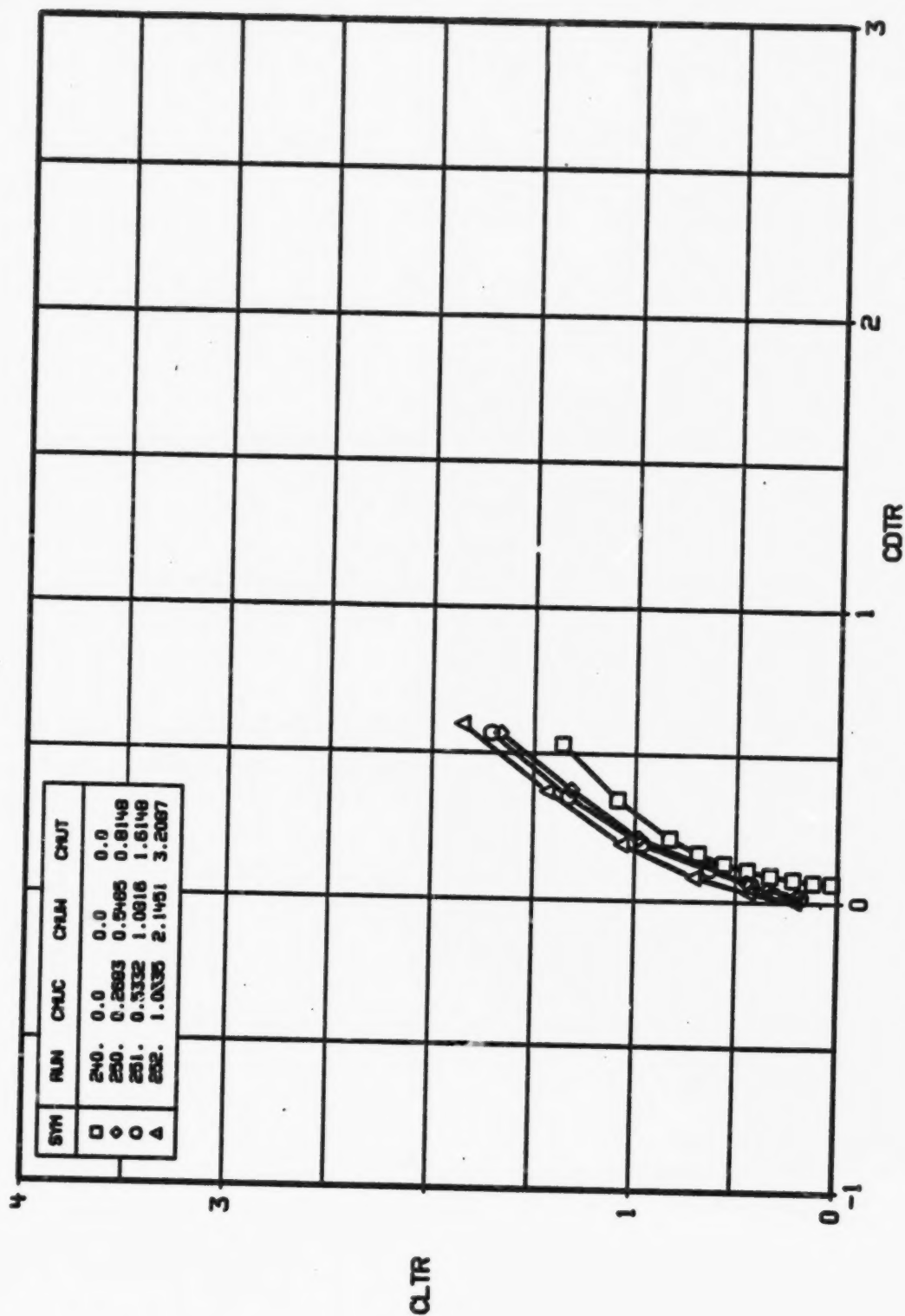


FIGURE A16f BASIC DATA EFFECT OF CHU
CONFIGURATION BC145V, (BM/B)C=1, (BM/B)W=0.5, DELF=0

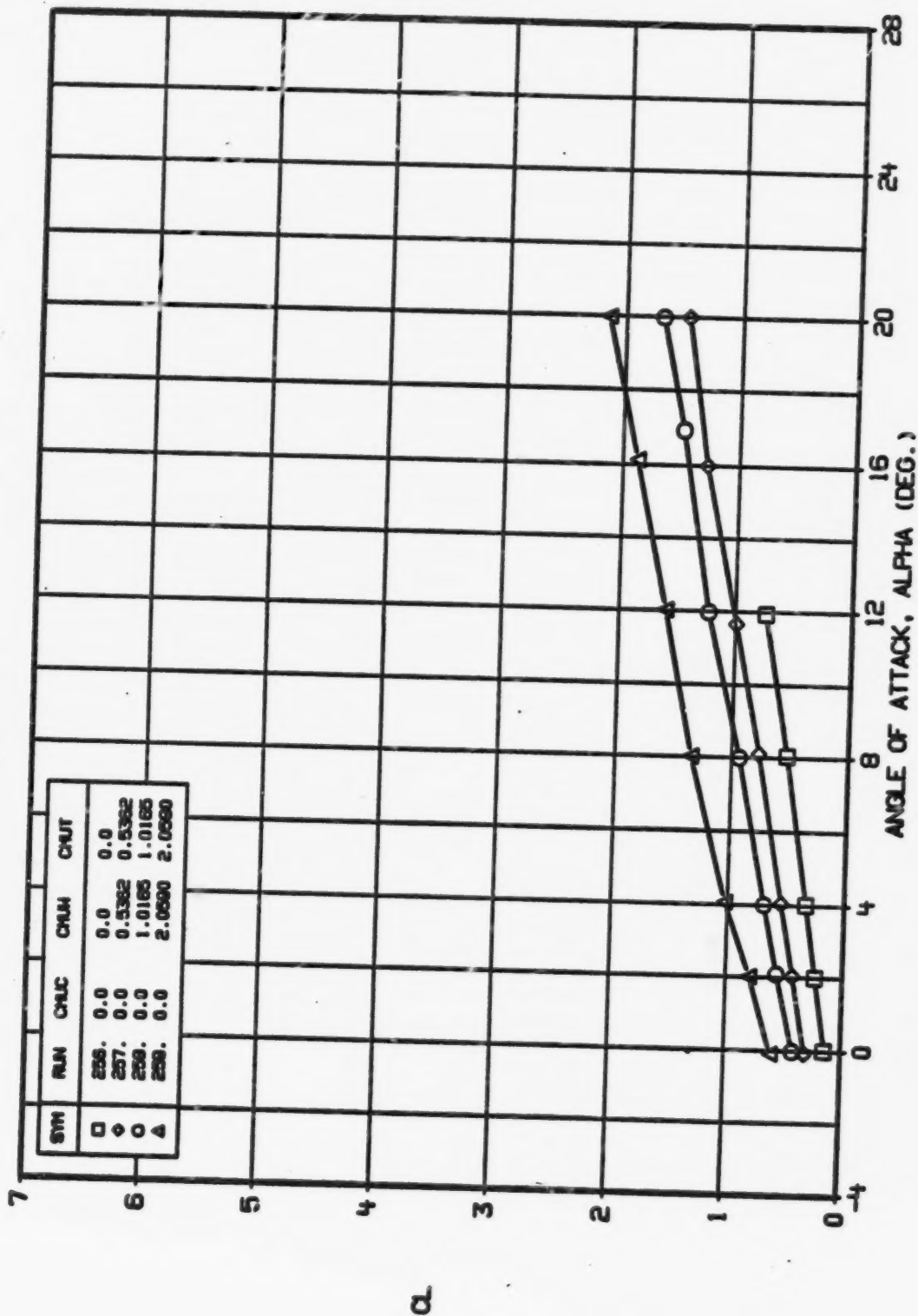


FIGURE A17a BASIC DATA EFFECT OF CMU
CONFIGURATION B45V, $BW/B=0.5$, $DEL F=0$

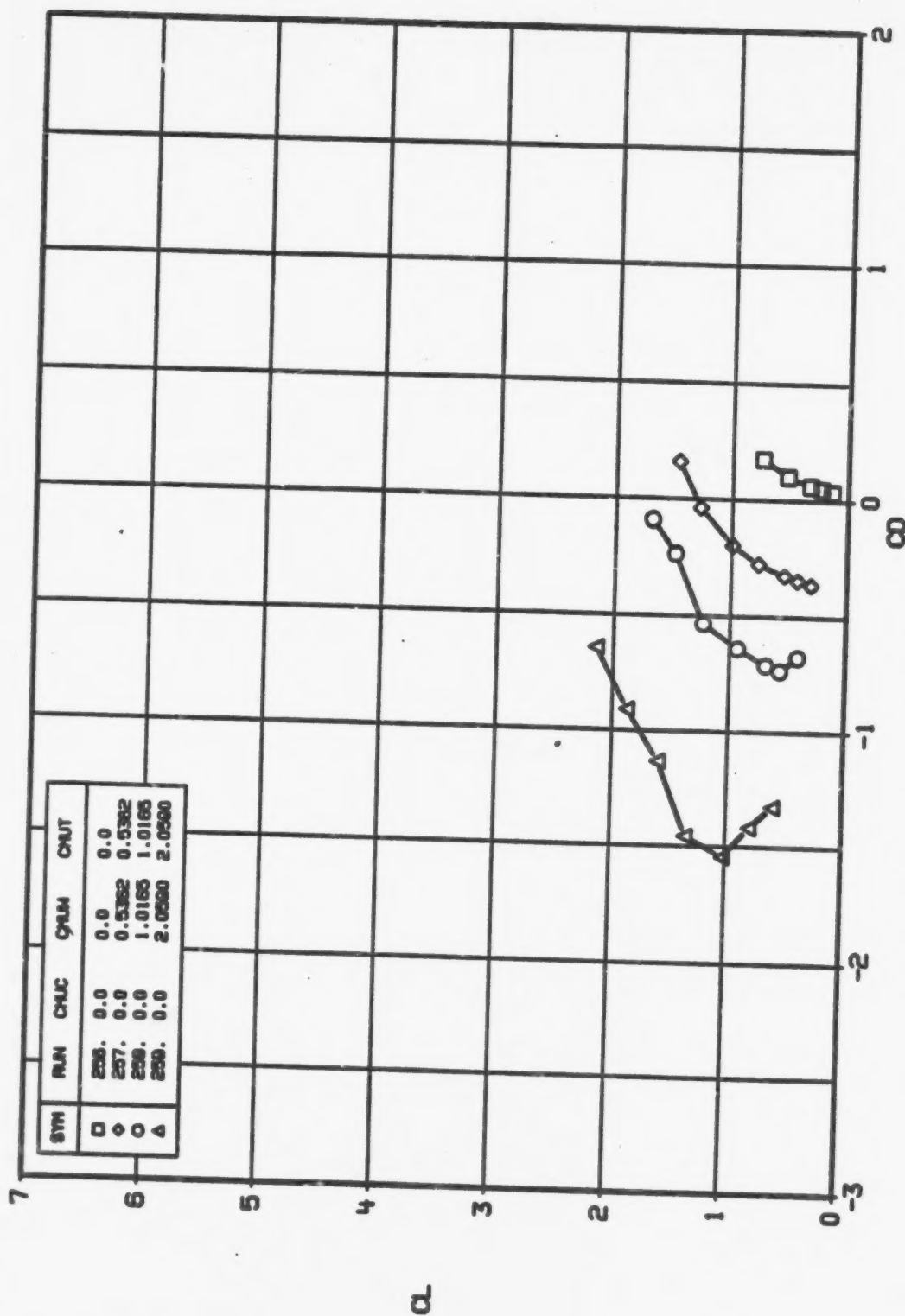


FIGURE A17b BASIC DATA EFFECT OF CMJ
CONFIGURATION B-5V, $BN/B=0.5$, $DEL F=0$

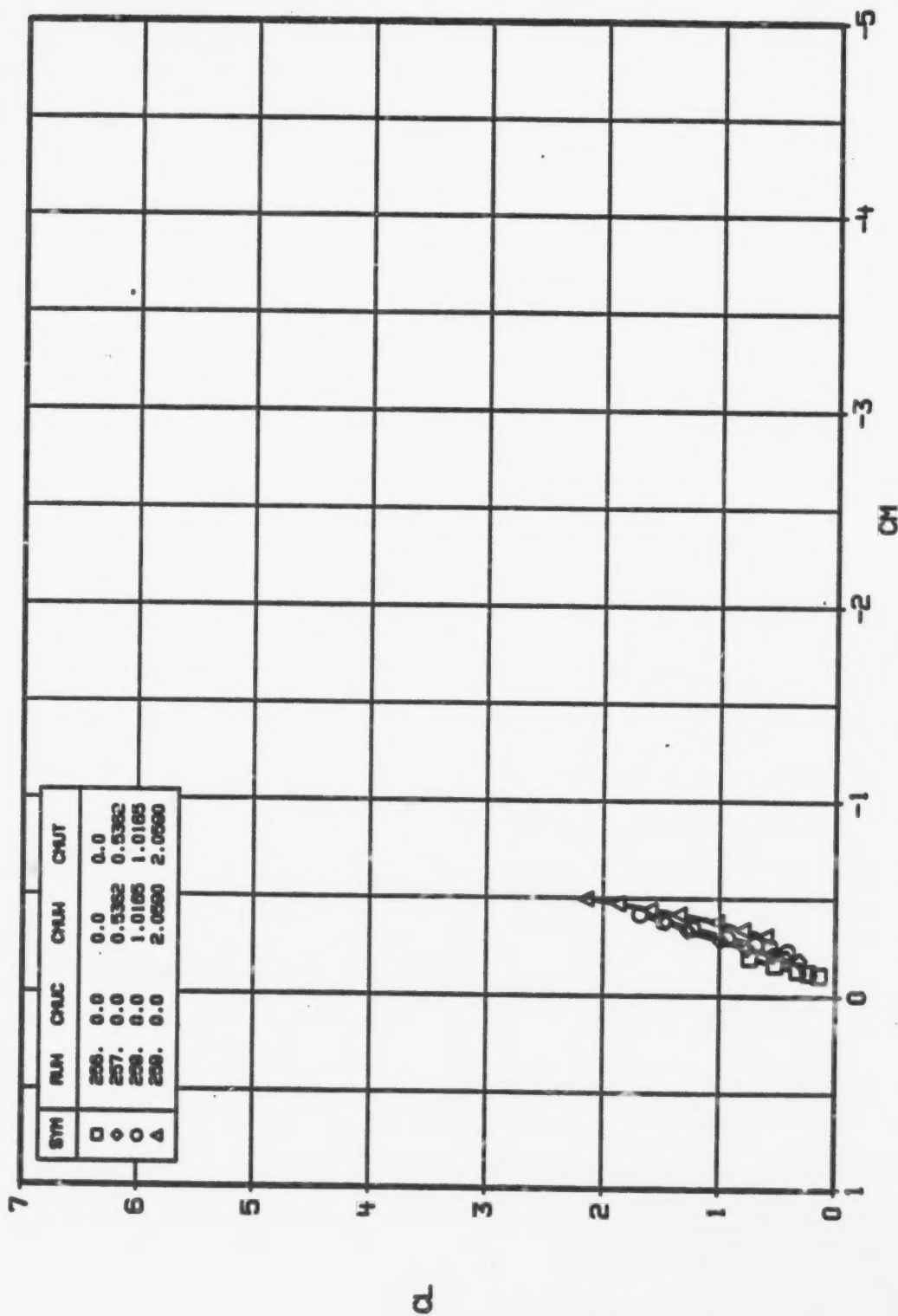


FIGURE A17c BASIC DATA EFFECT OF CMJ
CONFIGURATION BMSV, $\theta M/B=0.5$, $\Delta E/F=0$

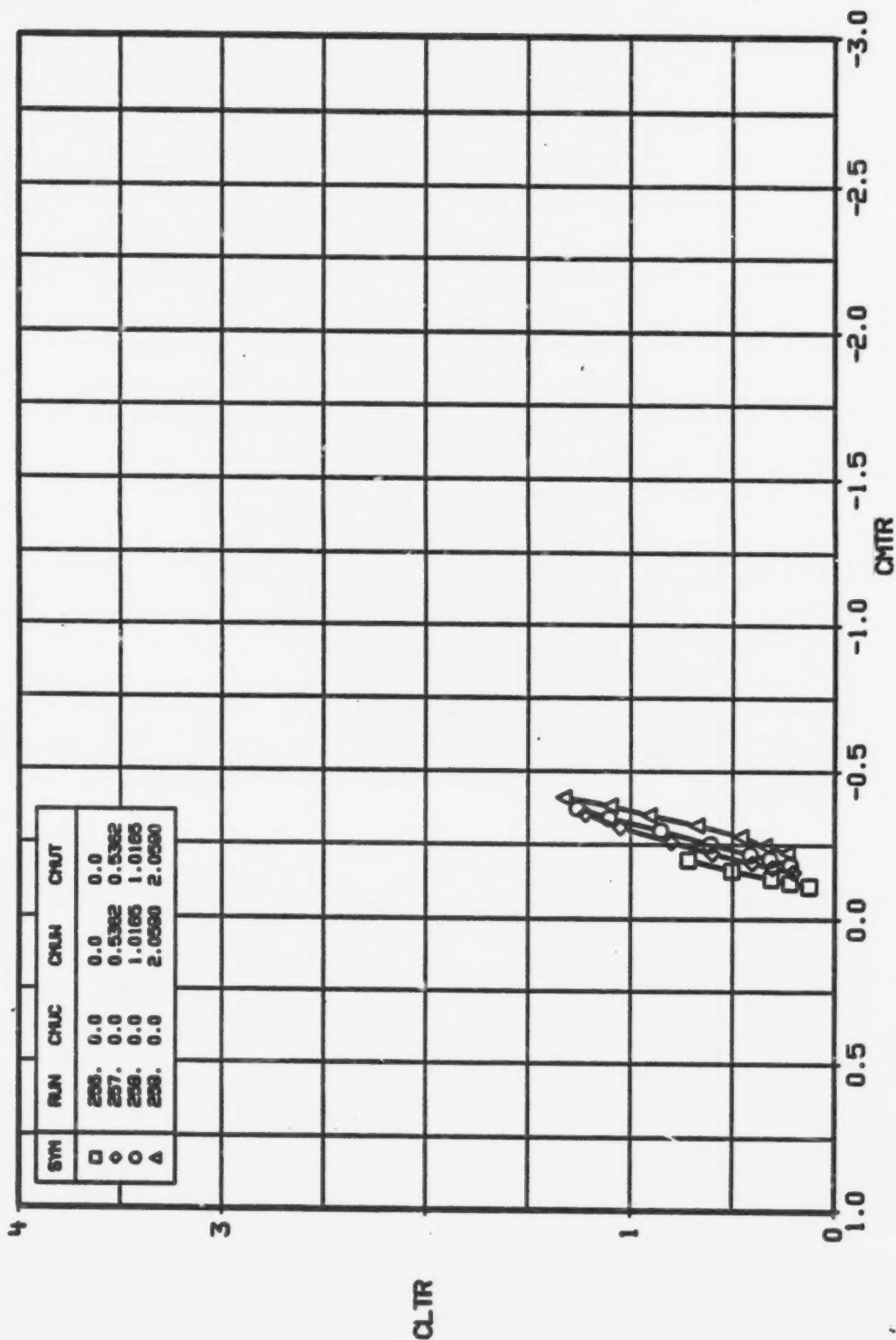


FIGURE A17d BASIC DATA EFFECT OF CMU
CONFIGURATION BM/B=0.5, DELF=0

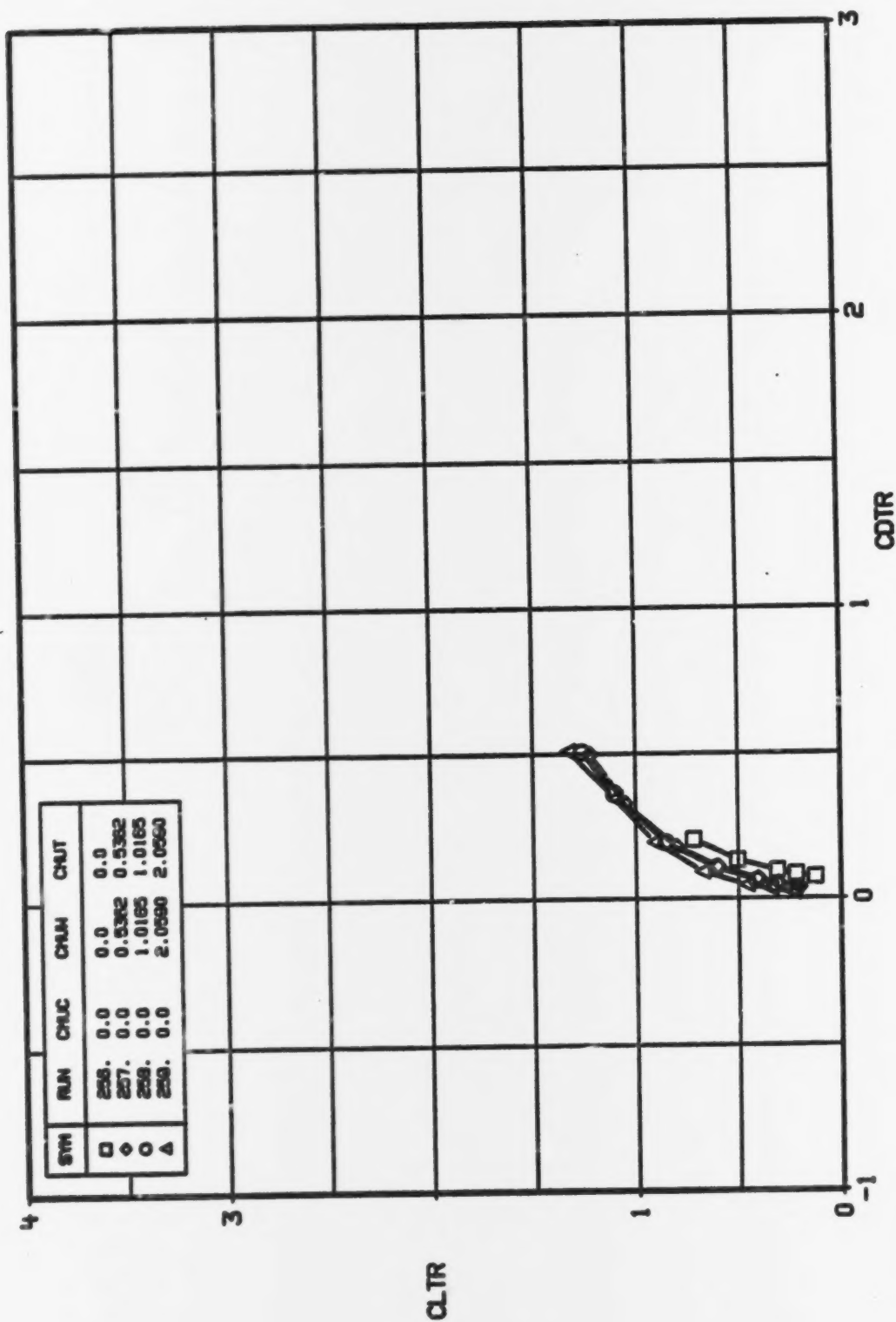


FIGURE A17e BASIC DATA EFFECT OF CHU
CONFIGURATION B46V, $BW/B=0.5$, $DEL F=0$

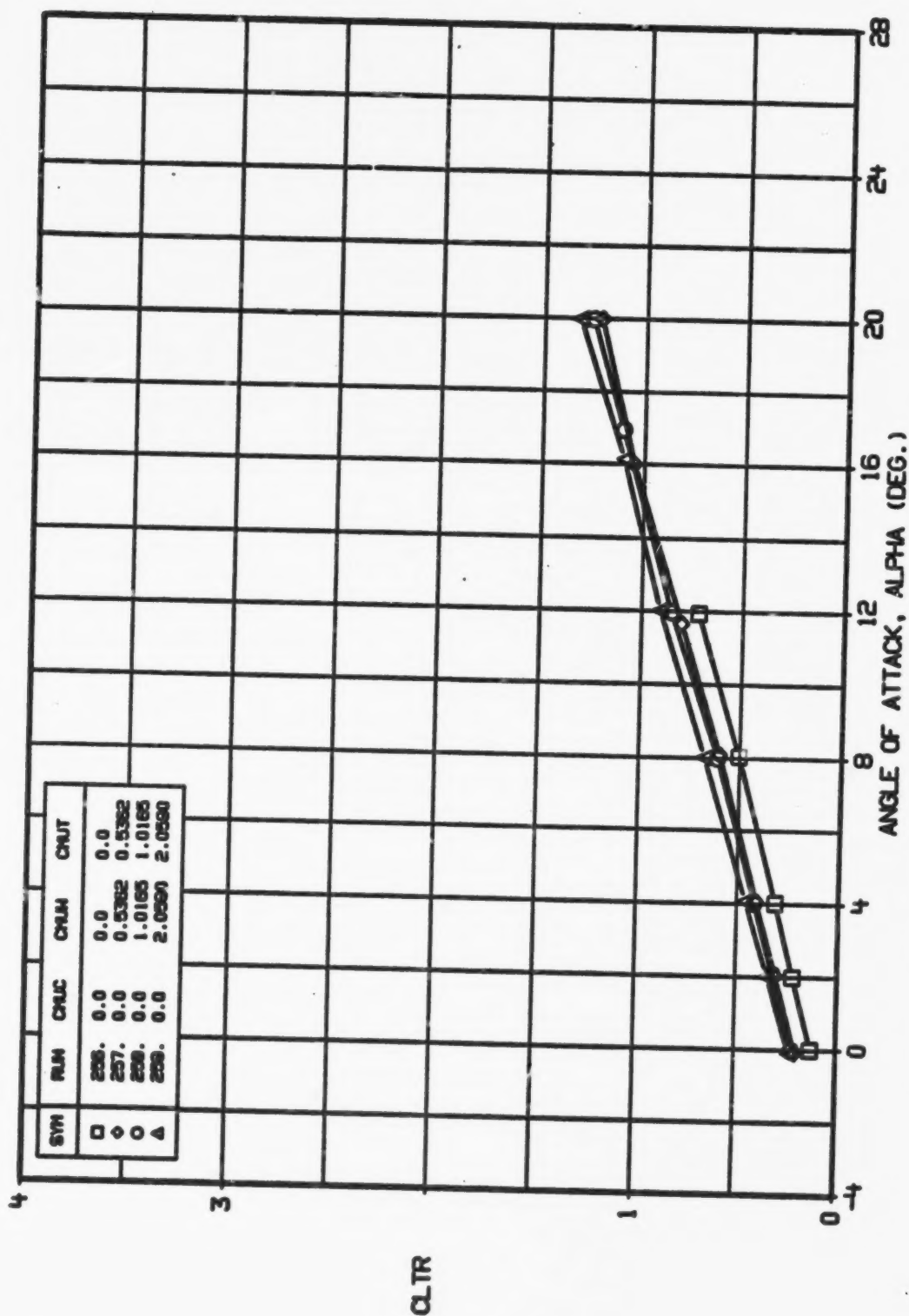


FIGURE A17f BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, $\eta_{in}/\eta = 0.5$, $\delta_{ELF} = 0$

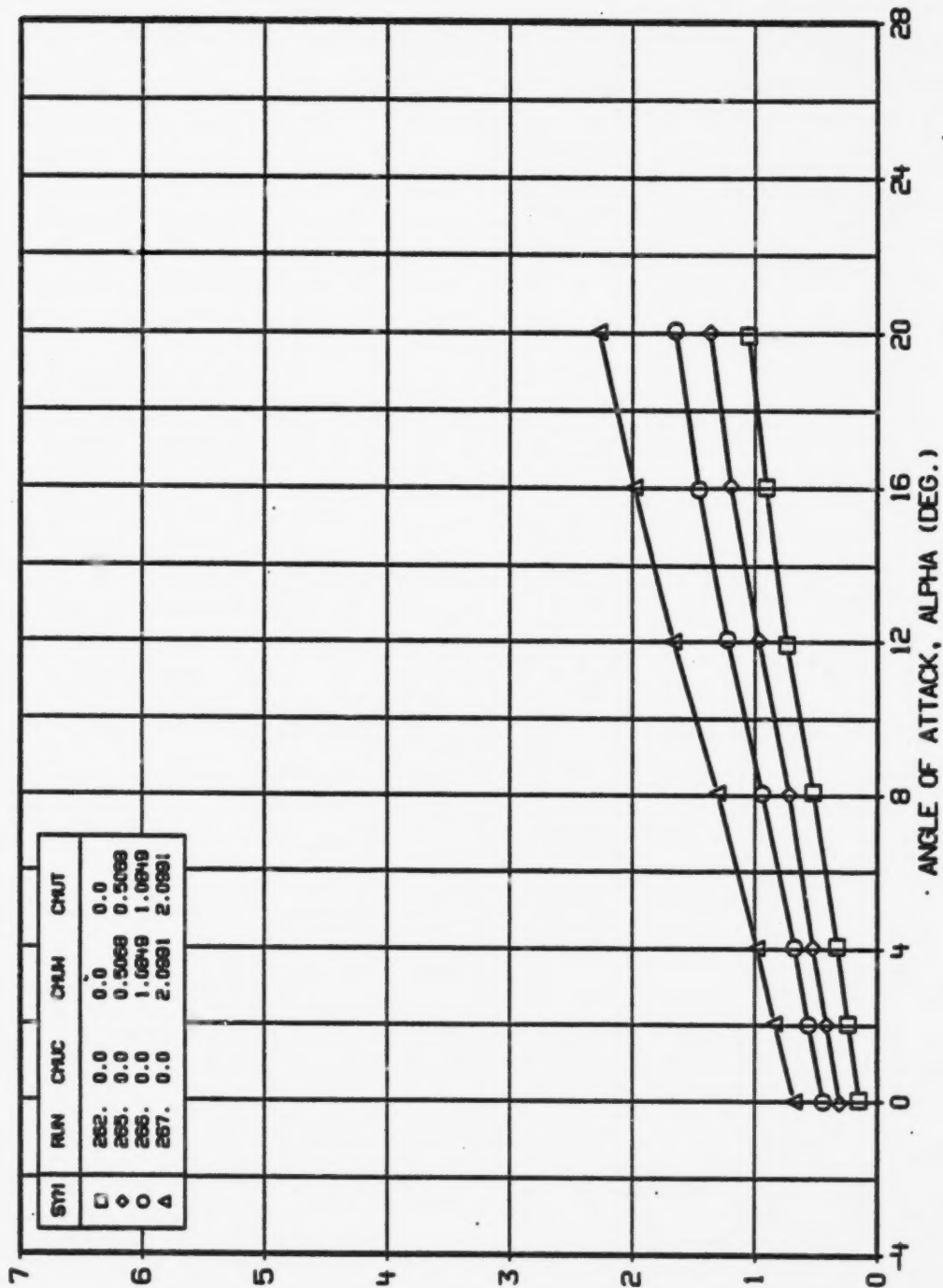


FIGURE A18a BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, BN/B=0.25, DELF=0

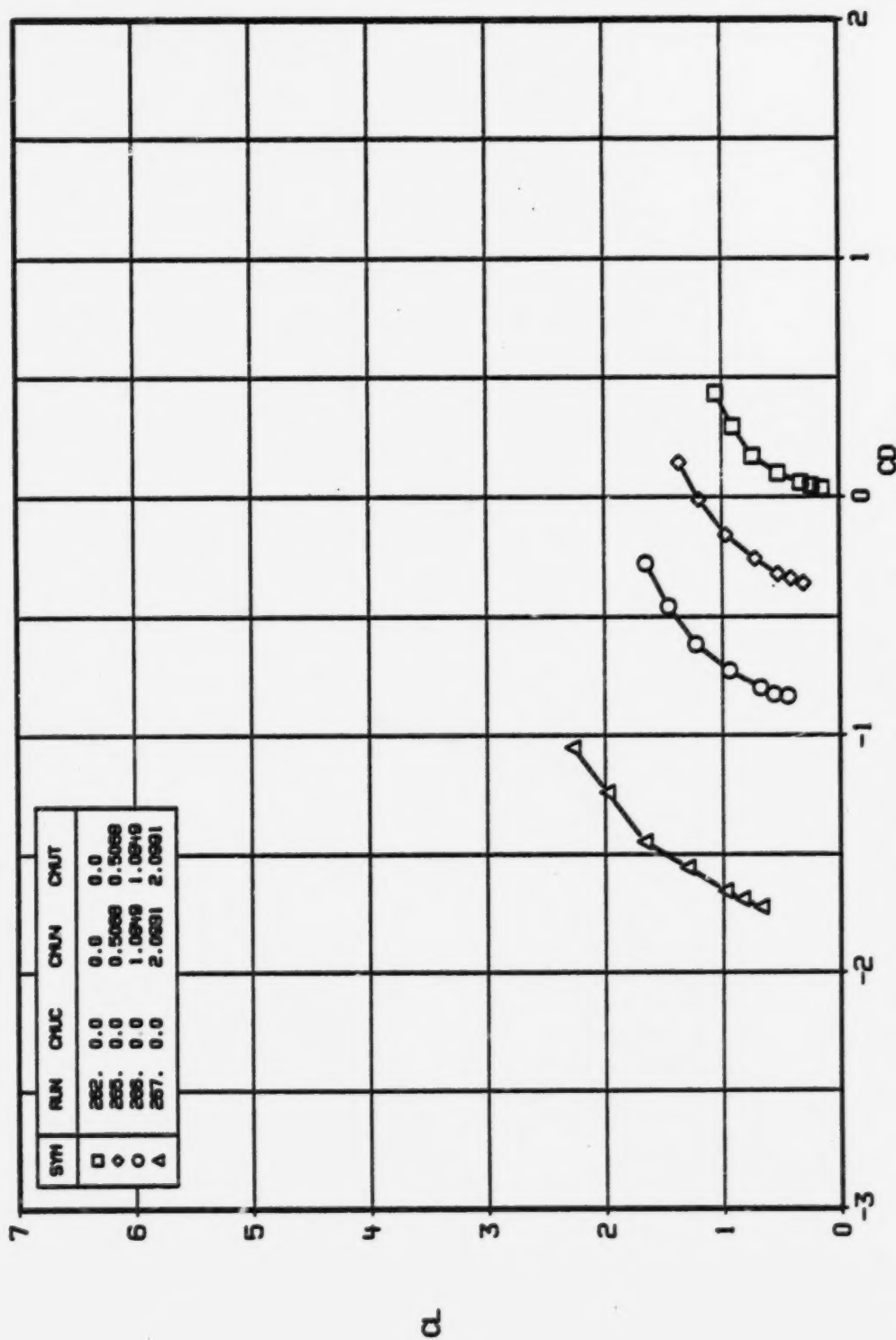


FIGURE A18b BASIC DATA EFFECT OF CHU
CONFIGURATION B46V, BN/B=0.25, DELF=0

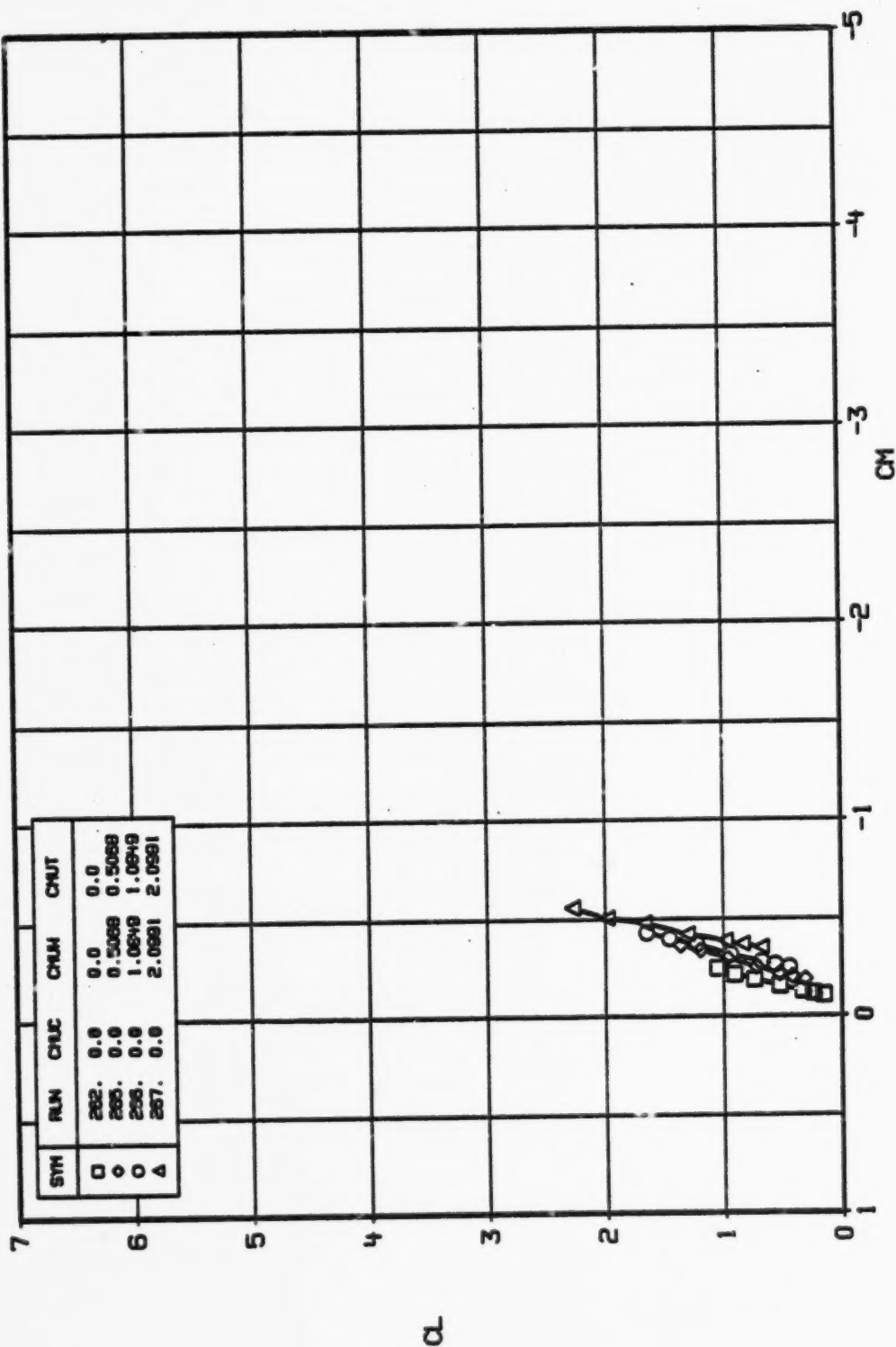


FIGURE A18c BASIC DATA EFFECT OF CMU
CONFIGURATION B45V, BN/B=0.25, DELF=0

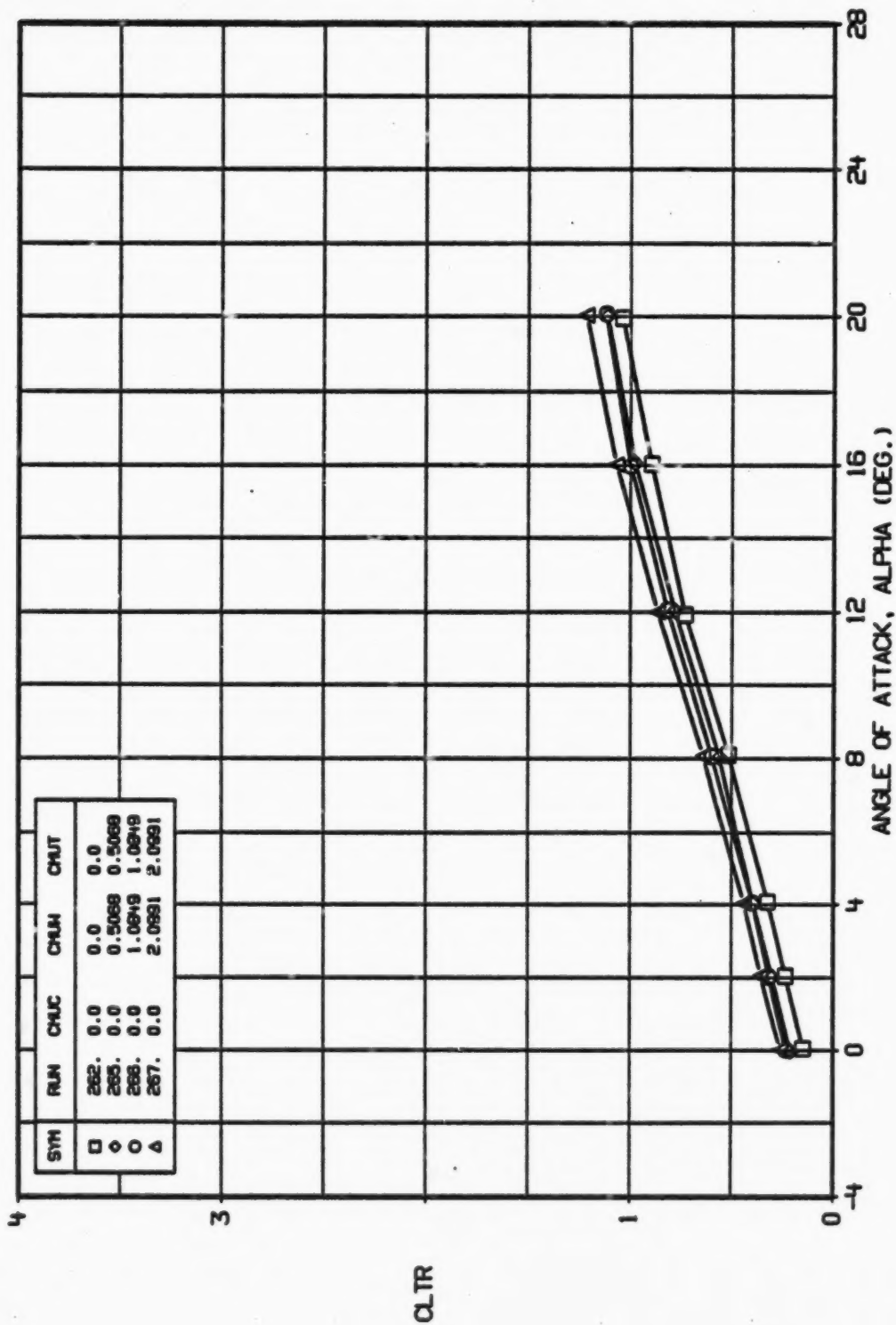


FIGURE A18d BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, BN/B=0.25, DELF=0

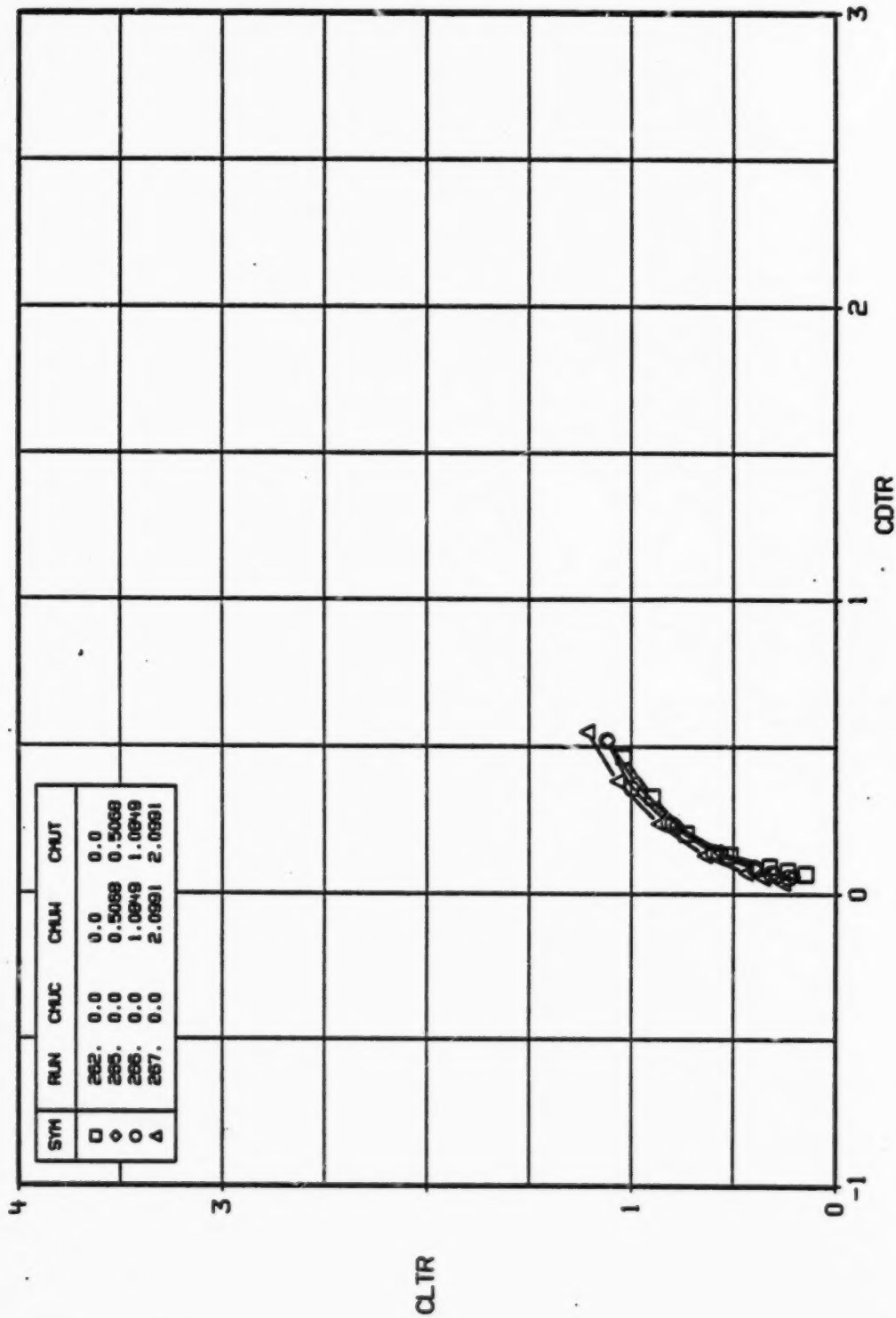


FIGURE A18e BASIC DATA EFFECT OF CHU
CONFIGURATION B45V, BN/B=0.25, DELF=0

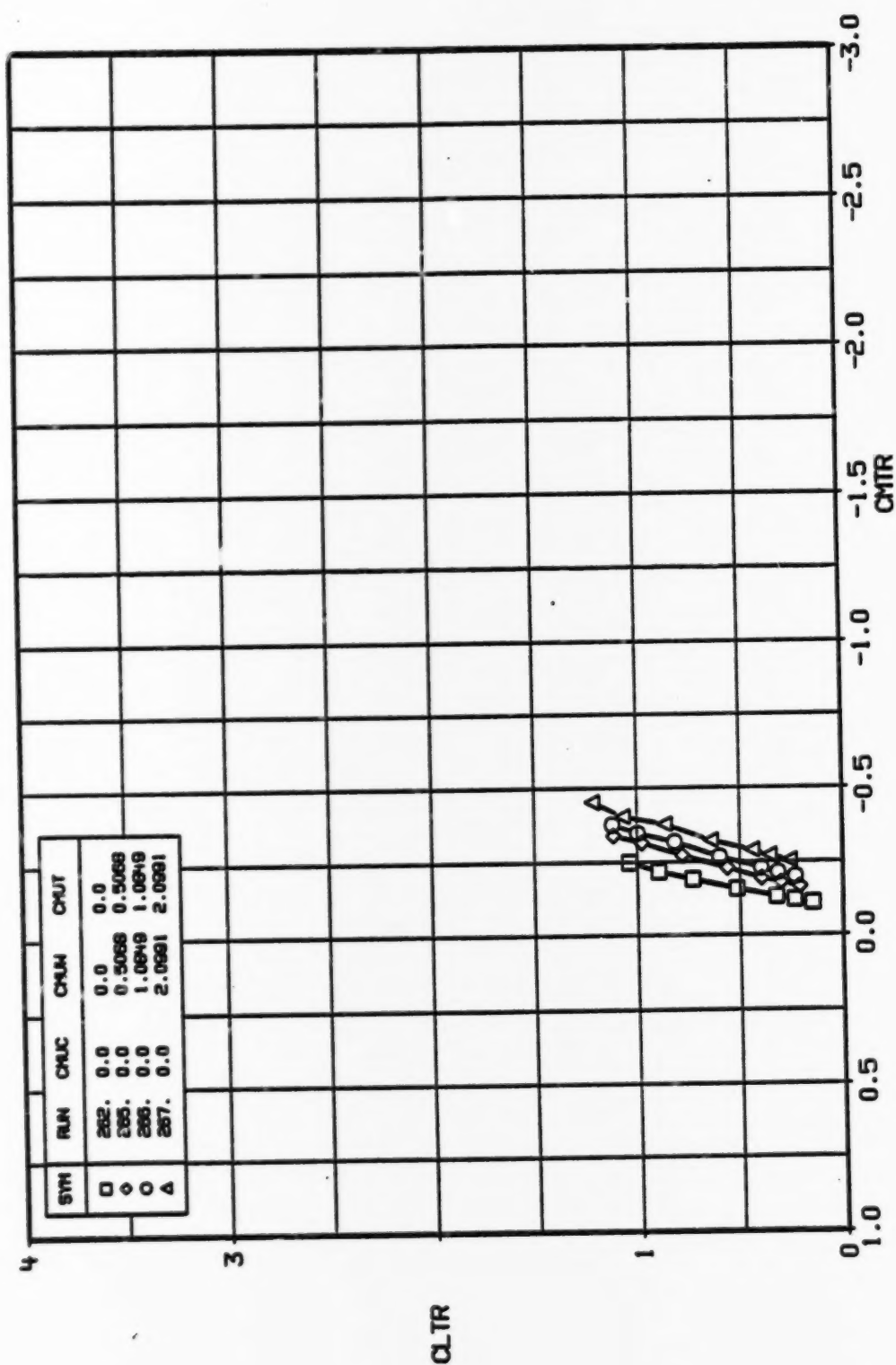


FIGURE A18f BASIC DATA EFFECT OF CMU
CONFIGURATION BMSV, BN/B=0.25, DELF=0

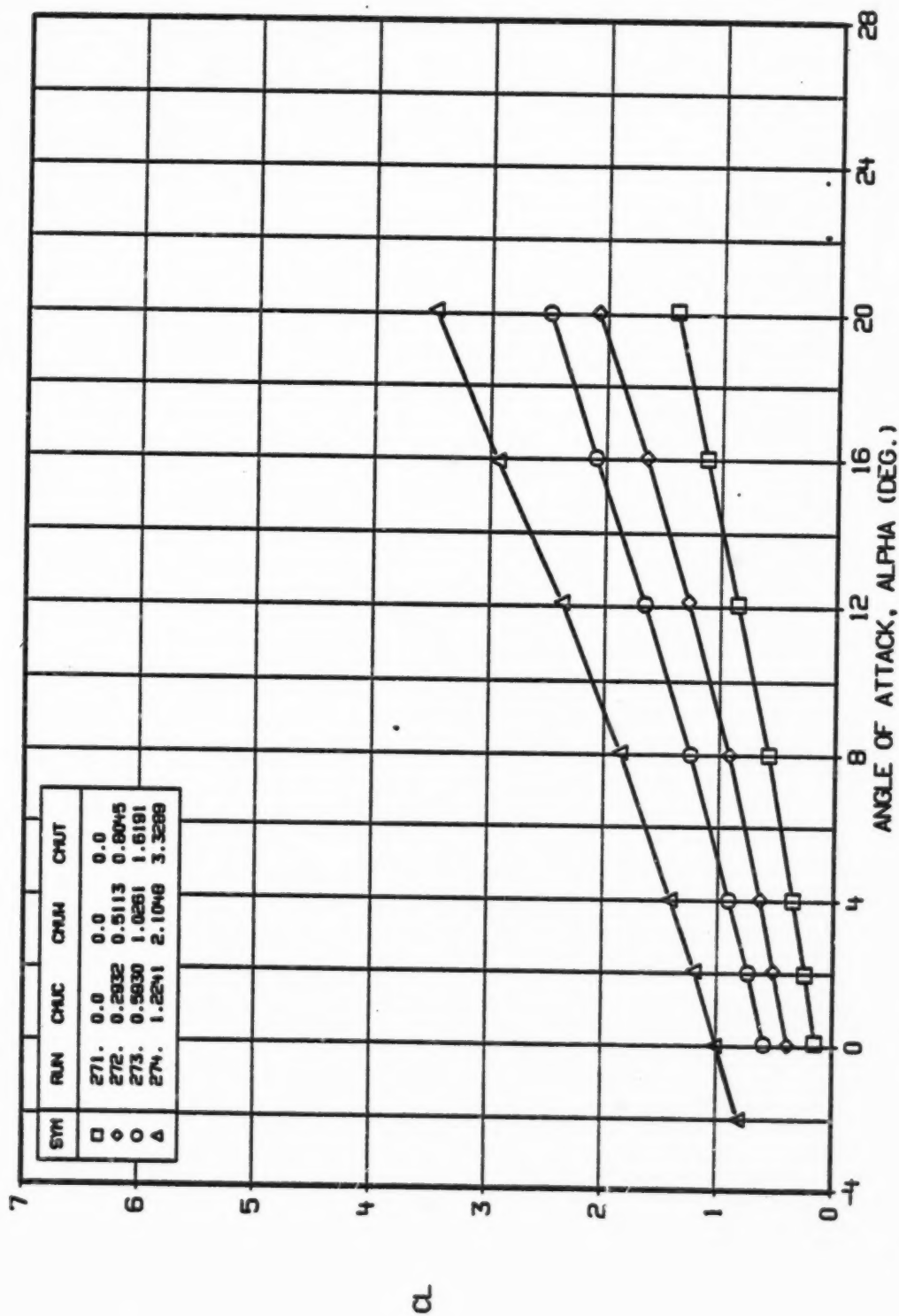


FIGURE A19a BASIC DATA EFFECT OF CHU
CONFIGURATION BC146V, (BN/B)C=1, (BN/B)W=0.25. DELF=0

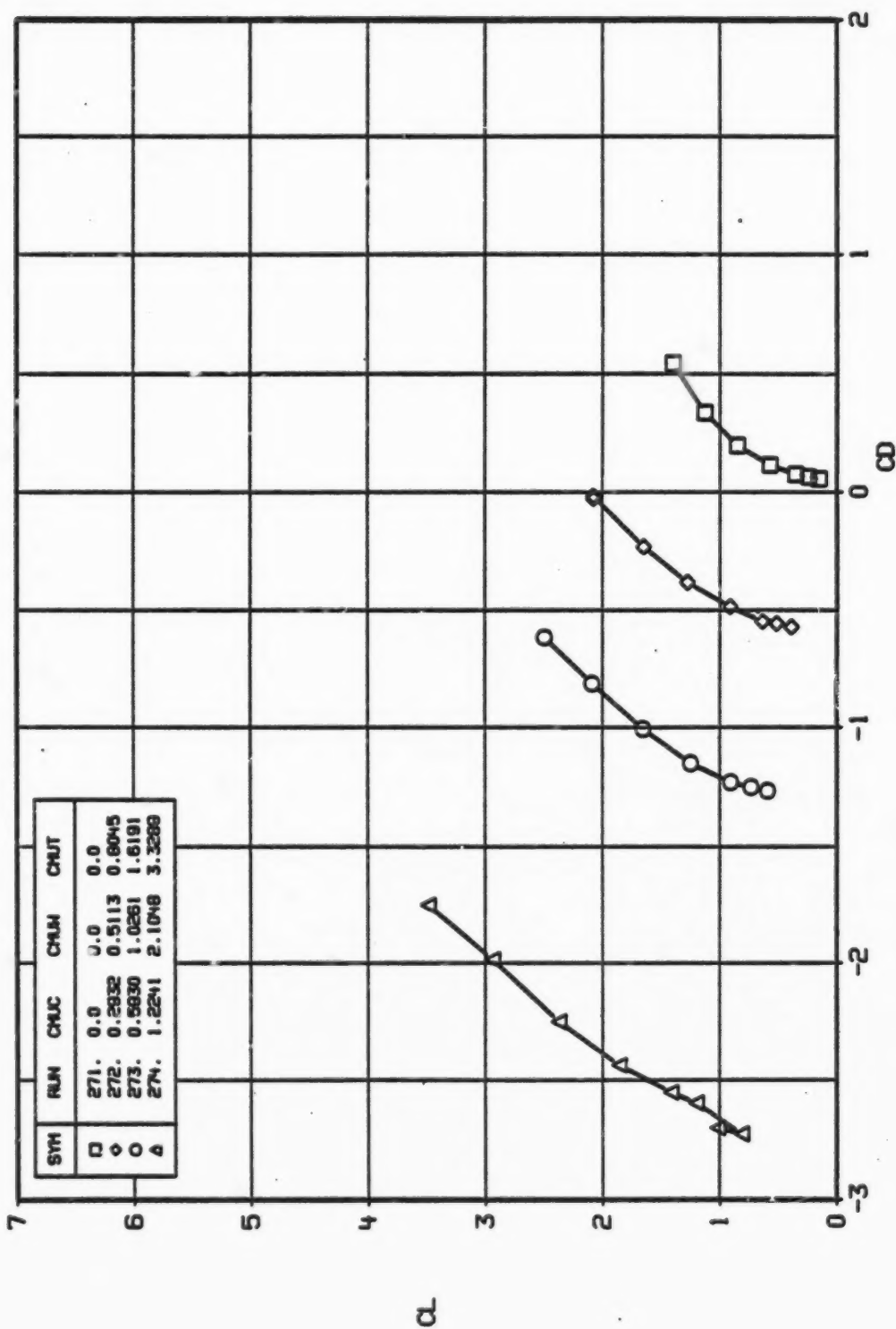


FIGURE A19b BASIC DATA EFFECT OF CMU
CONFIGURATION BC146V, (BN/B)C=1, (BN/B)W=0.25, DELF=0

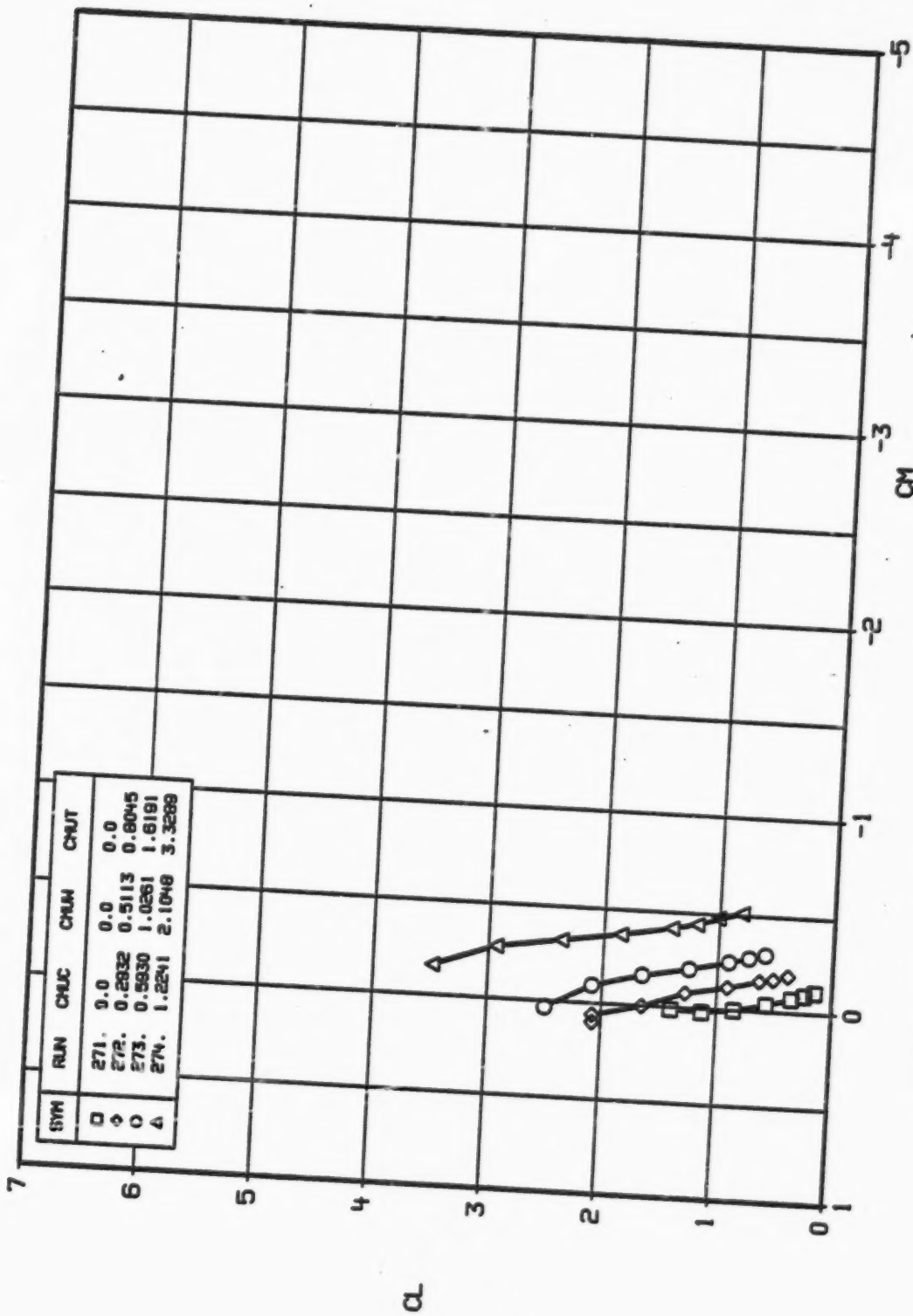


FIGURE A19c BASIC DATA EFFECT OF CMU
CONFIGURATION BC1W6V, (BN/B)C=1, (BN/B)W=0.25, DELF=0

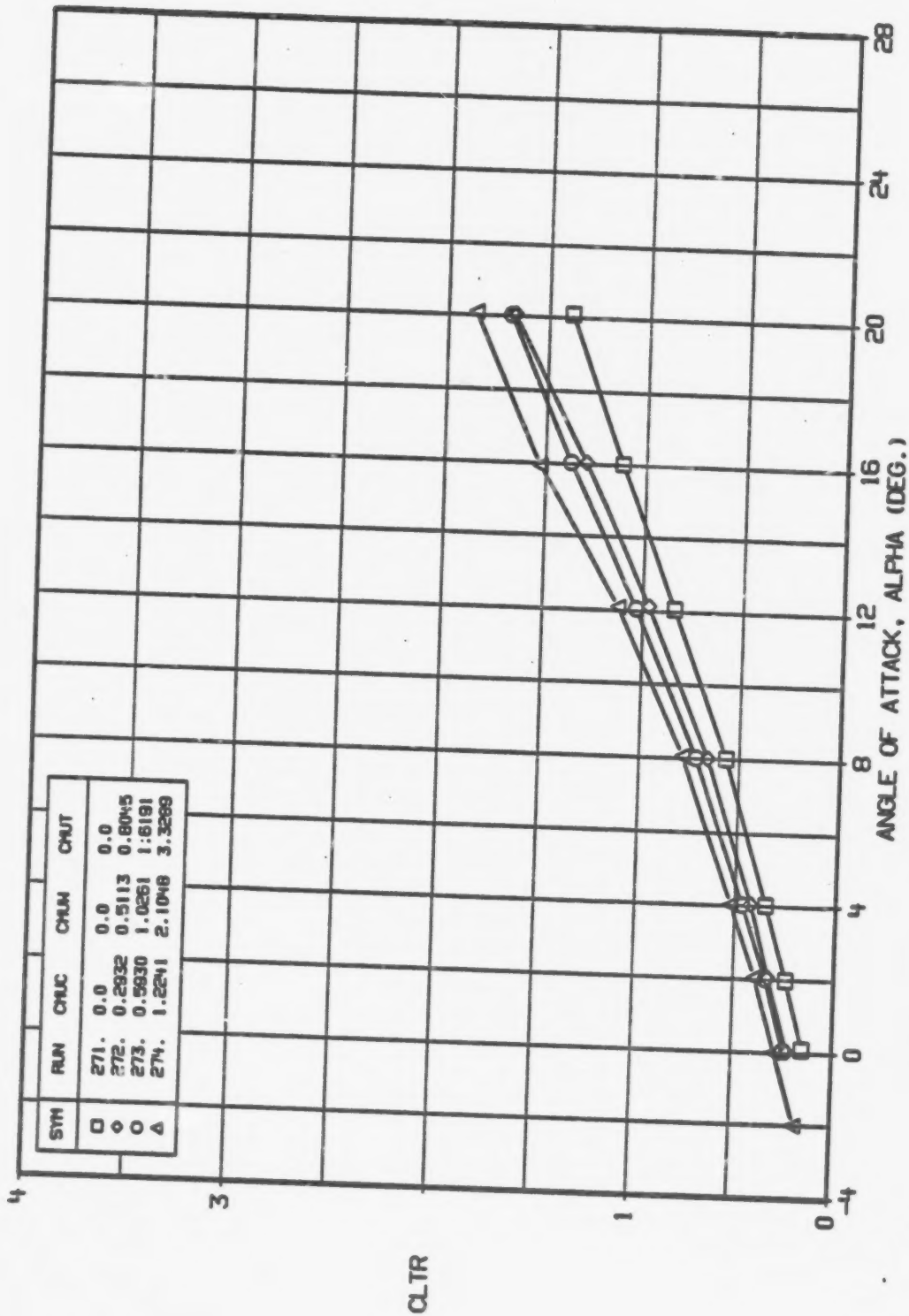


FIGURE A19d BASIC DATA EFFECT OF CMU
CONFIGURATION BC1W5V, (BN/B)C=1, (BN/B)W=0.25, DELF=0

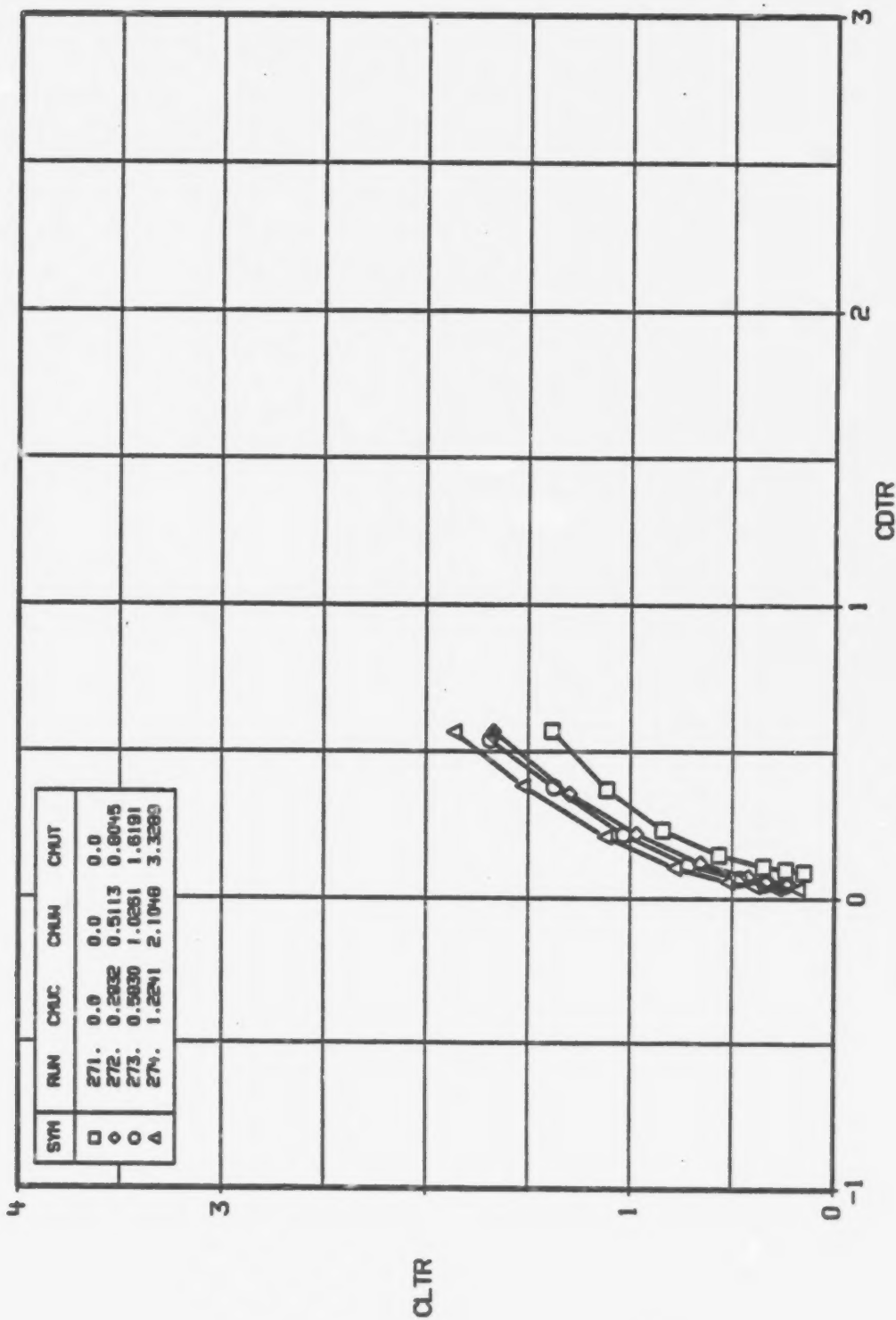


FIGURE A19e BASIC DATA EFFECT OF CMU
CONFIGURATION BC1M5V, (BN/B)C=1, (BN/B)W=0.25, DELF=0

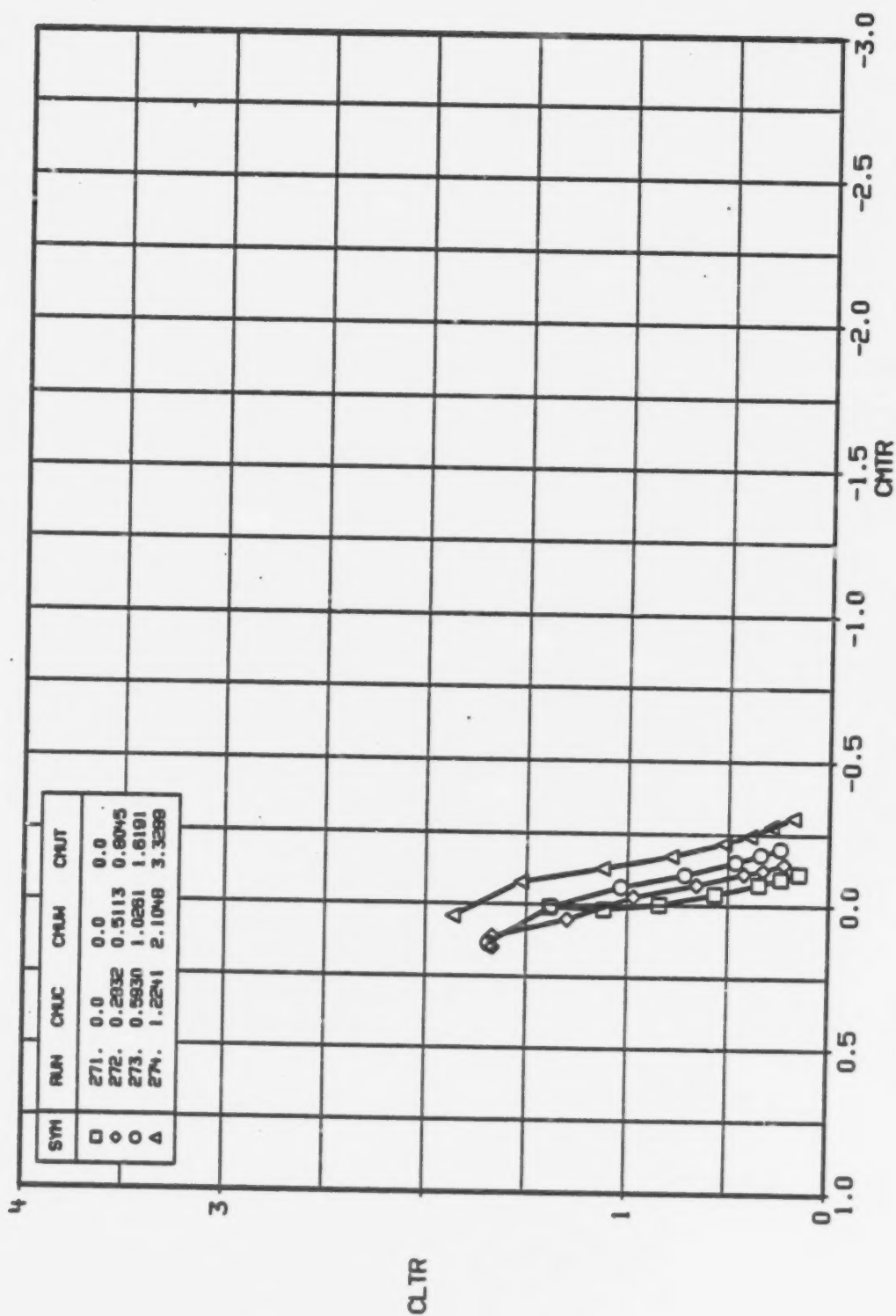


FIGURE A19f BASIC DATA EFFECT OF CMU
CONFIGURATION BC1WSV, (BN/B)C=1, (BN/B)W=0.25, DELF=0

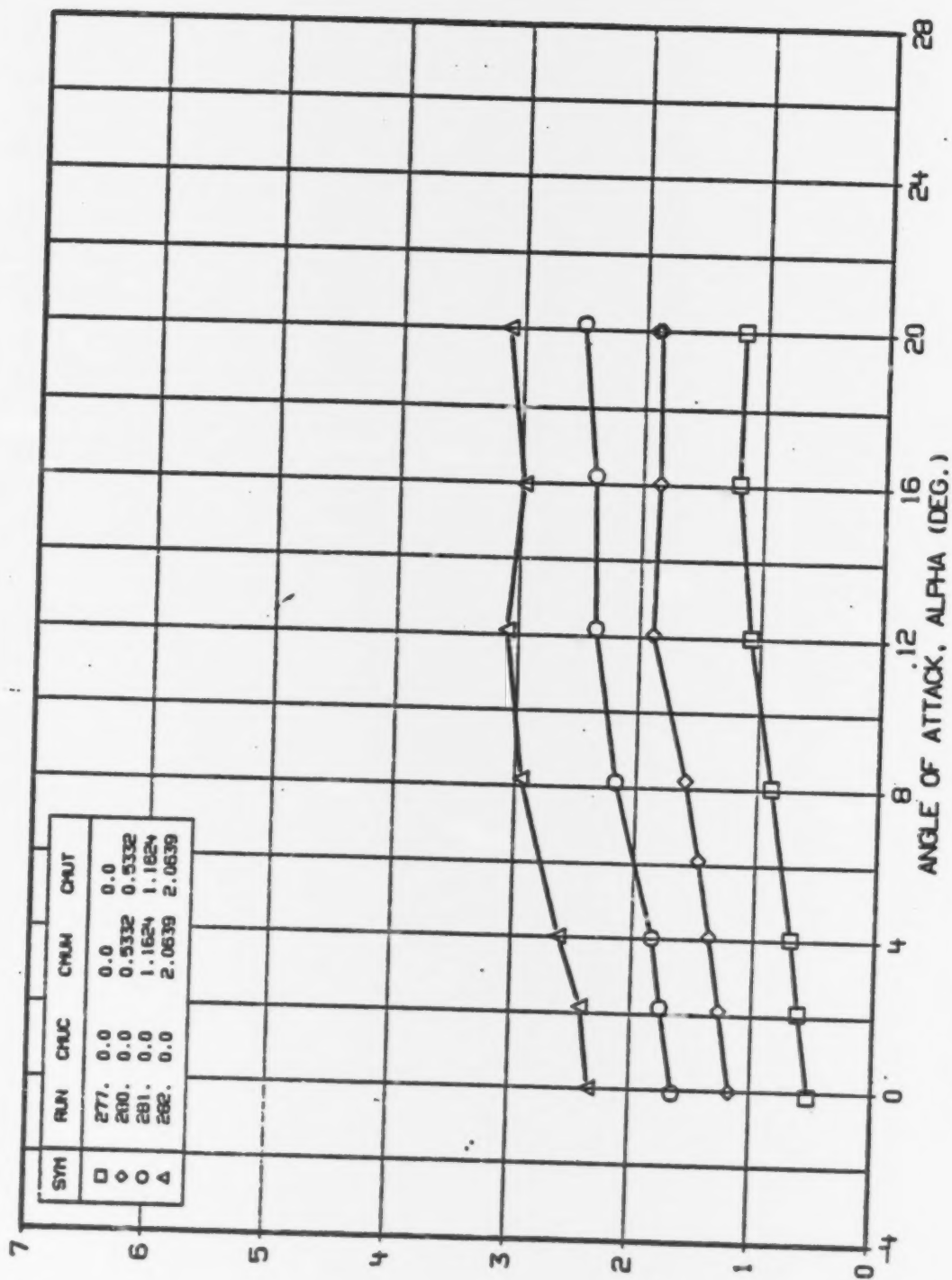


FIGURE A20a BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, DELF=45, BN/B=.25

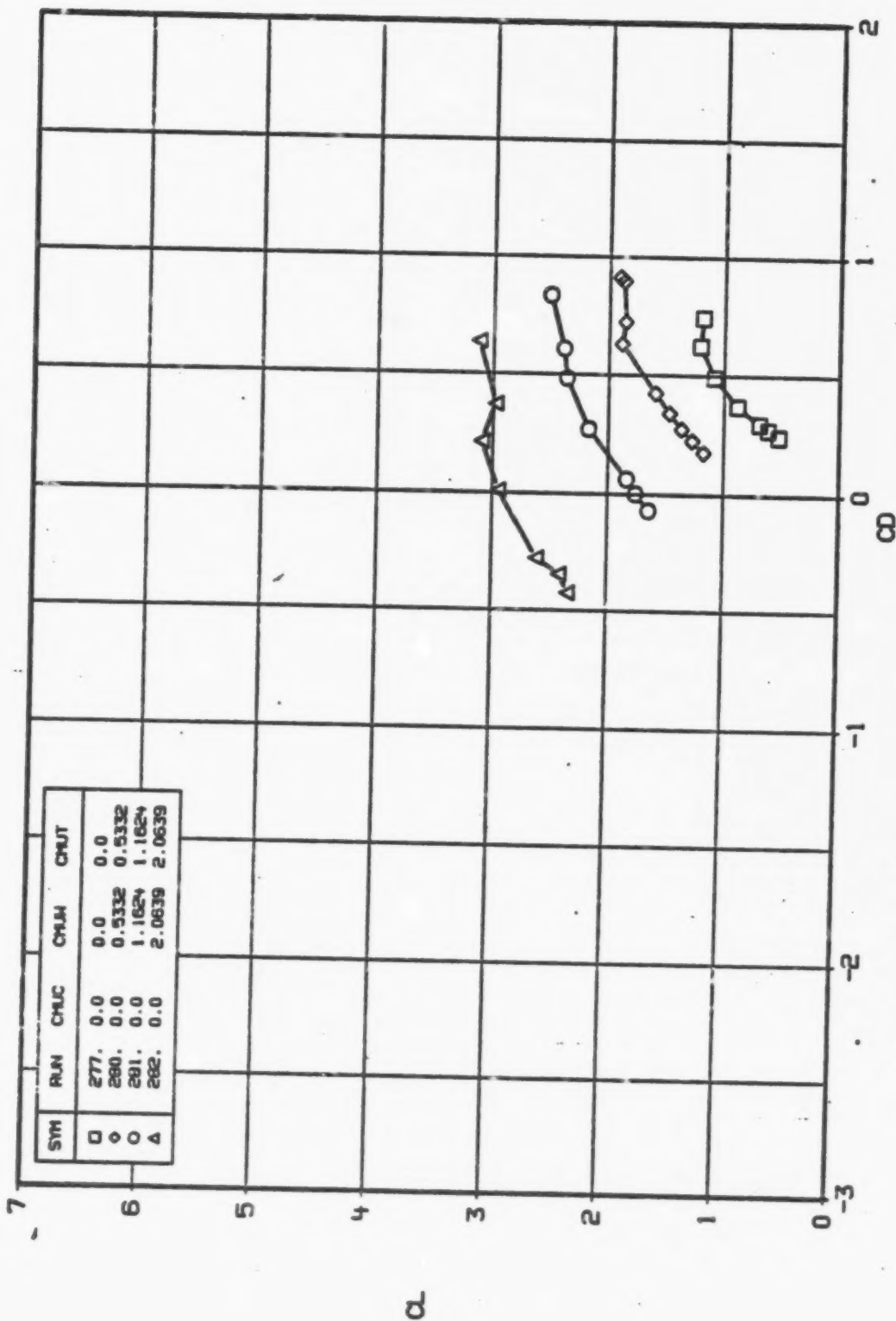


FIGURE A20b BASIC DATA EFFECT OF CMU
CONFIGURATION B45V, DELF=45, BN/B=.25

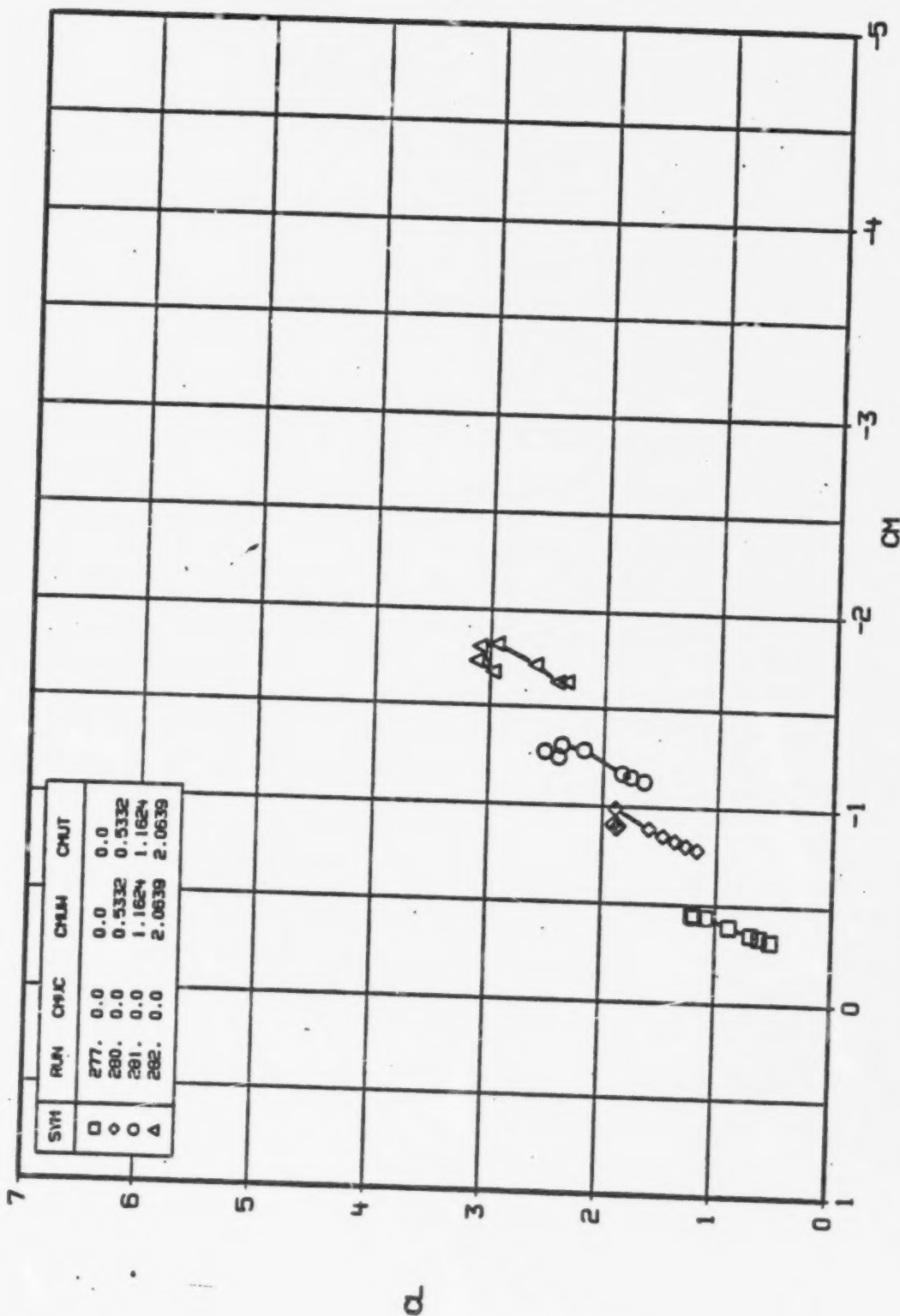


FIGURE A20c BASIC DATA EFFECT OF CHU
CONFIGURATION BN6V, DELF=45, BN/B=.25

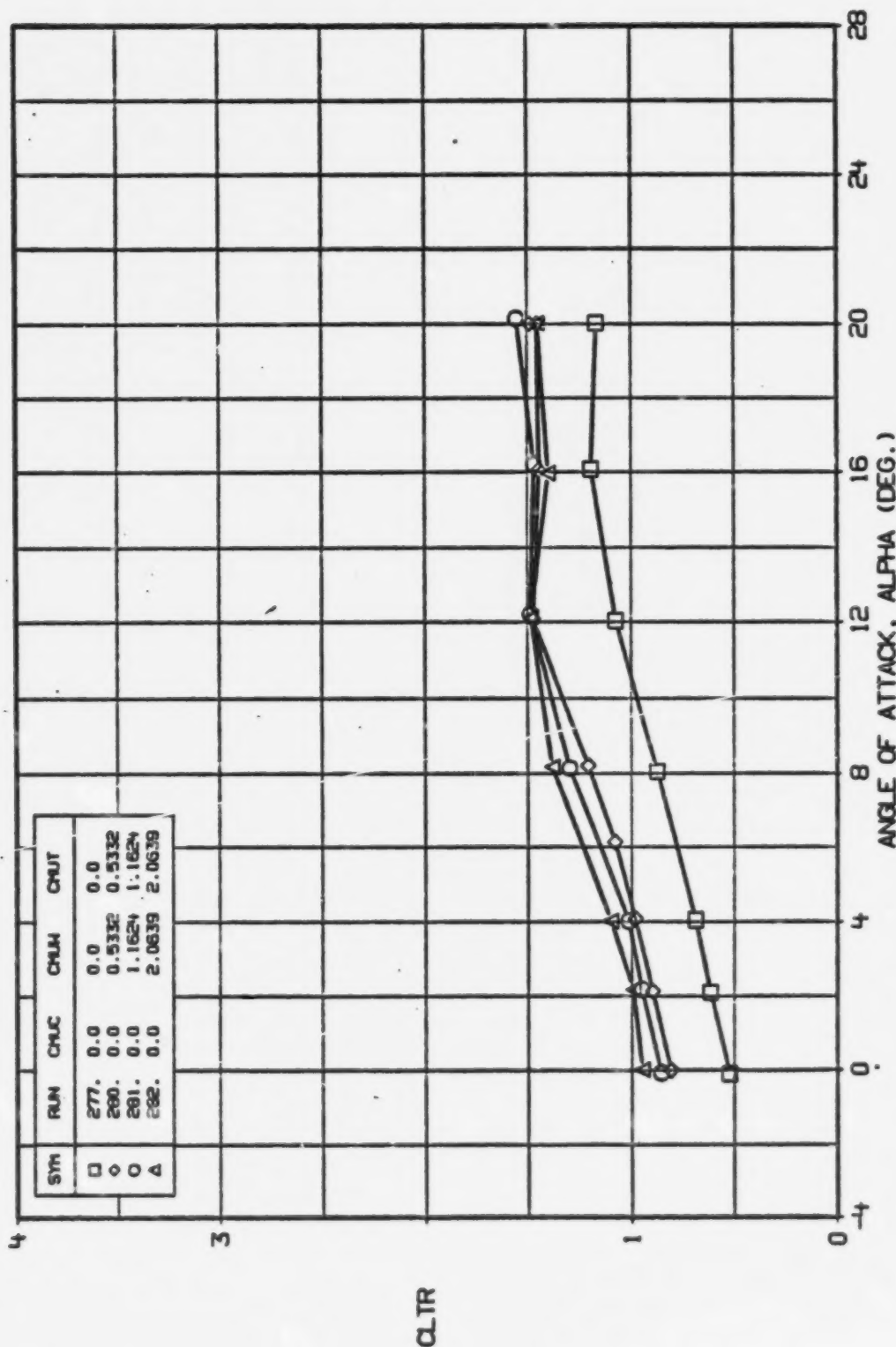


FIGURE A20d BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, DELF=45, BN/B=.25

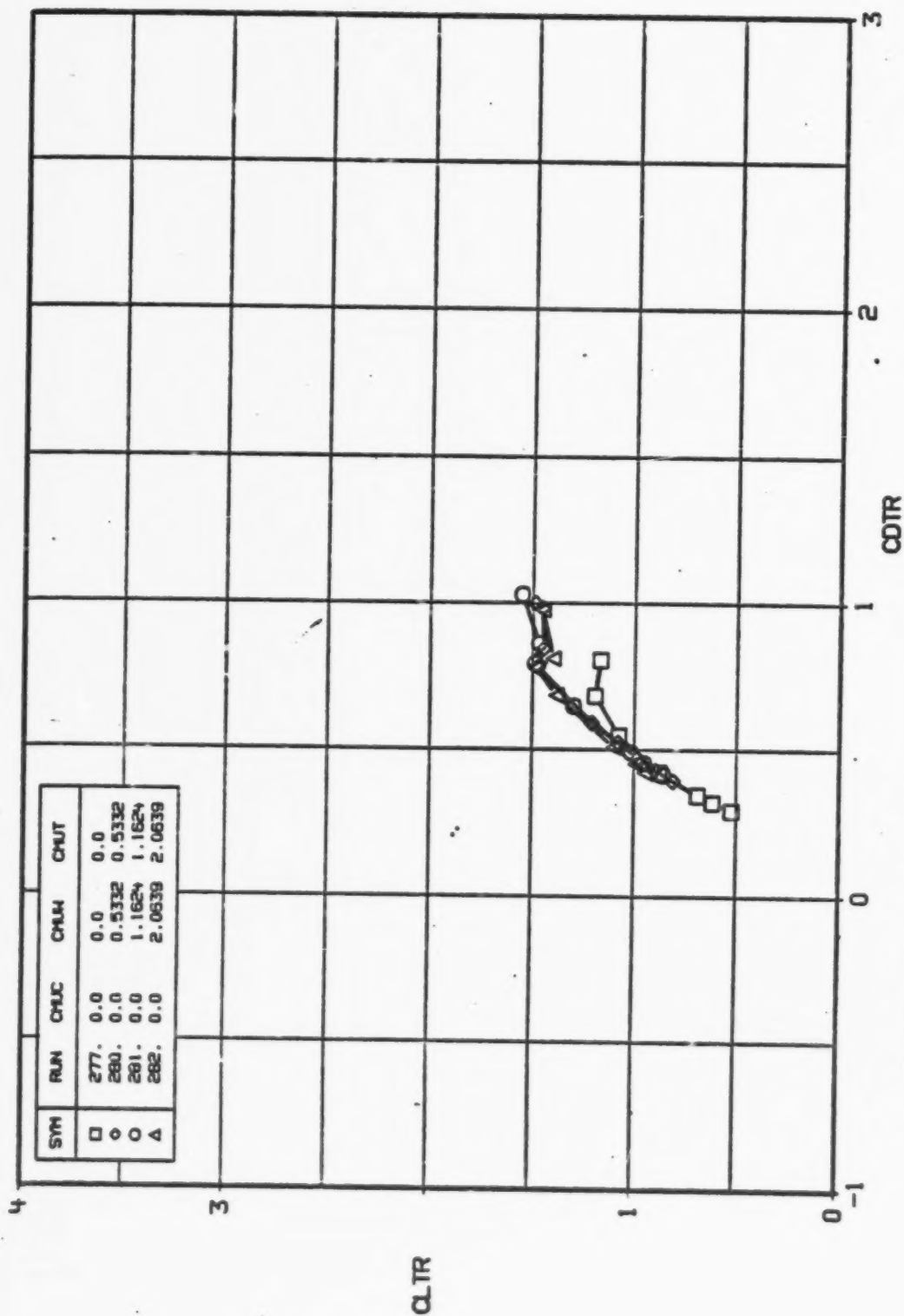


FIGURE A20e BASIC DATA EFFECT OF CHU
CONFIGURATION BN6V, DELF=45, BN/B=.25

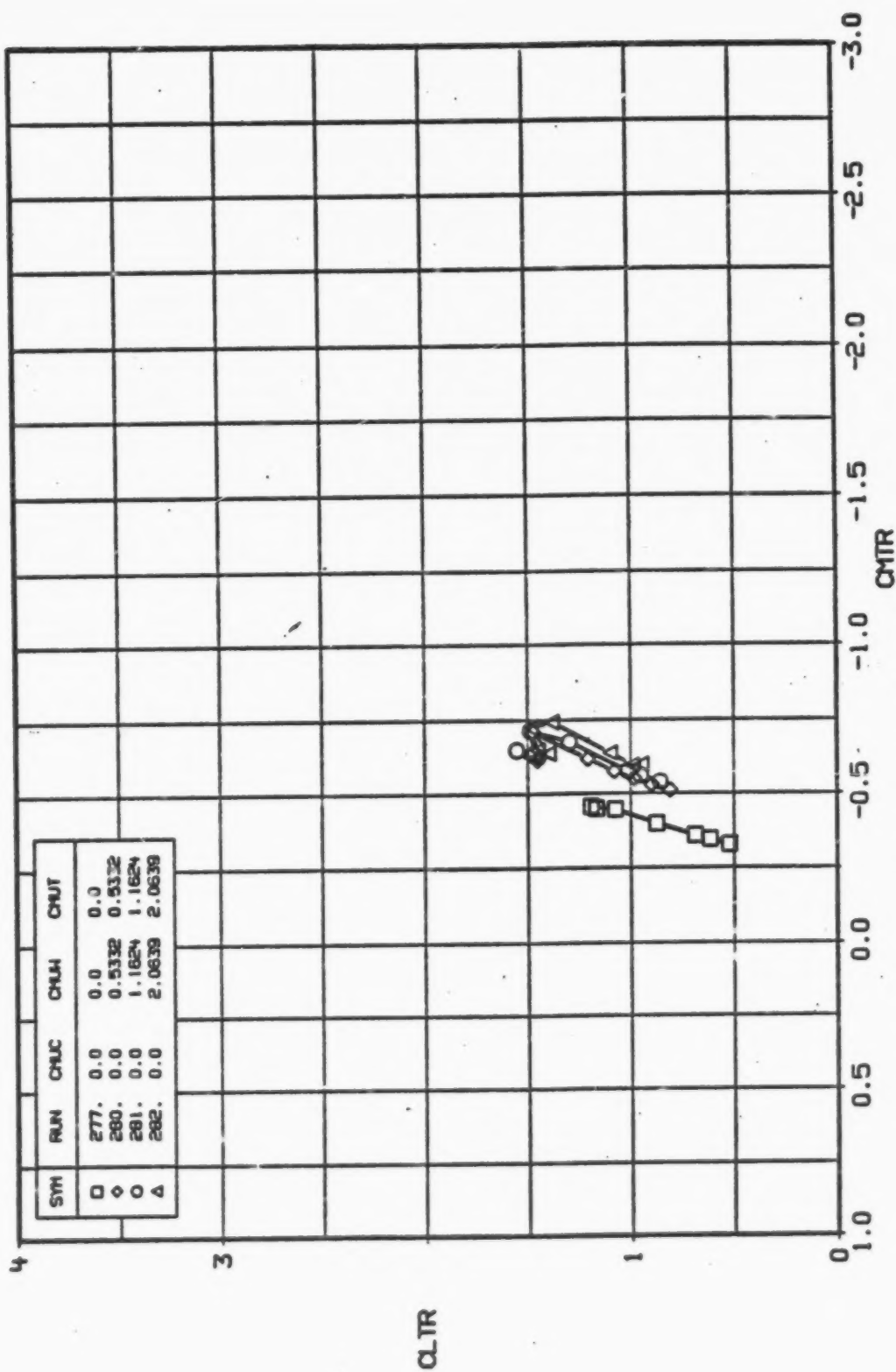


FIGURE A20f BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, DELF=45, BN/B=.25

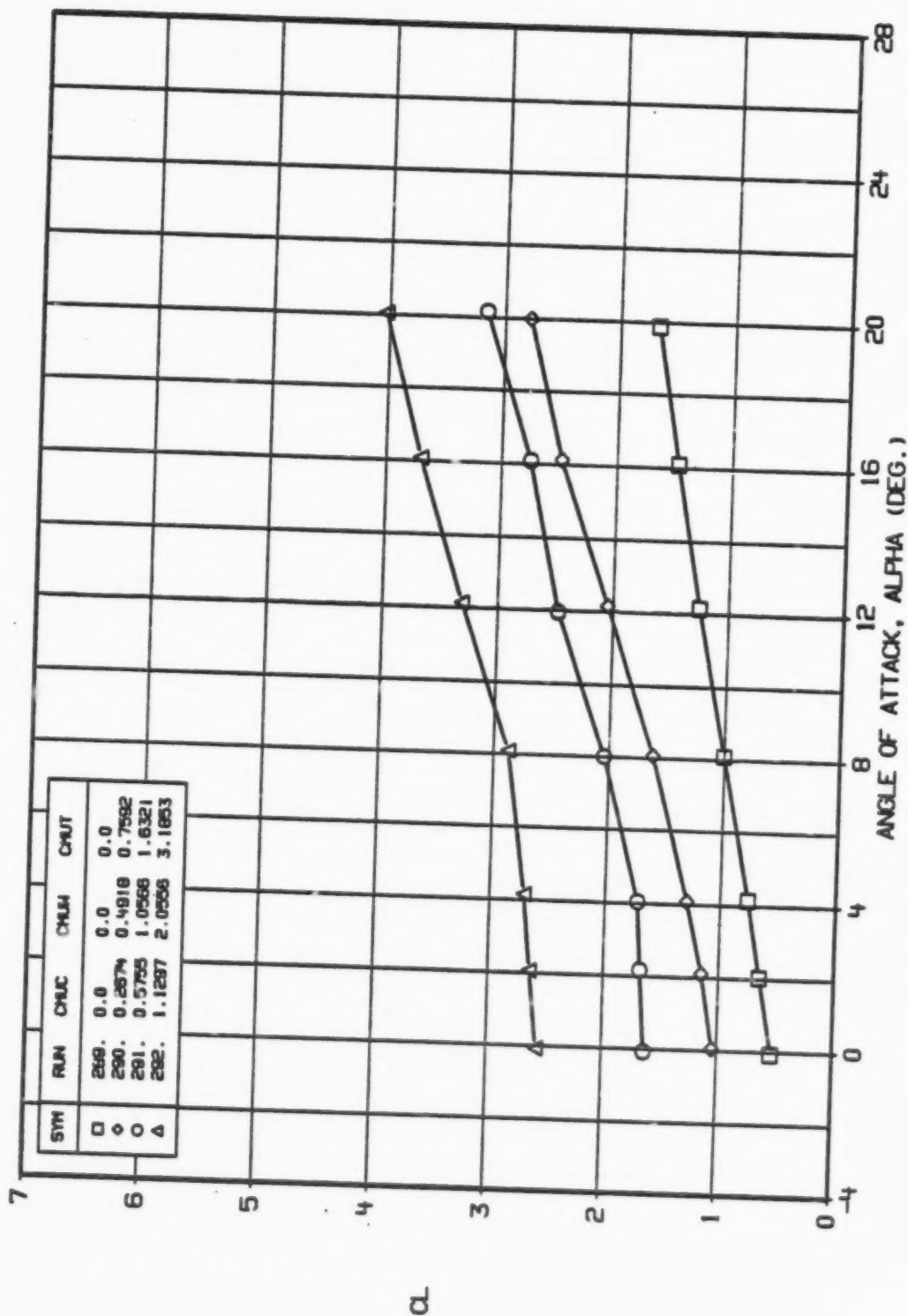


FIGURE A21a BASIC DATA EFFECT OF CHU
 CONFIG. BC1W6V, DELF=45, (BN/B)C=1, (BN/B)W=0.25

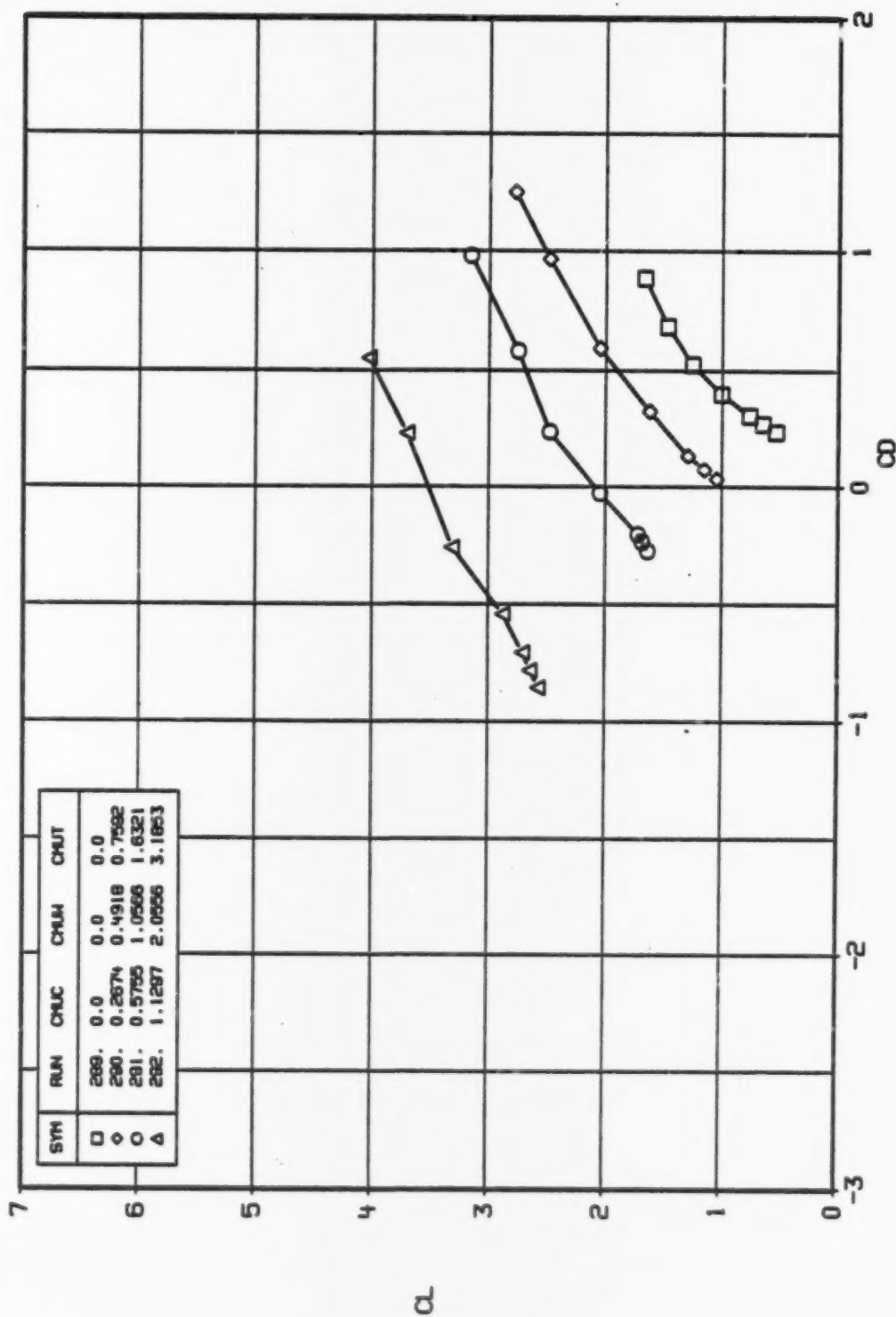


FIGURE A21b BASIC DATA EFFECT OF CHU
 CONFIG. BC1W6V, DELF=45, (BN/B)C=1, (BN/B)W=0.25

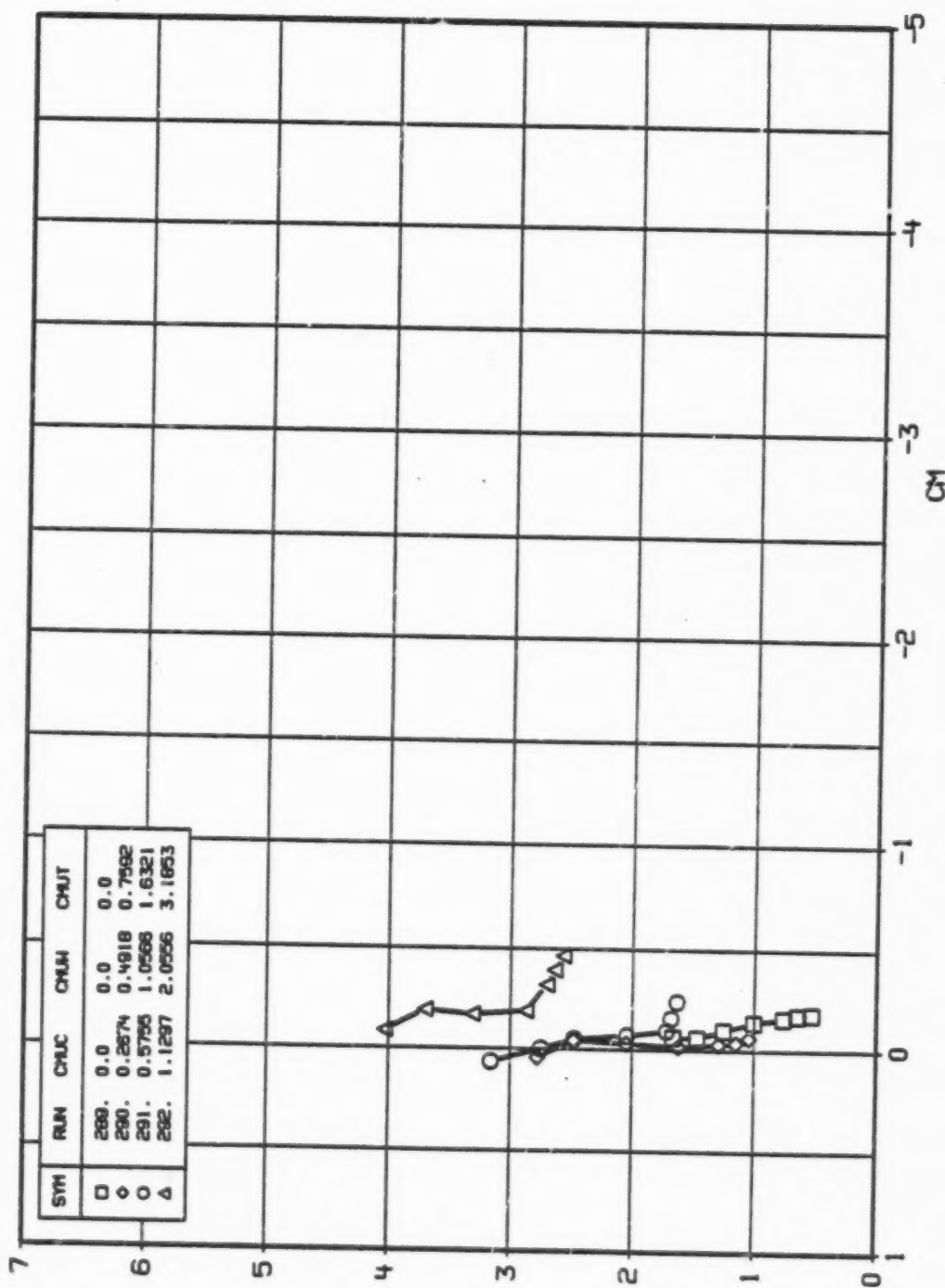


FIGURE A21c BASIC DATA EFFECT OF CMJ
CONFIG. BC1W6V, DELF=45, (BN/B)C=1, (BN/B)W=0.25

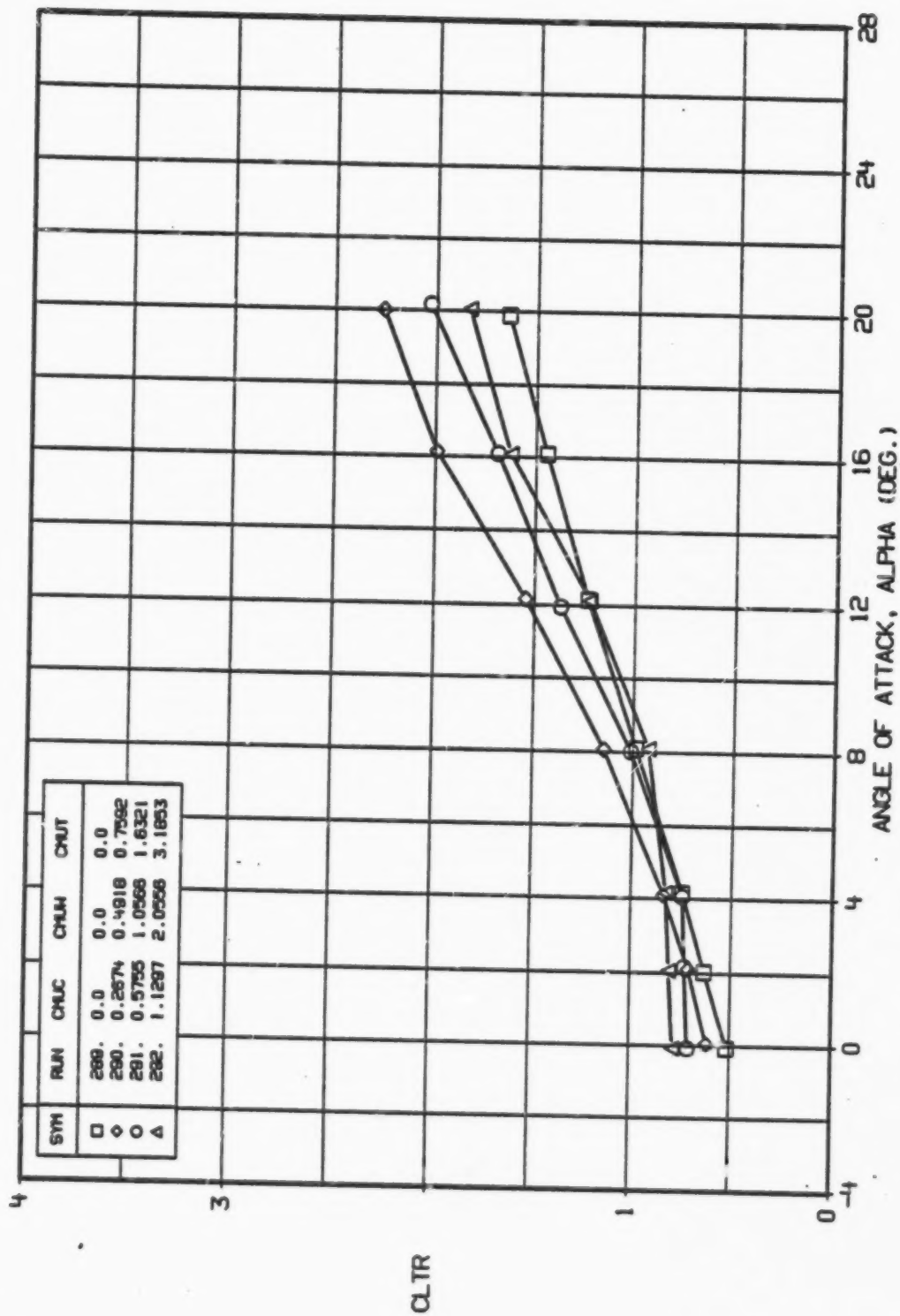


FIGURE A21d BASIC DATA EFFECT OF CMU
 CONFIG. BC1W6V, DELF=45, (BN/B)C=1, (BN/B)W=0.25

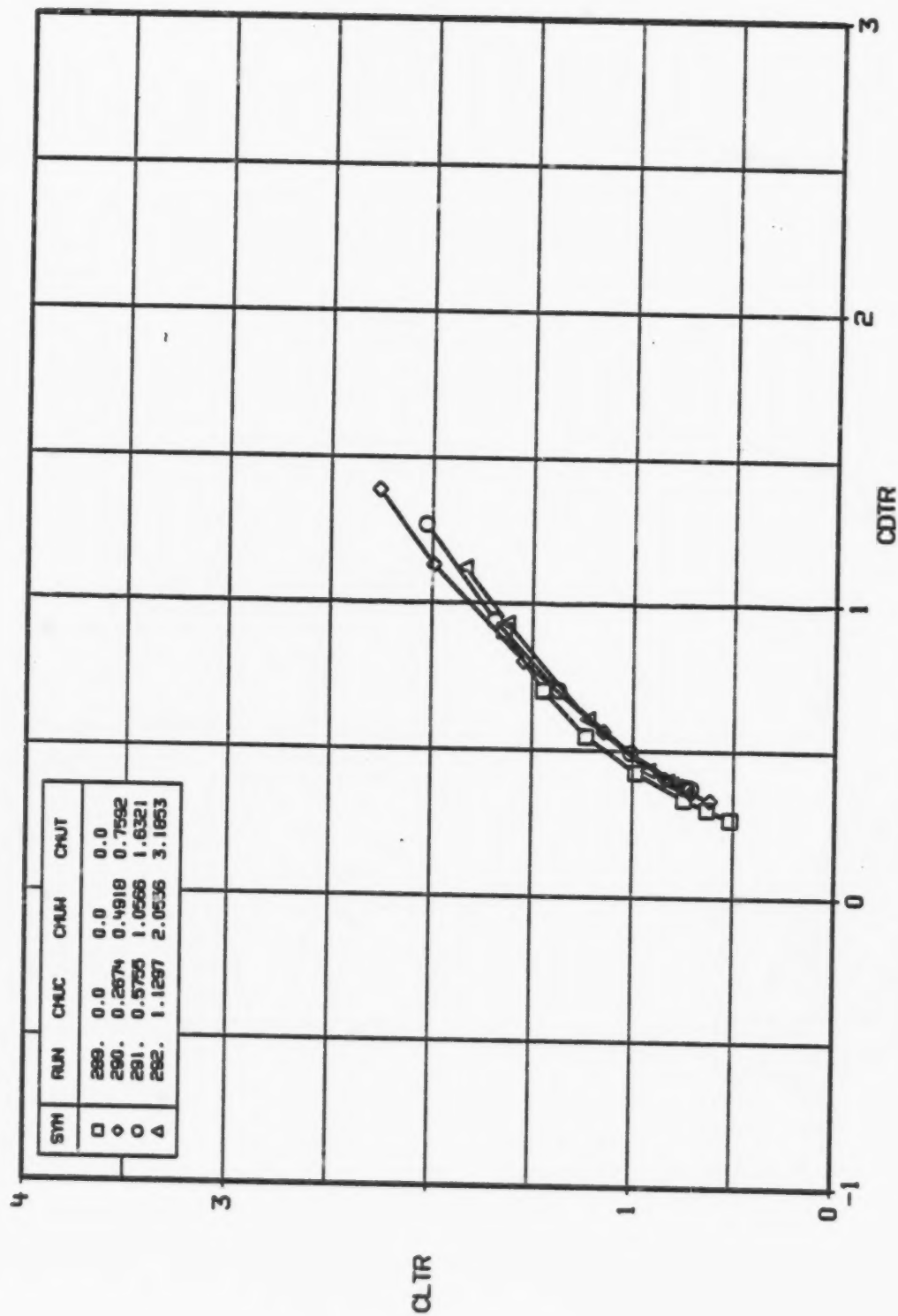


FIGURE A21e BASIC DATA EFFECT OF CMU
 CONFIG. BC1W6V, DELF=45, (BN/B)C=1, (BN/B)W=0.25

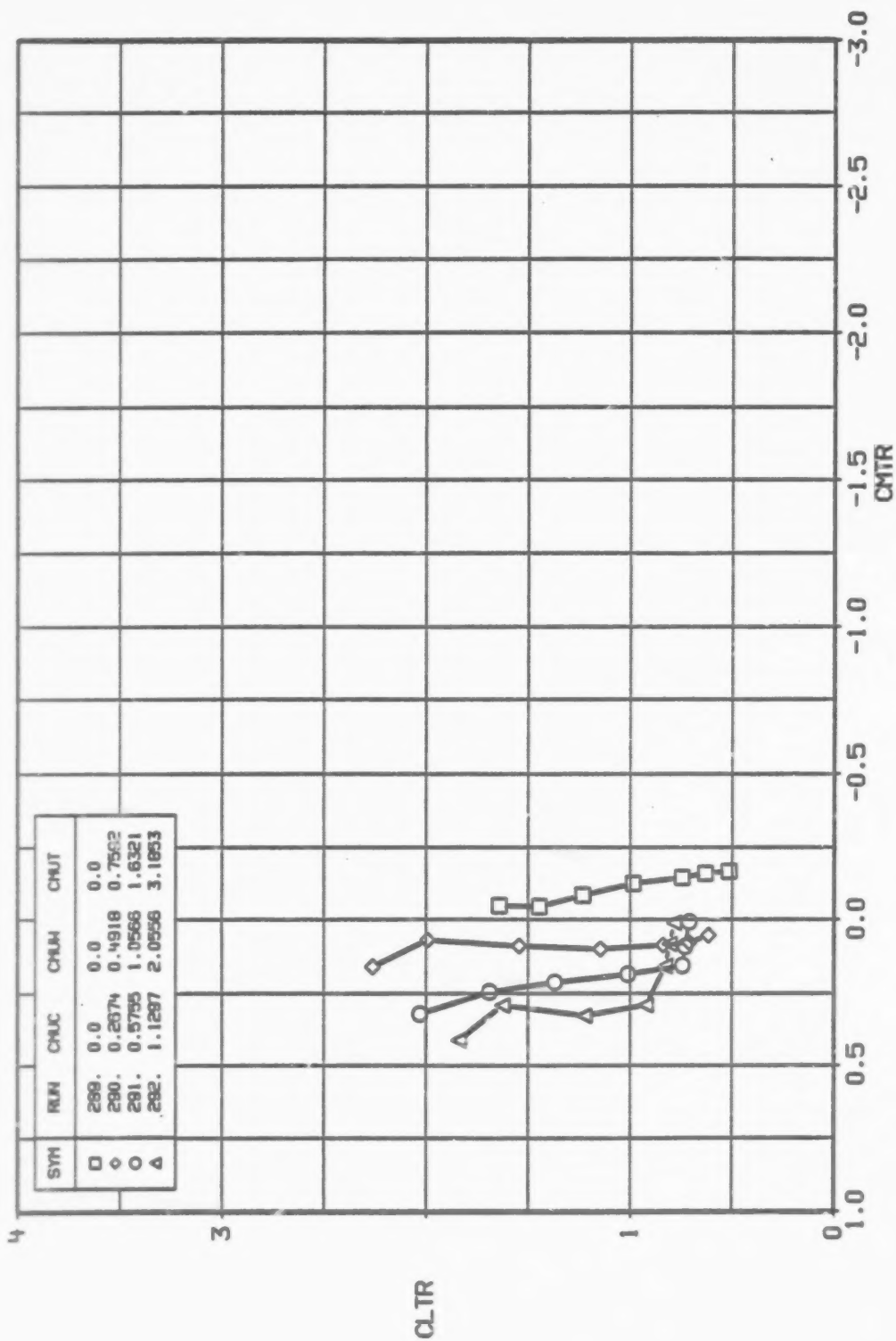


FIGURE A21f BASIC DATA EFFECT OF CMJ
 CONFIG. BC1W6V, DELF=45, (BN/B)C=1, (BN/B)W=0.25

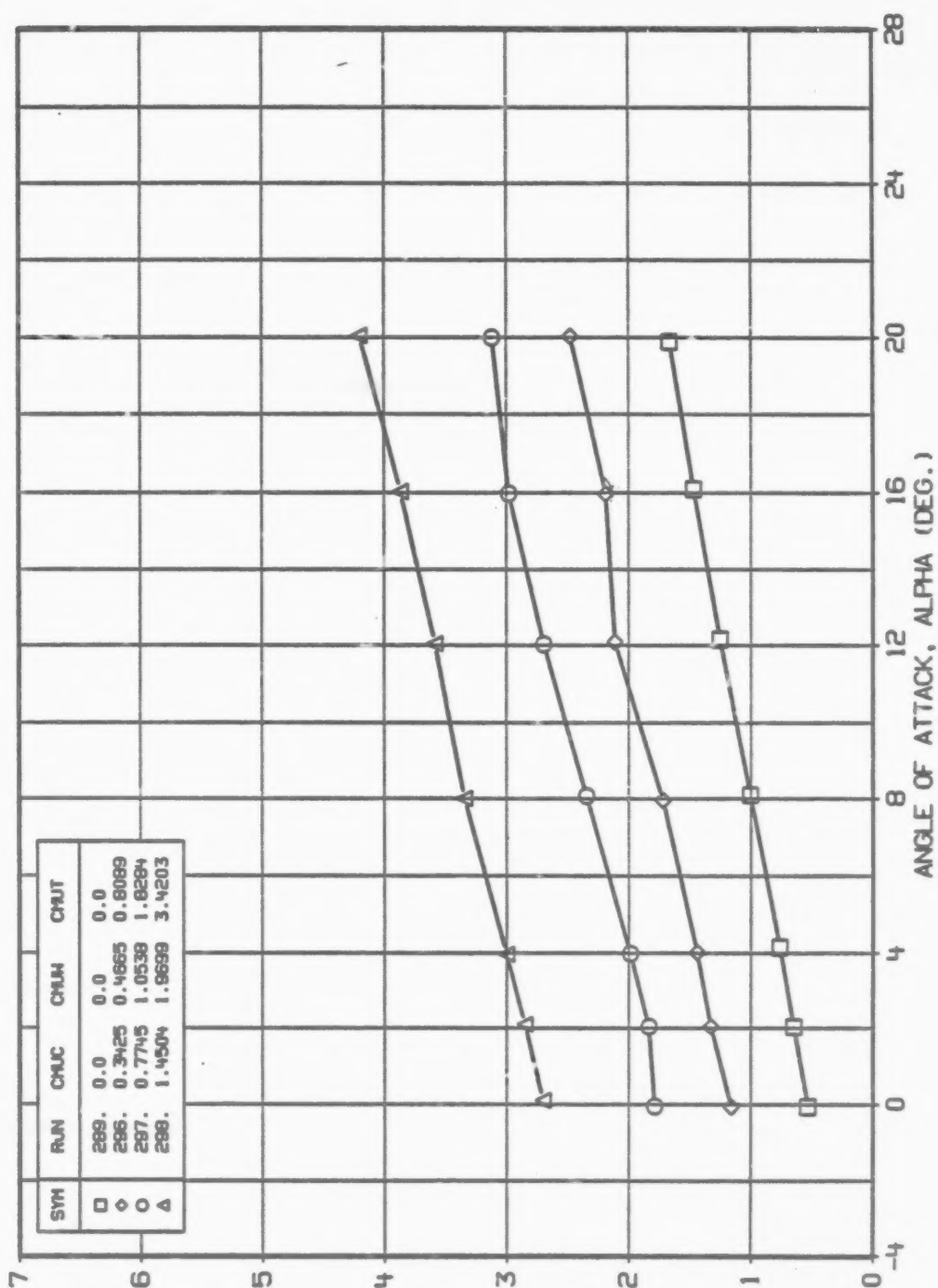


FIGURE A22a BASIC DATA EFFECT OF CMU
CONFIG. BC1W6V DELF=45 $(BN/B)_C=0.5$ $(BN/B)_W=0.25$

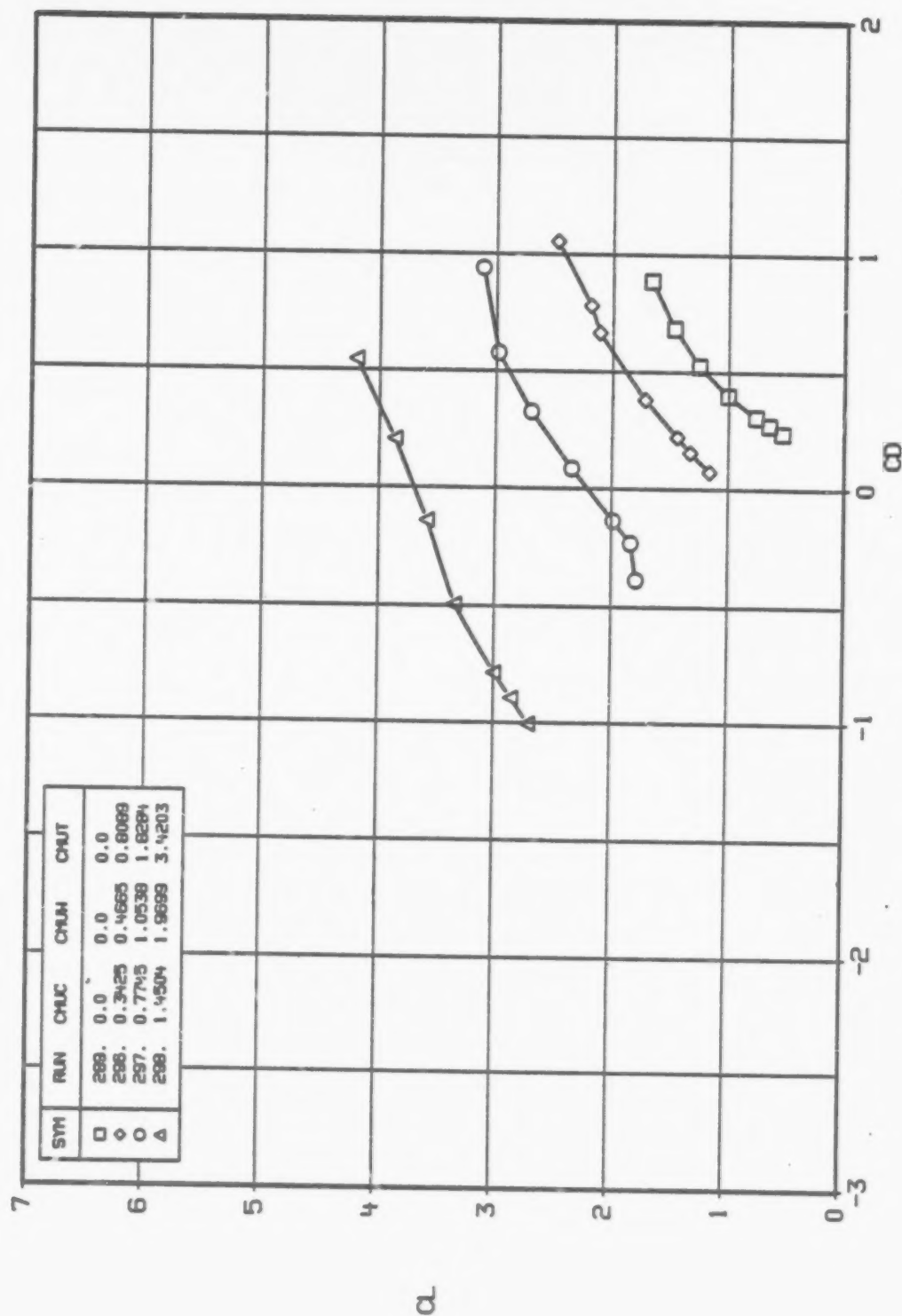


FIGURE A22b BASIC DATA EFFECT OF CMU
 CONFIG. BCW6V DELF=45 $(BN/B)_C=0.5$ $(BN/B)_W=0.25$

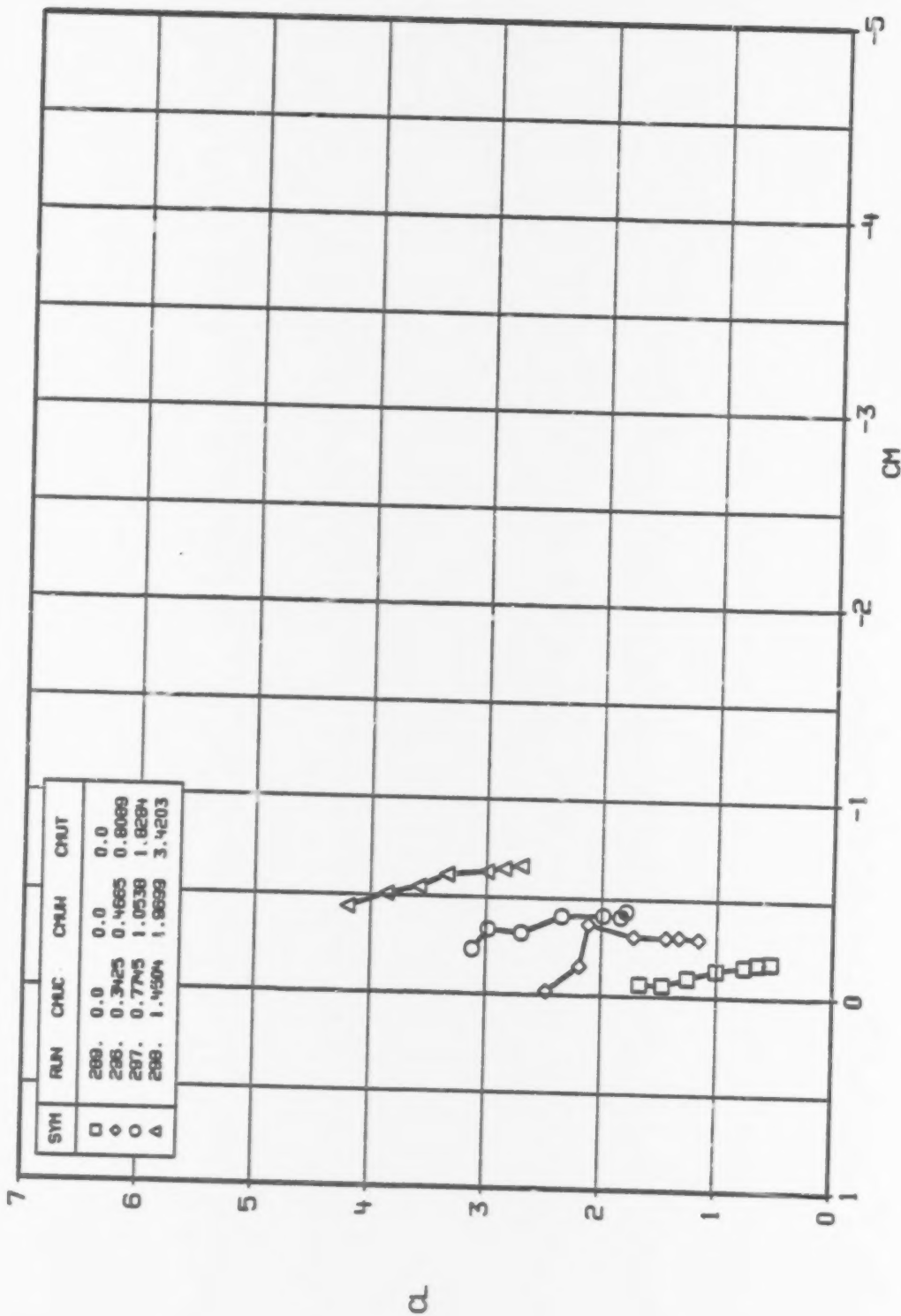


FIGURE A22c BASIC DATA EFFECT OF CMU
 CONFIG. BC1W6V DELF=45 (BN/B)_C=0.5 (BN/B)_W=0.25

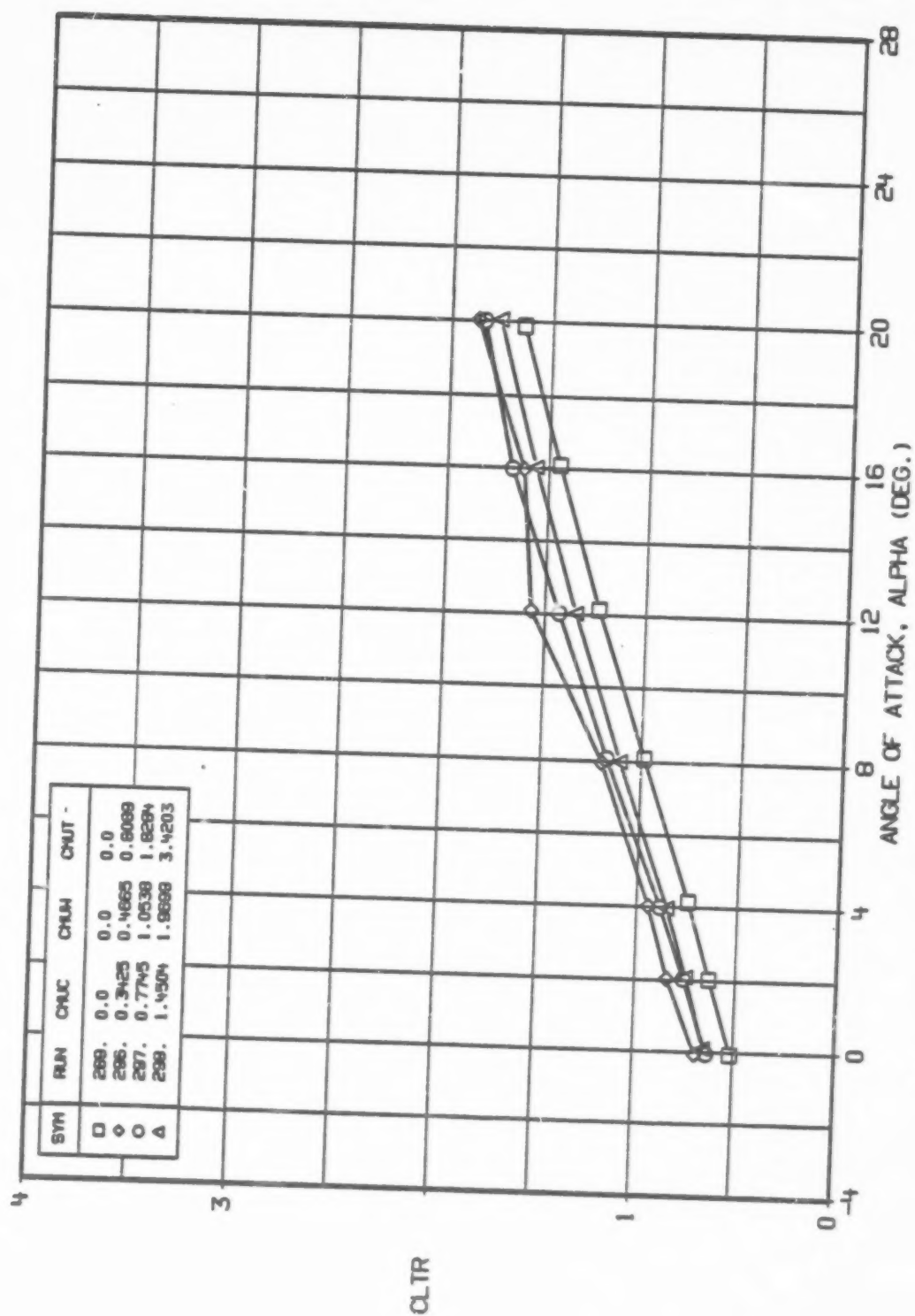


FIGURE A22d BASIC DATA EFFECT OF CMU
 CONFIG. BC1W6V DELF=45 $(BN/B)_C=0.5$ $(BN/B)_W=0.25$

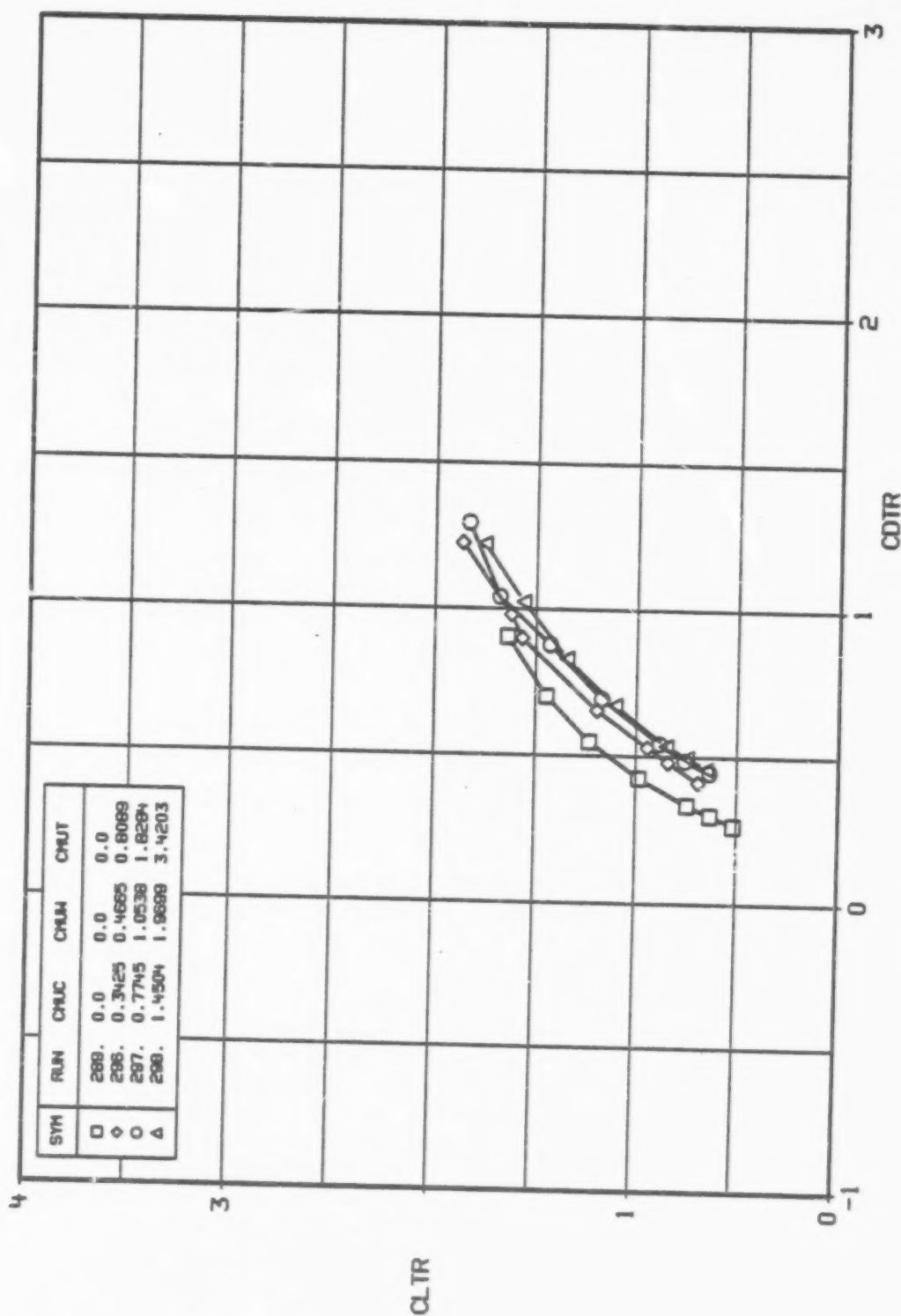


FIGURE A22e BASIC DATA EFFECT OF CMU
 CONFIG. BC1W6V DFLF=45 $(BN/B)_C=0.5$ $(BN/B)_W=0.25$

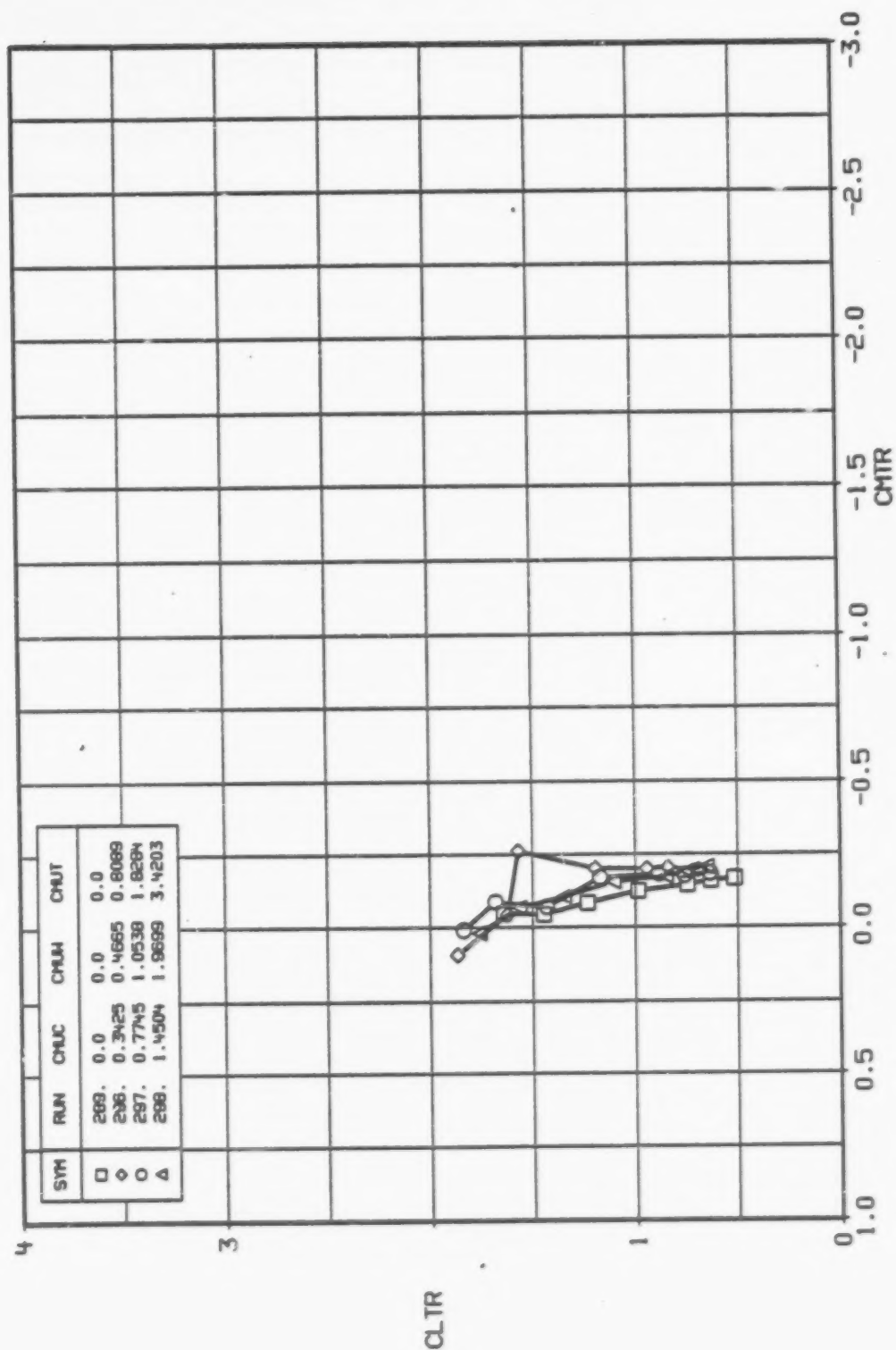


FIGURE A22f BASIC DATA EFFECT OF CMJ
 CONFIG. BC1W6V DELF=45 (BN/B)_C=0.5 (BN/B)_W=0.25

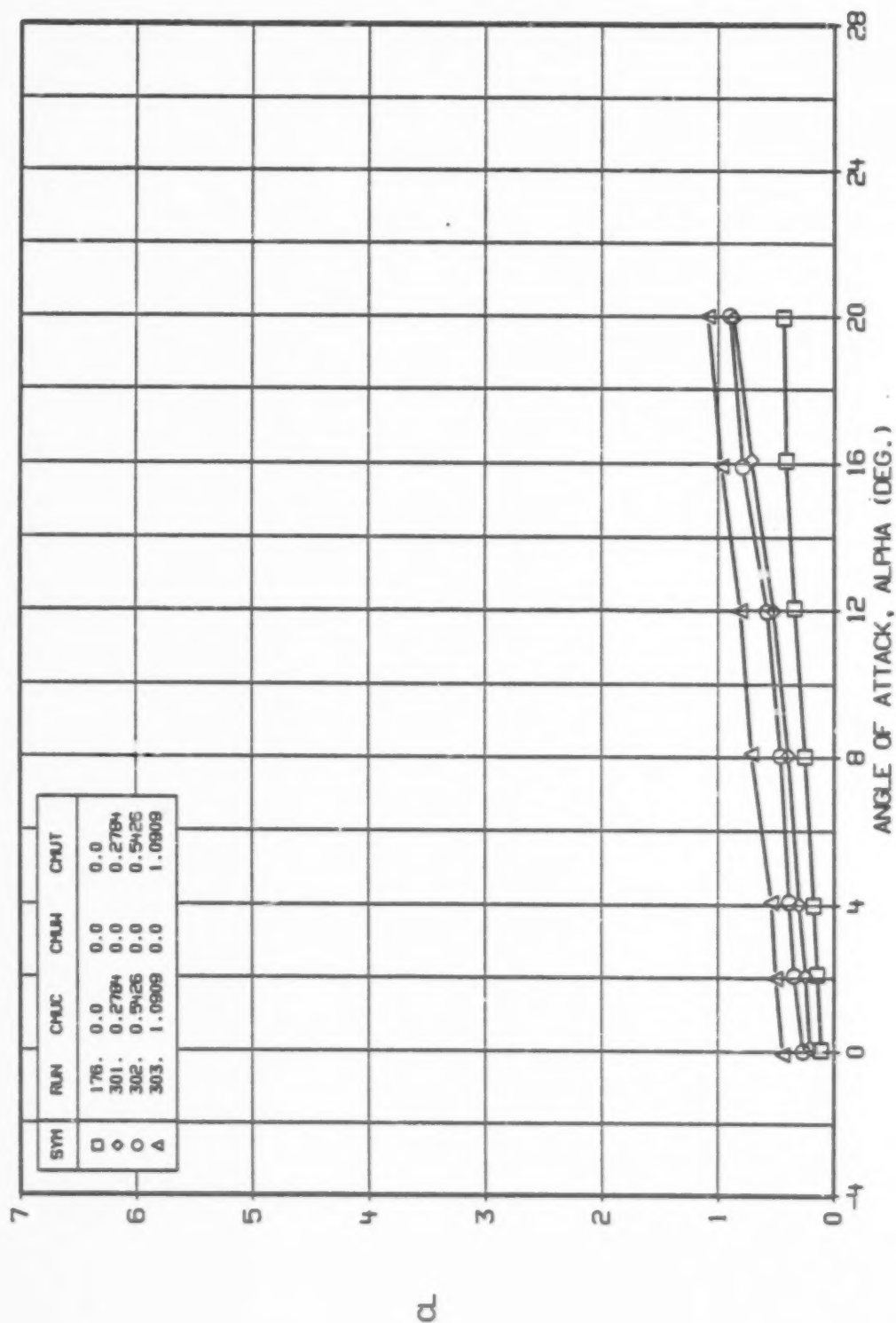


FIGURE A23a BASIC DATA EFFECT OF CHU
CONFIG. BCIV, DELF=45, (BN/B)C=0.5

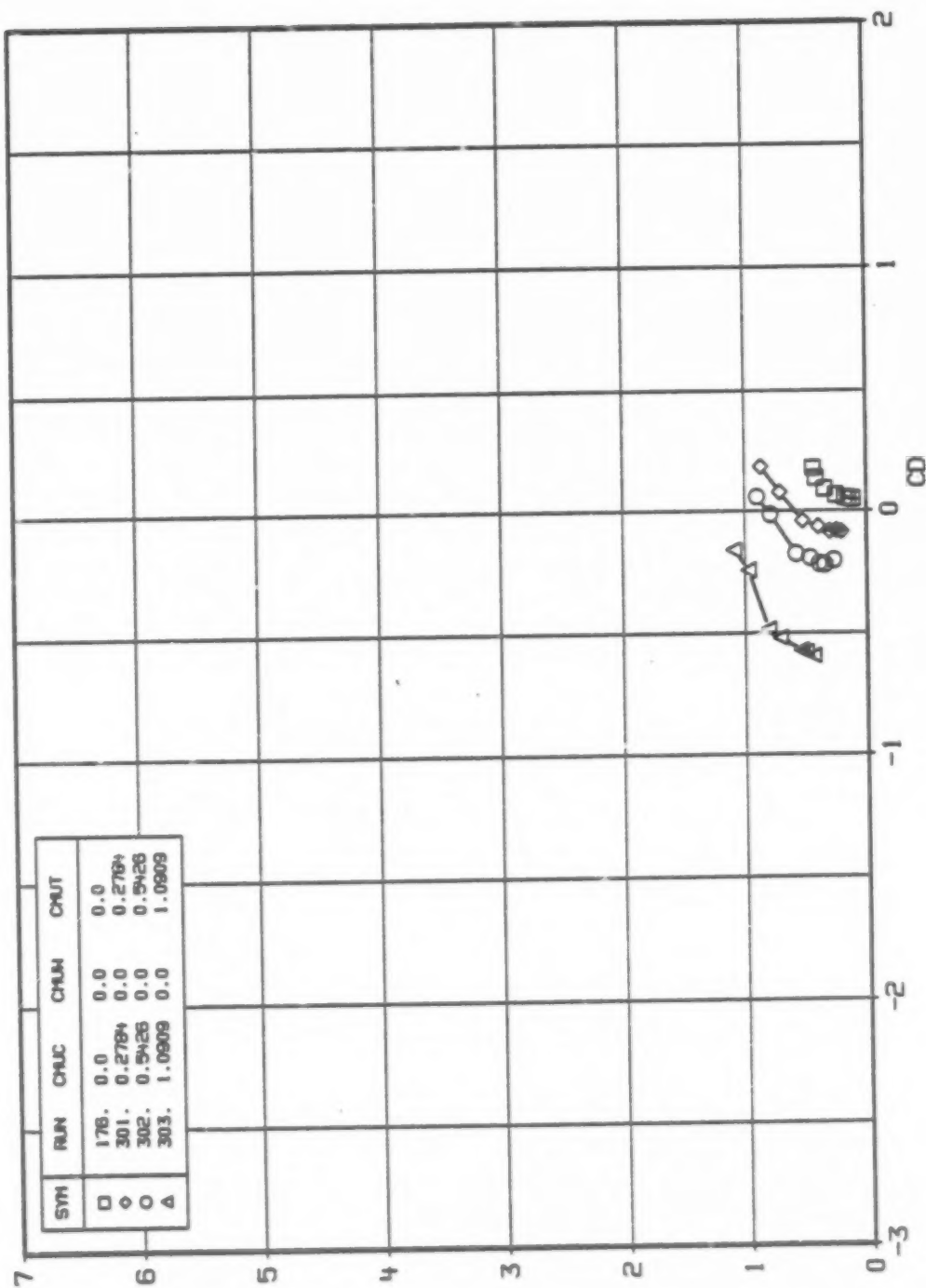


FIGURE A23b BASIC DATA EFFECT OF CMU
CONFIG. BCIV, DELF=45, (BN/B)C=0.5,

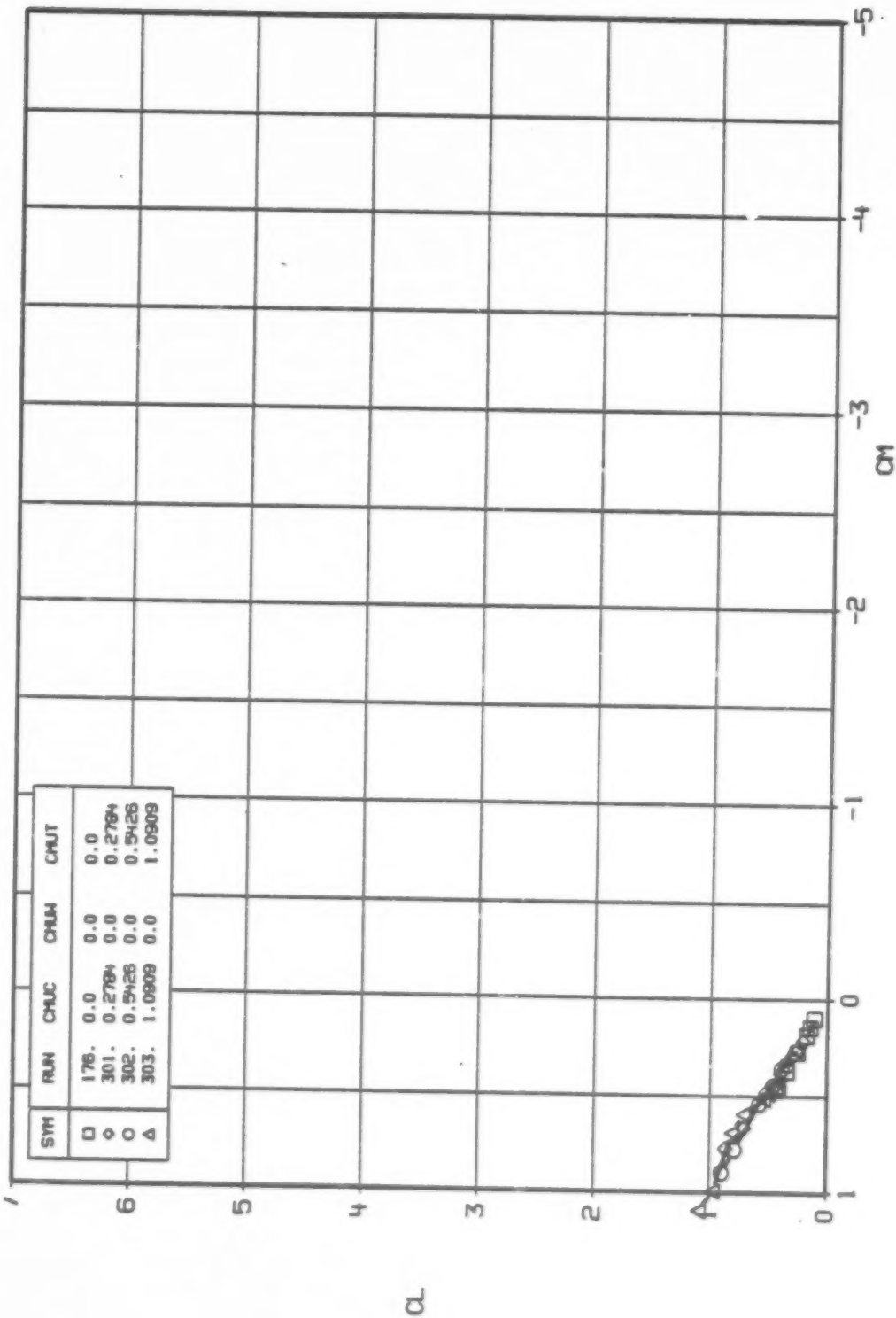


FIGURE A23c BASIC DATA EFFECT OF CMU
CONFIG. BCIV, DELF=45, (BN/B)C=0.5

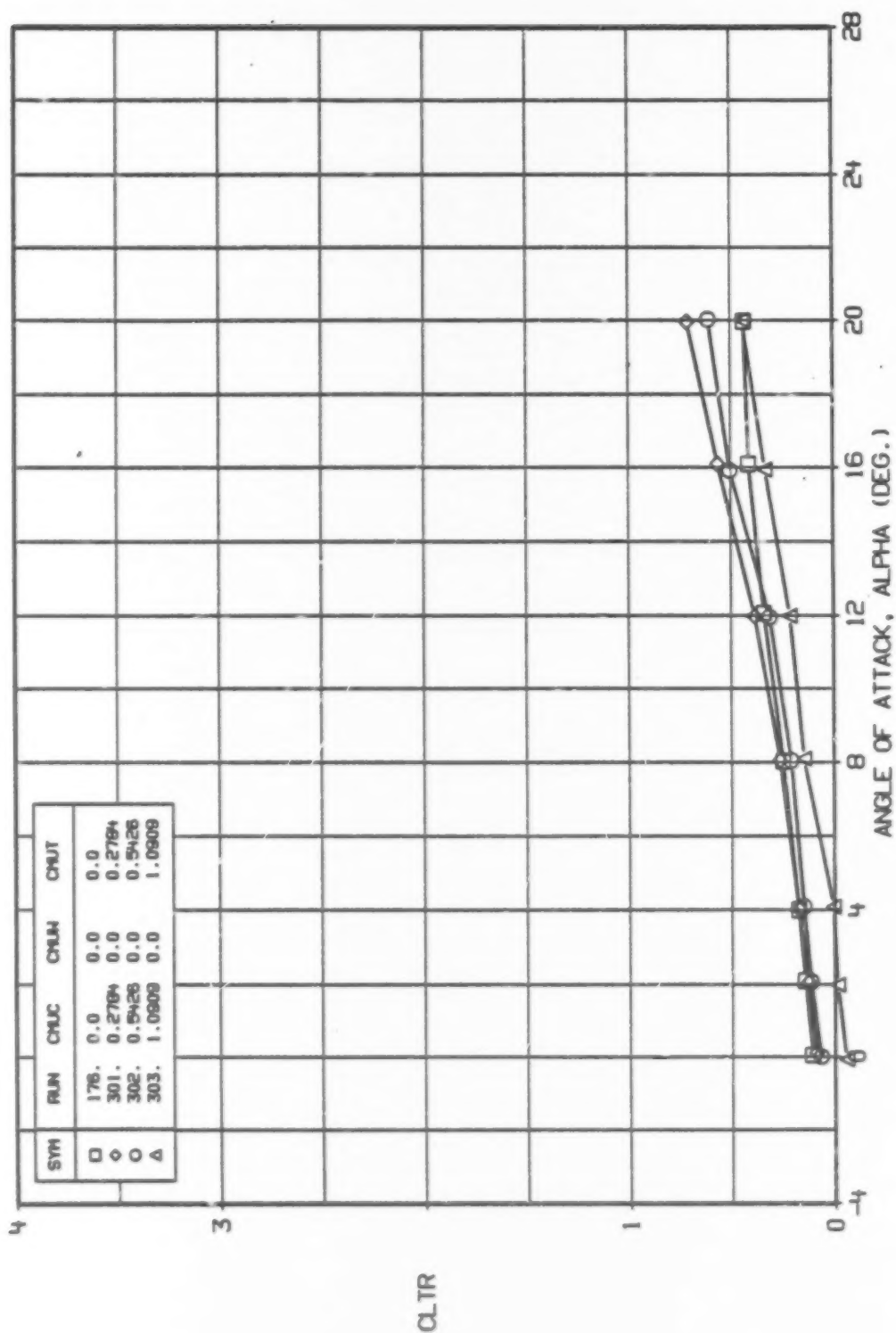


FIGURE A23d BASIC DATA EFFECT OF CMU
CONF'IG. BC1V, DELF=45, (BN/B)C=0.5, (BN/B)W=0

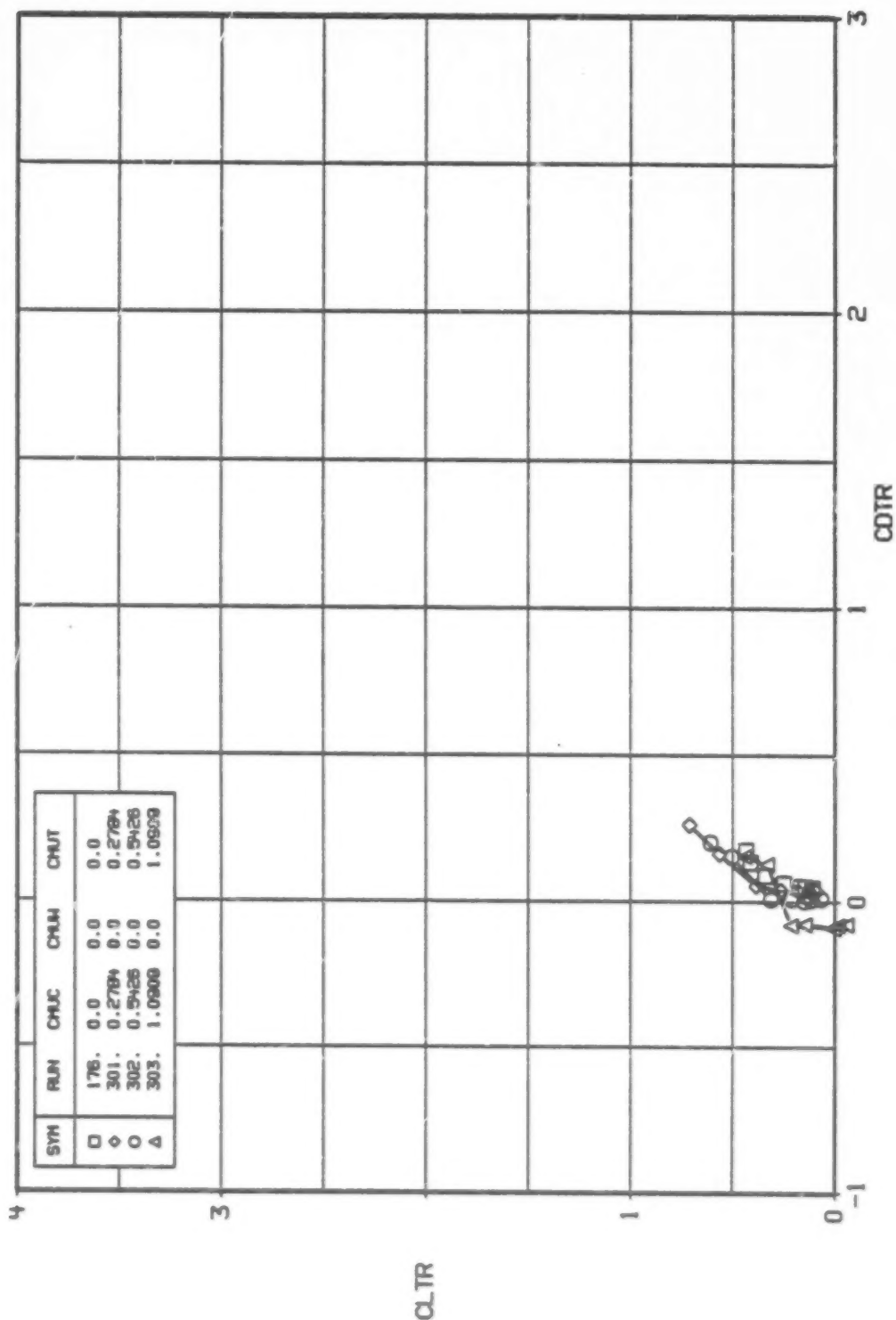


FIGURE A23e BASIC DATA EFFECT OF CMU
CONFIG. BCIV, DELF=45, (BN/B)C=0.5

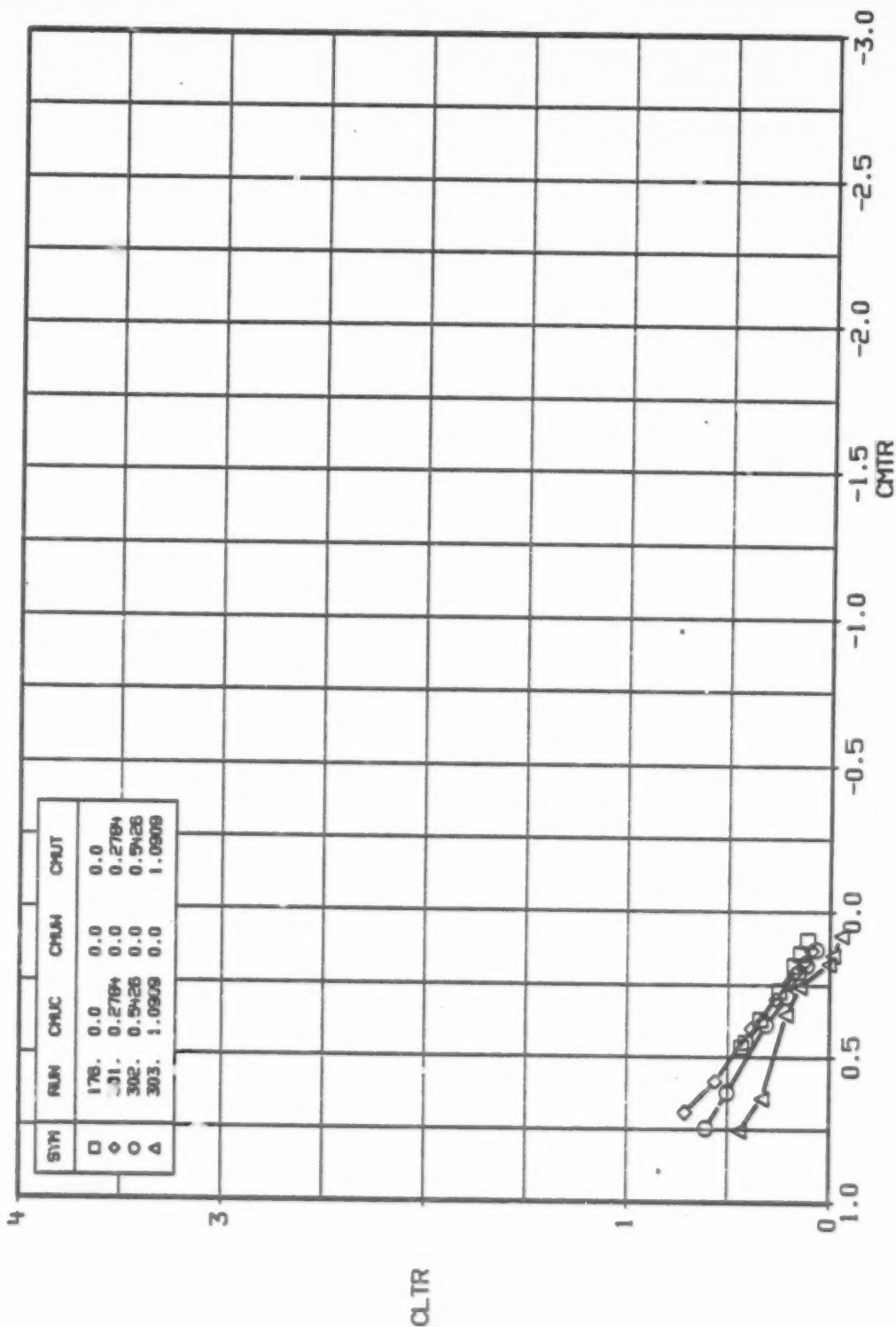


FIGURE A23f BASIC DATA EFFECT OF CMJ
CONFIG. BCIV, DELF=45, (BN/B)C=0.5,

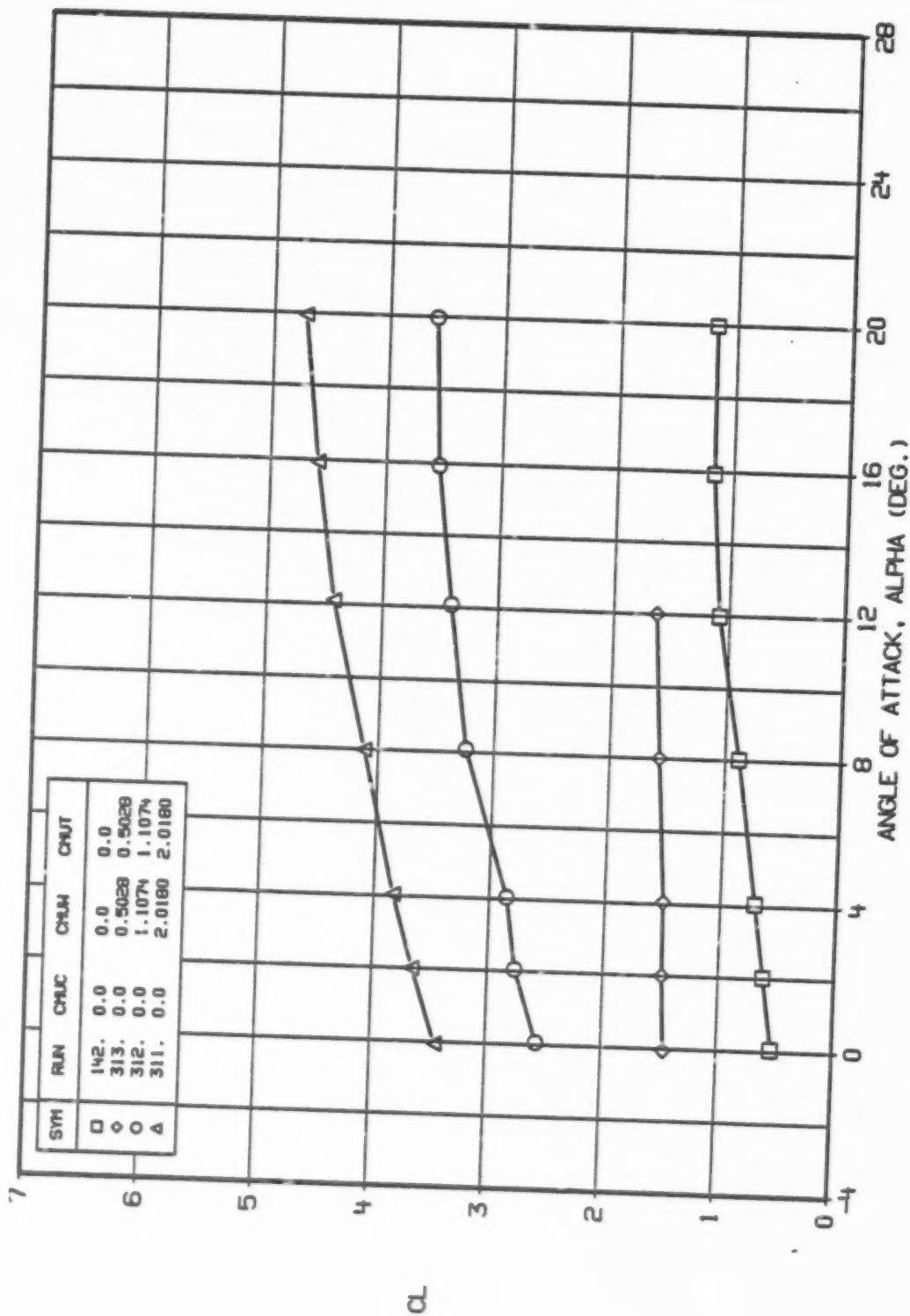


FIGURE A24a BASIC DATA EFFECT OF CHU
CONFIGURATION B46V, DELF=45, BN/B=1

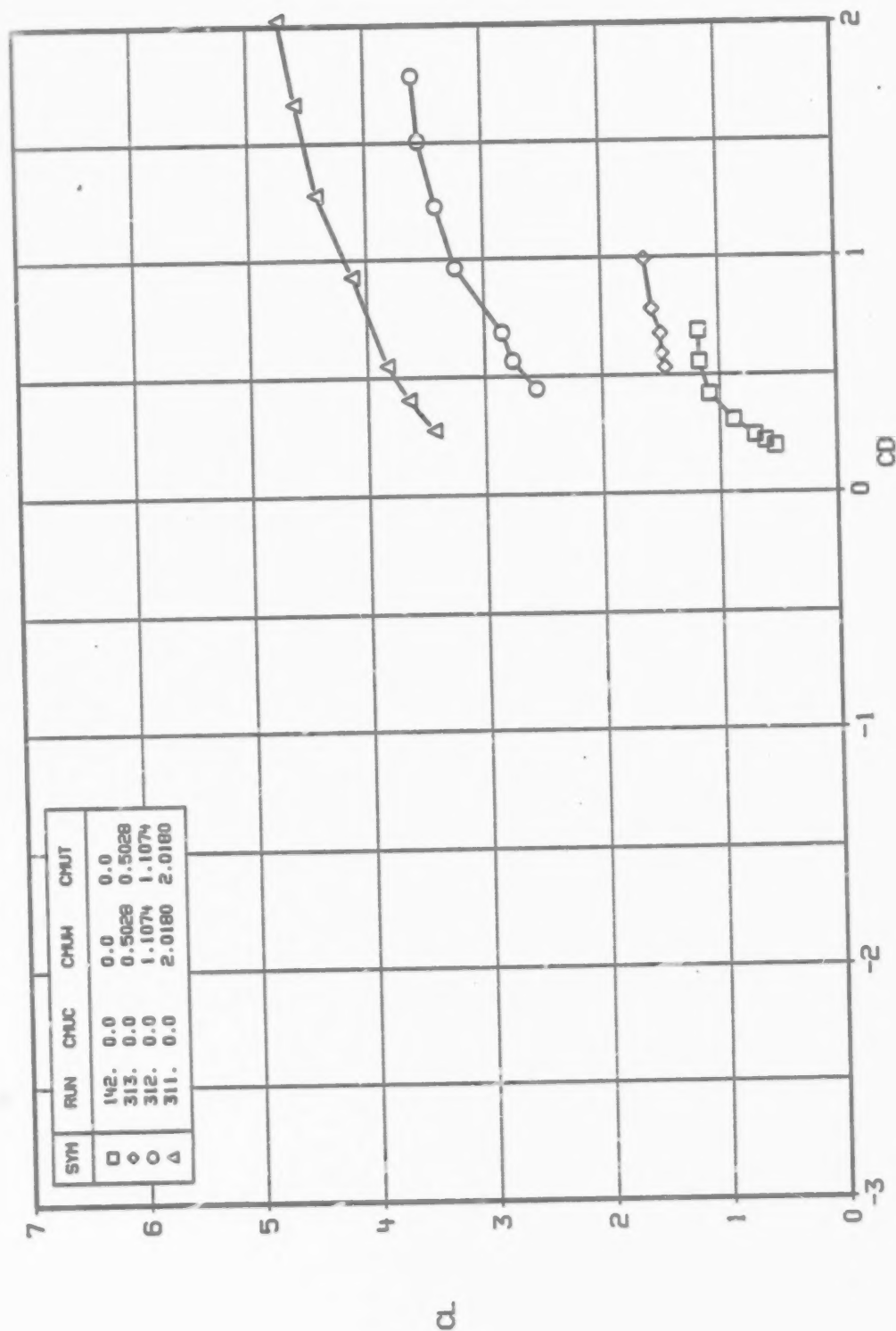


FIGURE A24b BASIC DATA EFFECT OF CMU
CONFIGURATION BMSV, DELF=45, BN/B=1

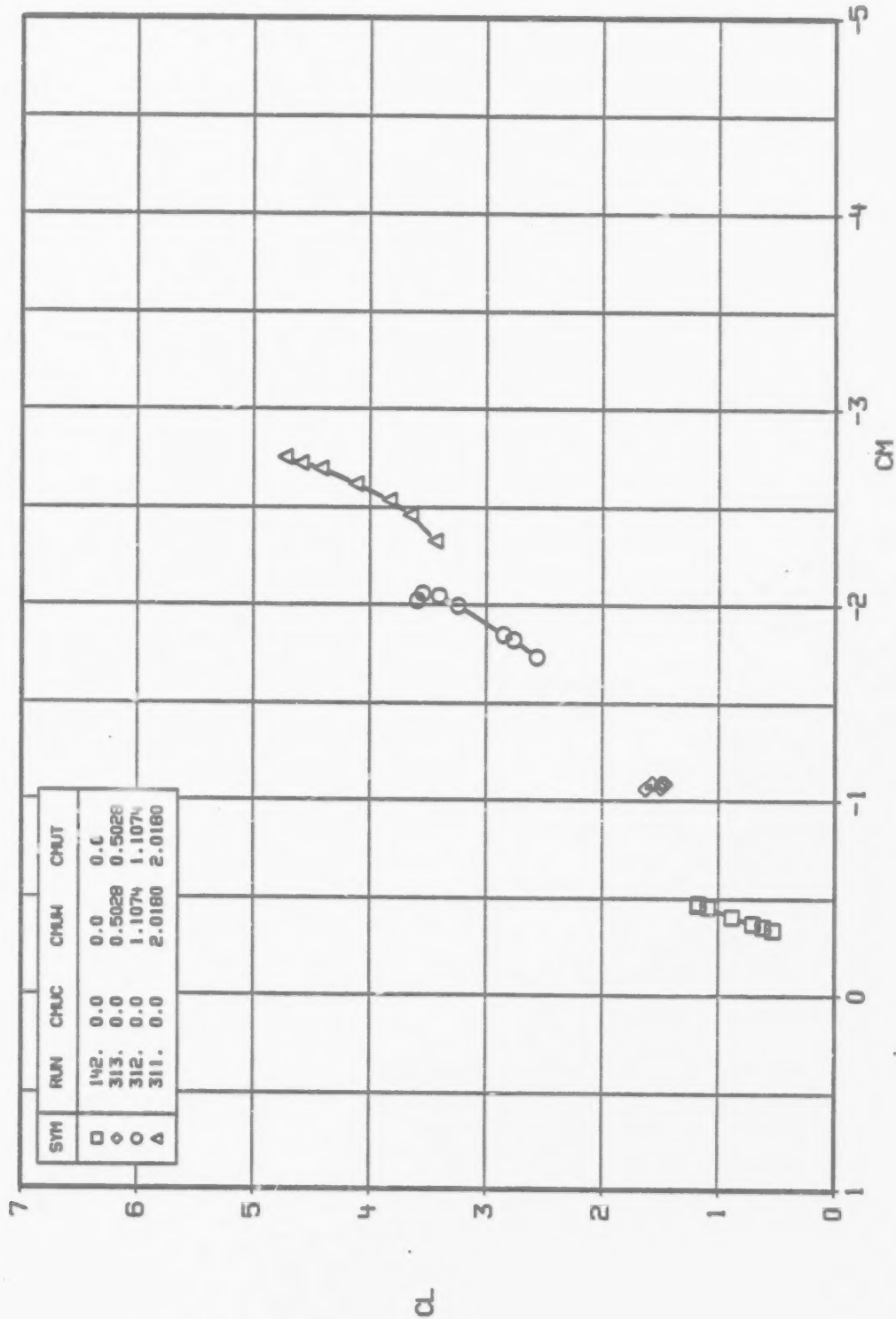


FIGURE A24c BASIC DATA EFFECT OF CMJ
CONFIGURATION B46V, DELF=45, BN/B=1

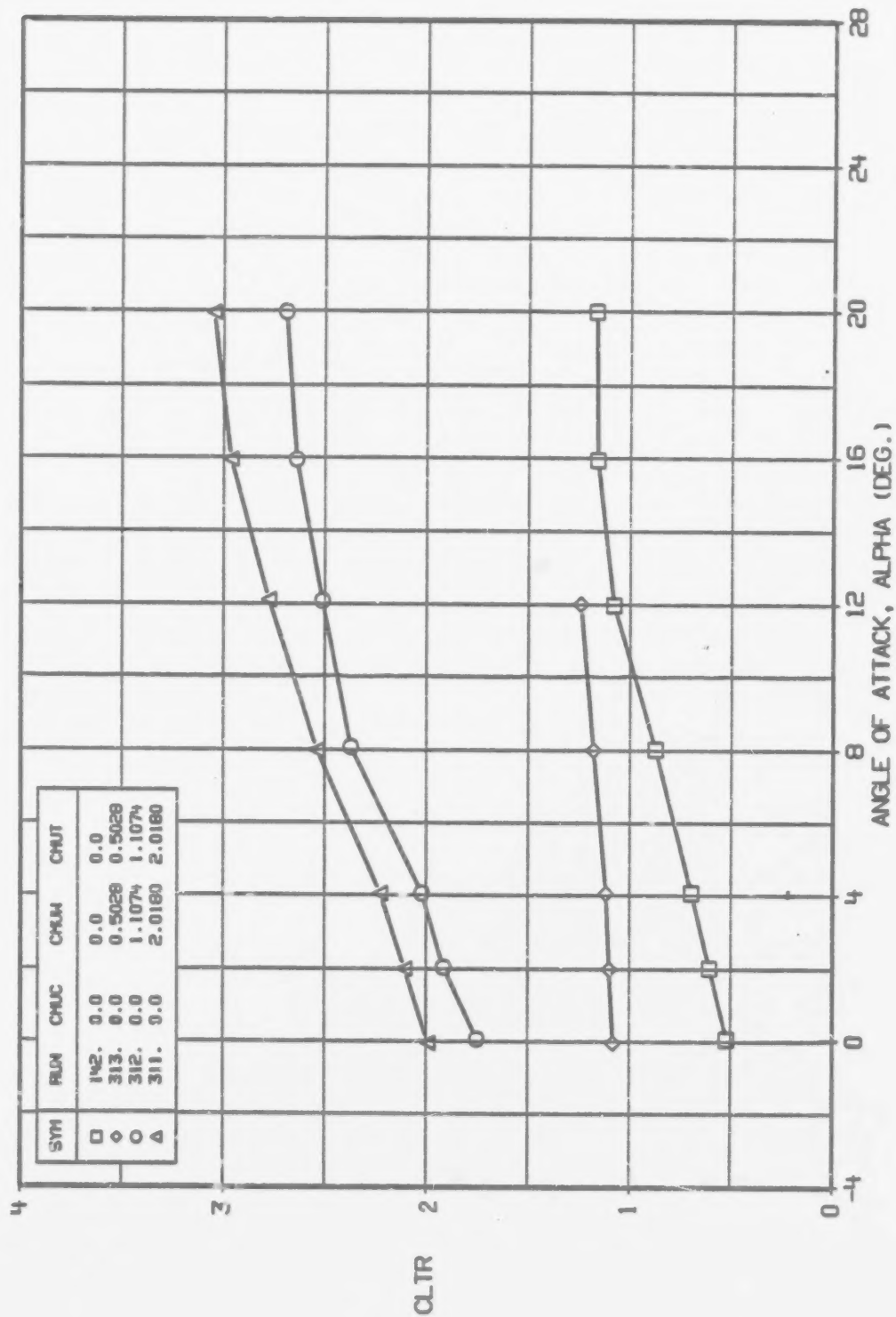


FIGURE A24d BASIC DATA EFFECT OF CMU
CONFIGURATION BM6V, DELF=45, BN/B=1

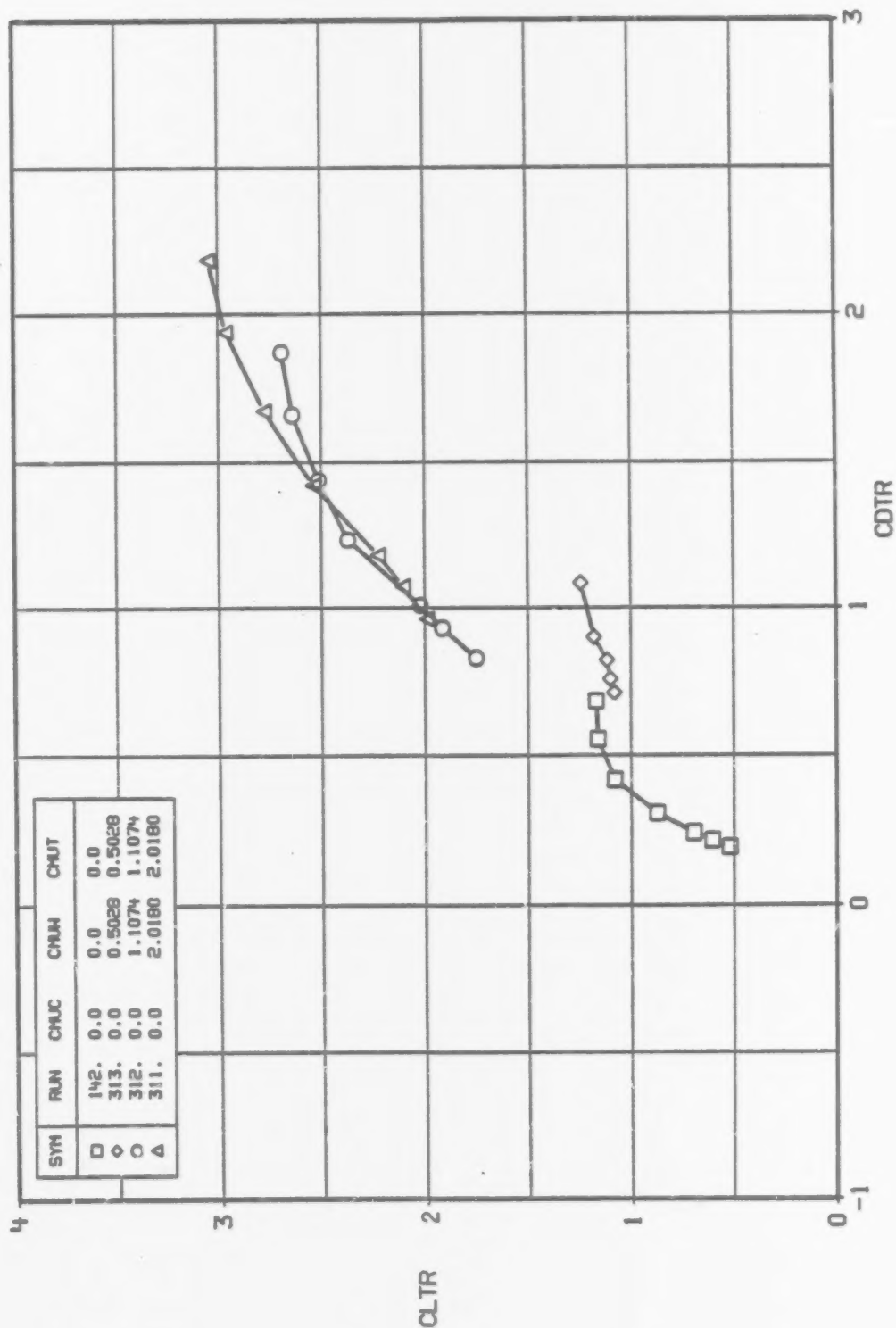


FIGURE A24e BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, DELF=45, BN/B=1

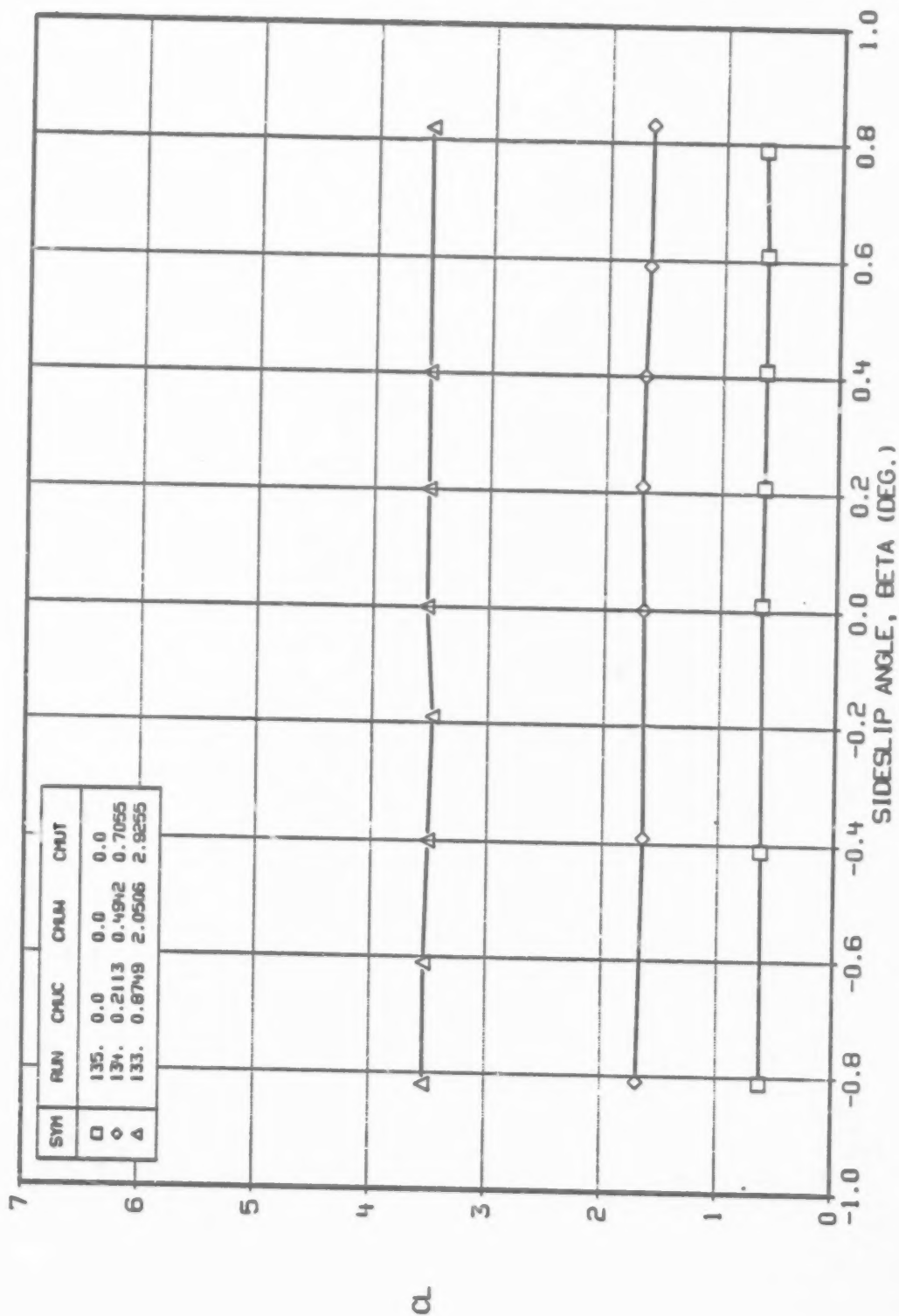


FIGURE A25a BASIC DATA EFFECT OF CMU
CONFIGURATION B45V, BN/B=1.0, DELF=45, $\alpha = 2$

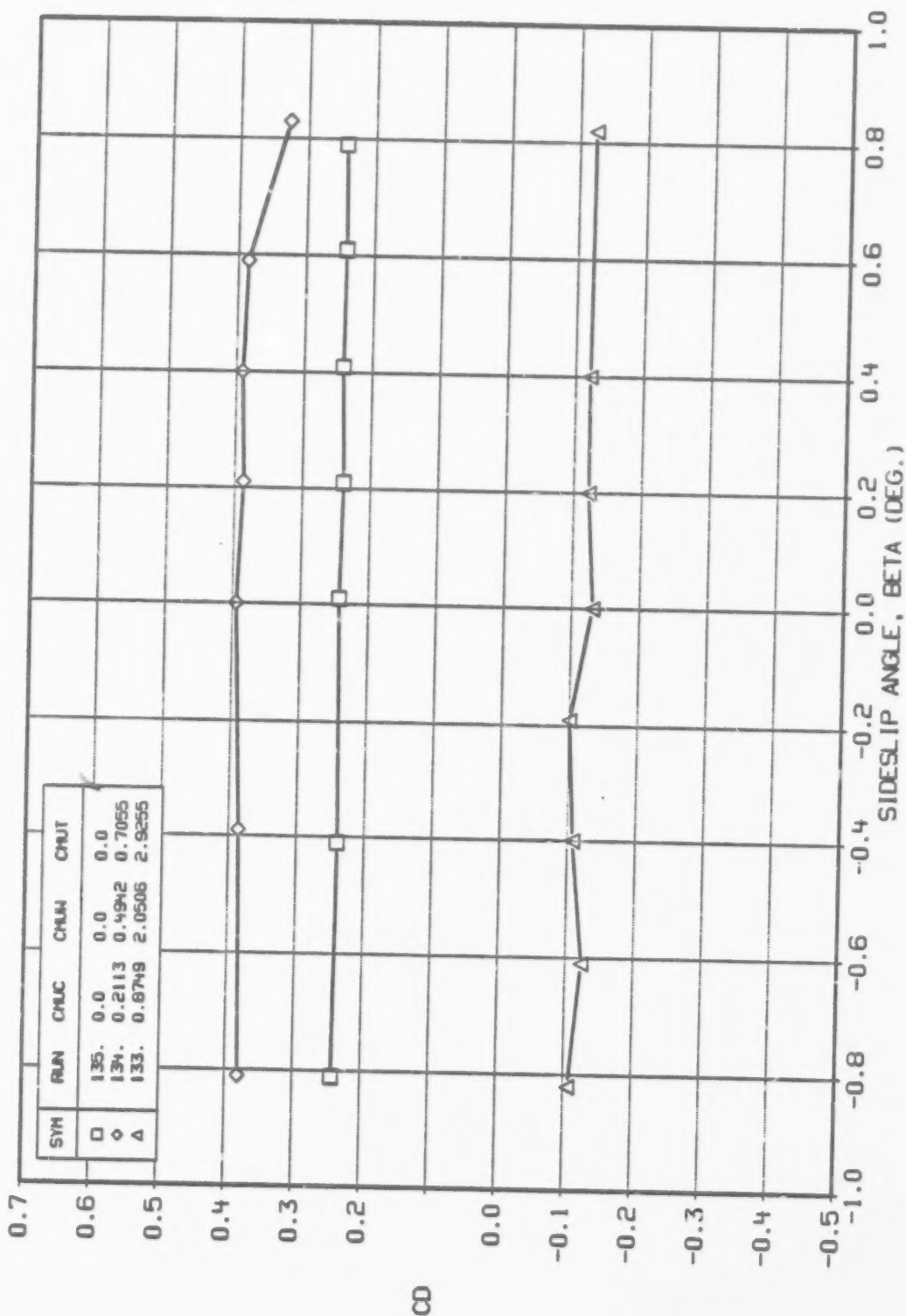


FIGURE A25b BASIC DATA EFFECT OF CMU
CONFIGURATION BMSV, BN/B=1.0, DELF=45, $\alpha = 2^\circ$

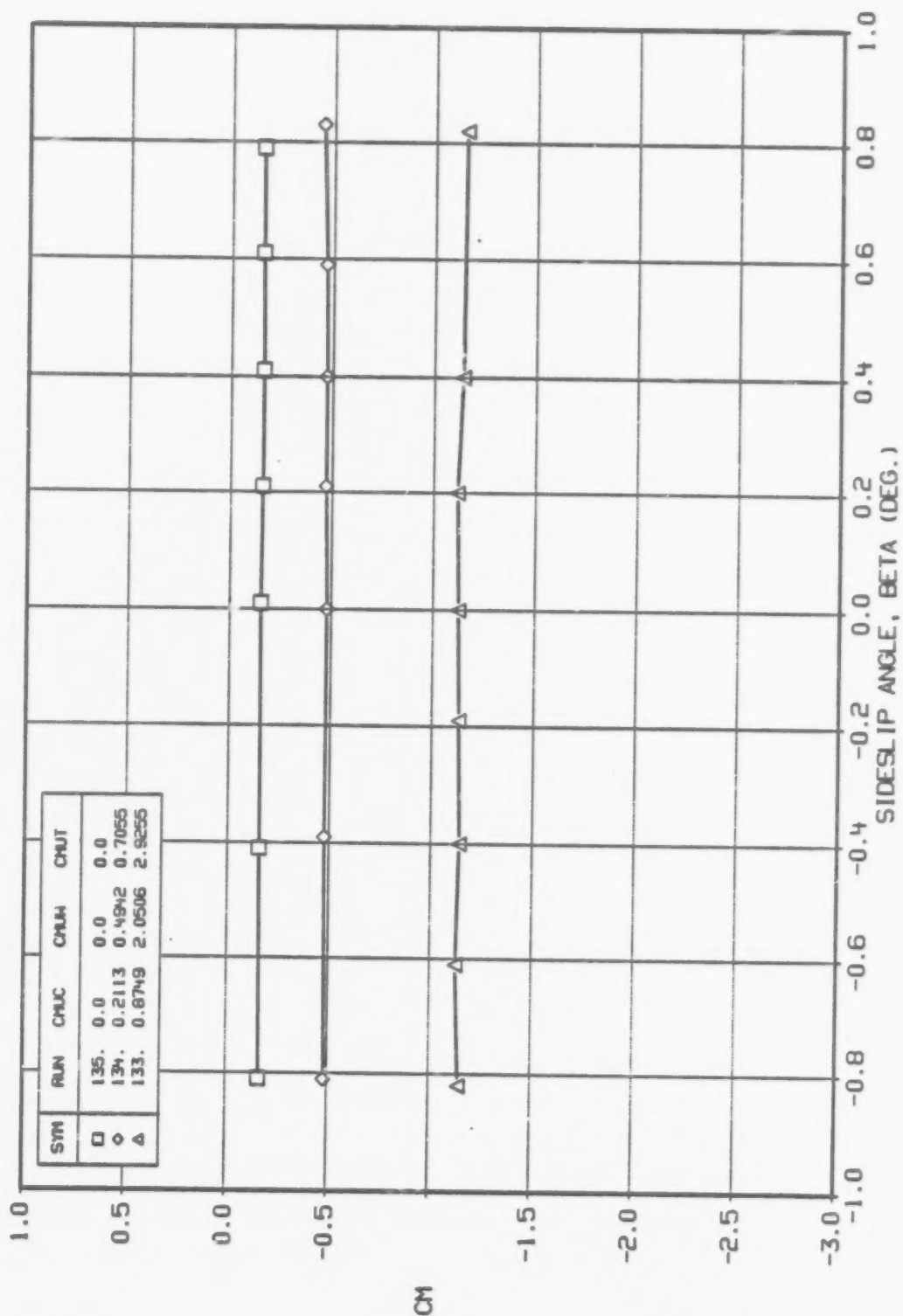


FIGURE A25c BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, BN/B=1.0, DELF=45, $\alpha = 2$

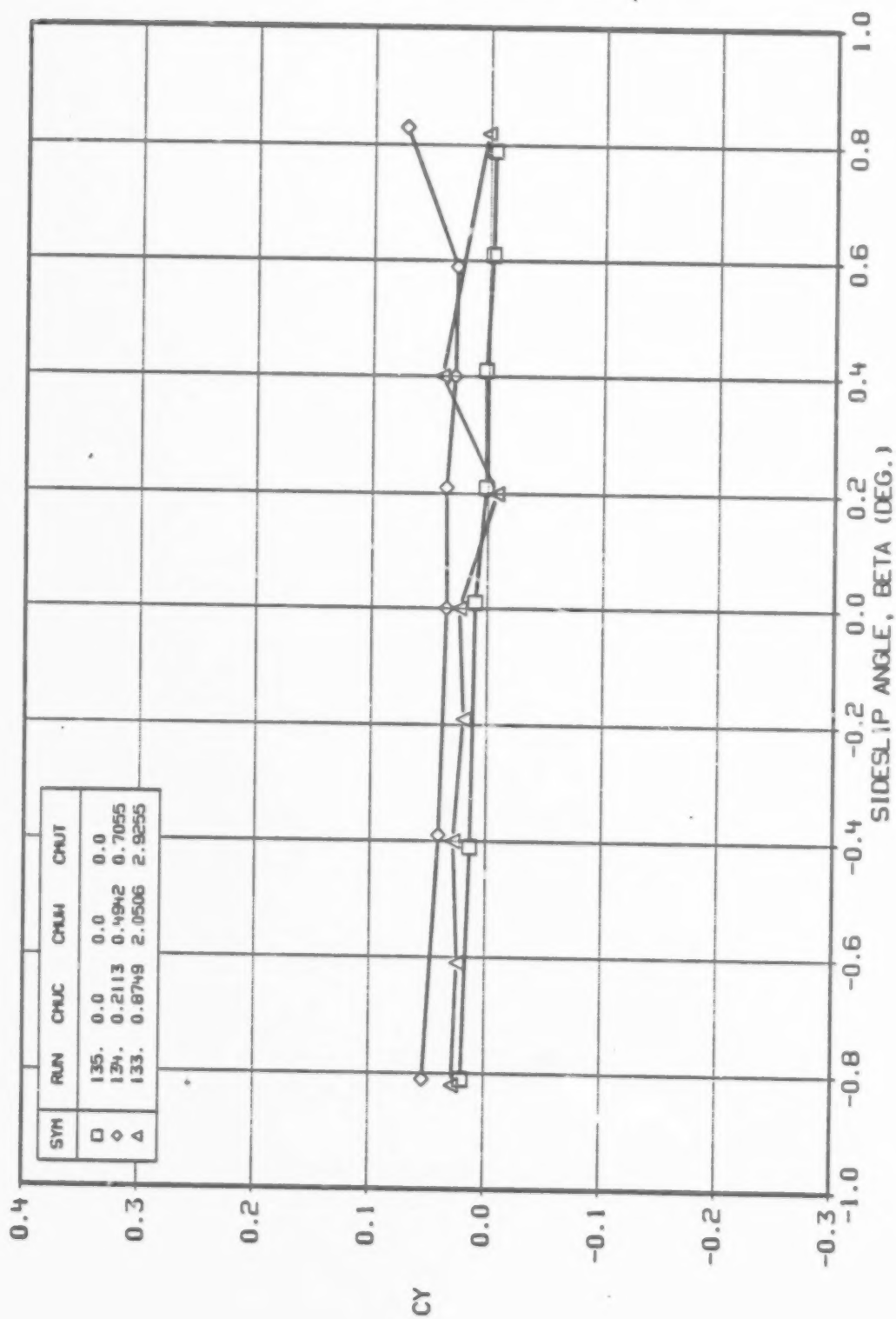


FIGURE A25d BASIC DATA EFFECT OF CHU
CONFIGURATION B46V, BN/B=1.0, DELF=45, a = 2

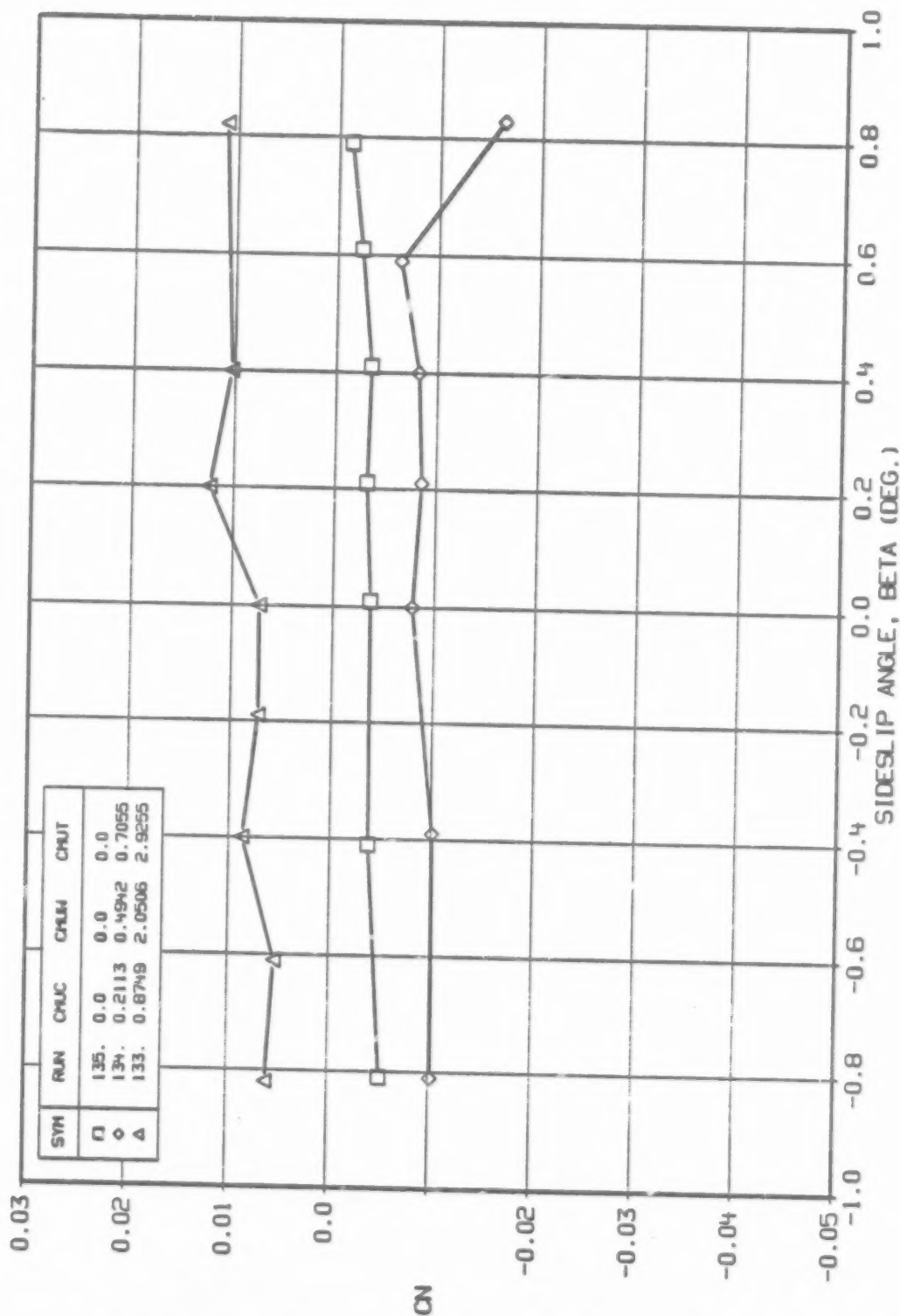


FIGURE A25c BASIC DATA EFFECT OF CHU
CONFIGURATION B45V, BN/B=1.0, DELF=45, $\alpha = 2$

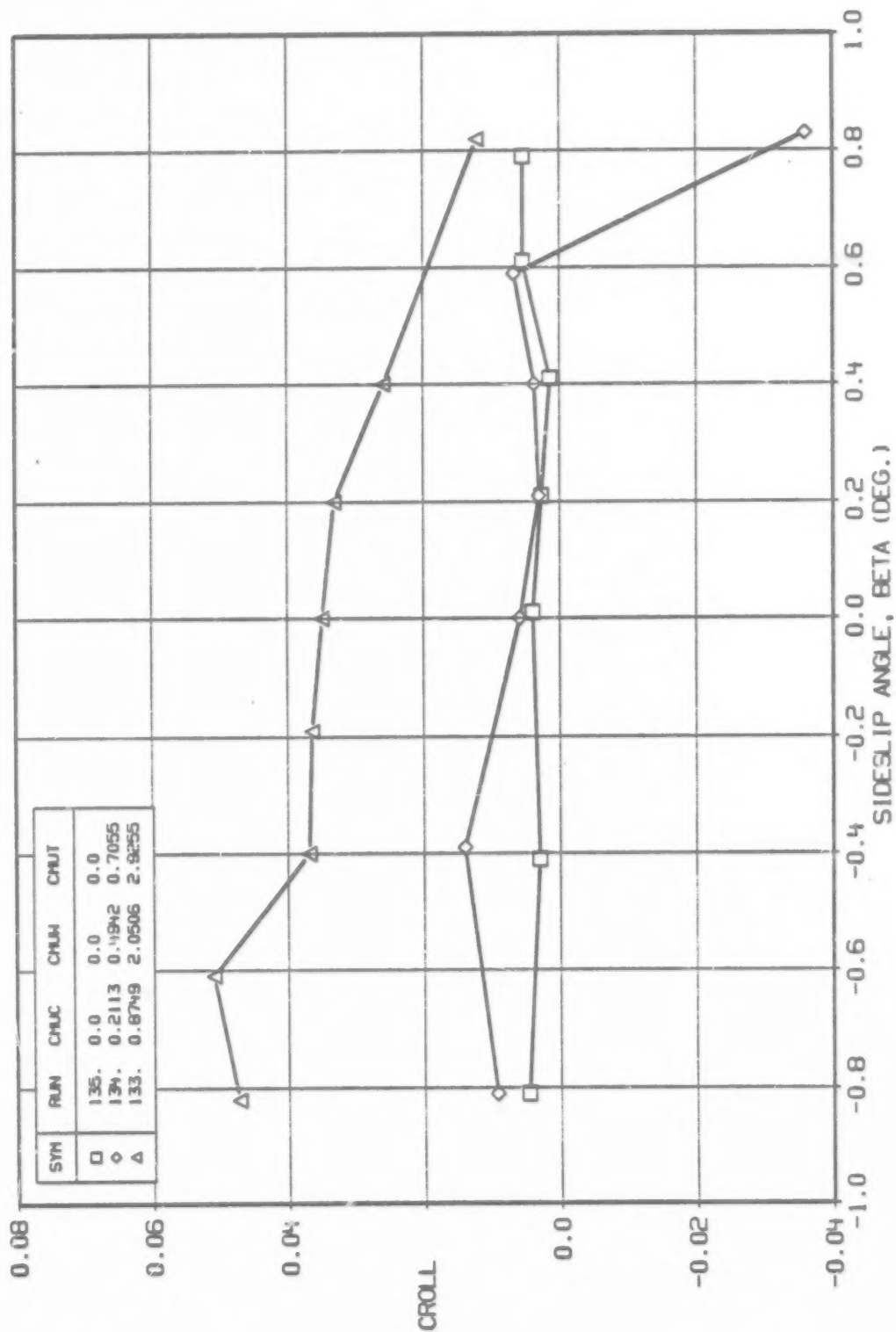


FIGURE A25f BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, BN/B=1.0, DELF=45, $\alpha = 2$

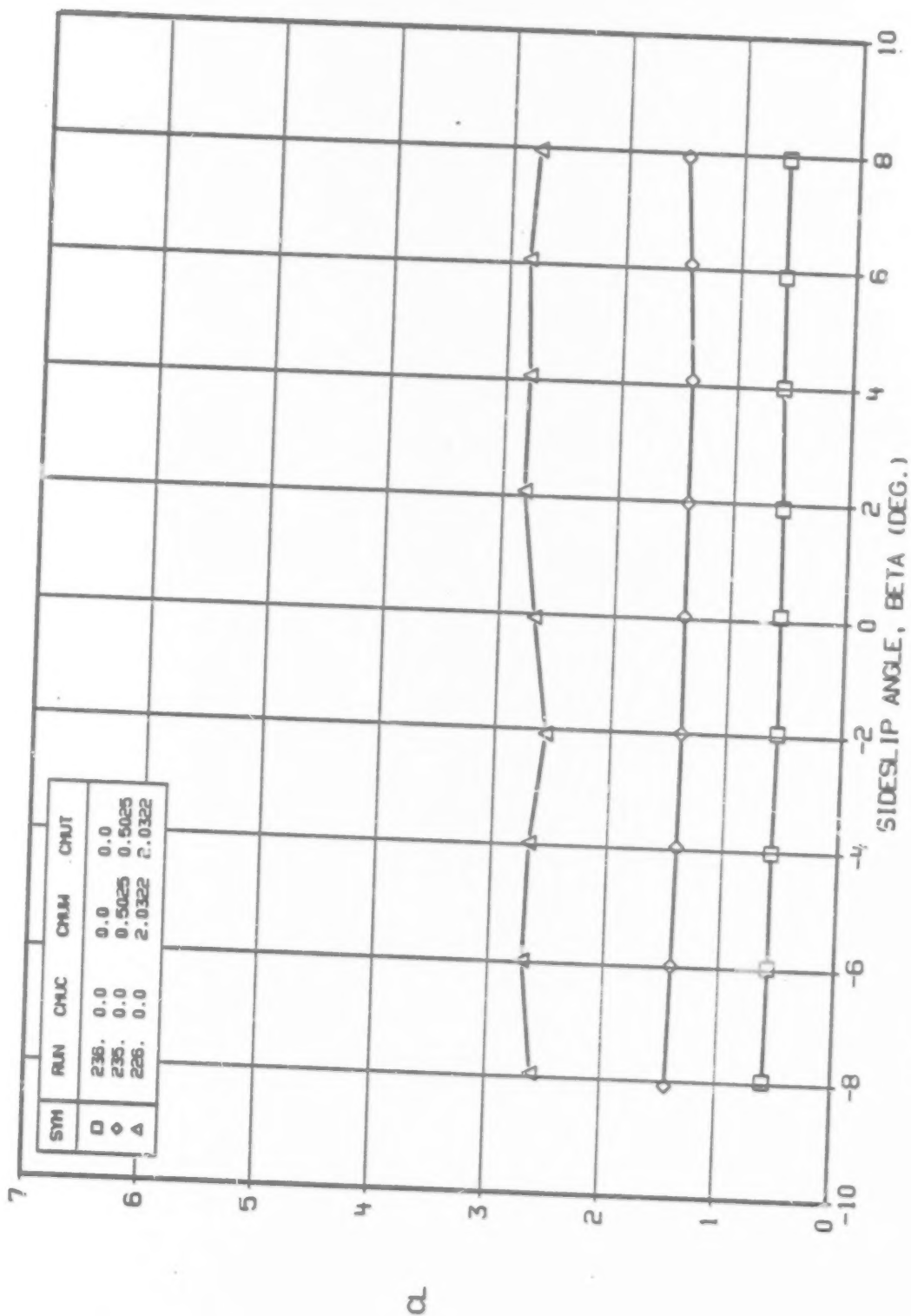


FIGURE A26a BASIC DATA EFFECT OF CHU
CONFIGURATION BHEV, BN/B=0.5 DELF=45

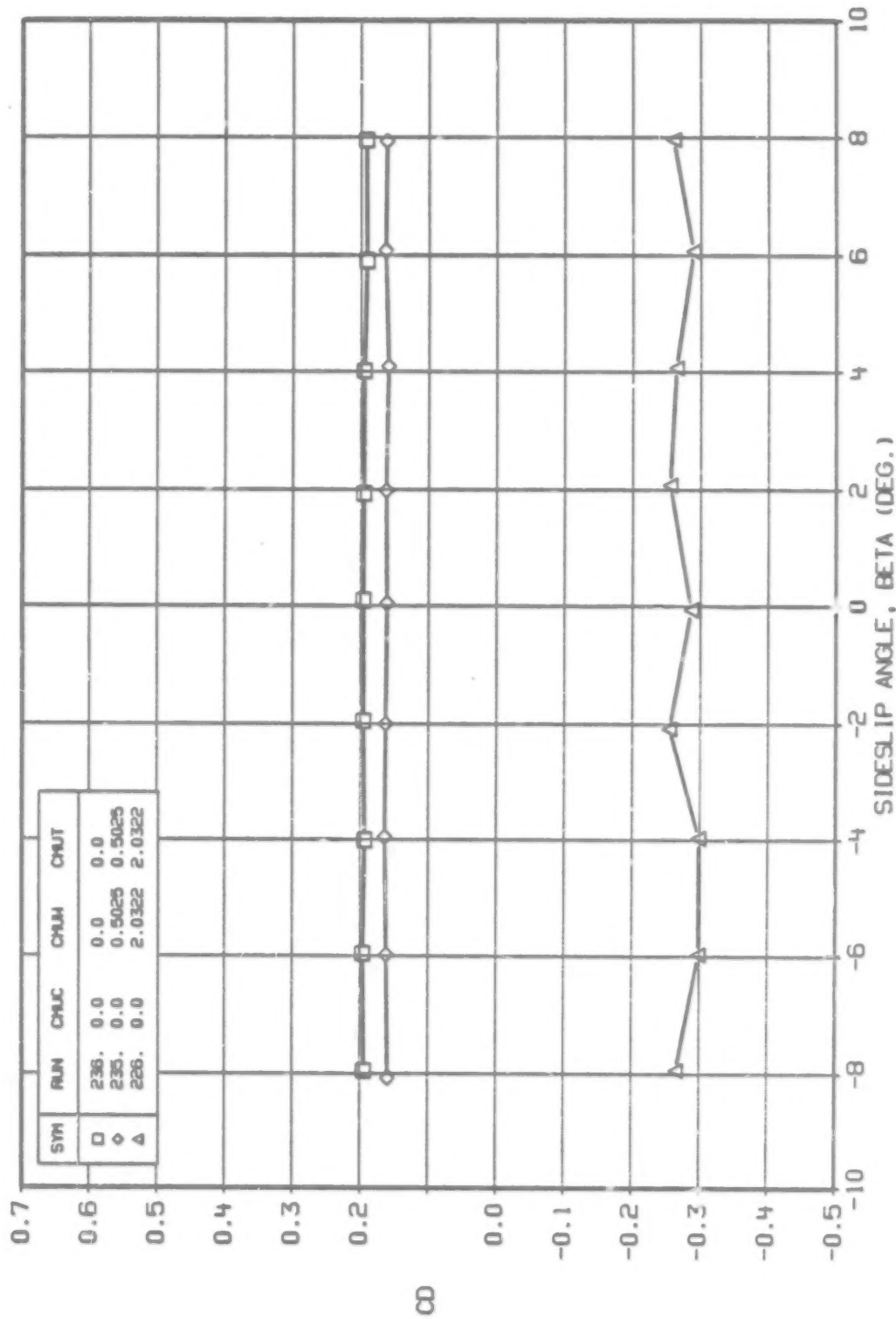


FIGURE A26b BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, BN/B=0.5 DELF=45

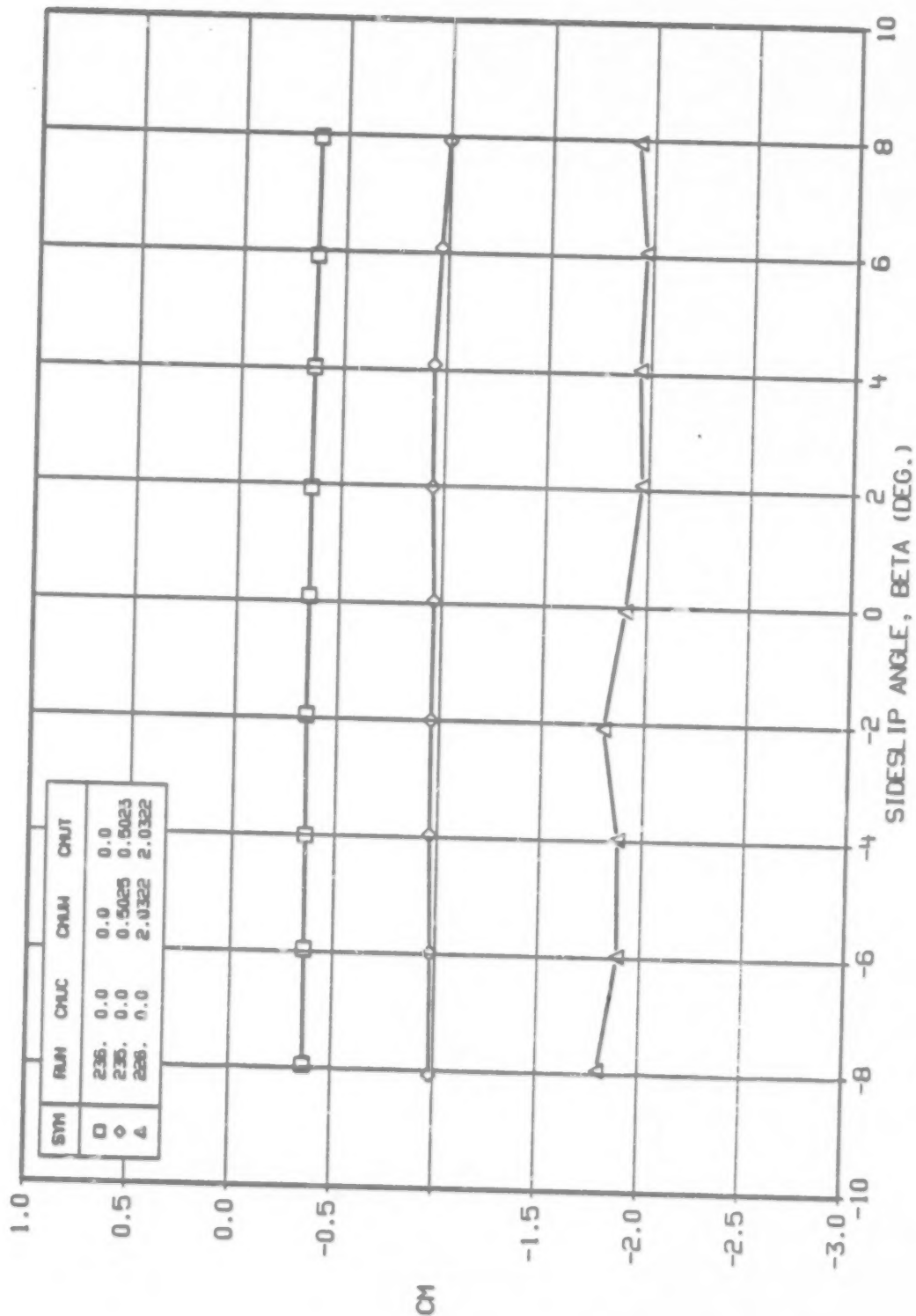


FIGURE A26c BASIC DATA EFFECT OF CMU
CONFIGURATION B45V, BN/B=0.5 DELF=45

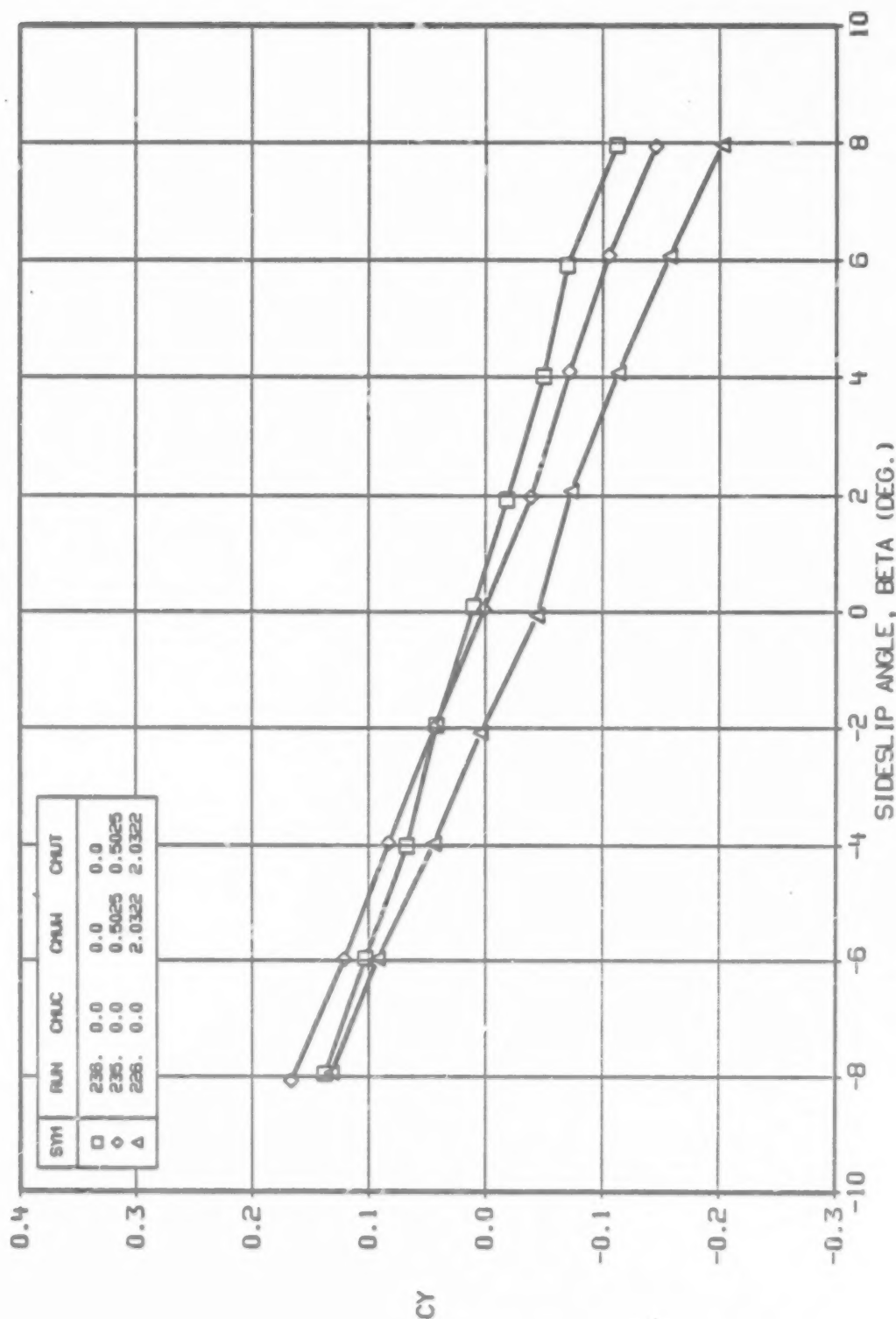


FIGURE A26d BASIC DATA EFFECT OF CMU
CONFIGURATION BASED, BN/B=0.5 DELF=45

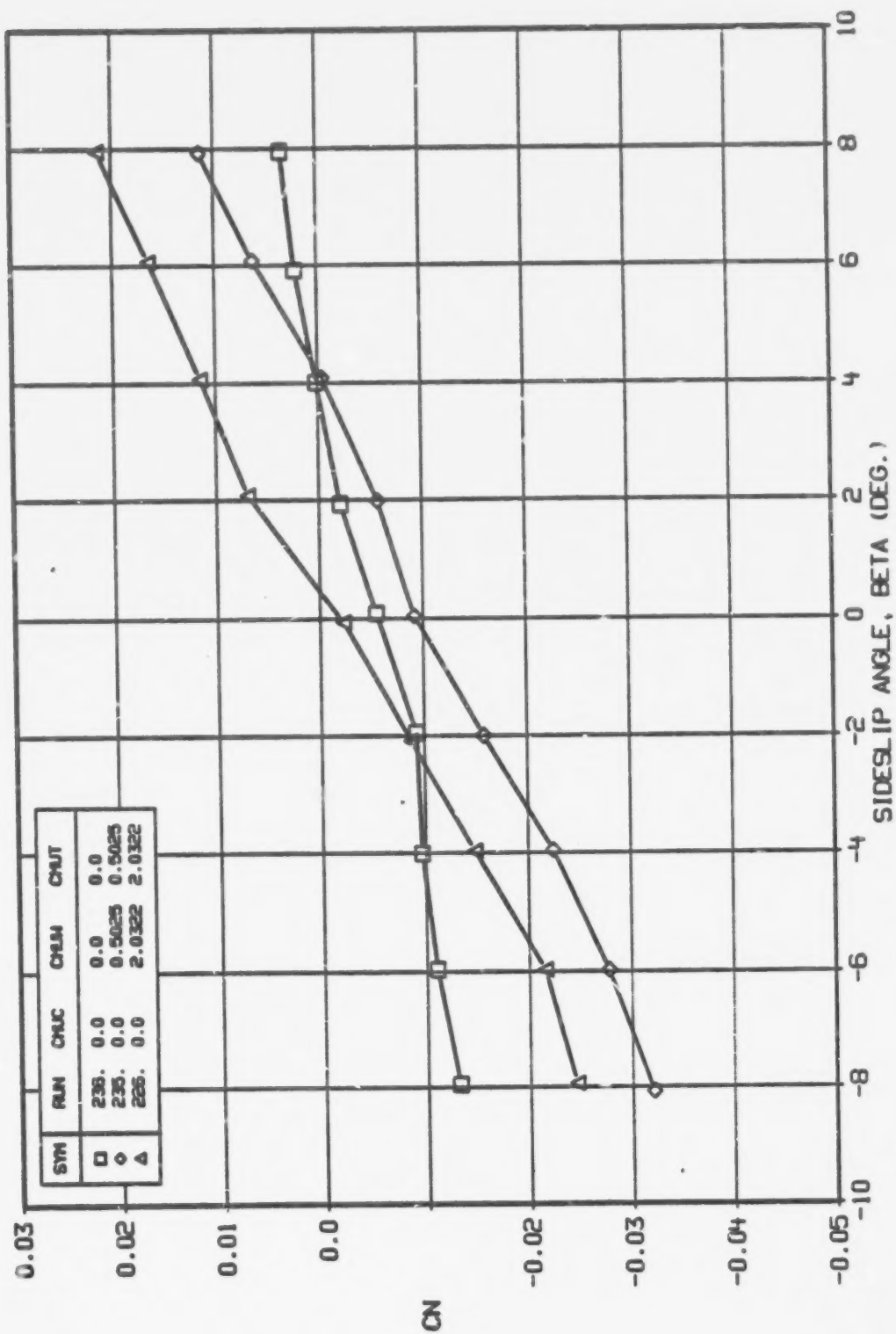


FIGURE A26e BASIC DATA EFFECT OF CMU
CONFIGURATION BN6V, BN/B=0.5 DELF=45

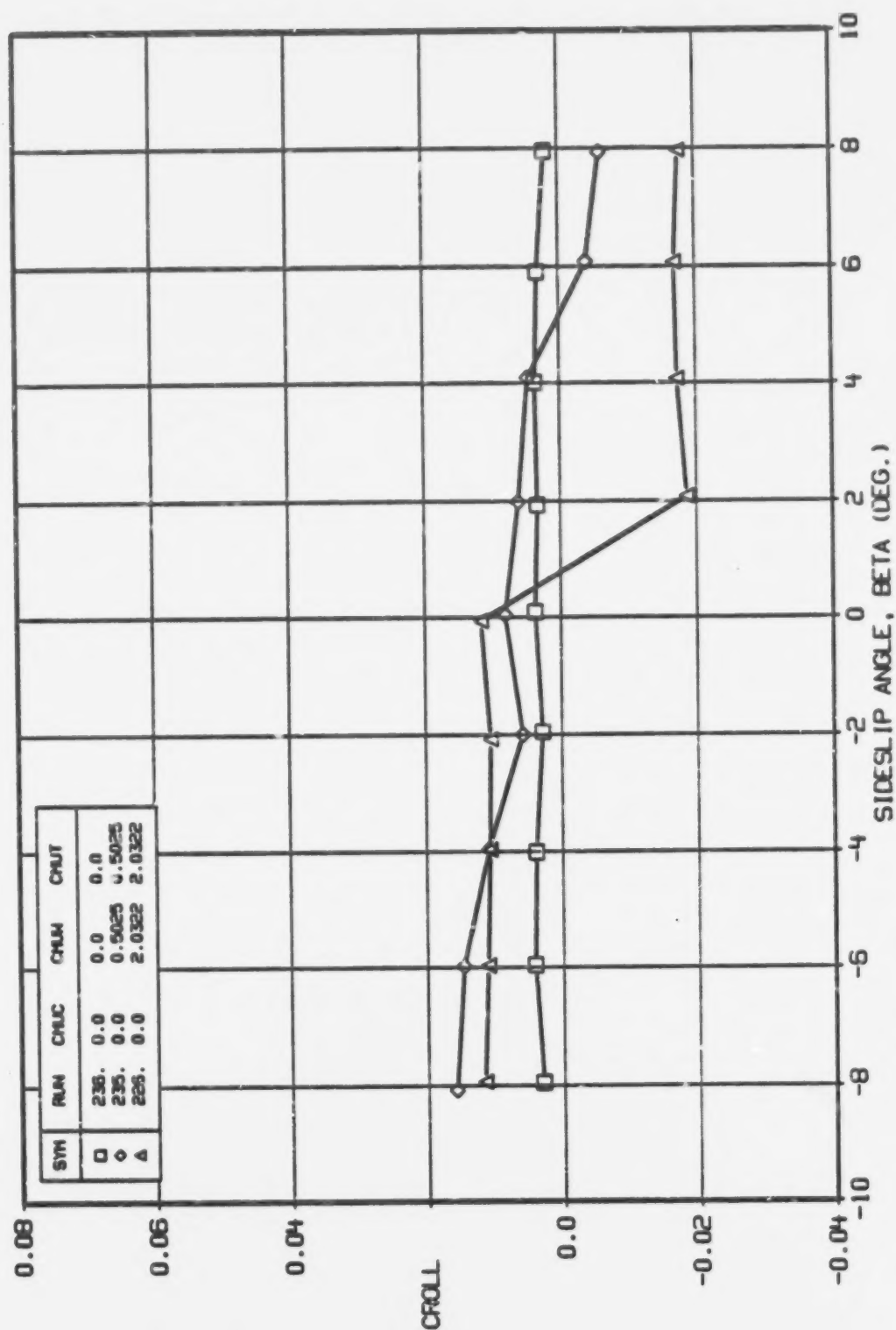


FIGURE A26f BASIC DATA EFFECT OF CMJ
CONFIGURATION BM6V, BN/B=0.5 DELF=45

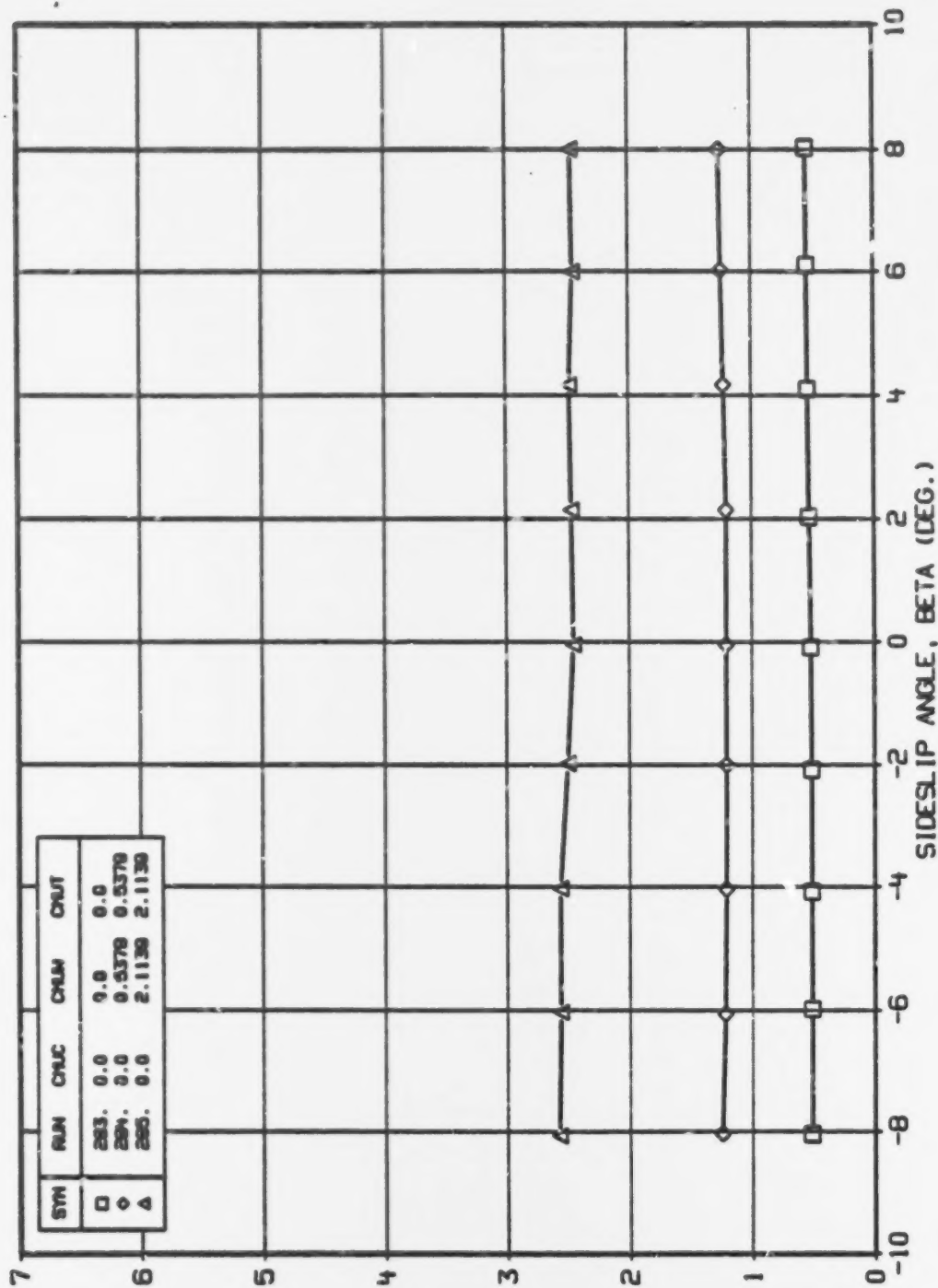


FIGURE A27a BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, DELF=45, BN/B=.25

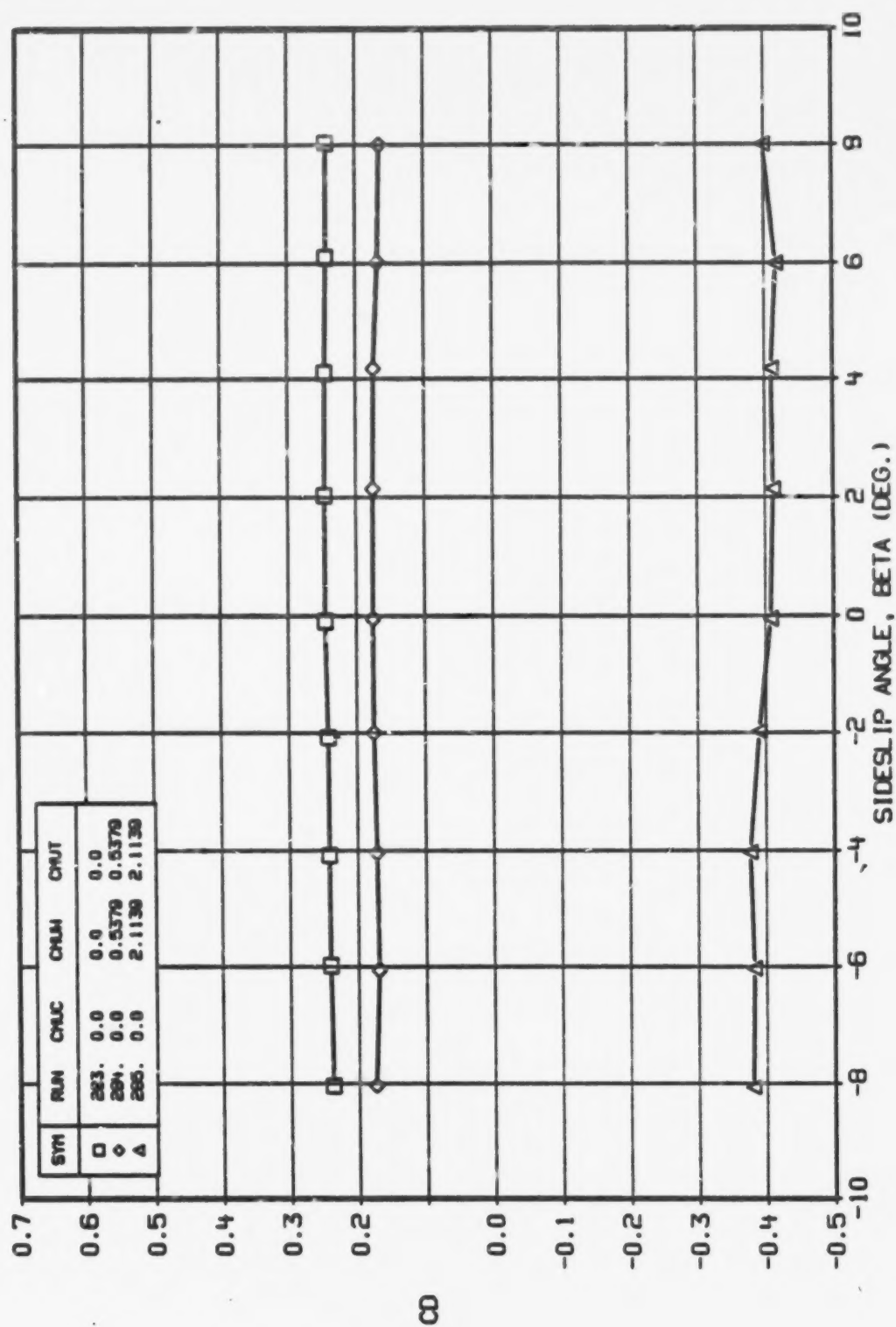


FIGURE A27b BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, DELF=45, BN/B=.25

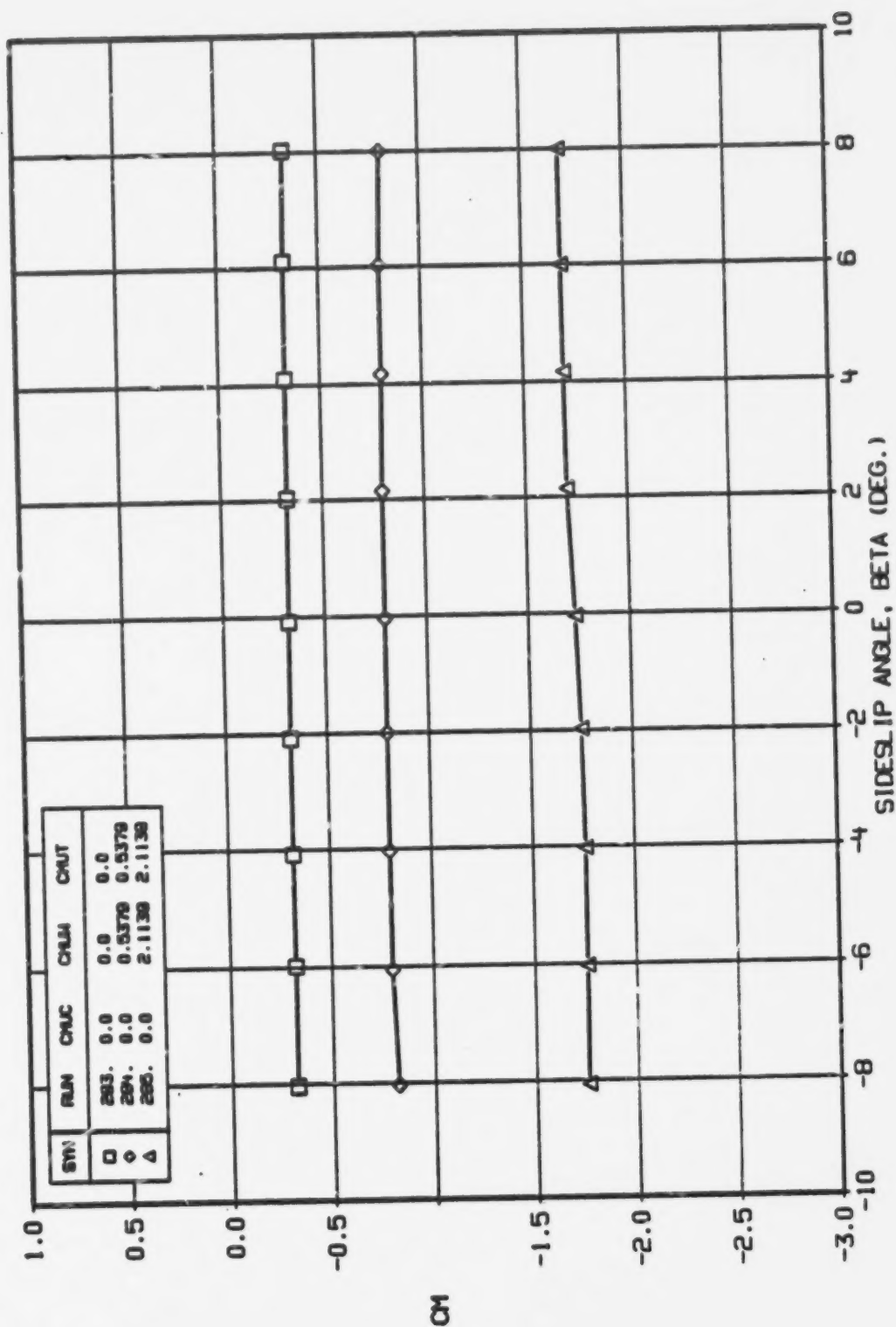


FIGURE A27c BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, DELF=, BN/B=.25

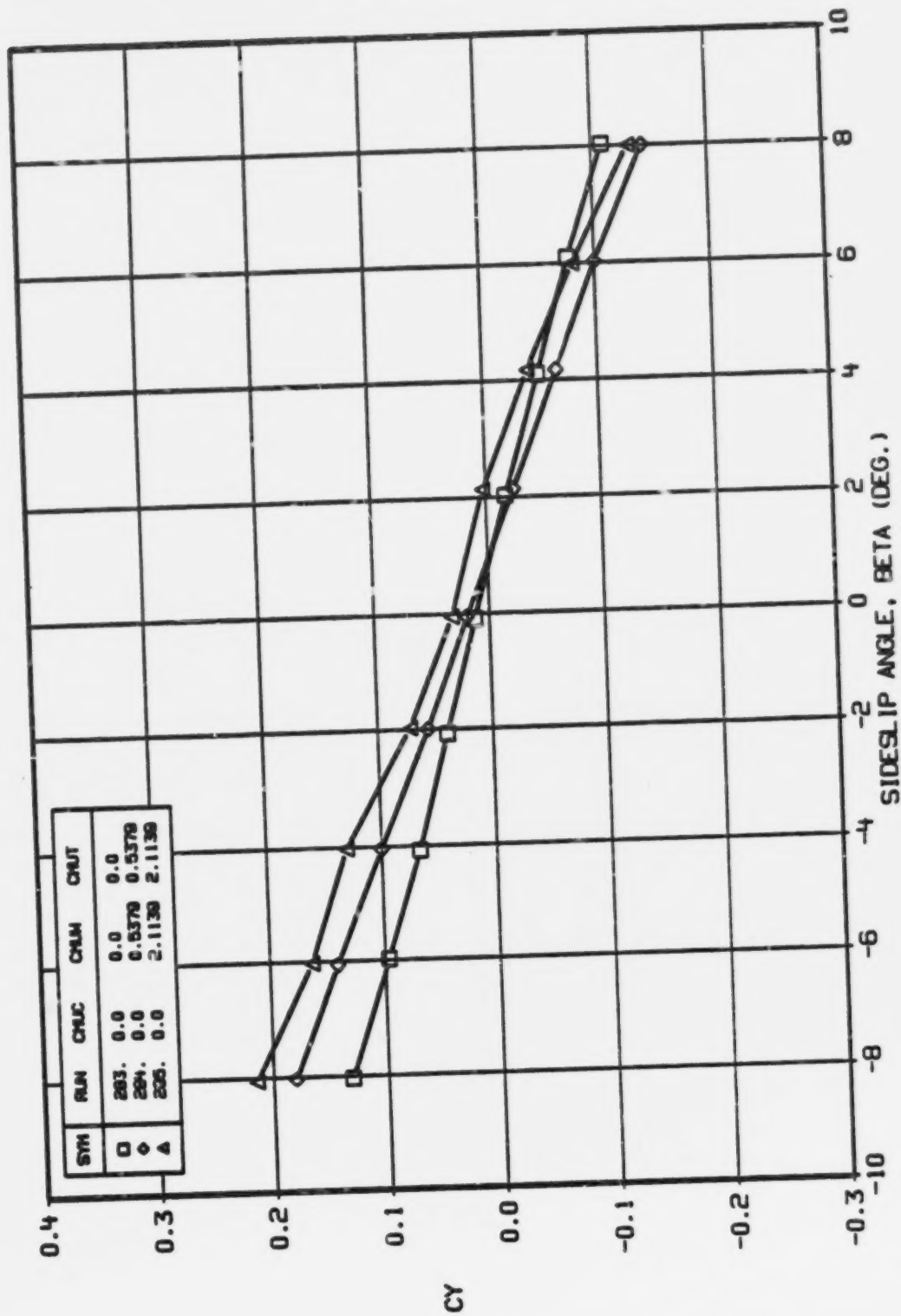


FIGURE A27d BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, DELF=45, EN/B=.25

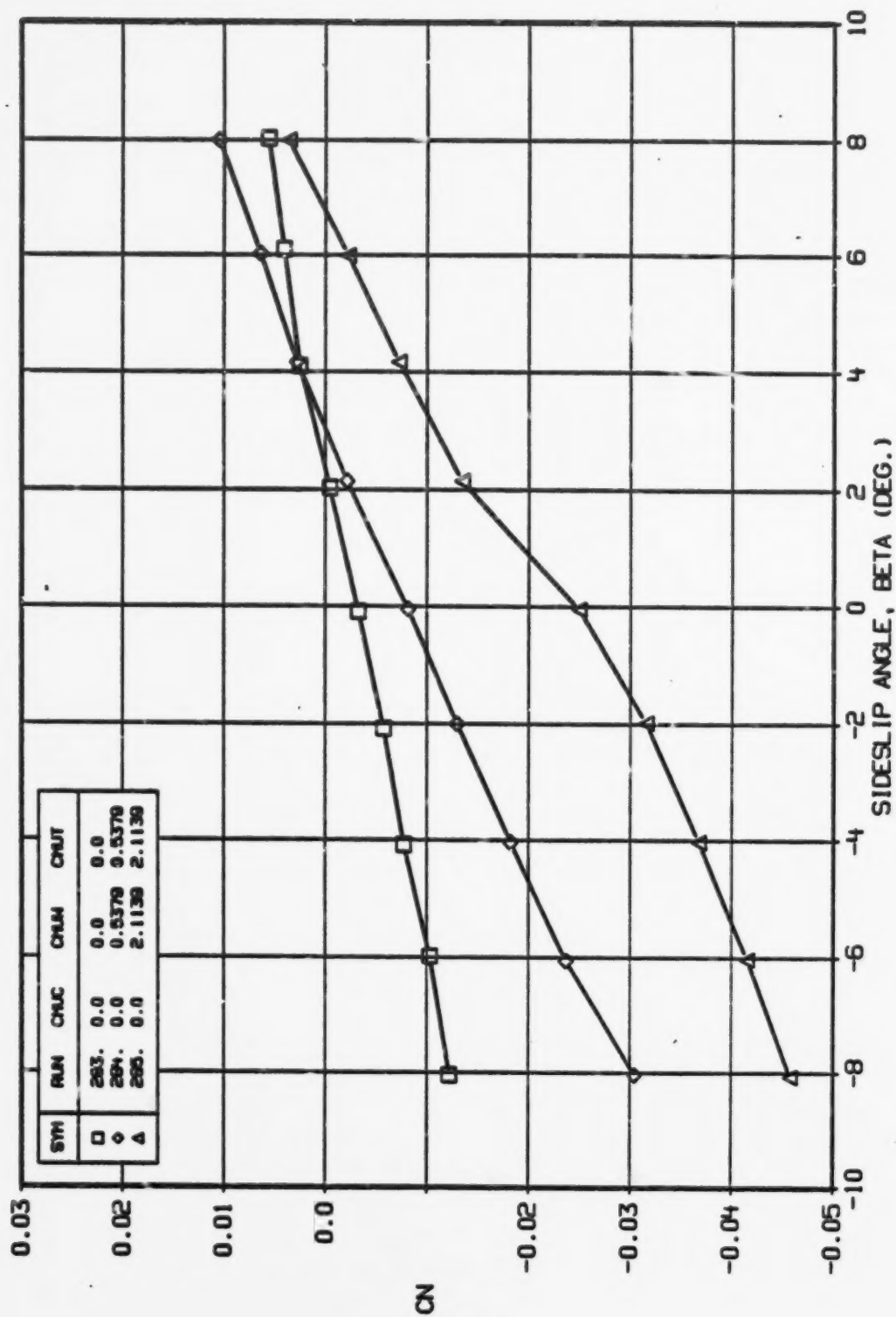


FIGURE A27e BASIC DATA EFFECT OF CMU
CONFIGURATION B45V, DELF=45, BN/B=.25

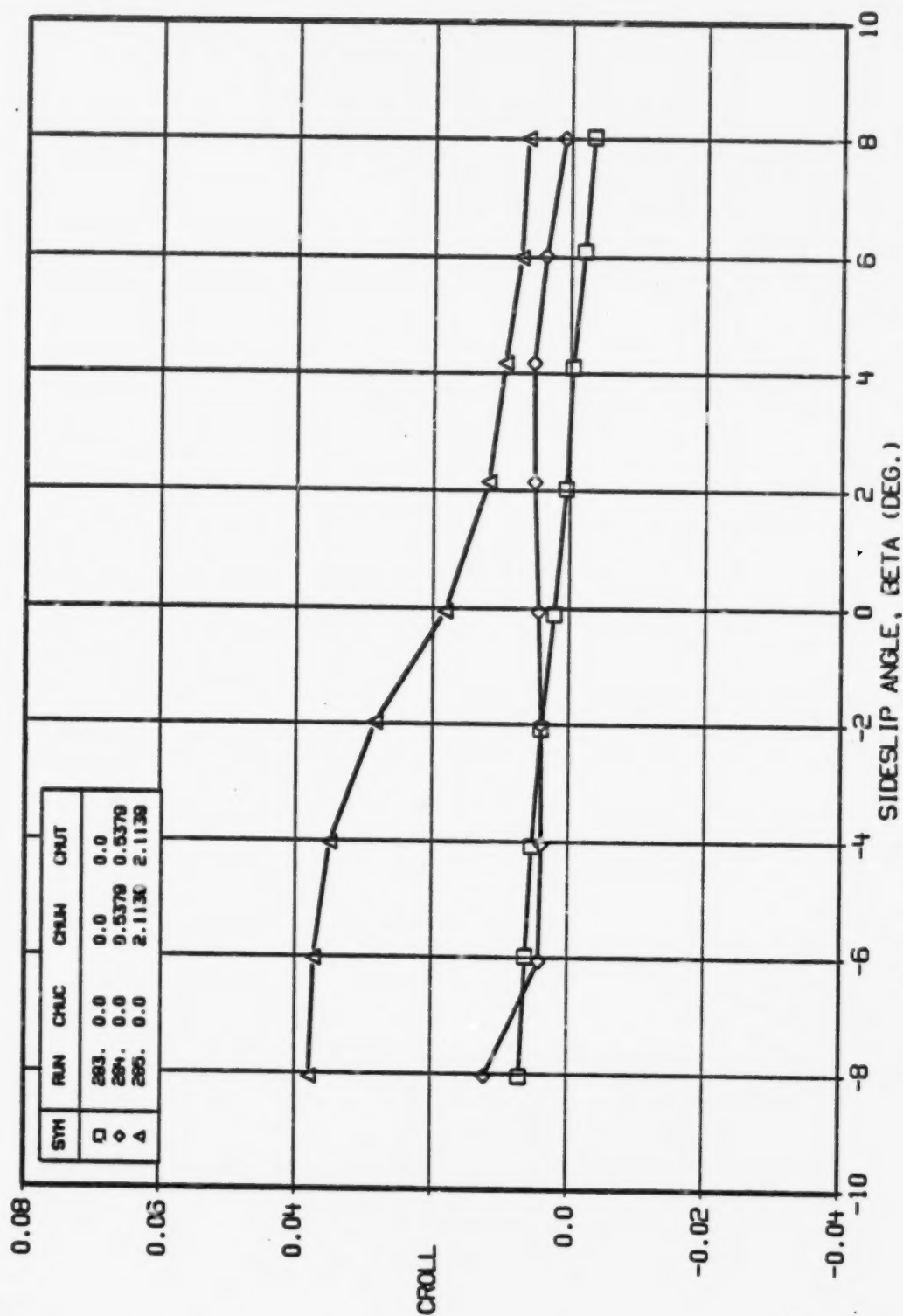


FIGURE A27f BASIC DATA EFFECT OF CMU
CONFIGURATION BW6V, DELF=45, BN/B=.25

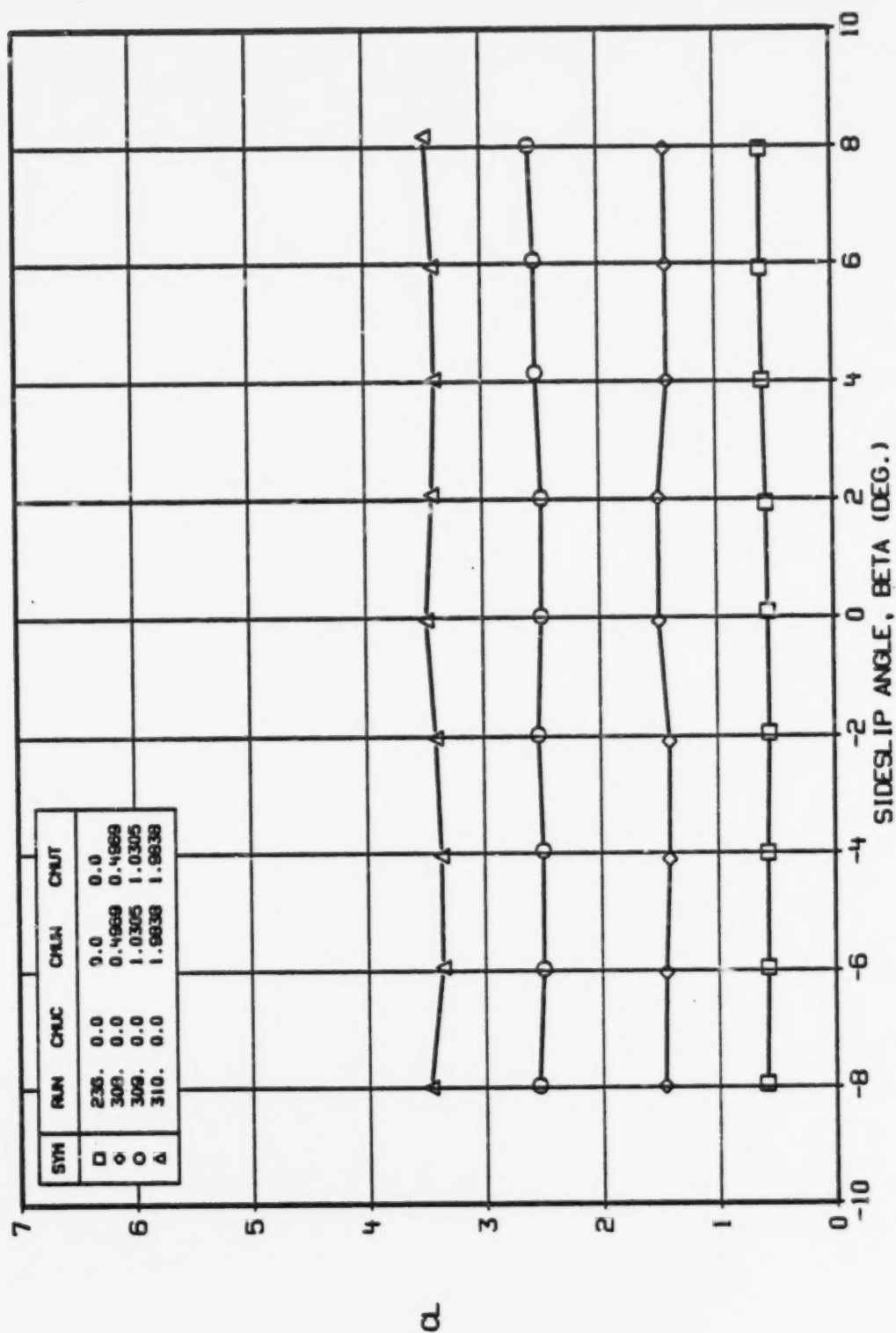


FIGURE A28a BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, DELF=45, BN/B=1

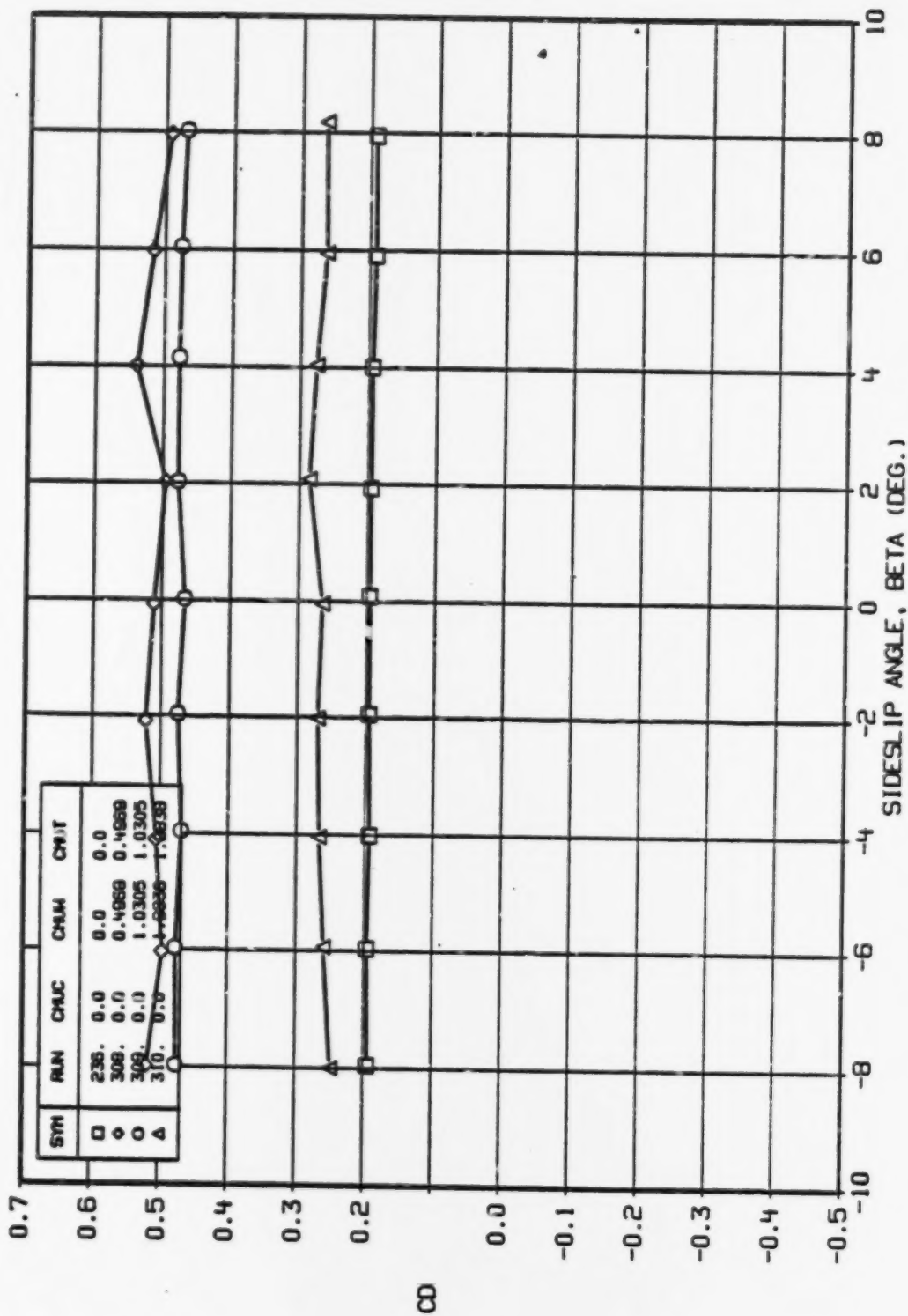


FIGURE A28b BASIC DATA EFFECT OF CMU
CONFIGURATION RM6V, DELF=45, BN/B=1

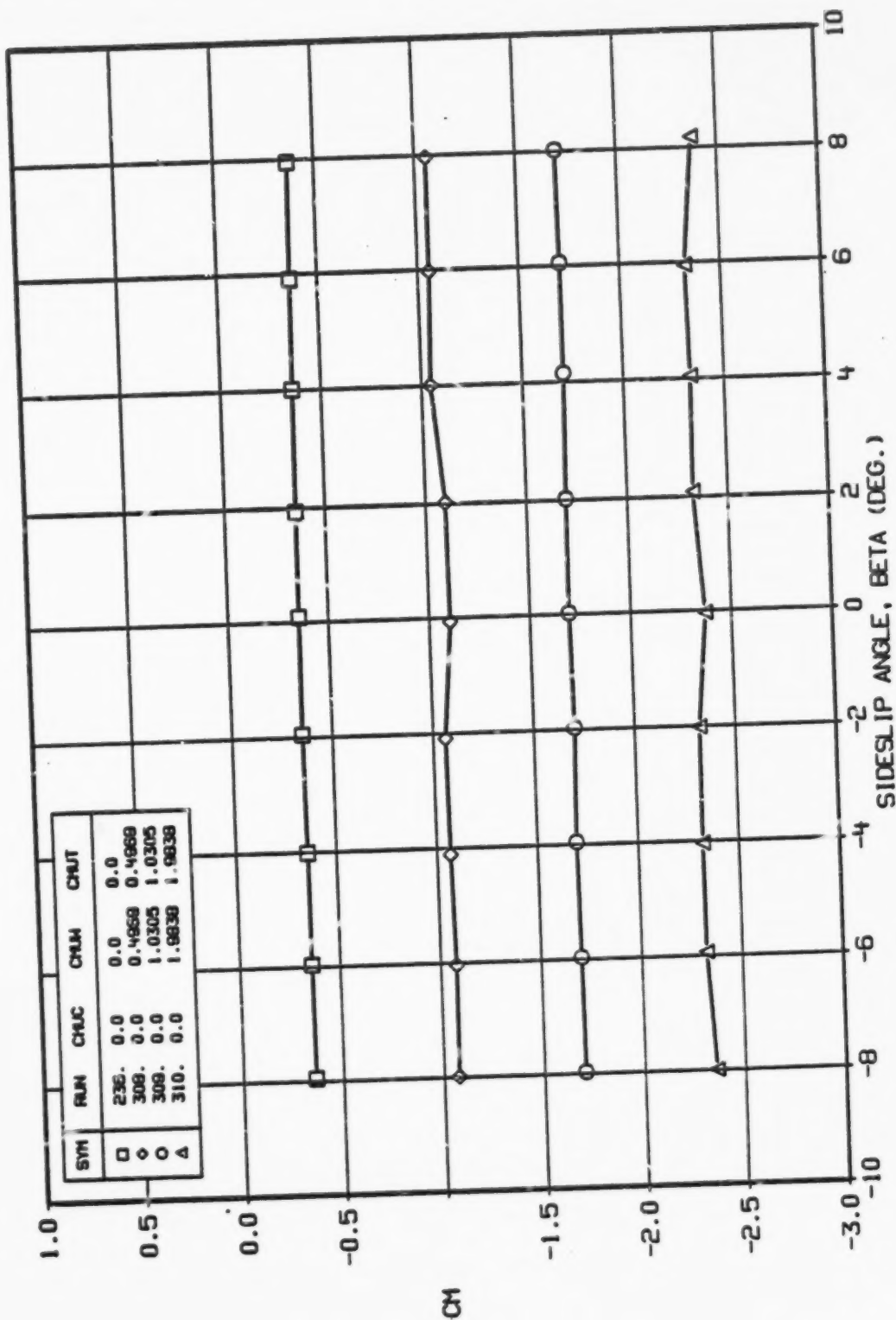


FIGURE A28c BASIC DATA EFFECT OF CMU
CONFIGURATION BM6V, DELF=45, BN/B=1

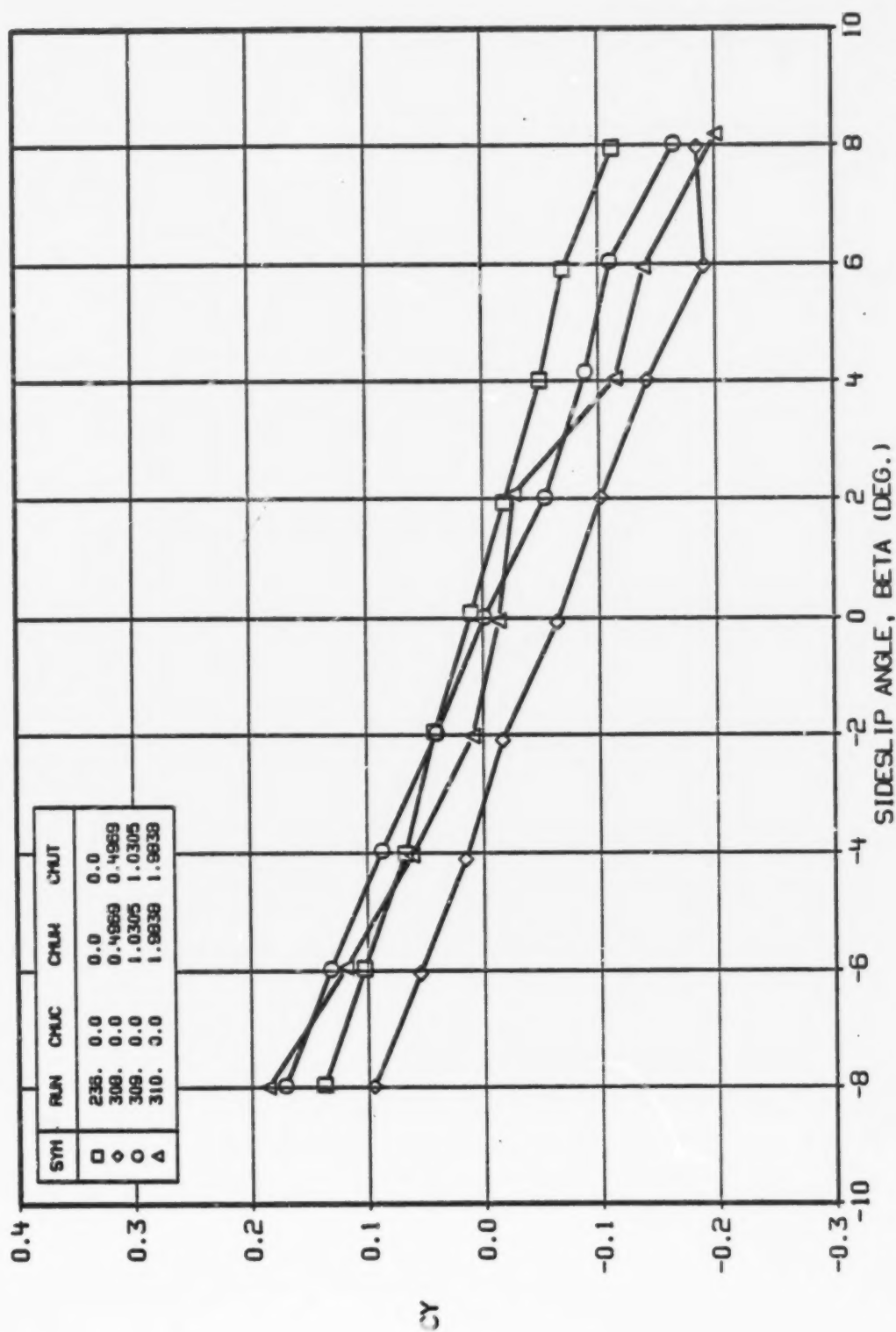


FIGURE A28d BASIC DATA EFFECT OF CMU
CONFIGURATION BMSV, DELF=45, BN/B=1

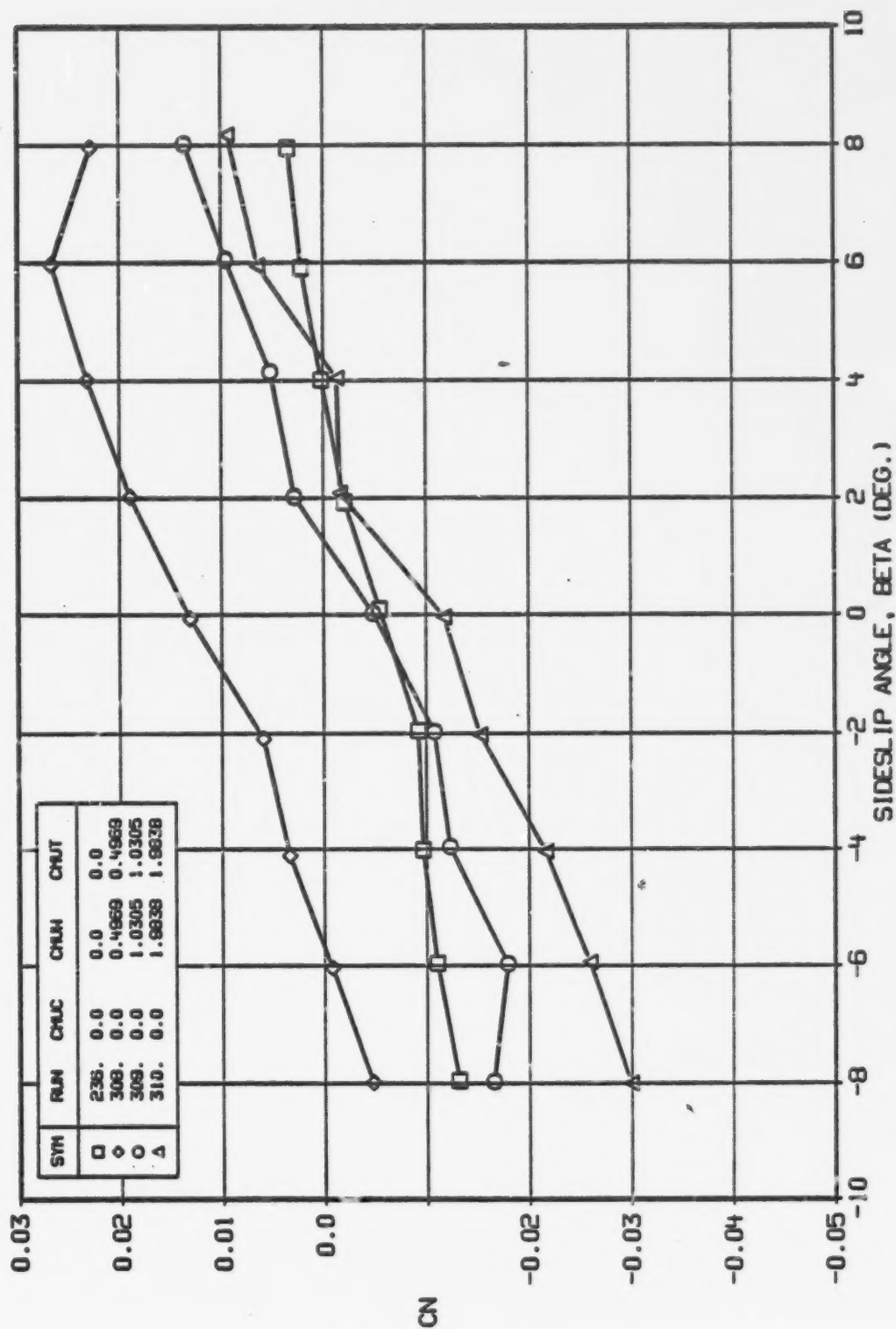


FIGURE A28e BASIC DATA EFFECT OF CMU
CONFIGURATION BMSV, DELF=45, BN/B=1

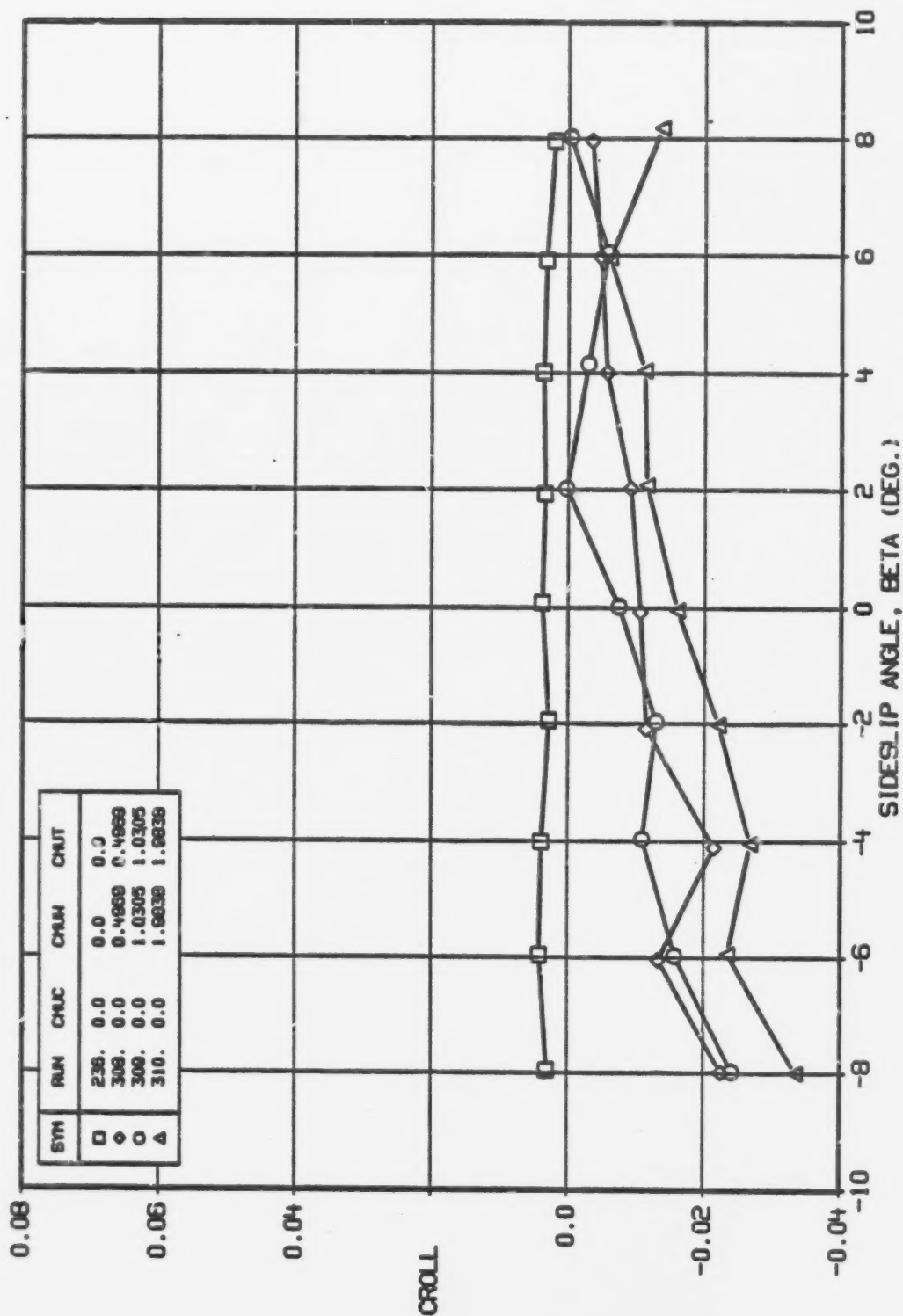


FIGURE A28f BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, DELF=45, BN/B=1

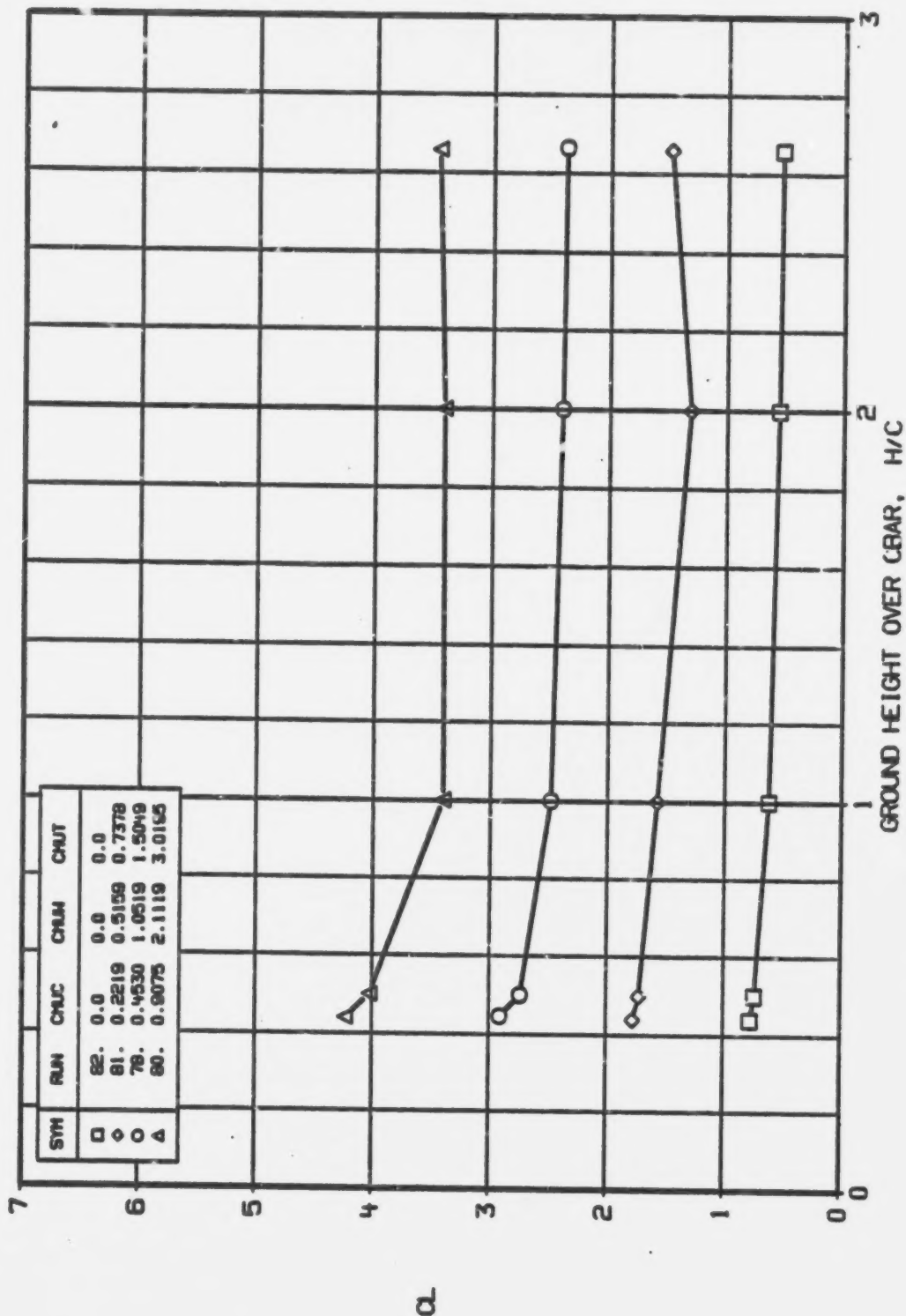


FIGURE A29a BASIC DATA EFFECT OF CMU
CONFIGURATION BC1W5V, DELF=45, BN/B=1

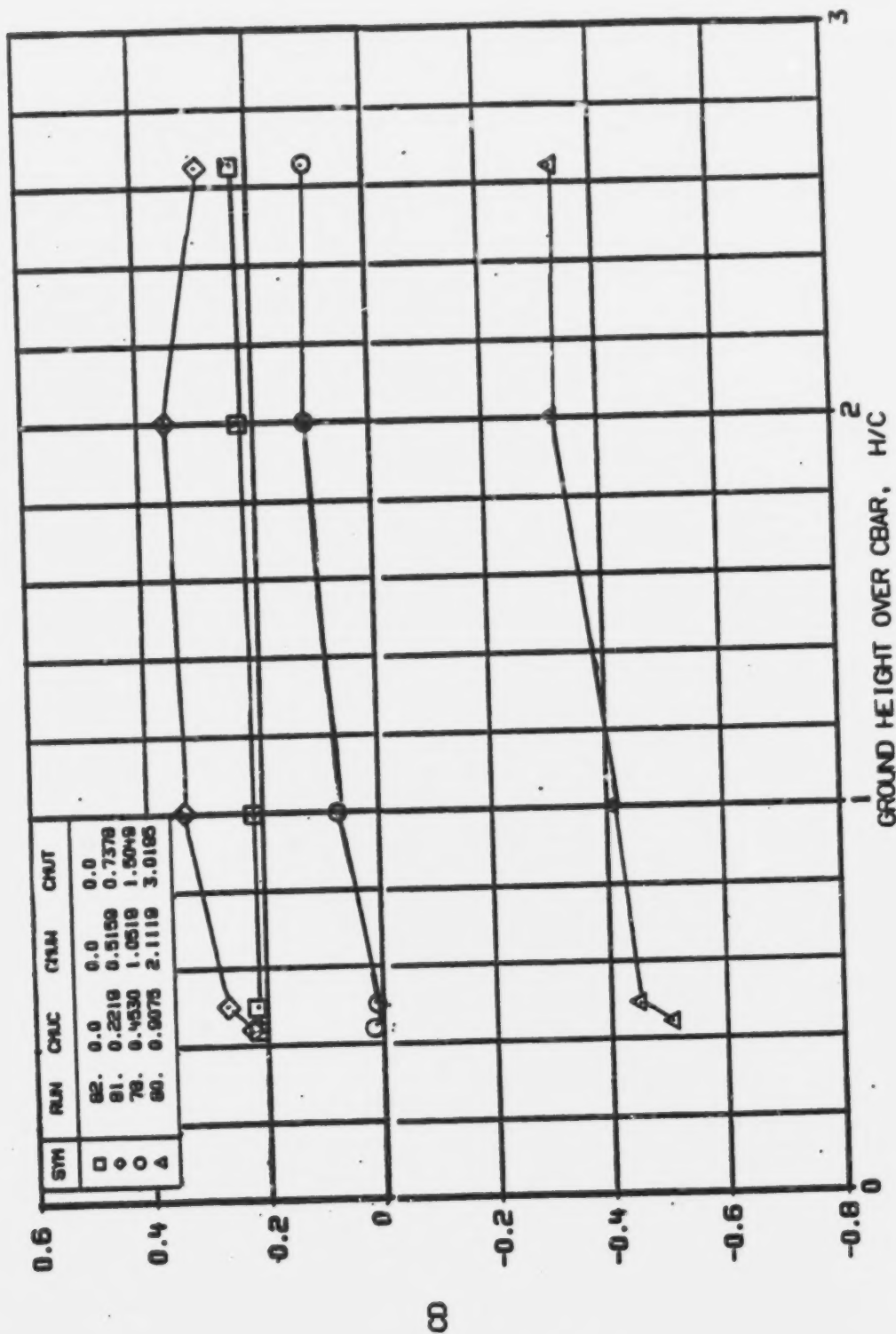


FIGURE A29b BASIC DATA EFFECT OF CMU
CONFIGURATION BC1W6V, DELF=45, BN/B=1

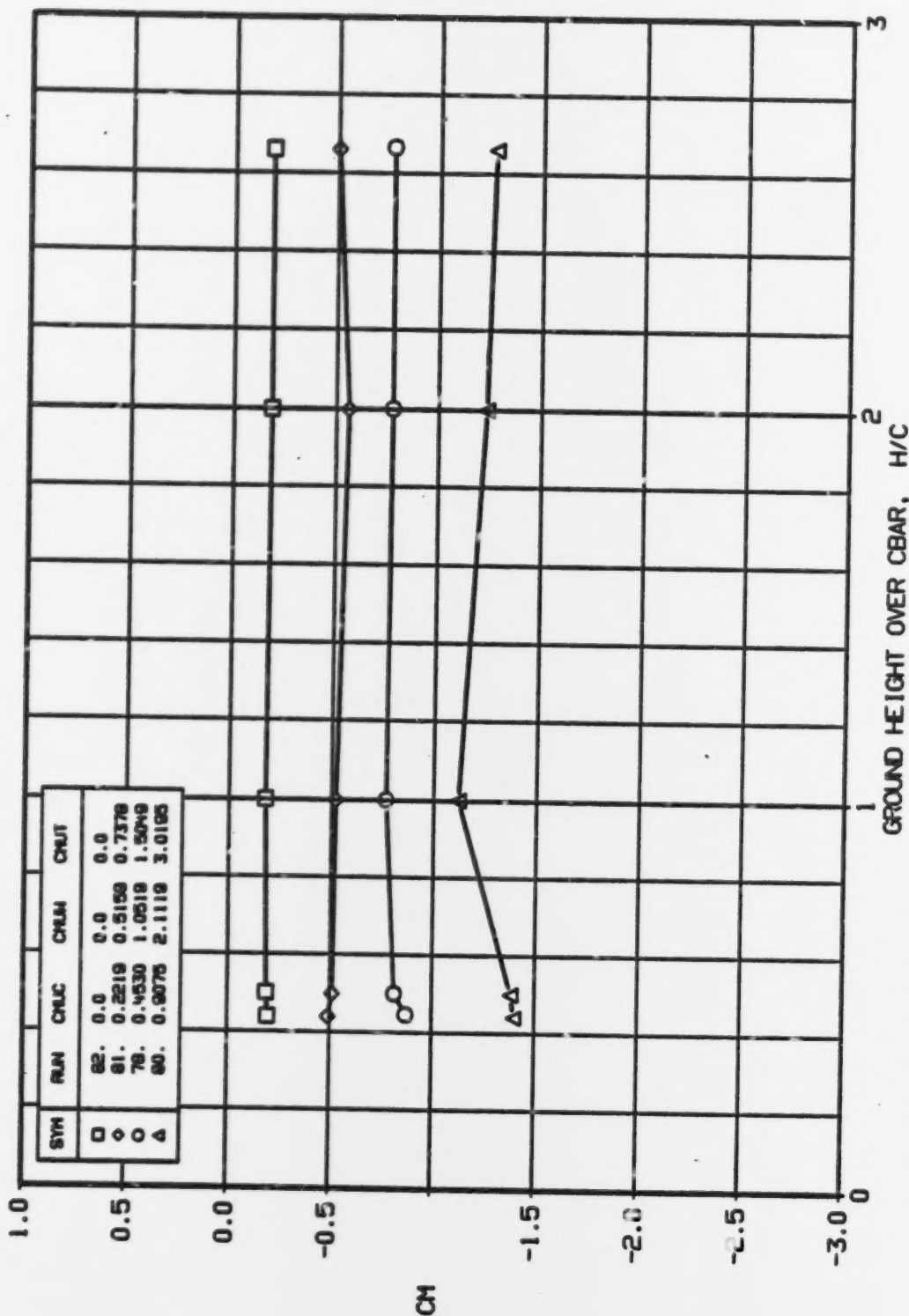


FIGURE A29c BASIC DATA EFFECT OF CMU
CONFIGURATION BC1W6V, DELF=45, BM/B=1

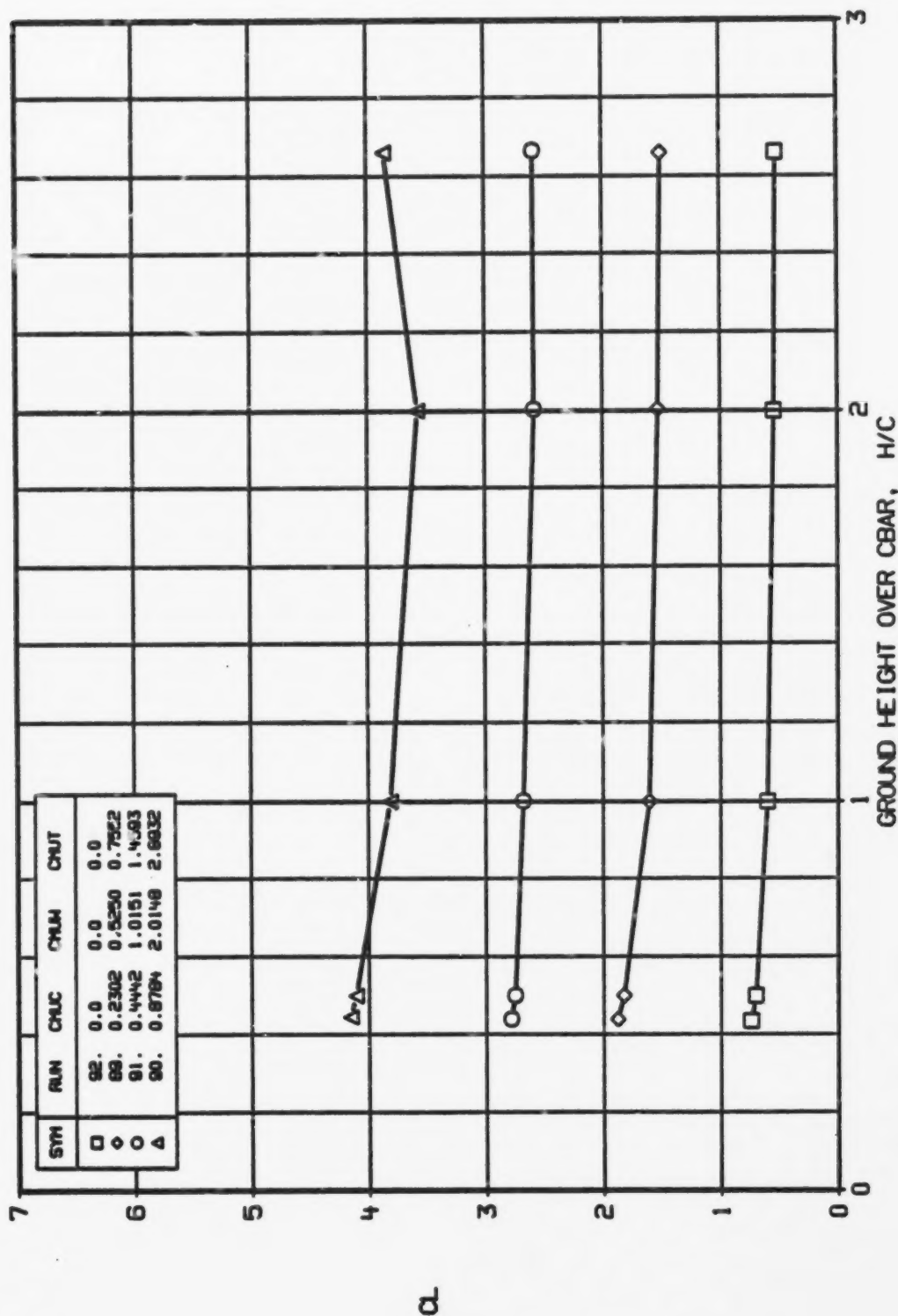


FIGURE A30a BASIC DATA EFFECT OF CMU
CONFIGURATION BC2WSV, DELF=45, BN/B=1

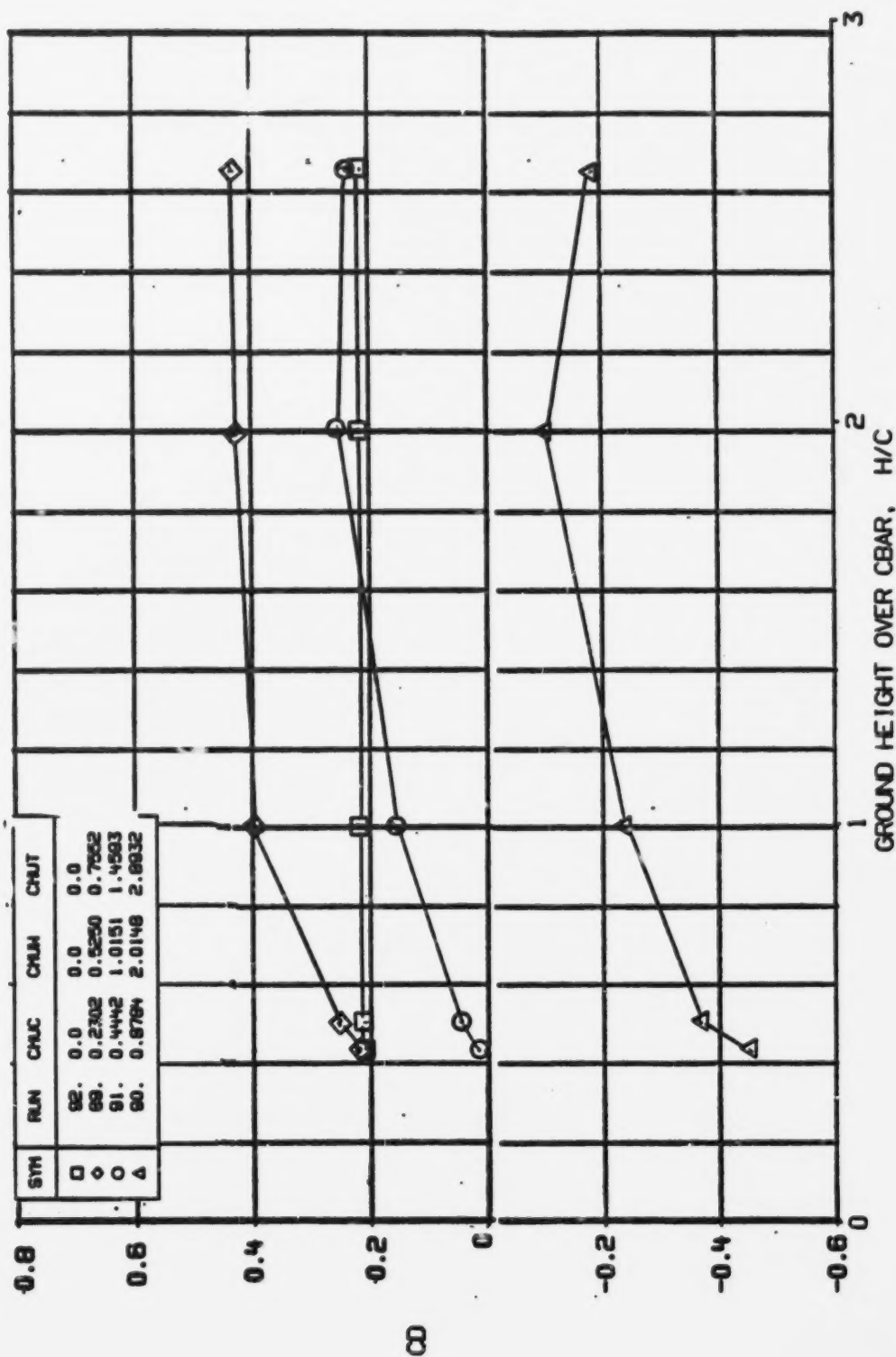


FIGURE A30b BASIC DATA EFFECT OF CMU
CONFIGURATION BC246V, DELF=45, BM/B=1

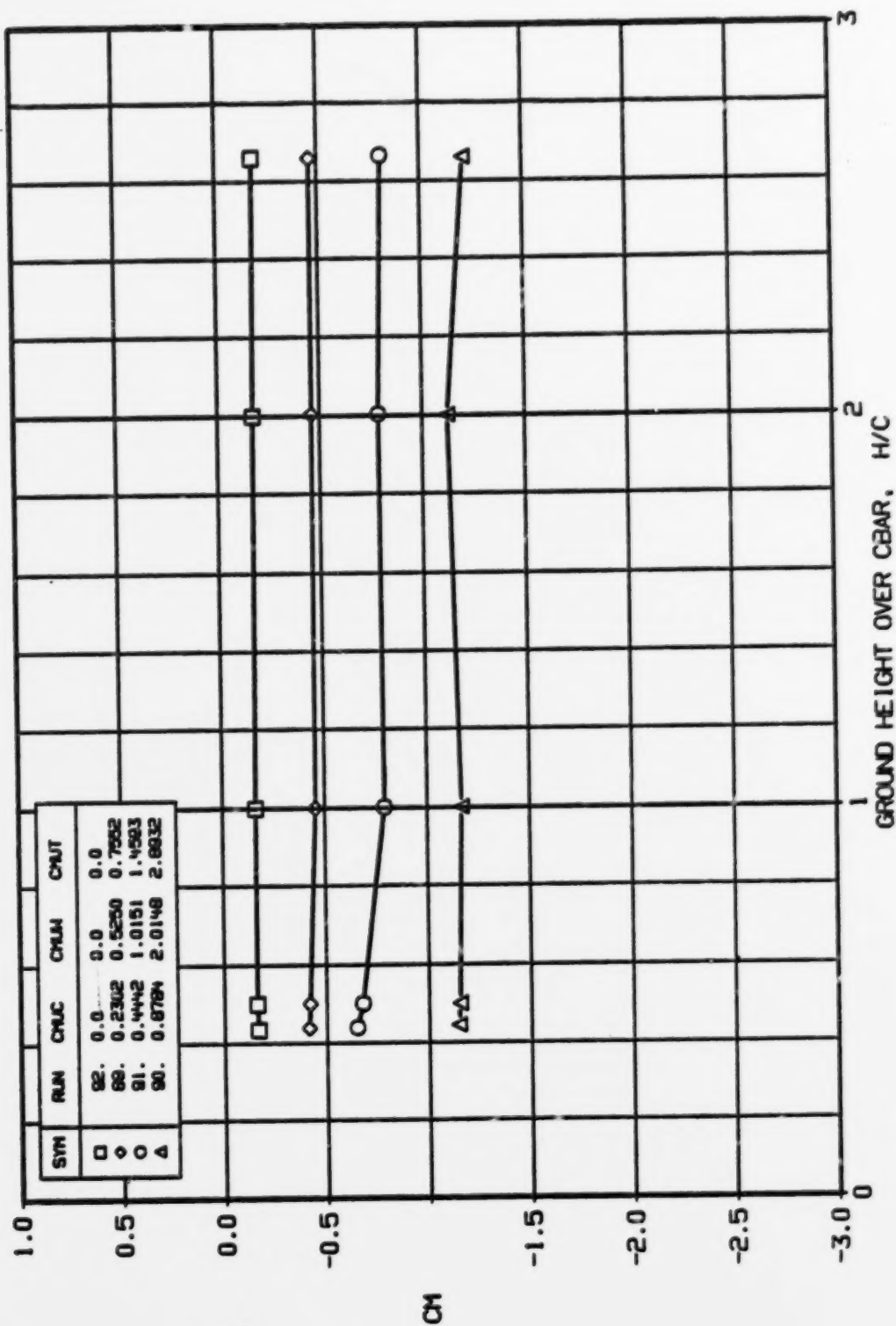


FIGURE A30c BASIC DATA EFFECT OF CHU
CONFIGURATION BC246V, DELF=45, BM/B=1.

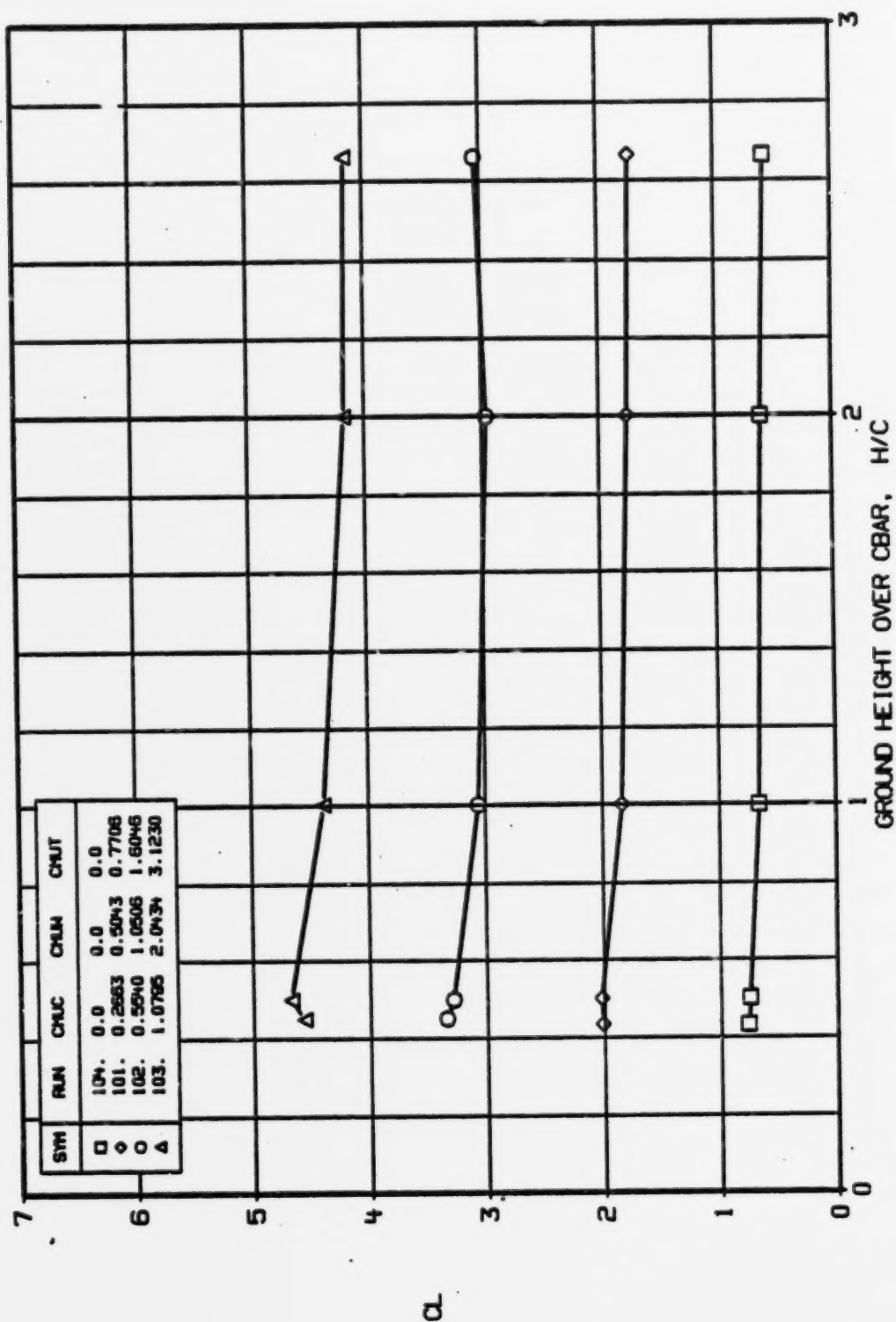


FIGURE A31a BASIC DATA EFFECT OF CHU
CONFIGURATION BC2W5V, DELF=45, BN/B=1

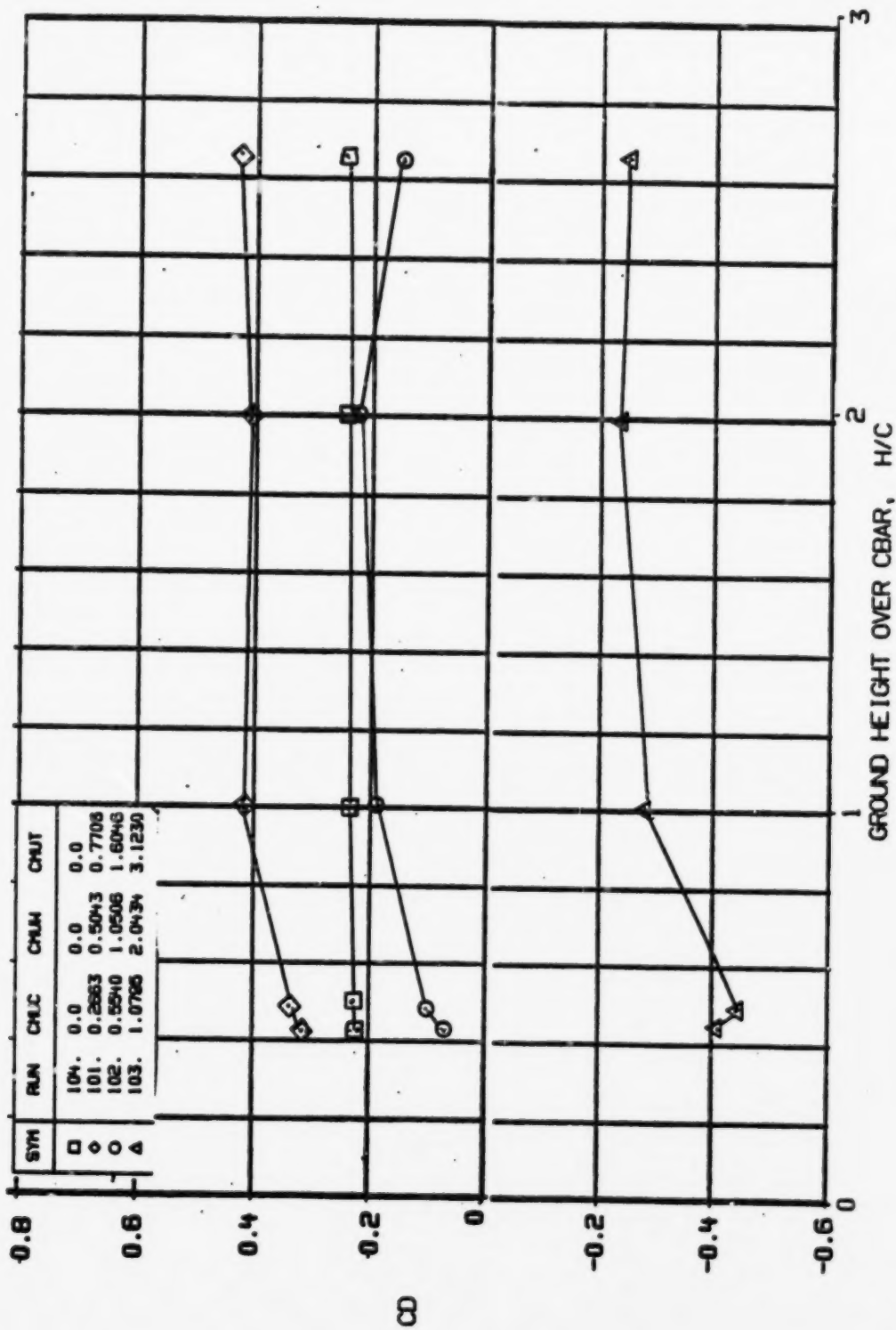


FIGURE A31b BASIC DATA EFFECT OF CMU
CONFIGURATION BC245V, DELF=45, BN/B=1

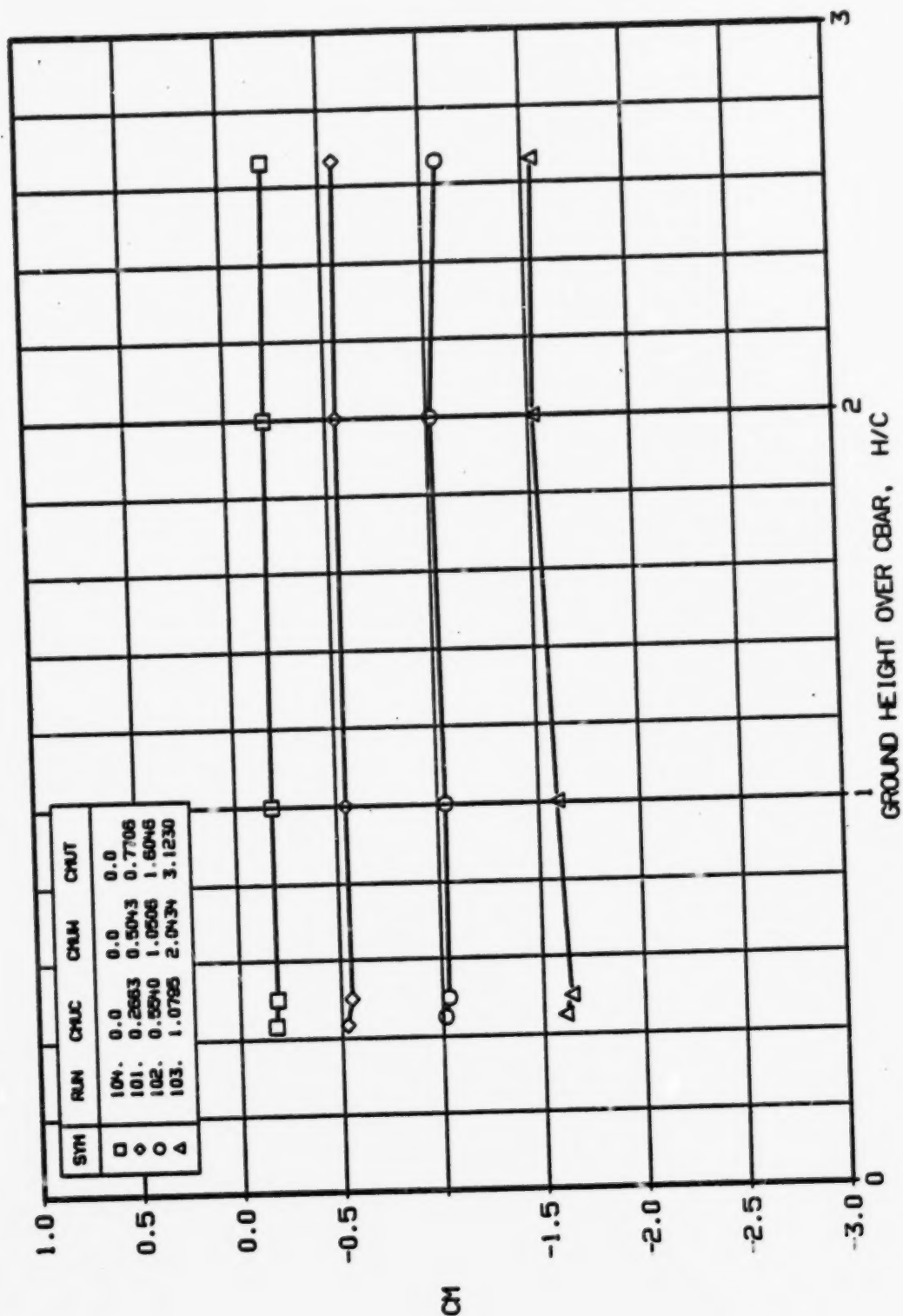


FIGURE A31c BASIC DATA EFFECT OF CMU
CONFIGURATION BC2W5V, DELF=45, BM/B=1.

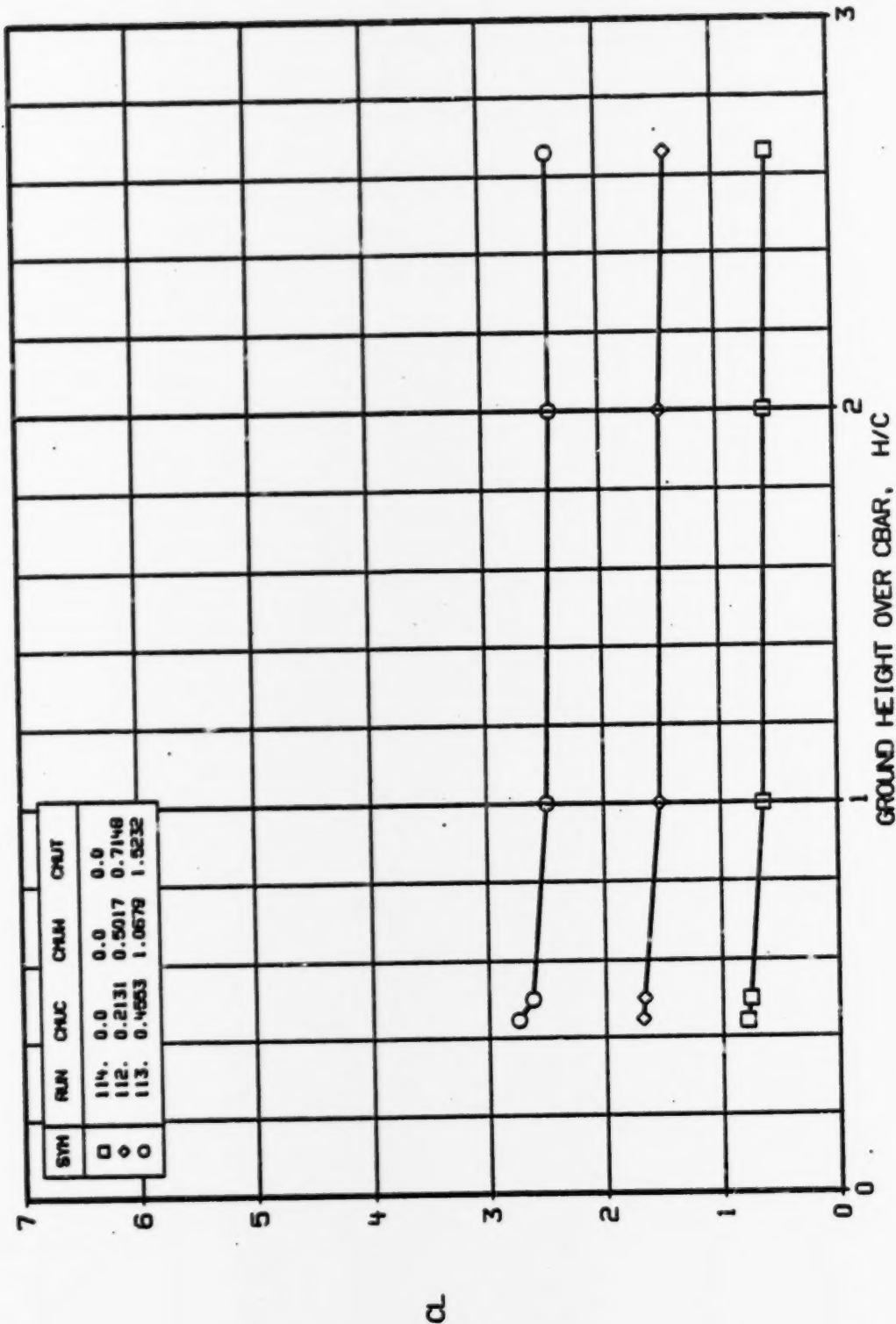


FIGURE A32a BASIC DATA EFFECT OF CMU
CONFIGURATION BC346V, DELF=45, BW/B=1

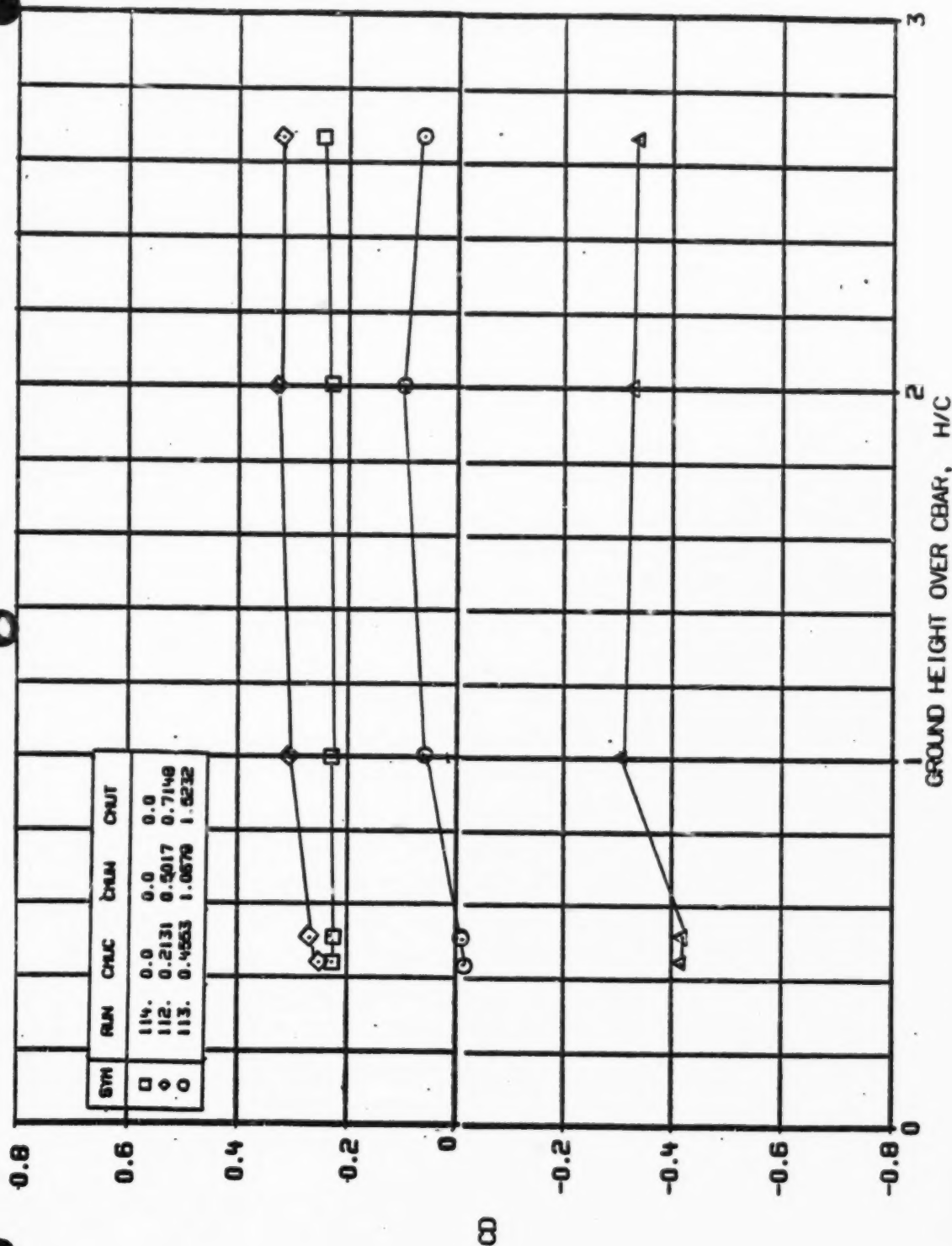


FIGURE A32b BASIC DATA EFFECT OF CMU
CONFIGURATION BC346V, DELF=45, BN/B=1

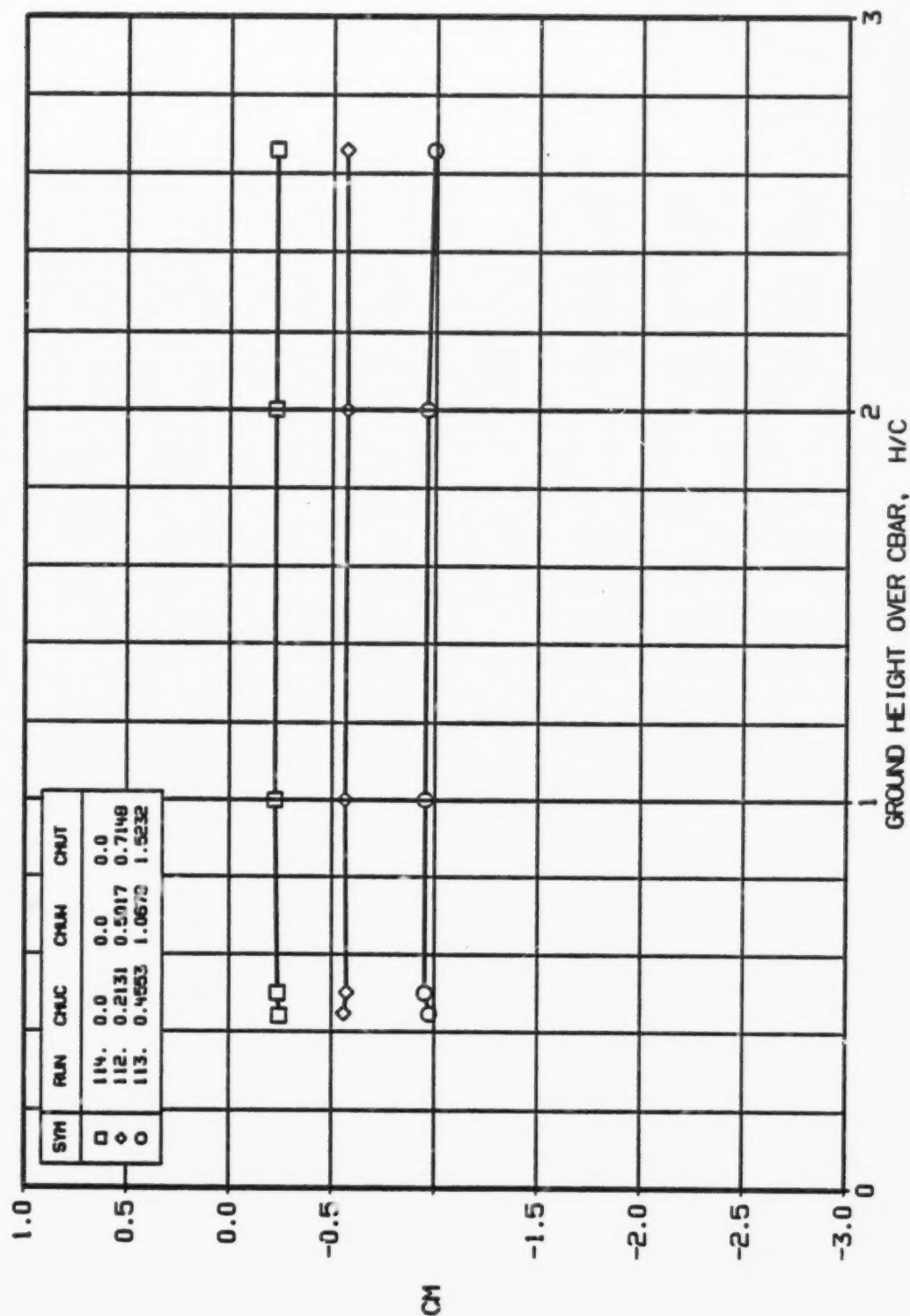


FIGURE A32c BASIC DATA EFFECT OF CMU
CONFIGURATION BC346V, DELF=45, BN/B=1

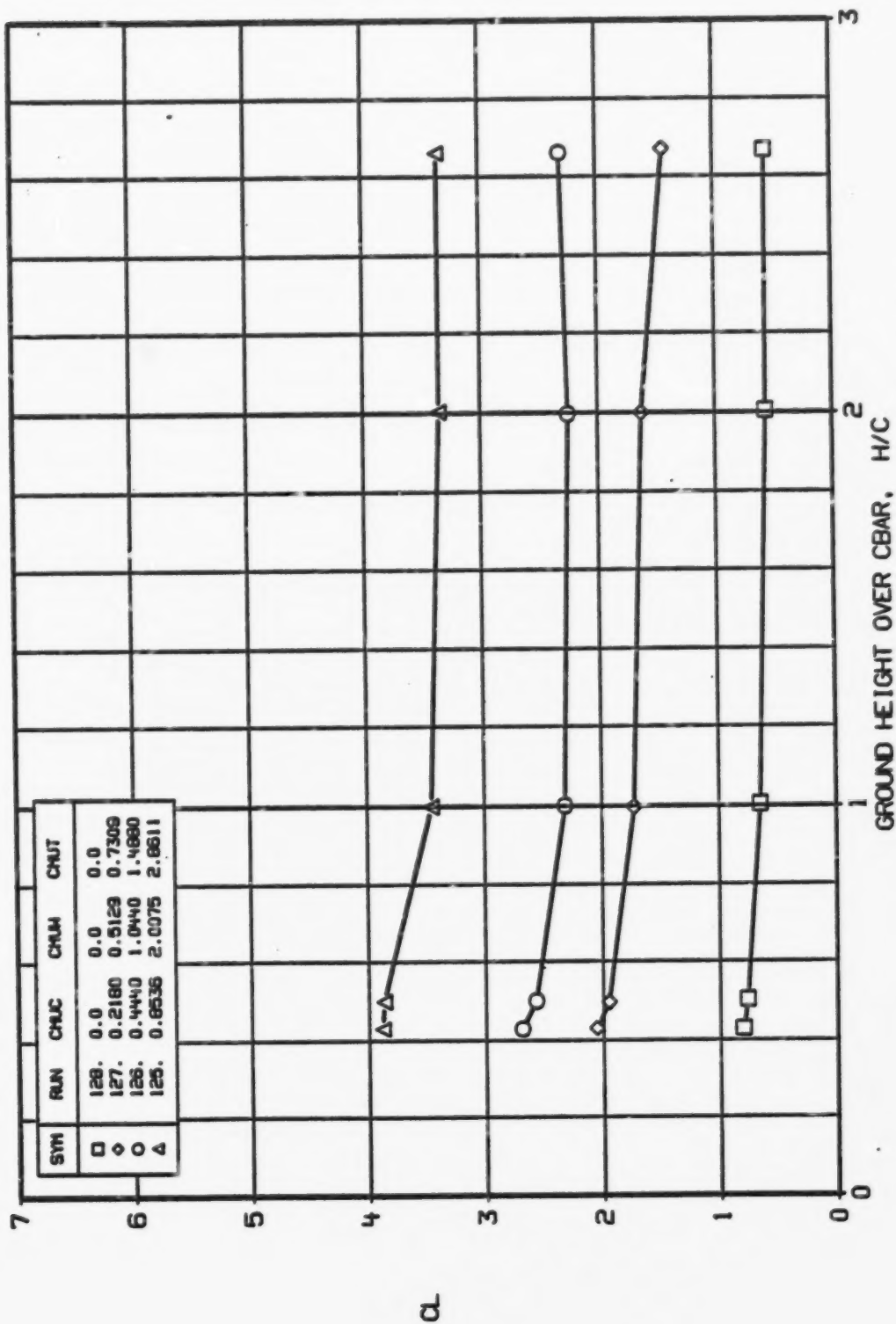


FIGURE A33a BASIC DATA EFFECT OF CMU
CONFIGURATION BC1N6V, DELF=45, BN/B=1, DELC=10°

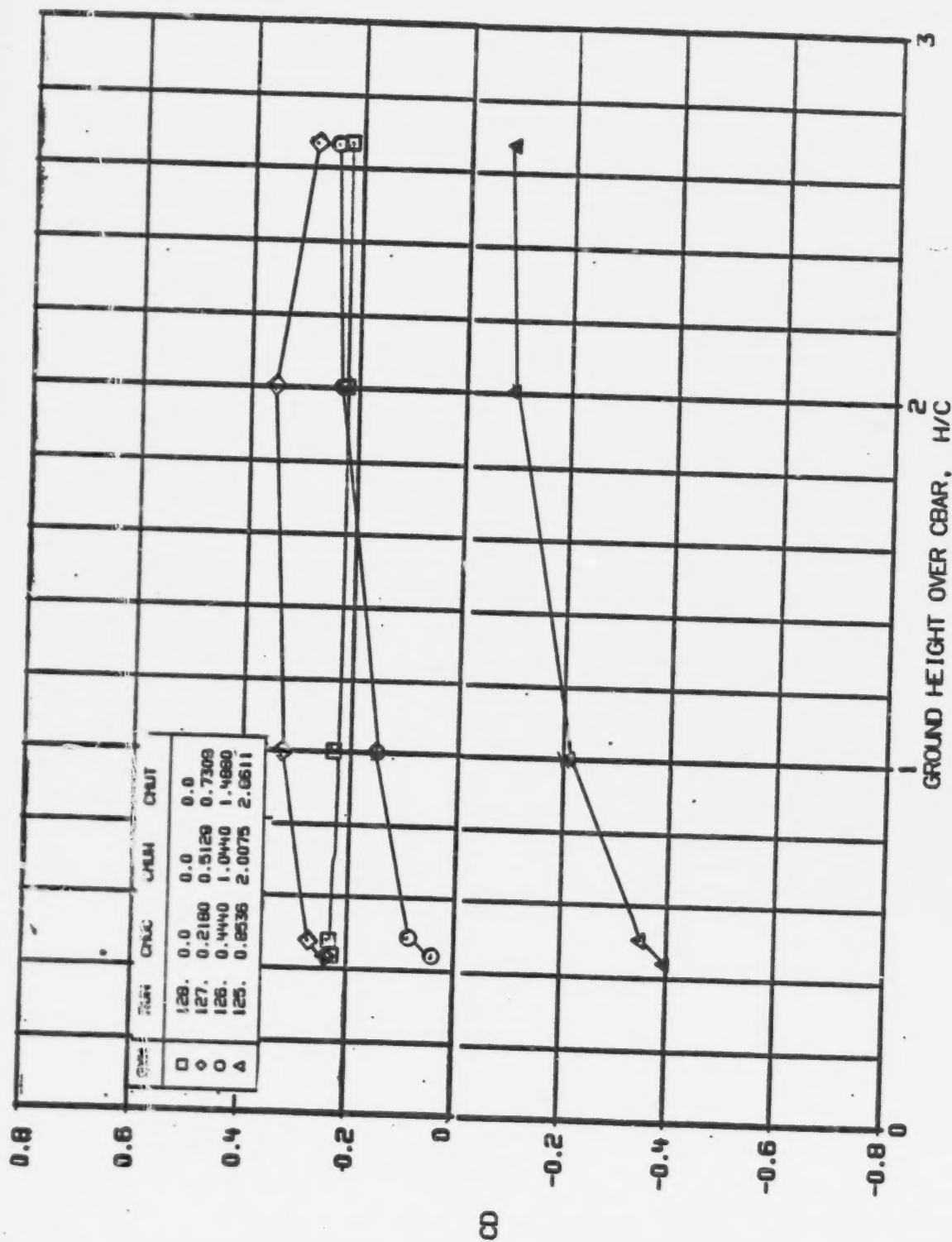


FIGURE A33b BASIC DATA EFFECT OF CHU
CONFIGURATION BC1W6V, DELF=45, BN/B=1, DELC=10°

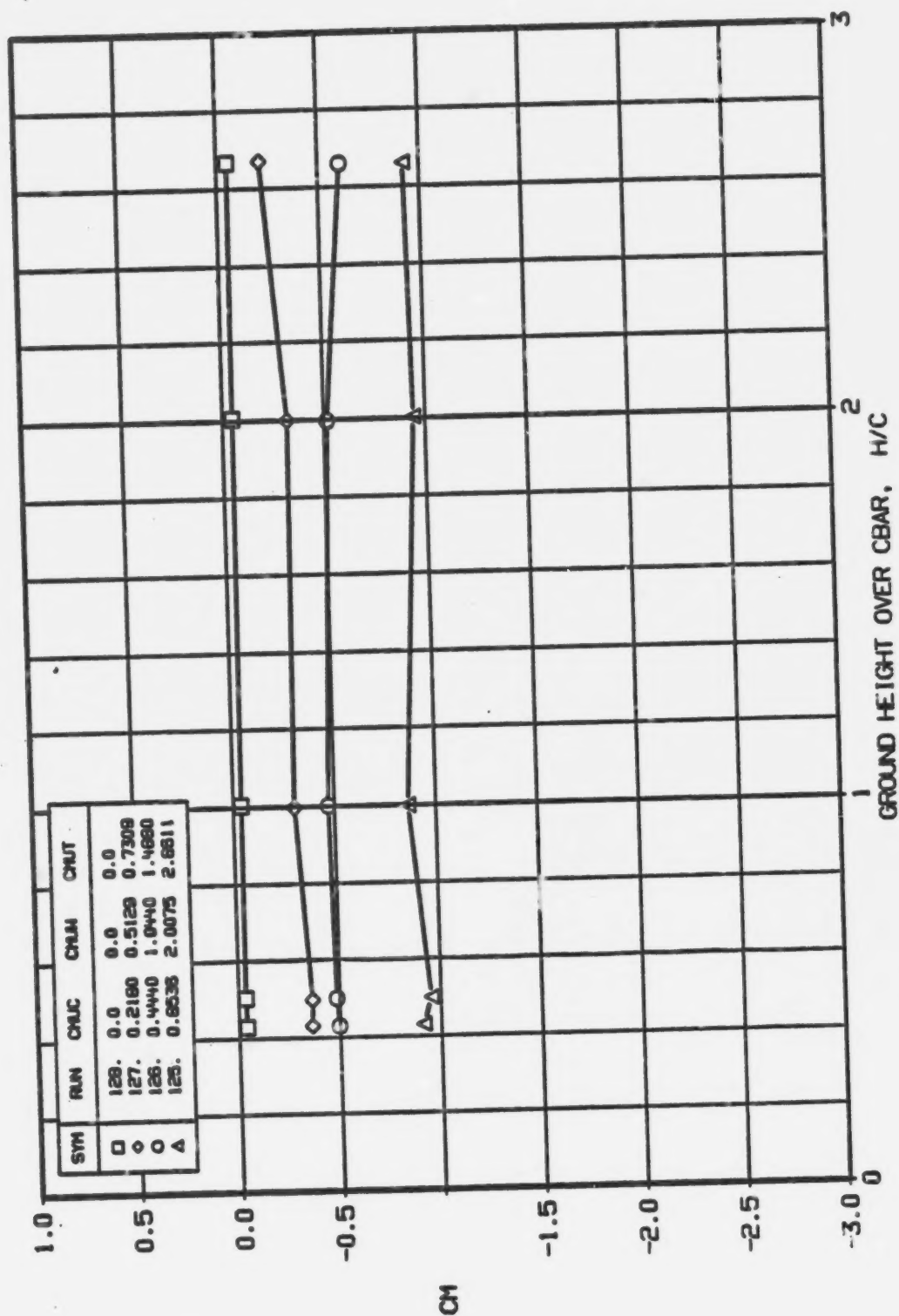


FIGURE A33C BASIC DATA EFFECT OF CMU
CONFIGURATION BC1W6V, DELF=45, BN/B=1, DELC=10°

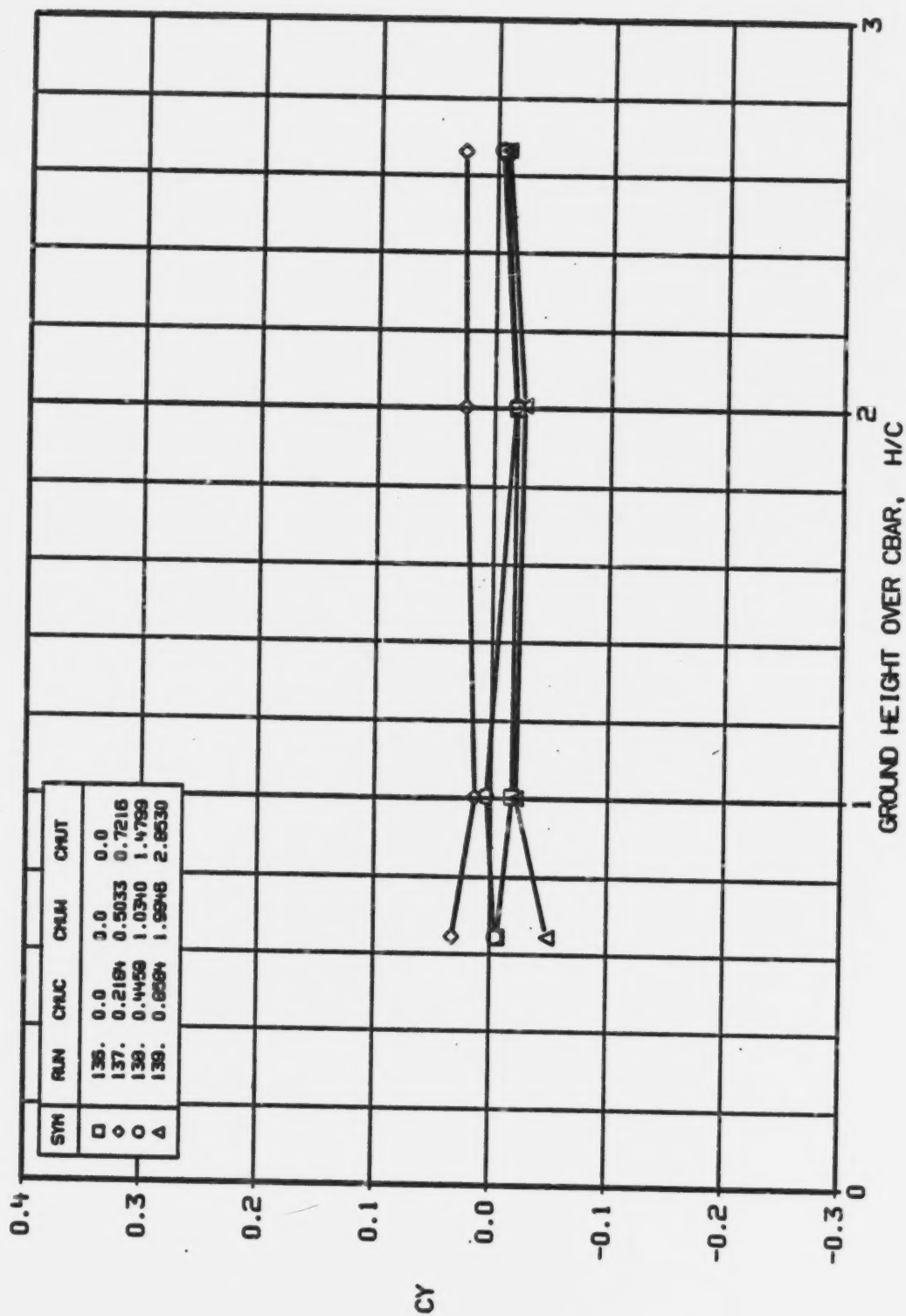


FIGURE A34a BASIC DATA EFFECT OF CHU
CONFIGURATION BC146V, DELF=45, $\beta = 0.8$, $\alpha = 2$

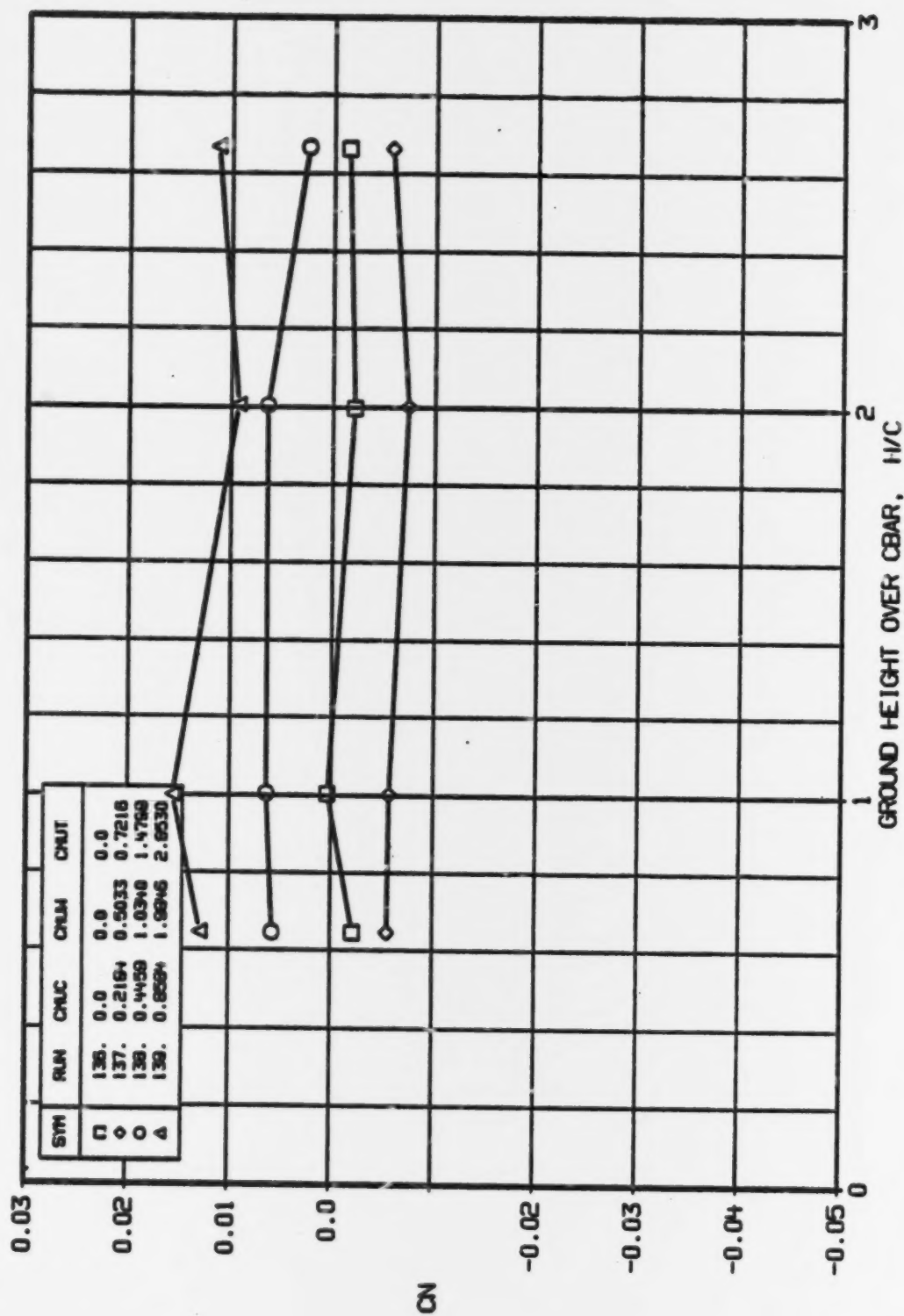


FIGURE A34b. BASIC DATA EFFECT OF CNU
CONFIGURATION BC146V, DELF=45, $\beta = 0.8$, $\alpha = 2$

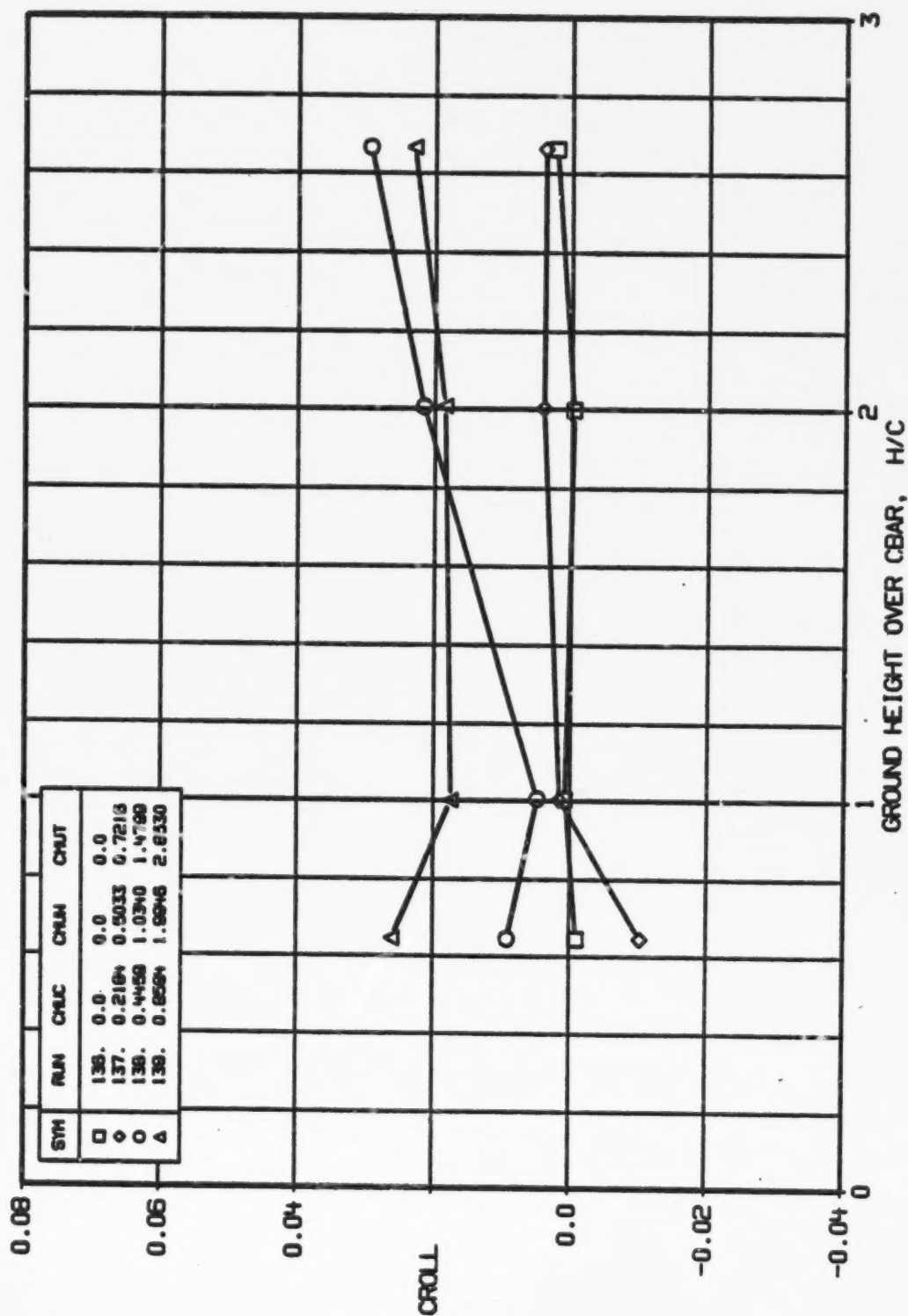


FIGURE A34c BASIC DATA EFFECT OF CHU
CONFIGURATION BC145V, DELF=45, BW/D=1, $\beta = 0.8$, $\alpha = 2$

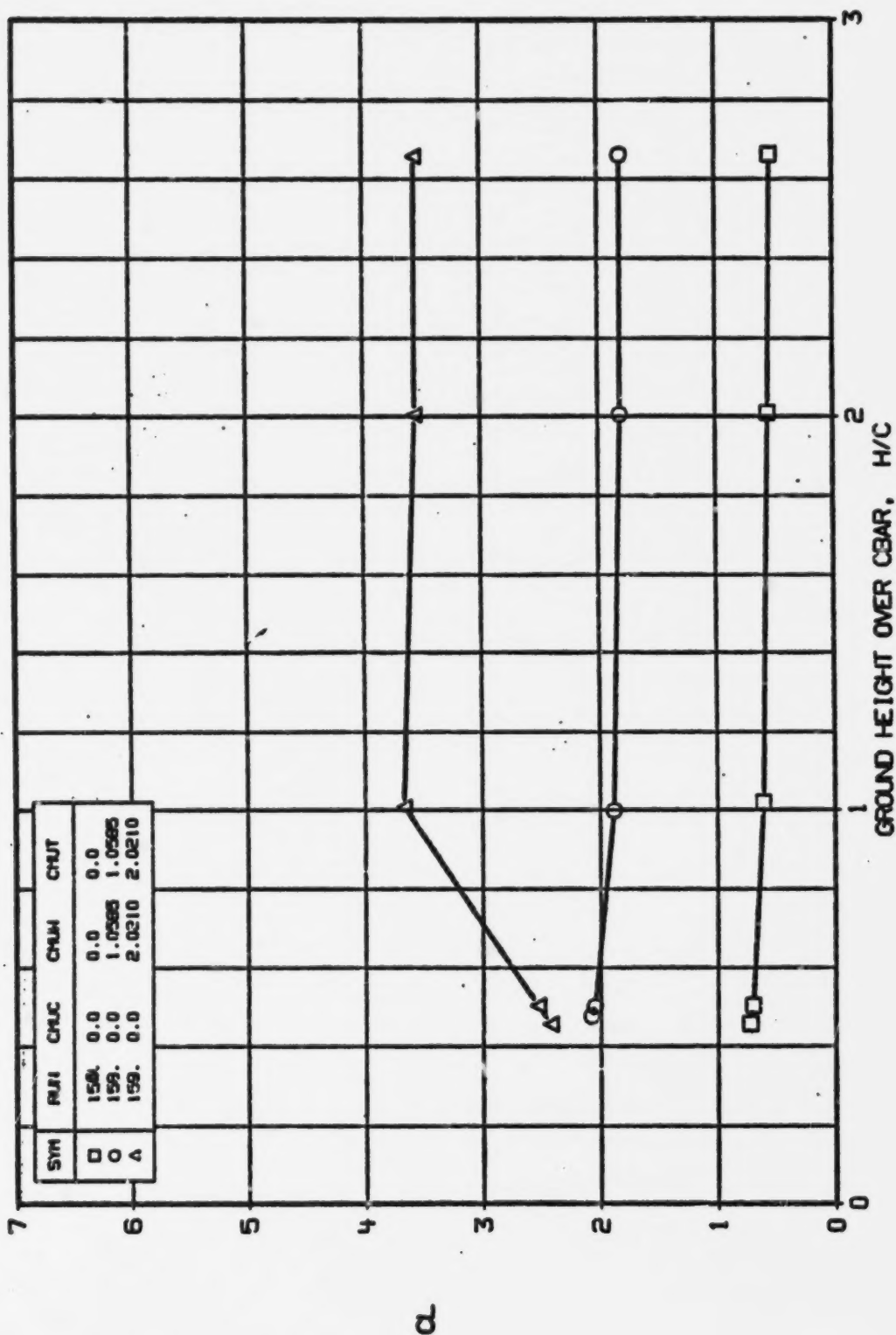


FIGURE A35a BASIC DATA EFFECT OF CMU
CONFIGURATION BMSV, DELF=45, BN/B=1

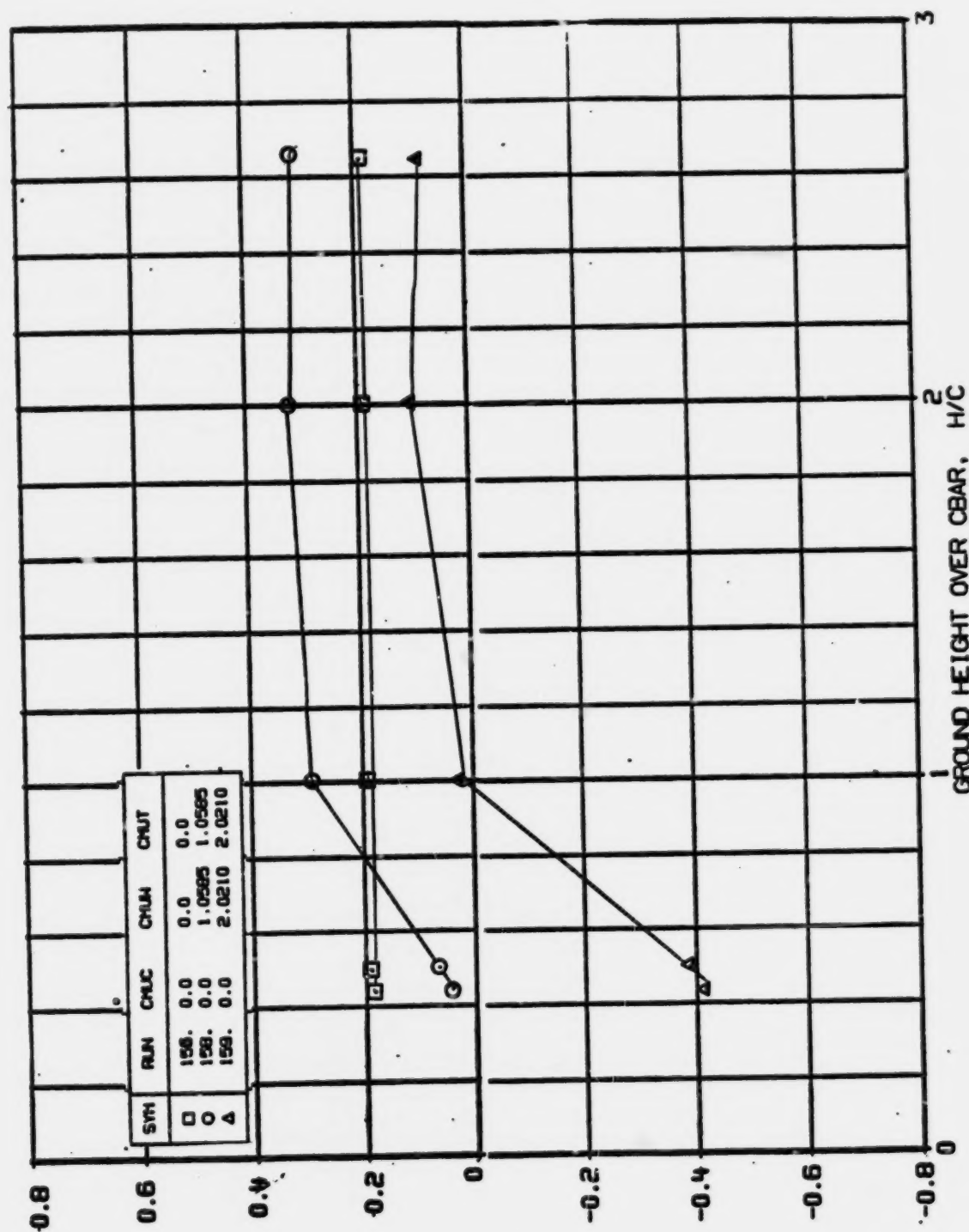


FIGURE A35b BASIC DATA EFFECT OF CMJ
CONFIGURATION BASED, DELF=45, SN/B=1

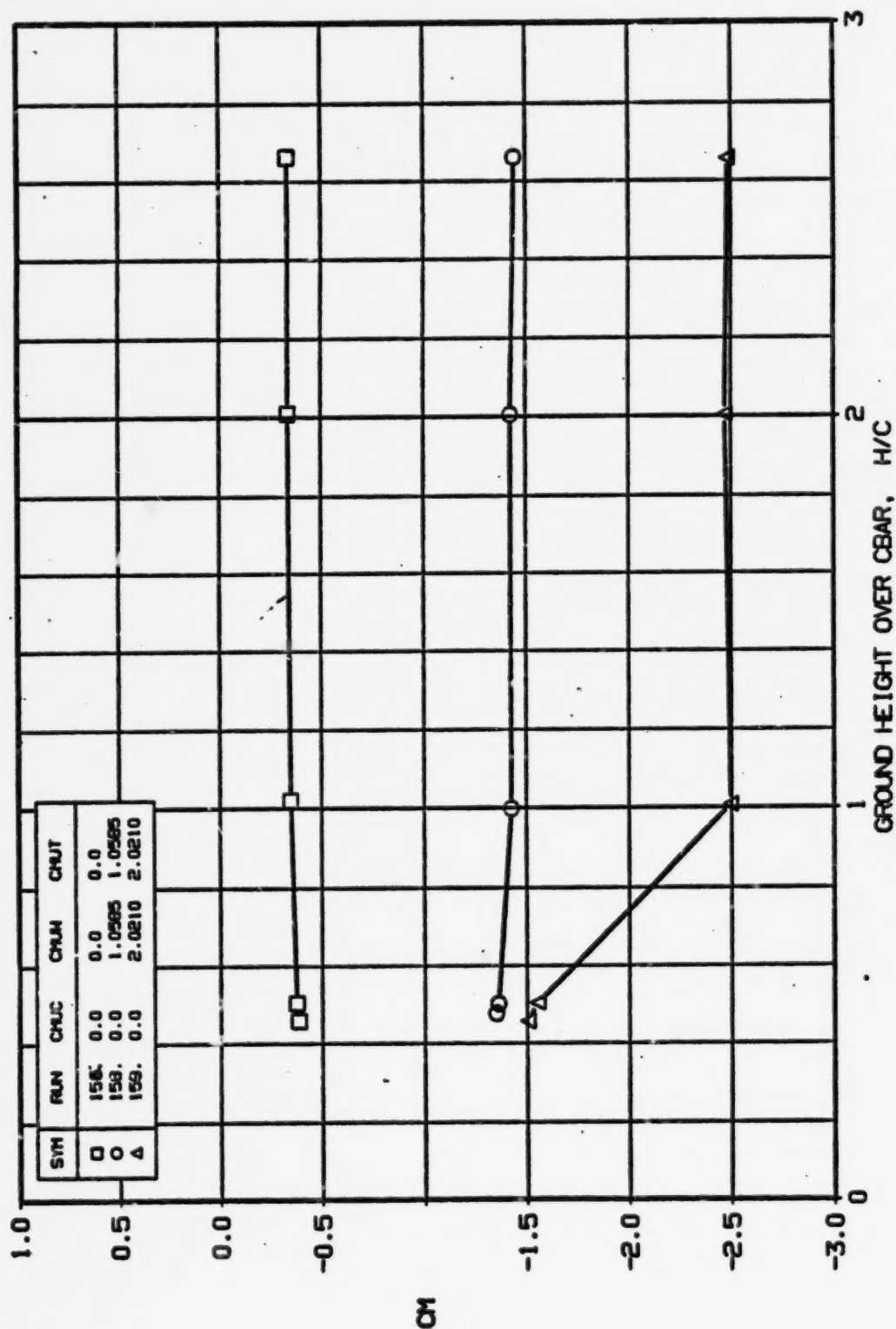


FIGURE A35c BASIC DATA EFFECT OF CMU
CONFIGURATION BMSV, DELF=45, BM/B=1

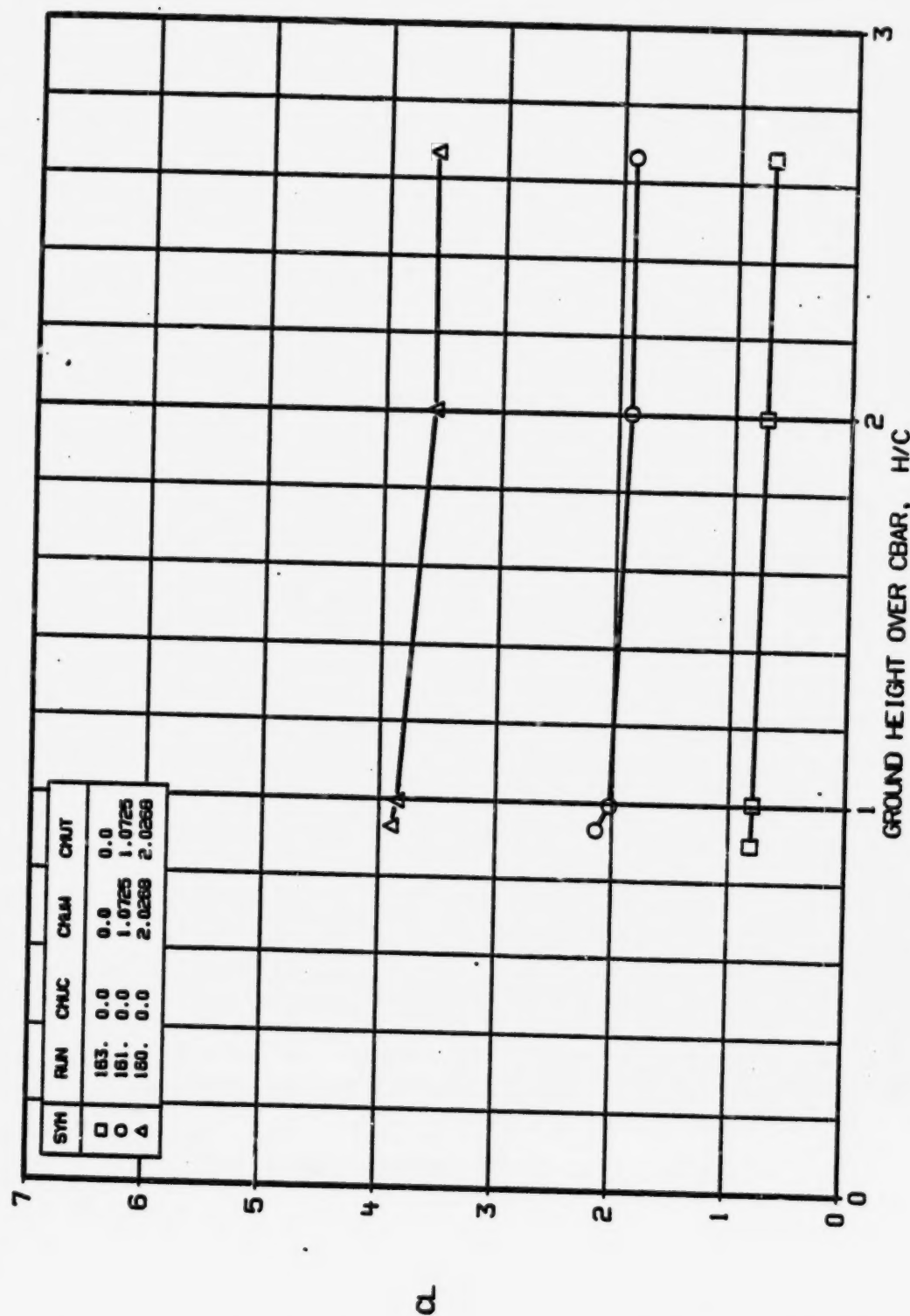


FIGURE A36a BASIC DATA EFFECT OF CMU
CONFIGURATION BMSV, DELF=45, BM/B=1 $\alpha = 4^\circ$

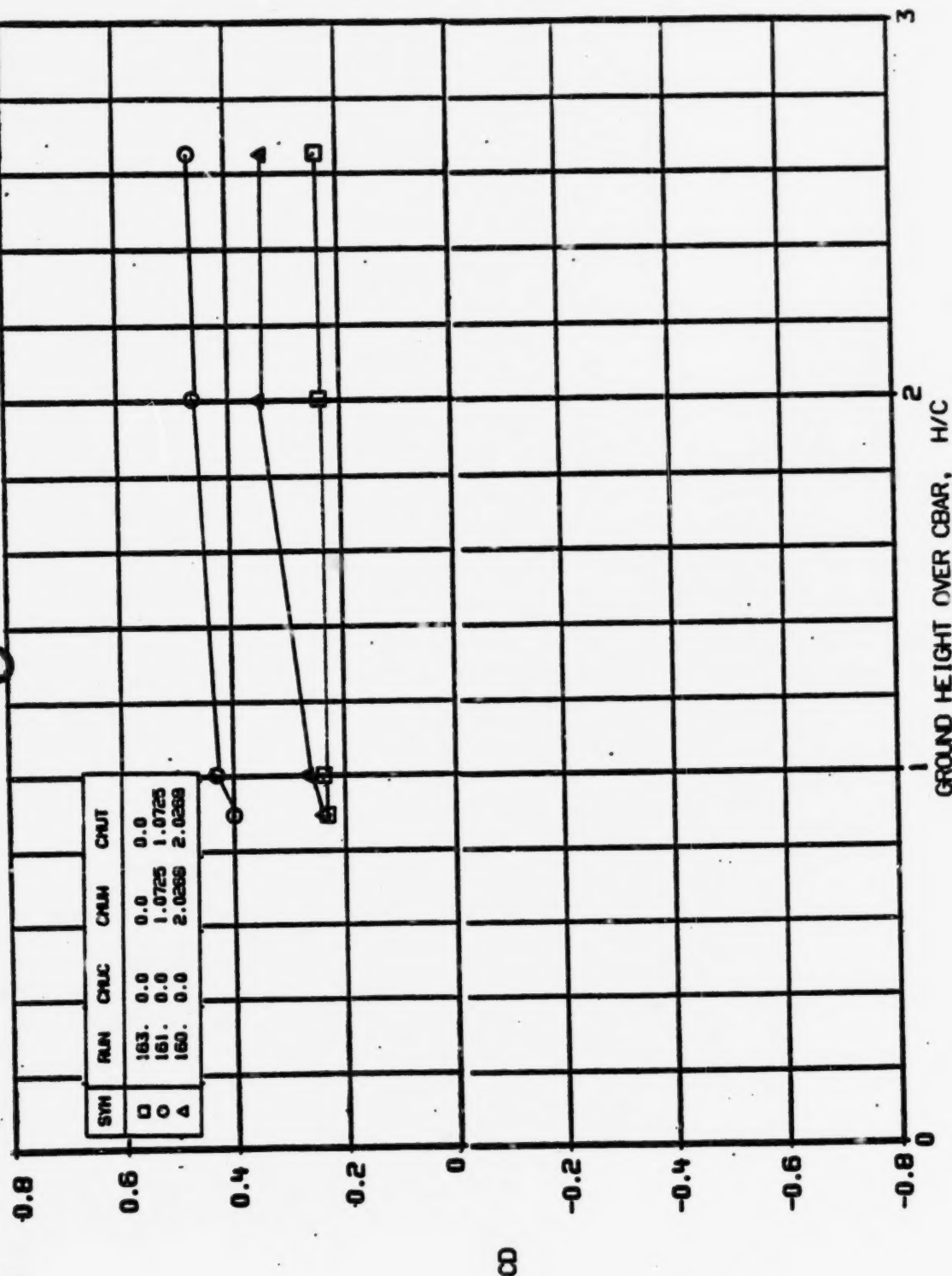


FIGURE A36b BASIC DATA EFFECT OF CMU
CONFIGURATION BMSV, DELF=45, $\theta N/3=1$ $\alpha = 4^\circ$

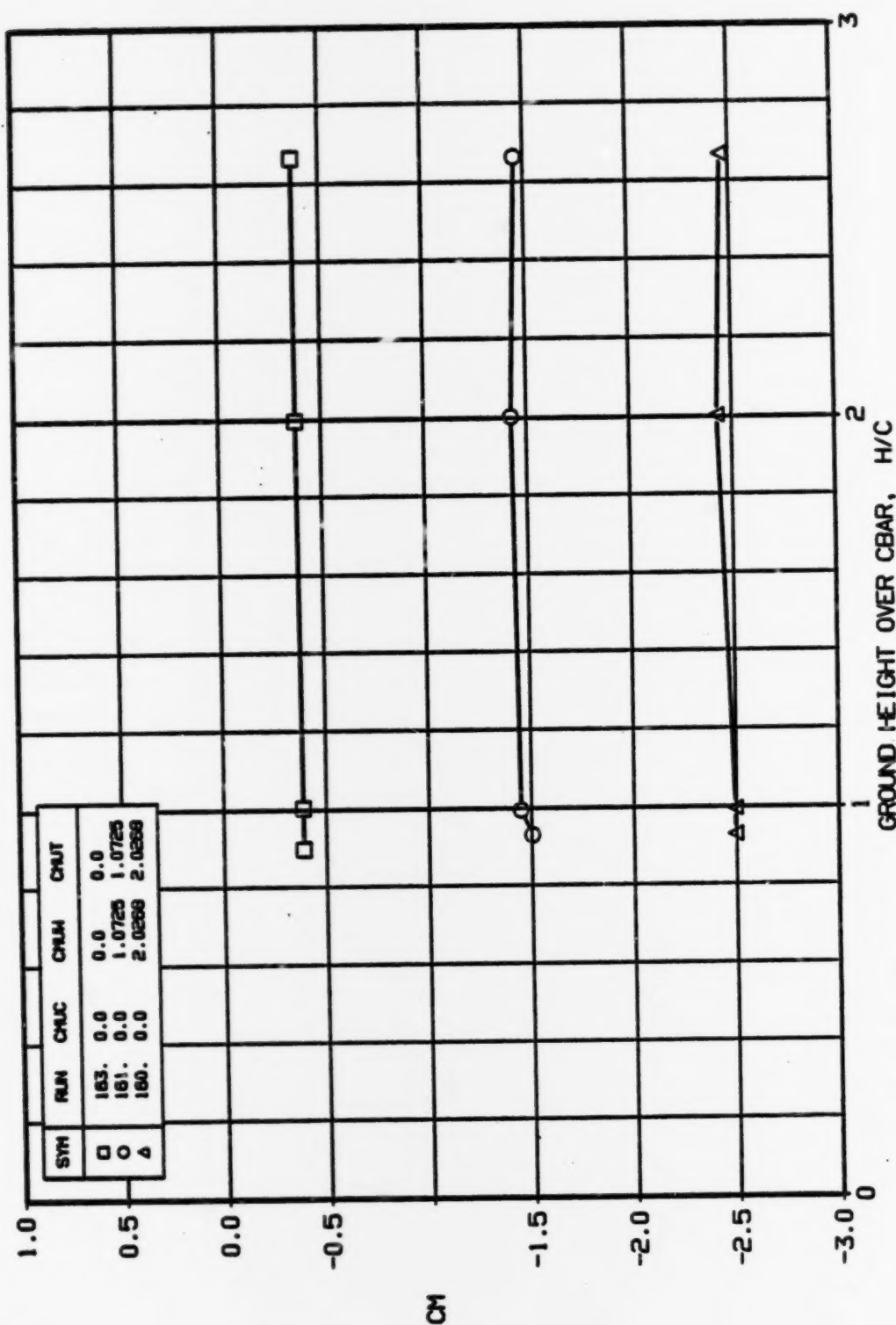


FIGURE A36C BASIC DATA EFFECT OF CMU
CONFIGURATION BAEV, DELF=45, BM/B=1 $\alpha = 4^\circ$

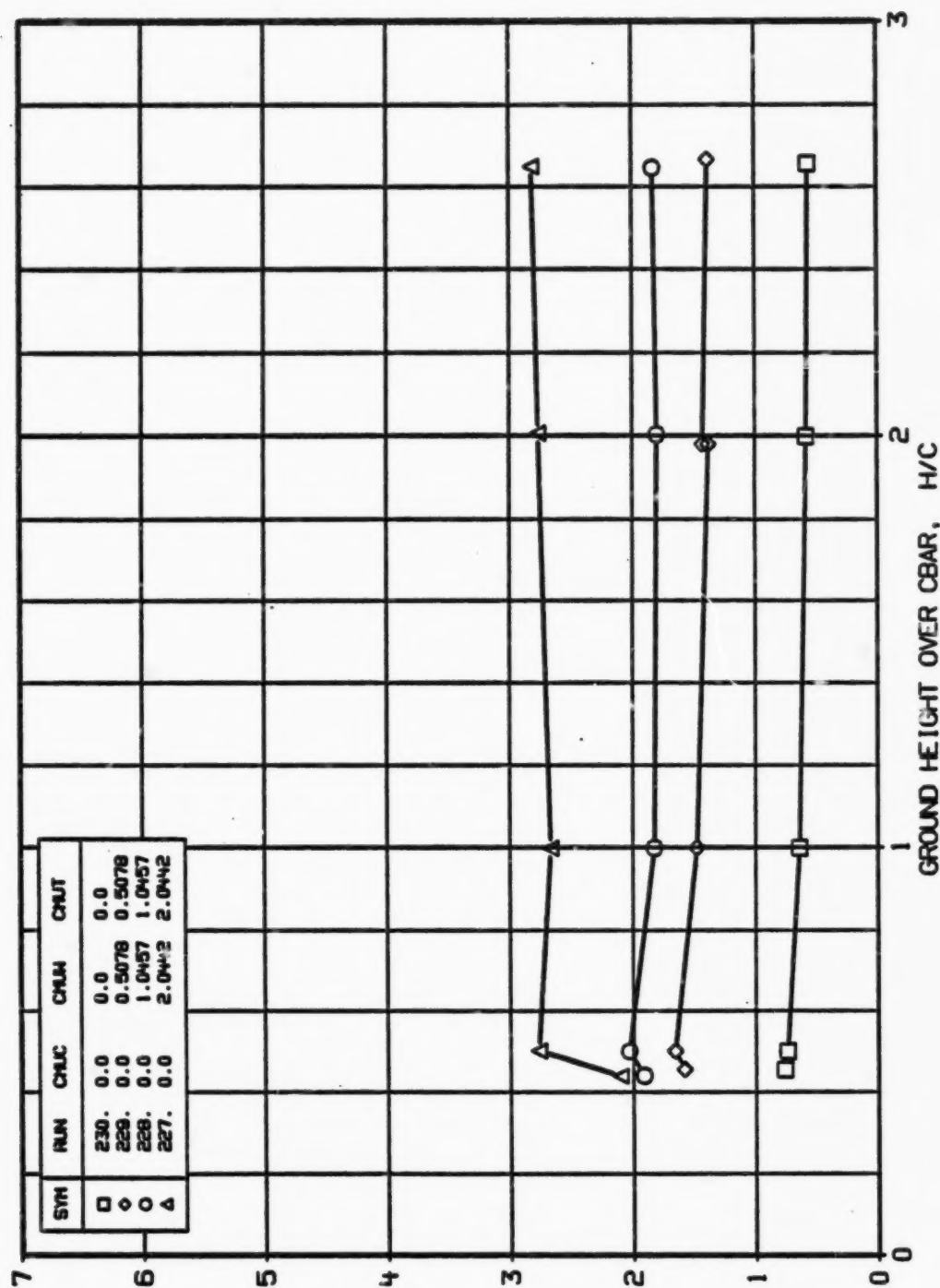


FIGURE A37a BASIC DATA EFFECT OF CMJ
CONFIGURATION BN/8=0.5, DELF=45

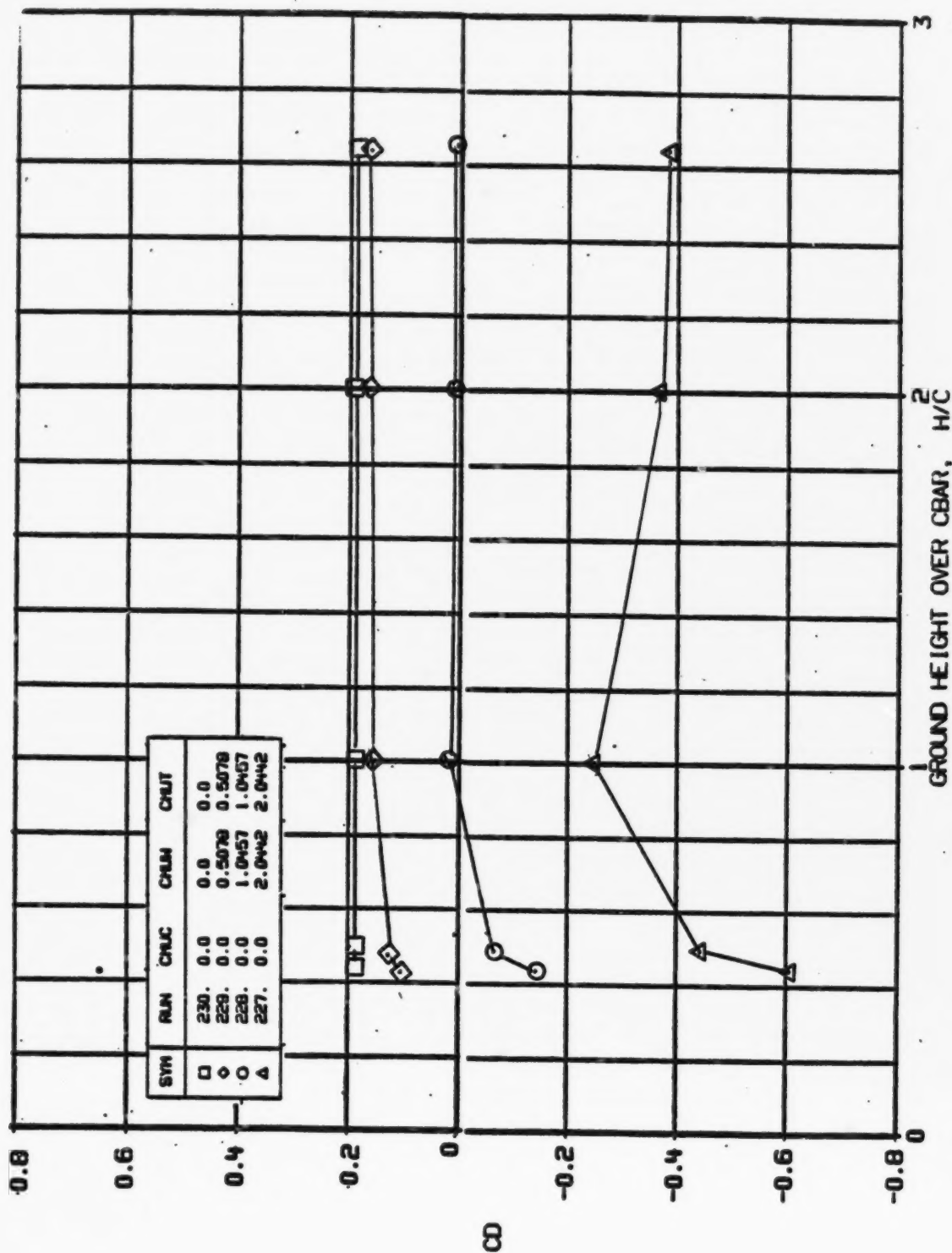


FIGURE A37b BASIC DATA EFFECT OF CMJ
CONFIGURATION BASED, BN/B=0.5, DELF=45

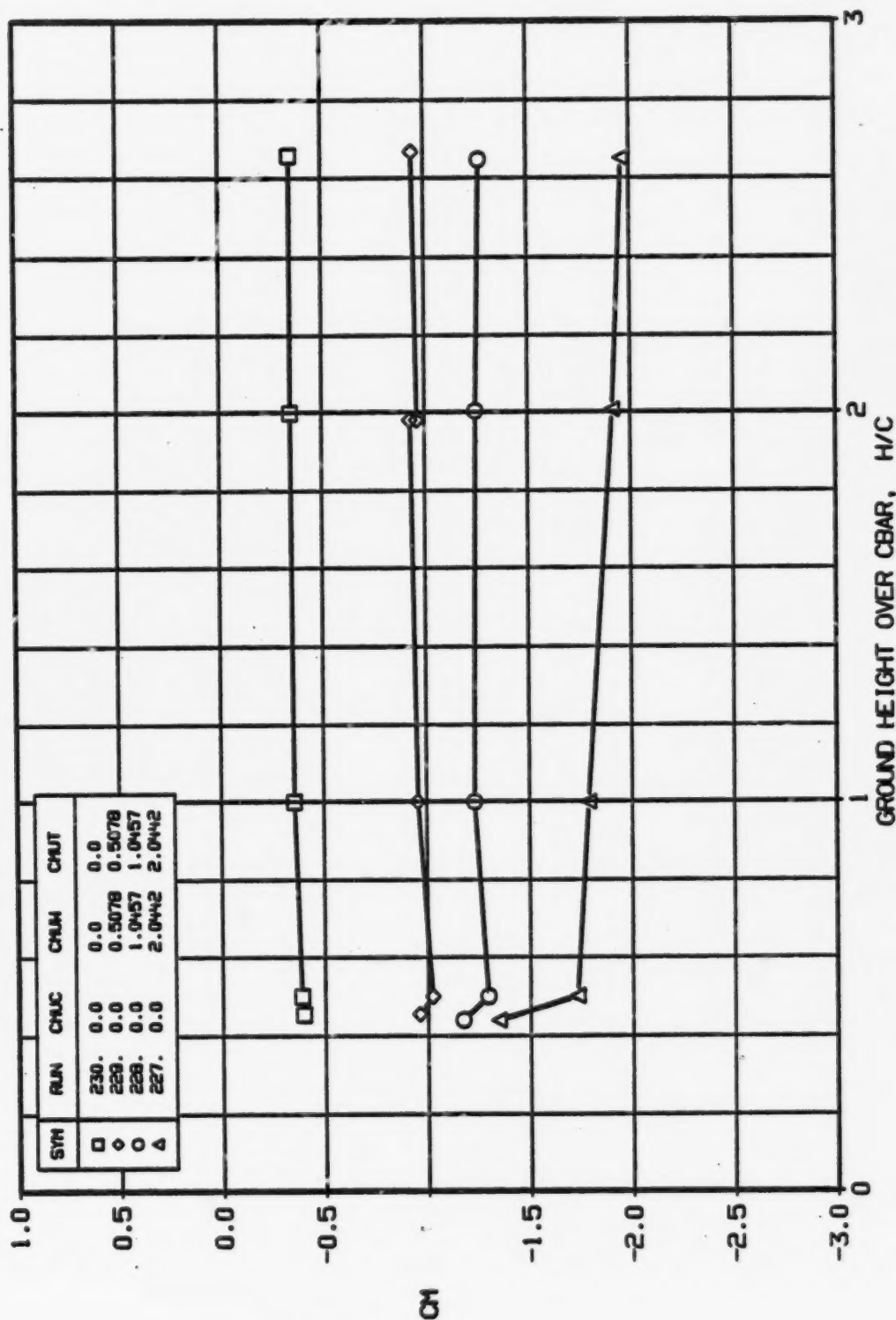


FIGURE A37c BASIC DATA EFFECT OF CMJ
CONFIGURATION BASED, $BN/B=0.5$, DELF=45

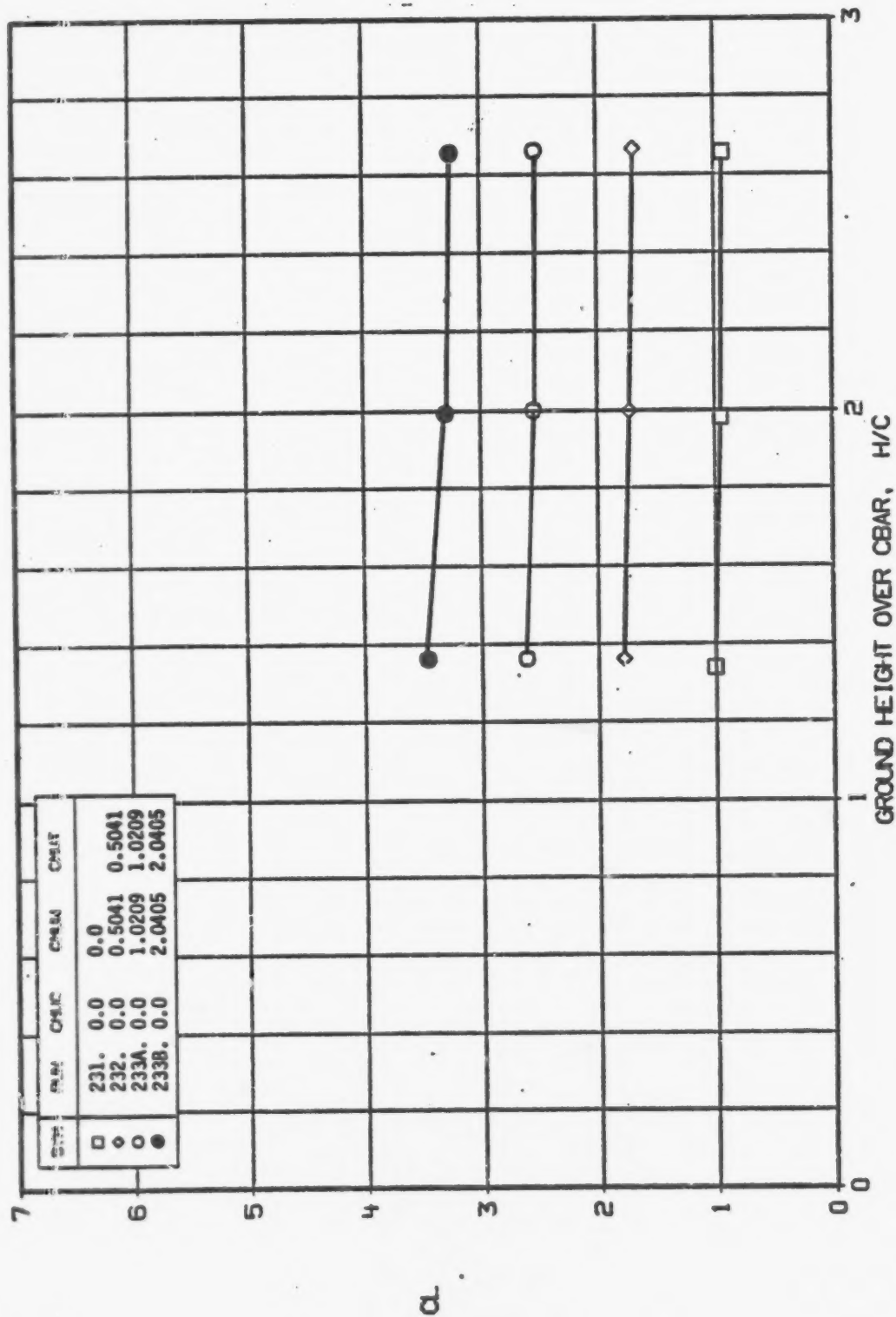


FIGURE A38a BASIC DATA EFFECT OF α_L
CONFIGURATION B46V, $BW/B=0.5$

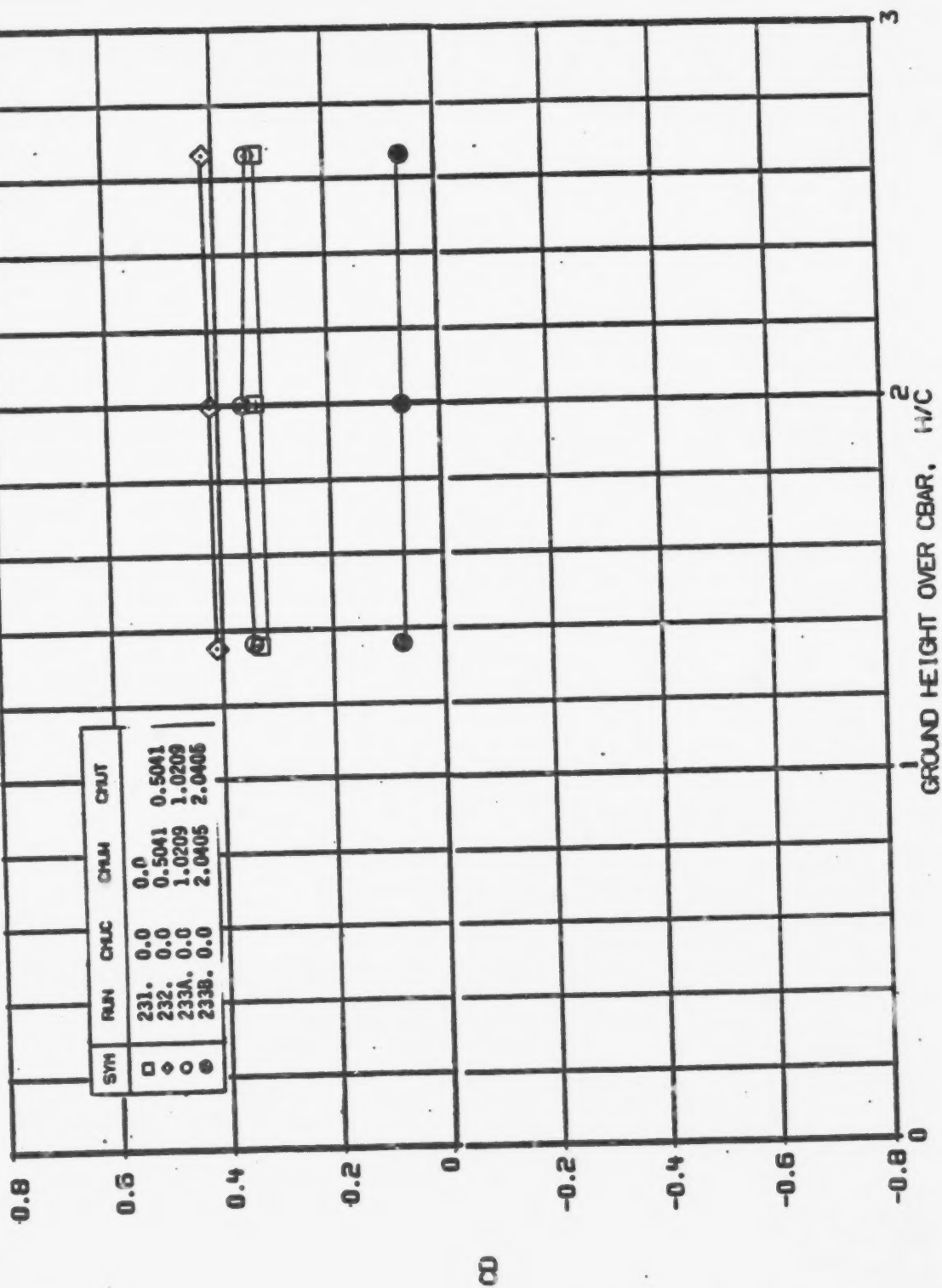


FIGURE A38b BASIC DATA EFFECT OF CMU
CONFIGURATION BWSV, BN/B=0.5

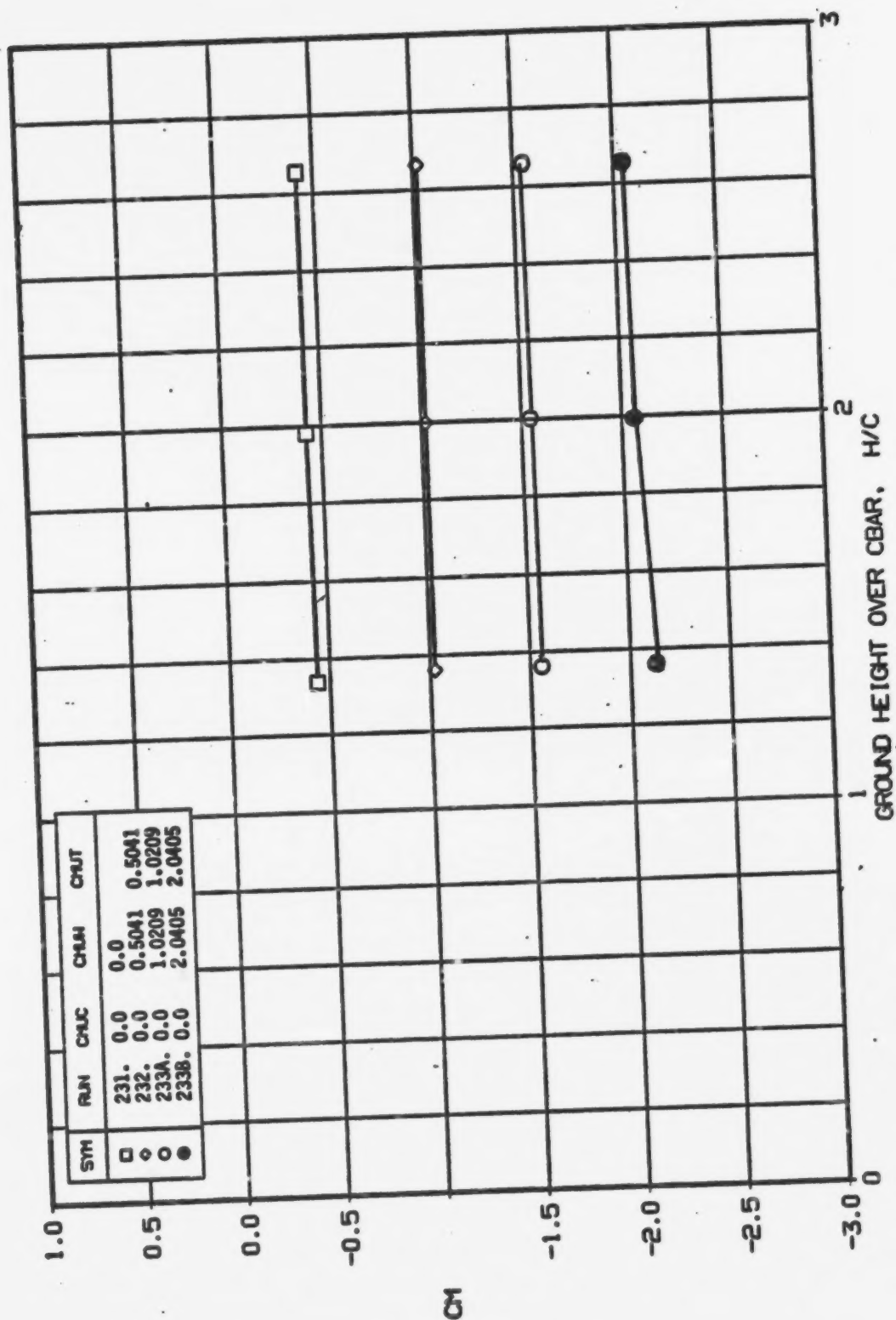


FIGURE A38c BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, $BH/B=0.5$

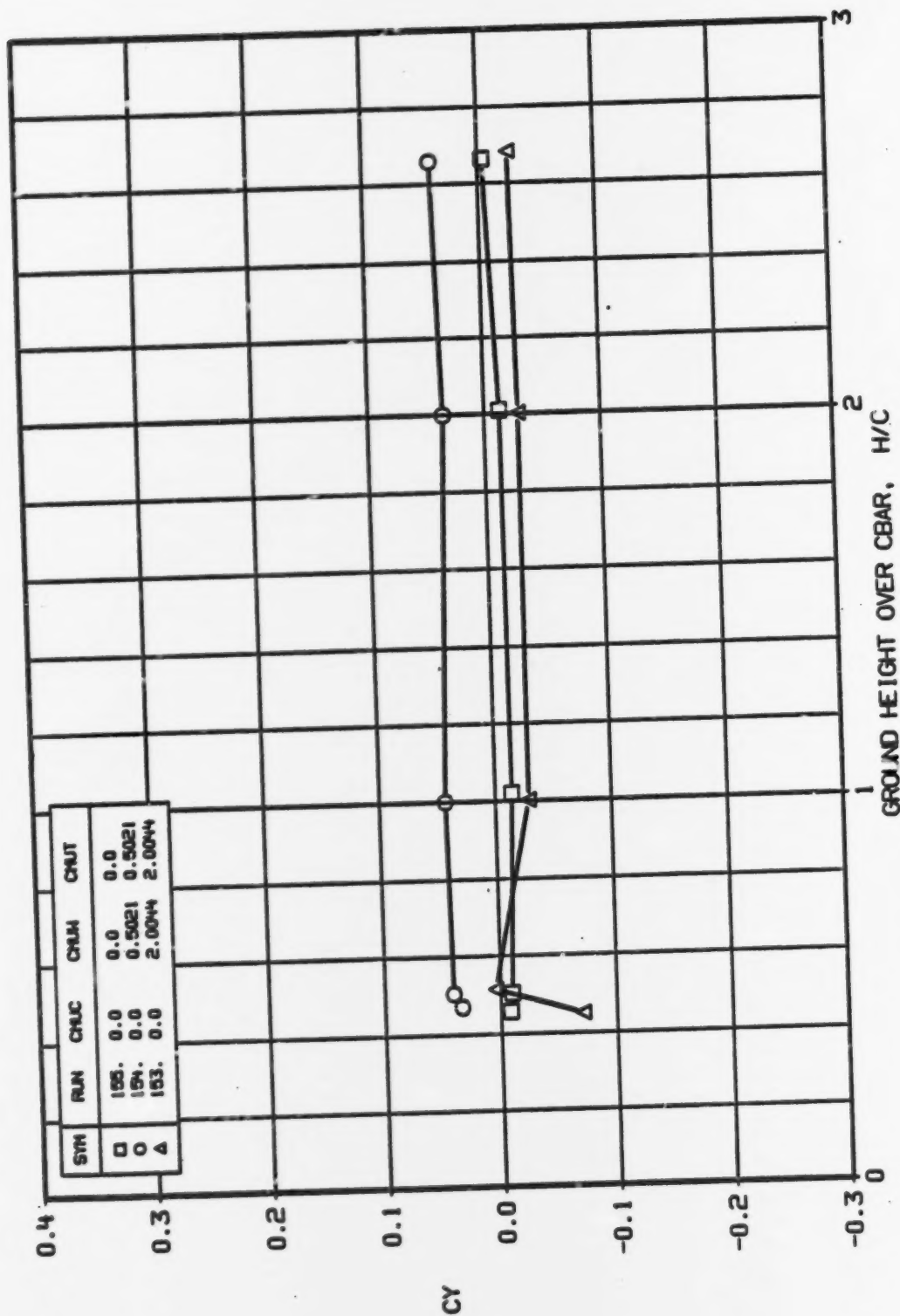


FIGURE A39a BASIC DATA EFFECT OF CMU
CONFIGURATION BWSV, DELF=45, $BW/B=1$, $\beta = 0.8$

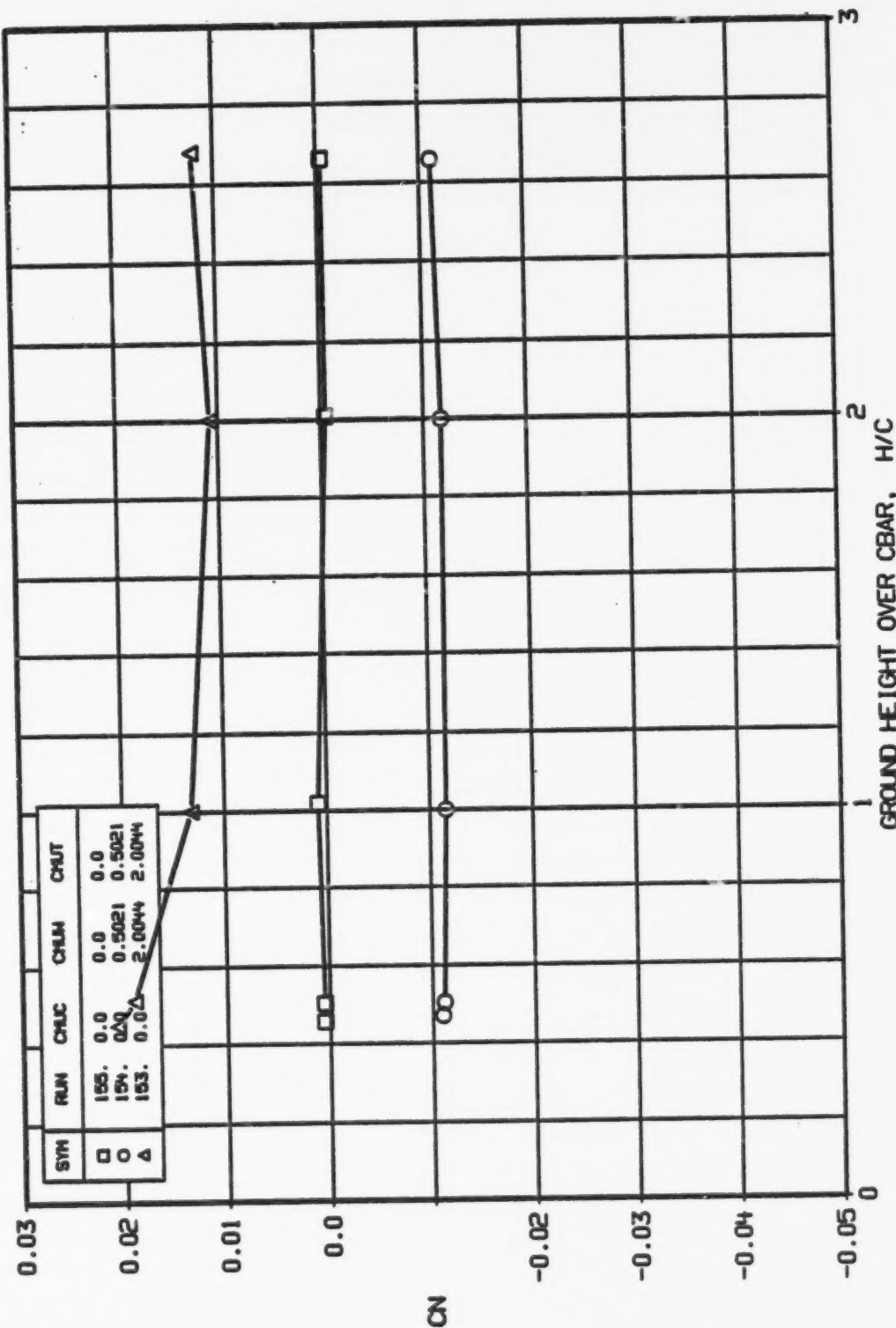


FIGURE A39b BASIC DATA EFFECT OF CMU
CONFIGURATION BMSV, DELF=45, BM/B=1, $\beta = 0.8$

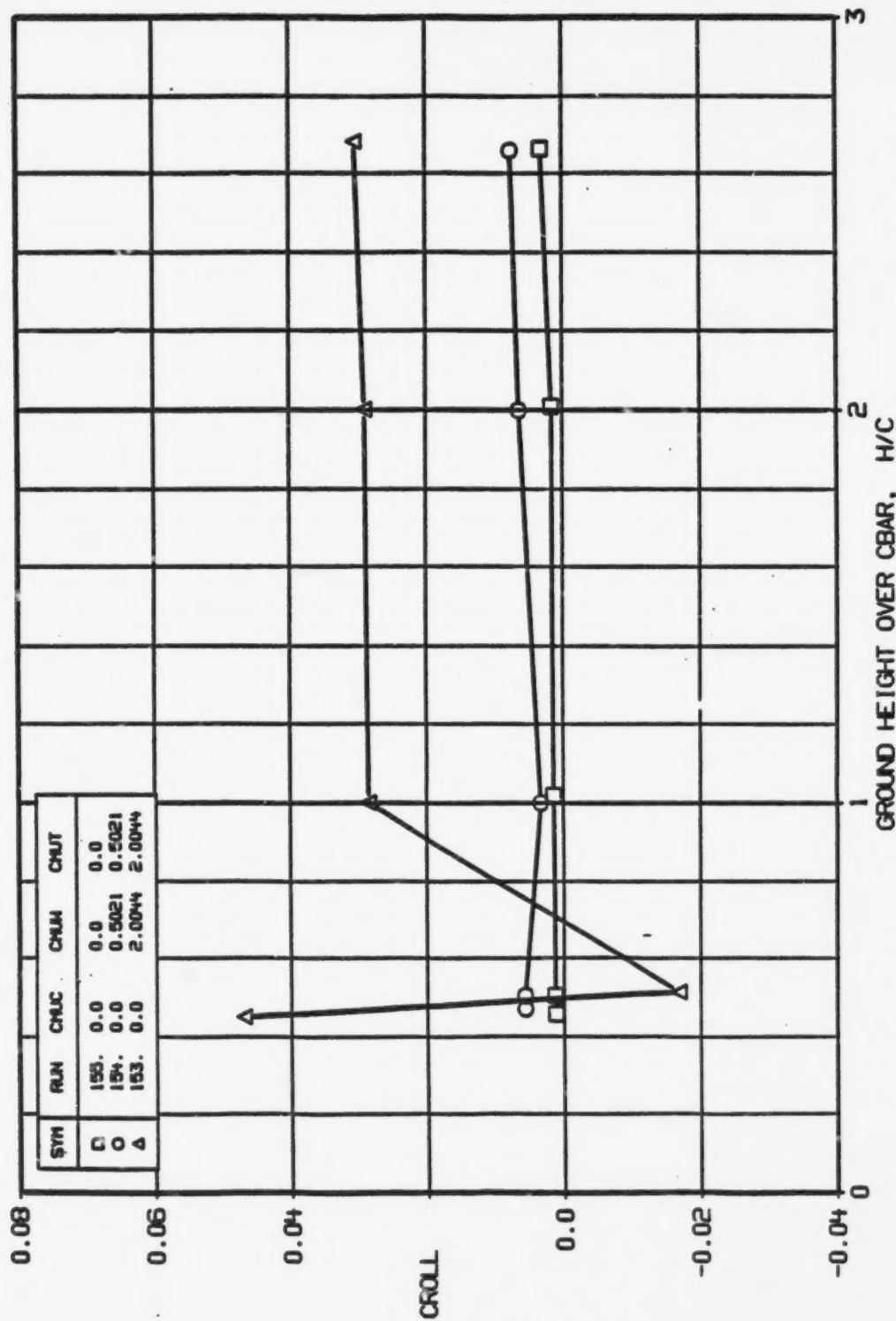


FIGURE A39c BASIC DATA EFFECT OF CMU
CONFIGURATION B46V, DELF=45, BM/B^*J , $\beta = 0.8$

A3.0 TABULATED SURFACE PRESSURE DATA

The surface pressure distribution for selected data runs is presented in Tables A1 to A50. The pressure coefficients are presented for the canard and wing with the locations described for each coefficient. The fuselage pressures are presented for various fuselage stations three inches to the left of the plane of symmetry. The wing pressures, presented as miscellaneous pressure coefficients, are as described below:

MISCELLANEOUS WING PRESSURES

	X/C	BP	
1	0.33	9	Upper
2	0.33	9	Lower
3	0.33	19	Upper
4	0.33	19	Lower
5	0.33	23.5	Upper
6	0.33	23.5	Lower
7			
8			
9			
10	Downwash probe pressure coefficients		
11			
12			

TABLE A1. (Concluded)

RUN: SEQ										PROPELLSIVE										WING / CANARD										PRESSURES										BASEPR = 8.1804										PAGE 79									
61 12 CLAERO = 1.0220 CDAERO = 0.2656 DCLC = 0.0										VEL YAW H/C										CMC										CMUT										HOT										CNTR									
ALPHA 11.59 2112.25 2100.27 11.98 100.59 0.01 2.67 0.0										CROLL CN CV										CNTR										CLTR										CDTR																			
BETA 1.50 -0.68 -0.52 0.01 -0.01 0.02																																																											
BP=3.375 BP=10.125										BP = 2 BP = 6 BP = 12 BP = 16 BP = 22										BP = 30 BP = 34 BP = 38 BP = 42 BP = 46 BP = 50										BP = 54 BP = 58 BP = 62 BP = 66 BP = 70																													
X/C										X/C										X/C										X/C										X/C																			
CP										CP										CP										CP										CP																			
0.0	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	0.0	-2.2452	-4.1417	-5.6645	-3.1072	-1.8429	38.2	-0.1874	1	-0.7428																																								
2.5	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	2.5	-1.4981	-2.2452	-3.8543	-2.3899	-1.6131	43.4	-0.1874	2	-0.1710																																								
5.0	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	5.0	-1.2104	-1.5556	-3.0498	-2.5038	-1.5556	50.4	-0.1792	3	-1.8228																																								
10.0	-0.2481	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	10.0	-0.9809	-1.1821	-2.7327	-2.6188	-1.5556	56.1	-0.2230	4	-0.0878																																								
15.0	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	15.0	-0.8659	-1.0384	-1.3832	-2.2452	-1.4981	62.5	-0.2449	5	-1.3413																																								
25.0	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	24.0	-0.7223	-0.8659	-0.9947	-1.6706	-1.4119	69.7	-0.2667	6	-0.1813																																								
35.0	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	33.0	-0.6597	-0.7428	-0.8269	-0.9089	-1.4904	76.9	-0.3106	7	-0.4499																																								
50.0	-0.2481	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	54.0	-0.5767	-0.6597	-0.6597	-0.6597	-1.4074	83.4	-0.2449	8	-0.3510																																								
65.0	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	65.0	-0.6822	-0.7259	-0.7478	-0.6385	-1.5789	89.4	-0.2658	9	-0.1378																																								
80.0	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	78.5	-1.2289	-1.2945	-1.3293	-1.0978	-2.0162	95.4	-0.2667	10	-0.4499																																								
76.0	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	79.5131	5552	131.5552	131.5552	131.5552	128.3078	101.1	-0.2230	11	-0.0838																																								
79.0	-0.2481	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	80.5	-56.8356	-48.6201	-60.4115	-55.4115	-44.2558	---	---	12	-0.1583																																								
80.5	-0.2854	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	81.3	-23.0846	74.2065	-3.6290	-5.3156	-3.4367	36.2	-0.0480																																										
81.0	-0.2558	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	82.0	28.8163	27.7511	20.0726	-4.9014	0.2916	43.4	-0.0043																																										
82.0	-0.2558	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	84.0	8.2048	14.1247	3.0286	-7.1803	0.7946	50.4	-0.0480																																										
84.0	-0.2558	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	87.0	3.3246	-1.3259	-1.6021	-0.6910	-0.6910	56.1	-0.0613																																										
87.0	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	-0.2707	89.0	0.0406	-0.1375	-2.1489	-1.6327	0.0049	62.5	0.1061																																										
89.0	-0.2449	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	93.0	0.2185	-0.3432	-0.1019	-0.4222	-1.8107	69.7	0.1488																																										
93.0	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	96.0	0.2449	-0.6369	-0.1618	-1.4846	-2.6651	76.9	0.1270																																										
96.0	-0.2449	-0.2449	-0.2449	-0.2449	-0.2449	-0.2449	-0.2449	-0.2449	-0.2449	100.0	-2.2957	-2.2021	-1.7039	-1.7395	-1.8997	83.4	0.1051																																										
00.0	-0.2449	-0.2449	-0.2449	-0.2449	-0.2449	-0.2449	-0.2449	-0.2449	-0.2449	98.0	0.0406	0.0406	-0.0307	-0.1731	-0.1553	89.4	0.0832																																										
96.0	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	84.0	0.0007	0.2363	0.3075	0.0939	-0.0484	95.4	0.0832																																										
84.0	-0.2449	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	73.5	-0.0782	0.0879	0.0879	-0.0879	-0.0782	101.1	-0.0043																																										
73.0	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	-0.2667	54.0	0.0048	0.0048	0.0048	-0.0782	-0.1613																																												
50.0	-0.2667	-0.2449	-0.2449	-0.2449	-0.2449	-0.2449	-0.2449	-0.2449	-0.2449	33.0	0.1710	0.1710	0.1710	0.1710	-0.0782																																												
35.0	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	24.0	0.1685	0.2259	0.1972	0.1710	-0.2259	0.0248																																											
25.0	-0.2481	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	10.0	0.3696	0.3409	0.3983	0.3983	0.4568	0.2541																																											
10.0	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	5.0	0.4845	0.4845	0.5133	0.5133	0.4202																																												
5.0	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	2.5	0.5995	0.5420	0.5133	0.5133	0.5033																																												
2.5	-0.2891	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686	-0.2686																																																		

TABLE A2. RUN 62. BWGV, DELF=0, CMJ=2.0, (BM/S)=1

RUN:SEQ		PROPLUISIVE										WING / CANARD										PRESSURES										BASEPR = 8.1904										PAGE 80									
62 2		CLAERO = 0.3651										DCLC = 0.0										DMLC = 0.8330										HGT										BN									
ALPHA		PTOT										Q										VEL										86.7146										0.450351E+08									
0.06		2112.25										70.40										0.01										2.65										2.051									
BETA		CL										CM										CROLL										CN										CNTR									
-0.01		0.90										-0.49										0.01										-0.01										0.32									
		-1.97										0.01										0.04										0.32										-0.35									

TABLE A2. (Continued)

RUN-SEQ										PROPLUSTIVE										WING / CANARD										PRESSURES										BASEPR = 8.1904										PAGE 8																																																											

TABLE A2. (Concluded)

PAGE 84

BASEPR = 8.1904
HOT
87.2420 0.460225E+06
CLTR 1.10 0.24

BP = 2 BP = 6 BP = 12 BP = 18 BP = 22
CP CP CP CP CP
BP = 3.375 BP = 10.125

PROPLUSIVE WING / CANARD PRESSURES
DCLC = 0.0 DMLC = 0.9205
CMJC CMUT
2.028 2.028
CNTR CNTR
1.12 -0.55

CLAERO = 1.1089 CDAERO = 0.3144
PSTAT PSTAT
2106.22 2106.22
CD CD
-1.49 -1.49

CLAERO = 1.1089 CDAERO = 0.3144
PSTAT PSTAT
2106.22 2106.22
CD CD
-1.49 -1.49

CLAERO = 1.1089 CDAERO = 0.3144
PSTAT PSTAT
2106.22 2106.22
CD CD
-1.49 -1.49

CLAERO = 1.1089 CDAERO = 0.3144
PSTAT PSTAT
2106.22 2106.22
CD CD
-1.49 -1.49

CLAERO = 1.1089 CDAERO = 0.3144
PSTAT PSTAT
2106.22 2106.22
CD CD
-1.49 -1.49

RUN: SEQ	X/C	BP = 2	BP = 6	BP = 12	BP = 18	BP = 22	MISC...
82 8	0.0	0.0	0.0	0.0	0.0	0.0	1 -0.7941
ALPHA	2.5	0.3276	0.3276	0.3276	0.3276	0.3276	2 0.1842
12.00	5.0	0.3276	0.3276	0.3276	0.3276	0.3276	3 -1.9354
BETA	10.0	0.3276	0.3276	0.3276	0.3276	0.3276	4 0.0212
-0.01	15.0	0.3276	0.3276	0.3276	0.3276	0.3276	5 -1.6082
	25.0	0.3276	0.3276	0.3276	0.3276	0.3276	6 -0.3050
	35.0	0.3276	0.3276	0.3276	0.3276	0.3276	7 1.0344
	50.0	0.3276	0.3276	0.3276	0.3276	0.3276	8 0.1260
	55.0	0.3276	0.3276	0.3276	0.3276	0.3276	9 0.4055
	70.0	0.3276	0.3276	0.3276	0.3276	0.3276	10 1.1042
	80.5	0.3276	0.3276	0.3276	0.3276	0.3276	11 0.6850
	81.0	0.3276	0.3276	0.3276	0.3276	0.3276	12 0.4055
	82.0	0.3276	0.3276	0.3276	0.3276	0.3276	
	84.0	0.3276	0.3276	0.3276	0.3276	0.3276	
	87.0	0.3276	0.3276	0.3276	0.3276	0.3276	
	89.0	0.3276	0.3276	0.3276	0.3276	0.3276	
	93.0	0.3276	0.3276	0.3276	0.3276	0.3276	
	96.0	0.3276	0.3276	0.3276	0.3276	0.3276	
	100.0	0.3276	0.3276	0.3276	0.3276	0.3276	
	96.0	0.3276	0.3276	0.3276	0.3276	0.3276	
	73.0	0.3276	0.3276	0.3276	0.3276	0.3276	
	50.0	0.3276	0.3276	0.3276	0.3276	0.3276	
	35.0	0.3276	0.3276	0.3276	0.3276	0.3276	
	25.0	0.3276	0.3276	0.3276	0.3276	0.3276	
	10.0	0.3276	0.3276	0.3276	0.3276	0.3276	
	5.0	0.3276	0.3276	0.3276	0.3276	0.3276	
	2.5	0.3276	0.3276	0.3276	0.3276	0.3276	

48

PAGE	
BASEPR - 8.1504	
HGT	RN
87.1804	0.103854E+07
CLTR	CDTR
0.47	0.12

0 CMUT 0.0 CMTR -0.31

PRESSURES
DWLC = 0
CMUW
0.0 CNTR
0.47

WING / CANARD	
DCLC = 0.0	CMUC
H/C	0.0
1 2.67	CN
-0.00	CV
	0.0

PROPLSIVE
R0 = 0.1113
VEL
29 159.16 O.
CM CROLL
31 0.00

2 2085.43 30
CD
0.18

RUN:SEQ	CLAE
64 3	PTOT
ALPHA	2115.
0.02	CL
BETA	0.4
-0.01	

***** CANARD *****				***** VING *****				***** FUSELAGE*****				***** MISC.***									
BP=3.375		BP=10.125		BP = 2		BP = 6		BP = 12		BP = 16		BP = 22		XLOC		CP		MD.		CP	
%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP
-0.2182	-0.2071	-0.2182	-0.2071	0.0	0.5345	0.5004	0.4095	0.3413	0.2617	38.2	-0.0721	1	-0.2810								
-0.2071	-0.2071	-0.2071	-0.2071	2.5	-0.2043	-0.2497	-0.4202	-0.6361	-0.5676	43.4	-0.0649	2	0.0147								
-0.2182	-0.2071	-0.2182	-0.2071	5.0	-0.2156	-0.2497	-0.3406	-0.4998	-0.4429	50.4	-0.0436	3	0.3159								
-0.2071	-0.2071	-0.2071	-0.2071	10.0	-0.2828	-0.3283	-0.3875	-0.4088	-0.4202	56.1	-0.0549	4	0.0147								
-0.2071	-0.2071	-0.2182	-0.2071	15.0	-0.2724	-0.2952	-0.3634	-0.4856	-0.4088	62.5	-0.1932	5	0.2481								
-0.2182	-0.2071	-0.2182	-0.2071	24.0	-0.2611	-0.2838	-0.3408	-0.3747	-0.3634	69.7	-0.1932	6	-0.0610								
-0.2071	-0.2071	-0.2071	-0.2071	33.0	-0.2152	-0.2481	-0.3139	-0.3128	-0.3129	75.9	-0.1154	7	0.5217								
-0.2071	-0.2071	-0.2071	-0.2071	54.0	-0.3159	-0.3138	-0.3796	0.1133	-0.3467	83.4	-0.1154	8	0.2035								
-0.2071	-0.2071	-0.2071	-0.2071	65.0	-0.4441	-0.4797	-0.4960	-0.5133	-0.4787	89.4	-0.1759	9	-0.0274								
-0.2071	-0.2071	-0.2071	-0.2071	78.5	-1.1015	-1.1448	-1.1880	-1.2140	-1.2313	95.4	-0.1068	10	0.5288								
-0.2182	-0.2071	-0.2182	-0.2071	79.5	-1.3958	-1.3988	-1.3637	-1.3088	-1.4456	101.1	-0.1759	11	0.2350								
-0.2071	-0.2071	-0.2071	-0.2071	80.5	-1.0536	-1.2261	-1.2116	-1.2467	-1.4164	---	---	12	-0.0345								
-0.2050	-0.1933	-0.2050	-0.1933	81.5	-0.6322	83.6188	-0.6780	-0.6248	-1.1236	38.2	-0.0482										
-0.1933	-0.1933	-0.1933	-0.1933	82.0	-0.6038	-1.2261	-0.7681	-0.8253	-0.9775	43.4	-0.0116										
-0.1933	-0.1933	-0.1933	-0.1933	84.0	-0.6205	-0.6839	-0.7083	-0.6946	-0.7785	50.4	-0.0649										
-0.1933	-0.1933	-0.1933	-0.1933	87.0	-0.5093	-0.5582	-0.5912	-0.5803	-0.6439	56.1	0.0057										
-0.1933	-0.1933	-0.1933	-0.1933	89.0	-0.4840	-0.4992	-0.5344	-0.5274	-0.5555	62.5	0.0057										
-0.1846	-0.1846	-0.1846	-0.1846	93.0	-0.3091	-0.3091	-0.3232	-0.3246	-0.3485	69.7	0.0144										
-0.1932	-0.1932	-0.1932	-0.1932	96.0	-0.2246	-0.2106	-0.2246	-0.2387	-0.4286	75.9	0.0144										
-0.1932	-0.1932	-0.1932	-0.1932	100.0	-0.1471	-0.0908	-0.1471	-0.1401	-0.2457	83.4	0.0480										
-0.1846	-0.1846	-0.1846	-0.1846	98.0	0.1415	0.2260	0.2260	0.1976	0.1838	89.4	0.1009										
-0.2019	-0.2019	-0.2019	-0.2019	84.0	0.3739	0.5076	-0.2457	0.4231	0.5428	95.4	0.1268										
-0.1932	-0.1932	-0.1932	-0.1932	73.5	0.2776	0.3104	0.3433	0.3433	0.3104	101.1	0.0317										
-0.2019	-0.2019	-0.2019	-0.2019	84.0	0.0804	0.0476	0.0476	0.0804	0.0147												
-0.1932	-0.1932	-0.1932	-0.1932	33.0	0.0147	0.0147	0.0147	0.0147	-0.0181												
-0.2071	-0.2071	-0.2182	-0.2071	24.0	-0.0679	-0.0451	-0.0585	-0.05													

TABLE A3. (Continued)

RUN: SEQ												PAGE 87											
CLASSED - 0.0000												BASELINE - 0.0000											
PTOT 2115.93												PSTAT 2085.53											
ALPHA 4.04												VEL 30.40											
BETA -0.01												CM 159.58											
												CD 0.15											
												CROLL 0.00											
												CN -0.34											
												H/C 0.01											
												CNUC 0.00											
												CMUJ 0.00											
												CNTR 0.66											
												CMTR -0.34											
												CLTR 0.65											
												CDTR 0.16											

TABLE A3.
(Concluded)

RUN:SEQ		PROPELLUSTIVE				WING		CANARD		PRESSURES		BASEP = 8.1904		PAGE	
64	9	CLAERO =	1.0835	CDARO =	0.3162	DCLC =	0.0	CHUC	CMUW	CMUT	0.0	HOT	87.3045	0.103263E+07	8
ALPHA	PTOT	Q	VEL	YAW	H/C							CLTR	0.32		1
12.03	2116.00	2085.83	30.17	159.09	0.01	2.67	0.0					CLTR	1.08	0.32	2
BETA	C.L.	CD	CM	CROLL	CN							CMTR			3
-0.01	1.08	0.32	-0.44	0.01	-0.00	0.00	1.12								4
***** CANARD *****															
BP=3.375 BP=10.125															
***** WING *****															
BP = 2 BP = 6 BP = 12 BP = 16 BP = 22															
%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP
0.0	-0.2600	0.0	-2.8436	0.0	-5.5699	0.0	-6.1860	0.0	-2.8649	0.0	-1.6001	0.0	-0.1018	0.0	-0.7141
2.5	-0.2437	2.5	-1.6001	2.5	-2.2846	2.5	-3.1856	2.5	-2.9119	2.5	-1.5772	2.5	-0.0831	2.5	-0.2753
5.0	-0.2437	5.0	-1.1780	5.0	-1.6001	5.0	-2.3186	5.0	-2.7979	5.0	-1.6001	5.0	-0.1278	5.0	-1.5386
10.0	-0.2356	10.0	-0.9384	10.0	-1.1663	10.0	-1.5316	10.0	-3.0375	10.0	-1.4632	10.0	-0.1625	10.0	-0.2094
15.0	-0.2437	15.0	-0.8015	15.0	-1.0297	15.0	-1.1437	15.0	-2.4900	15.0	-1.5316	15.0	-0.2148	15.0	-1.3078
20.0	-0.2519	20.0	-0.6760	20.0	-0.7873	20.0	-0.8700	20.0	-1.5048	20.0	-1.5202	20.0	-0.2148	20.0	-0.0315
25.0	-0.2519	25.0	-0.6152	25.0	-0.6482	25.0	-0.7801	25.0	-1.0109	25.0	-1.4057	25.0	-0.2148	25.0	-0.0315
30.0	-0.2193	30.0	-0.5162	30.0	-0.5832	30.0	-0.6482	30.0	-0.3513	30.0	-1.4727	30.0	-0.2148	30.0	-0.1581
35.0	-0.2275	35.0	-0.5967	35.0	-0.6314	35.0	-0.6835	35.0	-0.6140	35.0	-1.1002	35.0	-0.2148	35.0	-0.0186
40.0	-0.2275	40.0	-1.1523	40.0	-1.1697	40.0	-1.1697	40.0	-1.1697	40.0	-1.4727	40.0	-0.2148	40.0	-0.1581
45.0	-0.2193	45.0	-1.2840	45.0	-1.3310	45.0	-1.3310	45.0	-1.3310	45.0	-1.4073	45.0	-0.2148	45.0	-0.1581
50.0	-0.2193	50.0	-1.2311	50.0	-1.2370	50.0	-1.2370	50.0	-1.2370	50.0	-1.4727	50.0	-0.2148	50.0	-0.1581
55.0	-0.2275	55.0	-0.8256	55.0	-0.8320	55.0	-0.8320	55.0	-0.8320	55.0	-1.5248	55.0	-0.2148	55.0	-0.1581
60.0	-0.2275	60.0	-0.7377	60.0	-1.3545	60.0	-0.7436	60.0	-0.8611	60.0	-1.5777	60.0	-0.2148	60.0	-0.0379
65.0	-0.2267	65.0	-0.6614	65.0	-0.7025	65.0	-0.6908	65.0	-0.7436	65.0	-1.3545	65.0	-0.2148	65.0	-0.0379
70.0	-0.2267	70.0	-0.5439	70.0	-0.5815	70.0	-0.5791	70.0	-0.6320	70.0	-1.2805	70.0	-0.2148	70.0	-0.0379
75.0	-0.2267	75.0	-0.4832	75.0	-0.4902	75.0	-0.5255	75.0	-0.6033	75.0	-1.1474	75.0	-0.2148	75.0	-0.0379

TABLE A4. (Continued)

TABLE A4. (Concluded)

TABLE A5. RUN 66, 886V, DELF=15, CMU=1.0, (BN/3)=1

RUN: SEQ										PAGE 103									
66	3	CLARO =	0.7803	CDARO =	0.3068	WING / CANARD	PRESSURES	BASEPR =	8.1904										
ALPHA	0.09	PSTAT	0	VEL	YAW	H/C	CMUC	CMU	CMUT										
BETA	-0.01	CL	2104.43	13.34	105.36	0.01	2.66	0.0	1.054										
		CD	-0.60	CM	CKOLL	CN	CV	CNTR	CMTR										
				-0.85	0.00	-0.00	0.01	0.81	-1.50										
			</																

TABLE A5. (Continued)

PROPELLSIVE										WING / CANARD										PRESSURES										BASEPR = 8.1904										PAGE 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TABLE A5. (Concluded)

TABLE A6. (Concluded)

RUN:SEQ		CLAERO =		1.3178		CDAERO =		0.6275		WING / CANARD		PRESSURES		DMLC =		1.2361		BASEPR =		8.1004		PAGE		110	
67 6		PTOT		PSTAT		Q		VEL		YAW		H/C		CMUC		CMUW		HGT		RN					
8.01		2118.90		2111.78		7.12		76.66		0.01		2.66		0.0		2.007		87.1003		0.508532E+06					
BETA		CL		CD		CM		CROLL		CN		CY		CNR		CMT		CLTR		CDTR					
-0.01		2.55		-0.95		-1.33		0.00		-0.01		0.02		1.45		-2.56		1.42		0.33					
***** CANARD *****		BP=3.375		BP=10.125																					
XX/C		CP		CP		XX/C		CP		BP = 2		BP = 6		BP = 12		BP = 16		BP = 22							
0.0		-0.4507		-0.4161		0.0		-1.6131		-3.4499		-5.2383		-3.7882		-3.4016		-2.2898							
2.5		-0.4161		-0.4507		2.5		-1.3232		-1.8065		-2.9183		-3.4016		-3.4016		-1.9999							
5.0		-0.4507		-0.4507		5.0		-1.0815		-1.4198		-2.0482		-3.3049		-1.9514		-1.9514							
10.0		-0.4507		-0.4507		10.0		-0.9847		-1.2264		-1.5648		-3.2565		-1.9514		-1.9514							
15.0		-0.4851		-0.4507		15.0		-0.8881		-0.9847		-1.3232		-2.2415		-1.8548		-1.8548							
25.0		-0.4507		-0.4507		25.0		-0.3398		-0.8881		-1.0815		-1.3232		-1.8065		-1.8065							
35.0		-0.4507		-0.4507		35.0		-0.9594		-0.9594		-1.0991		-0.9594		-1.8582		-1.8582							
50.0		-0.4507		-0.4851		50.0		-1.1000		-1.2838		-1.3574		-2.9159		-1.8582		-1.8582							
65.0		-0.4507		-0.4161		65.0		-2.7554		-2.9761		-3.1969		-1.8517		-1.8517		-1.8517							
75.0		-0.4507		-0.4161		75.0		-1.4161		-47.4098		-91.0632		-73.7162		-80.3845		-3.8590							
79.0		-0.4507		-0.4507		80.5		-19.5602		0.8988		7.4181		29.5179		-7.1662		-7.1662							
80.5		-0.4216		-0.4216		81.3		16.8007		204.6313		6.6714		-9.0825		-13.0893		-13.0893							
81.0		-0.4216		-0.3967		82.0		-6.7599		-5.7476		5.8515		-13.3631		-5.9217		-5.9217							
82.0		-0.4216		-0.3967		84.0		2.5899		-0.6456		0.9472		-8.7341		-1.1931		-1.1931							
84.0		-0.4216		-0.3967		87.0		4.4813		-3.9307		0.8975		0.8975		-0.9691		-0.9691							
87.0		-0.3967		-0.4010		89.0		-0.5601		-0.6199		-3.7639		-3.0153		0.8174		0.8174							
89.0		-0.3642		-0.4010		93.0		-0.1109		0.2484		-0.5900		-0.6199		-2.7759		-2.7759							
93.0		-0.4010		-0.4010		96.0		-0.1109		-1.3685		1.1467		1.9552		-4.3029		-4.3029							
96.0		-0.4010		-0.4010		100.0		-3.0454		-2.8957		-2.4165		-2.4464		-2.5363		-2.5363							
100.0		-0.4377		-0.4010		96.0		0.1287		0.1885		0.0388		-0.0388		-0.1109		-0.1109							
96.0		-0.4010		-0.4377		84.0		0.4281		-0.6199		1.6258		0.3682		-0.4104		-0.4104							
84.0		-0.4377		-0.4010		73.5		0.1585		0.2983		0.2983		0.2983		0.2983		0.2983							
73.0		-0.4010		-0.4377		54.0		0.0188		0.0188		0.1585		0.1585		0.1585		0.1585							
50.0		-0.4010		-0.4010		35.0		0.1585		0.1585		0.1585		0.1585		0.1585		0.1585							
35.0		-0.4507		-0.4507		25.0		0.1270		0.1753		0.1753		0.1753		0.1753		0.1753							
25.0		-0.4507		-0.4161		10.0		0.2720		0.3203		0.3585		0.3585		0.3585		0.3585							
10.0		-0.4507		-0.4507		5.0		0.4170		0.4170		0.4653		0.4653		0.4653		0.4653							
5.0		-0.4507		-0.4507		2.5		0.4653		0.4653		0.5126		0.4853		0.4853		0.4853							
2.5		-0.4507		-0.4507																					

TABLE A7. RUN 75. BC16V. DELF=48. CMU=0. (BN/S)=1

PAGE 133

RUN: SEQ		CLARO =		PROPLUSIVE		WING / CANARD		PRESSURES		BASEPR = 8.1914		HGT		RN	
75 10		PTOT		VEL		YAW		H/C		87.4824		O.108414E+07		CDTR	
ALPHA		2133.33		30.06		186.41		0.01		2.87		0.0		0.0	
BETA		CL		CM		CROLL		CN		CY		CNR		0.52	
-0.01		0.53		-0.18		0.00		-0.00		0.01		0.52		-0.18	
		CD		0.21											

TABLE A7. (Continued)

RUN:SEQ										PROPLUSTIVE										WING / CANARD PRESSURES										PAGE	
75	12	CLAERO =	0.7283	CDAERO =	0.2632	DCLC =	0.0	CMJC	CMUJ	CMUT	0.0	DMLC = 0.0										BASEPR = 8.1914									
ALPHA	PTOT	PSTAT	2103.08	30.17	156.90	0.01	2.67	0.0	0.0	0.0	0.0	0.0										HGT RM									
4.01	2133.26	CD	0.26	CM	CROLL	CM	0.0	0.00	0.00	0.00	0.00	0.00										87.4835 0.106275E+07									
BETA	CL	CD	0.26	CM	CROLL	CM	0.0	0.00	0.00	0.00	0.00	0.00										CLTR CDR									
-0.01	0.73	0.26	-0.14	0.00	0.00	-0.00	0.00	0.00	0.00	0.00	0.00	0.74										0.72 0.26									
***** CANARD *****										***** WING *****										***** FUSELAGE *****											
BP=3.375 BP=10.125		BP=2 BP=6 BP=12 BP=16 BP=22		BP=2 BP=6 BP=12 BP=16 BP=22		BP=2 BP=6 BP=12 BP=16 BP=22		BP=2 BP=6 BP=12 BP=16 BP=22		BP=2 BP=6 BP=12 BP=16 BP=22		BP=2 BP=6 BP=12 BP=16 BP=22		BP=2 BP=6 BP=12 BP=16 BP=22		BP=2 BP=6 BP=12 BP=16 BP=22		BP=2 BP=6 BP=12 BP=16 BP=22		BP=2 BP=6 BP=12 BP=16 BP=22											
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP								
0.0	0.1546	0.0	0.1453	0.0	0.2480	0.0	0.2996	0.0	0.3833	0.0	0.4578	0.0	0.5078	0.0	0.5445	0.0	0.5731	0.0	0.5966	0.0	0.6115	0.0	0.6267								
2.5	-0.6021	2.5	0.0769	2.5	-0.0486	2.5	-0.0727	2.5	-0.0841	2.5	-0.0966	2.5	-0.1078	2.5	-0.1186	2.5	-0.1286	2.5	-0.1371	2.5	-0.1448	2.5	-0.1515								
5.0	-0.5370	5.0	0.0084	5.0	-0.0084	5.0	-0.0157	5.0	-0.0217	5.0	-0.0277	5.0	-0.0327	5.0	-0.0377	5.0	-0.0421	5.0	-0.0458	5.0	-0.0486	5.0	-0.0513								
10.0	-0.0650	10.0	-0.0084	10.0	-0.0084	10.0	-0.0157	10.0	-0.0217	10.0	-0.0277	10.0	-0.0327	10.0	-0.0377	10.0	-0.0421	10.0	-0.0458	10.0	-0.0486	10.0	-0.0513								
15.0	-0.4537	15.0	-0.0153	15.0	-0.0231	15.0	-0.0311	15.0	-0.0383	15.0	-0.0449	15.0	-0.0508	15.0	-0.0561	15.0	-0.0608	15.0	-0.0645	15.0	-0.0674	15.0	-0.0694								
20.0	-0.3742	20.0	-0.0208	20.0	-0.0278	20.0	-0.0353	20.0	-0.0421	20.0	-0.0483	20.0	-0.0538	20.0	-0.0586	20.0	-0.0628	20.0	-0.0665	20.0	-0.0694	20.0	-0.0719								
25.0	-0.3092	25.0	-0.0254	25.0	-0.0318	25.0	-0.0383	25.0	-0.0449	25.0	-0.0508	25.0	-0.0561	25.0	-0.0608	25.0	-0.0645	25.0	-0.0674	25.0	-0.0694	25.0	-0.0719								
30.0	-0.3010	30.0	-0.0318	30.0	-0.0383	30.0	-0.0449	30.0	-0.0508	30.0	-0.0561	30.0	-0.0608	30.0	-0.0645	30.0	-0.0674	30.0	-0.0694	30.0	-0.0694	30.0	-0.0719								
35.0	-0.3092	35.0	-0.0318	35.0	-0.0383	35.0	-0.0449	35.0	-0.0508	35.0	-0.0561	35.0	-0.0608	35.0	-0.0645	35.0	-0.0674	35.0	-0.0694	35.0	-0.0694	35.0	-0.0719								
40.0	-0.3092	40.0	-0.0318	40.0	-0.0383	40.0	-0.0449	40.0	-0.0508	40.0	-0.0561	40.0	-0.0608	40.0	-0.0645	40.0	-0.0674	40.0	-0.0694	40.0	-0.0694	40.0	-0.0719								
45.0	-0.3092	45.0	-0.0318	45.0	-0.0383	45.0	-0.0449	45.0	-0.0508	45.0	-0.0561	45.0	-0.0608	45.0	-0.0645	45.0	-0.0674	45.0	-0.0694	45.0	-0.0694	45.0	-0.0719								
50.0	-0.3092	50.0	-0.0318	50.0	-0.0383	50.0	-0.0449	50.0	-0.0508	50.0	-0.0561	50.0	-0.0608	50.0	-0.0645	50.0	-0.0674	50.0	-0.0694	50.0	-0.0694	50.0	-0.0719								
55.0	-0.3092	55.0	-0.0318	55.0	-0.0383	55.0	-0.0449	55.0	-0.0508	55.0	-0.0561	55.0	-0.0608	55.0	-0.0645	55.0	-0.0674	55.0	-0.0694	55.0	-0.0694	55.0	-0.0719								
60.0	-0.3092	60.0	-0.0318	60.0	-0.0383	60.0	-0.0449	60.0	-0.0508	60.0	-0.0561	60.0	-0.0608	60.0	-0.0645	60.0	-0.0674	60.0	-0.0694	60.0	-0.0694	60.0	-0.0719								
65.0	-0.3092	65.0	-0.0318	65.0	-0.0383	65.0	-0.0449	65.0	-0.0508	65.0	-0.0561	65.0	-0.0608	65.0	-0.0645	65.0	-0.0674	65.0	-0.0694	65.0	-0.0694	65.0	-0.0719								
70.0	-0.3092	70.0	-0.0318	70.0	-0.0383	70.0	-0.0449	70.0	-0.0508	70.0	-0.0561	70.0	-0.0608	70.0	-0.0645	70.0	-0.0674	70.0	-0.0694	70.0	-0.0694	70.0	-0.0719								
75.0	-0.3092	75.0	-0.0318	75.0	-0.0383	75.0	-0.0449	75.0	-0.0508	75.0	-0.0561	75.0	-0.0608	75.0	-0.0645	75.0	-0.0674	75.0	-0.0694	75.0	-0.0694	75.0	-0.0719								
80.0	-0.3092	80.0	-0.0318	80.0	-0.0383	80.0	-0.0449	80.0	-0.0508	80.0	-0.0561	80.0	-0.0608	80.0	-0.0645	80.0	-0.0674	80.0	-0.0694	80.0	-0.0694	80.0	-0.0719								
85.0	-0.3092	85.0	-0.0318	85.0	-0.0383	85.0	-0.0449	85.0	-0.0508	85.0	-0.0561	85.0	-0.0608	85.0	-0.0645	85.0	-0.0674	85.0	-0.0694	85.0	-0.0694	85.0	-0.0719								
90.0	-0.3092	90.0	-0.0318	90.0	-0.0383	90.0	-0.0449	90.0	-0.0508	90.0	-0.0561	90.0	-0.0608	90.0	-0.0645	90.0	-0.0674	90.0	-0.0694	90.0	-0.0694	90.0	-0.0719								
95.0	-0.3092	95.0	-0.0318	95.0	-0.0383	95.0	-0.0449	95.0	-0.0508	95.0	-0.0561	95.0	-0.0608	95.0	-0.0645	95.0	-0.0674	95.0	-0.0694	95.0	-0.0694	95.0	-0.0719								
100.0	-0.3092	100.0	-0.0318	100.0	-0.0383	100.0	-0.0449	100.0	-0.0508	100.0	-0.0561	100.0	-0.0608	100.0	-0.0645	100.0	-0.0674	100.0	-0.0694	100.0	-0.0694	100.0	-0.0719								
105.0	-0.3092	105.0	-0.0318	105.0	-0.0383	105.0	-0.0449	105.0	-0.0508	105.0	-0.0561	105.0	-0.0608	105.0	-0.0645	105.0	-0.0674	105.0	-0.0694	105.0	-0.0694	105.0	-0.0719								
110.0	-0.3092	110.0	-0.0318	110.0	-0.0383	110.0	-0.0449	110.0	-0.0508	110.0	-0.0561	110.0	-0.0608	110.0	-0.0645	110.0	-0.0674	110.0	-0.0694	110.0	-0.0694	110.0	-0.0719								
115.0	-0.3092	115.0	-0.0318	115.0	-0.0383	115.0	-0.0449	115.0	-0.0508	115.0	-0.0561	115.0	-0.0608	115.0	-0.0645	115.0	-0.0674	115.0	-0.0694	115.0	-0.0694	115.0	-0.0719								
120.0	-0.3092	120.0	-0.0318	120.0	-0.0383	120.0	-0.0449	120.0	-0.0508	120.0	-0.0561	120.0	-0.0608	120.0	-0.0645	120.0	-0.0674	120.0	-0.0694	120.0	-0.0694	120.0	-0.0719								
125.0	-0.3092	125.0	-0.0318	125.0	-0.0383	125.0	-0.0449	125.0	-0.0508	125.0	-0.0561	125.0	-0.0608	125.0	-0.0645	125.0	-0.0674	125.0	-0.0694	125.0	-0.0694	125.0	-0.0719								
130.0	-0.3092	130.0	-0.0318	130.0	-0.0383	130.0	-0.0449	130.0	-0.0508	130.0	-0.0561	130.0	-0.0608	130.0	-0.0645	130.0	-0.0674	130.0	-0.0694	130.0	-0.0694	130.0	-0.0719								
135.0	-0.3092	135.0	-0.0318	135.0	-0.0383	135.0	-0.0449	135.0	-0.0508	135.0	-0.0561	135.0	-0.0608	135.0	-0.0645	135.0	-0.0674	135.0	-0.0694	135.0	-0.0694	135.0	-0.0719								
140.0	-0.3092	140.0	-0.0318	140.0	-0.0383	140.0	-0.0449	140.0	-0.0508	140.0	-0.0561	140.0	-0.0608	140.0	-0.0645	140.0	-0.0674	140.0	-0.0694	140.0	-0.0694	140.0	-0.0719								
145.0	-0.3092	145.0	-0.0318	145.0	-0.0383	145.0	-0.0449	145.0	-0.0508	145.0	-0.0561	145.0	-0.0608	145.0	-0.0645	145.0	-0.0674	145.0	-0.0694	145.0	-0.0694	145.0	-0.0719								
150.0	-0.3092	150.0	-0.0318	150.0	-0.0383	150.0	-0.0449	150.0	-0.0508	150.0	-0.0561	150.0	-0.0608	150.0	-0.0645	150.0	-0.0674	150.0	-0.0694	150.0	-0.0694	150.0	-0.0719								
155.0	-0.3092	155.0	-0.0318	155.0	-0.0383	155.0	-0.0449	155.0	-0.0508	155.0	-0.0561	155.0	-0.0608	155.0	-0.0645	155.0	-0.0674	155.0	-0.0694	155.0	-0.0694	155.0	-0.0719								
160.0	-0.3092	160.0	-0.0318	160.0	-0.0383	160.0	-0.0449	160.0	-0.0508	160.0	-0.0561	160.0	-0.0608	160.0	-0.0645	160.0	-0.0674	160.0	-0.0694	160.0	-0.0694	160.0	-0.0719								
165.0	-0.3092	165.0	-0.0318	165.0	-0.0383	165.0	-0.0449	165.0	-0.0508	165.0	-0.0561	165.0	-0.0608	165.0	-0.0645	165.0	-0.0674	165.0	-0.0694	165.0	-0.0694	165.0	-0.0719								
170.0	-0.3092	170.0	-0.0318	170.0	-0.0383	170.0	-0.0449	170.0	-0.0508	170.0	-0.0561	170.0	-0.0608	170.0	-0.0645	170.0	-0.0674	170.0	-0.0694	170.0	-0.0694	170.0	-0.0719								
175.0	-0.3092	175.0	-0.0318	175.0	-0.0383	175.0	-0.0449	175.0	-0.0508	175.0	-0.0561	175.0	-0.0608	175.0	-0.0645	175.0	-0.0674	175.0	-0.0694	175.0	-0.0694	175.0	-0.0719								
180.0	-0.3092	180.0	-0.0318	180.0	-0.0383	180.0	-0.0449	180.0	-0.0508	180.0	-0.0561	180.0	-0.0608	180.0	-0.0645	180.0	-0.0674	180.0	-0.0694	180.0	-0.0694	180.0	-0.0719								
185.0	-0.3092	185.0	-0.0318	185.0	-0.0383	185.0	-0.0449	185.0	-0.0508	185.0	-0.0561	185.0	-0.0608	185.0	-0.0645	185.0	-0.0674	185.0	-0.0694	185.0	-0.0694	185.0	-0.0719								
190.0	-0.3092	190.0	-0.0318	190.0	-0.0383	190.0	-0.0449	190.0	-0.0508	190.0	-0.0561	190.0	-0.0608	190.0	-0.0645	190.0	-0.0674	190.0	-0.0694	190.0	-0.0694	190.0	-0.0719								
195.0	-0.3092	195.0	-0.0318	195.0	-0.0383	195.0	-0.0449	195.0	-0.0508	195.0	-0.0561	195.0	-0.0608	195.0	-0.0645	195.0	-0.0674	195.0	-0.0694	195.0	-0.0694	195.0	-0.0719								
200.0	-0.3092	200.0	-0.0318	200.0	-0.0383	200.0	-0.0449	200.0	-0.0508	200.0	-0.0561	200.0	-0.0608	200.0	-0.0645	200.0	-0.0674	200.0	-0.0694	200.0	-0.0694	200.0	-0.0719								
205.0	-0.3092	205.0	-0.0318	205.0	-0.0383	205.0	-0.0449	205.0	-0.0508	205.0	-0.0561	205.0	-0.0608	205.0	-0.0645	205.0	-0.0674	205.0	-0.0694	205.0	-0.0694	205.0	-0.0719								
210.0	-0.3092	210.0	-0.0318	210.0	-0.0383	210.0	-0.0449	210.0	-0.0508	210.0	-0.0561	210.0	-0.0608	210.0	-0.0645	210.0	-0.0674	210.0	-0.0694	210.0	-0.0694	210.0	-0.0719								
215.0	-0.3092	215.0	-0.0318	215.0	-0.0383	215.0	-0.0449	215.0	-0.0508	215.0	-0.0561	215.0	-0.0608	215.0	-0.0645	215.0	-0.0674</														

TABLE A7. (Concluded)

RUN-SEQ		PROPLUSIVE				WING / CANARD		PRESSURES		BASEPR = 8.1914		PAGE 137	
75 16	CLARO = 1.1935	CDARO = 0.4592	DCLC = 0.0	DMC = 0.0	CMUT	CMUT	CMUT	CMUT	CMUT	CMUT	CMUT	CMUT	CMUT
ALPHA	PSTAT	VEL	YAW	H/C	CMC	CMC	CMC	CMC	CMC	CMC	CMC	CMC	CMC
12.08	2133.54	2103.48	30.06	156.80	0.01	2.66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
BETA	CL	CD	CM	CROLL	CN	CV	CNTR	CNTR	CNTR	CNTR	CNTR	CNTR	CNTR
-0.01	1.19	0.46	-0.06	0.00	-0.00	0.00	1.25	-0.06	1.18	0.46	0.46	0.46	0.46
***** CANARD *****													
BP=3.375	BP=10.125	BP=2	BP=6	BP=12	BP=16	BP=22	*****						
%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	XLOC	CP	NO.	CP	**MISC.**	
-5.0868	-1.7054	0.0	0.0018	-1.0746	-4.4754	-3.6533	-1.5784	38.2	-0.3180	1	-0.6242	1	-0.6242
-2.3427	-1.5748	2.5	0.4104	-0.9142	-2.0593	-3.5363	-1.9555	43.4	-0.2831	2	0.3028	2	0.3028
-1.6074	-1.5746	5.0	0.3875	-0.7196	-1.3723	-3.5592	-1.5097	50.4	-0.2134	3	1.1207	3	1.1207
-0.0556	-1.5339	10.0	0.4562	-0.6623	-1.0631	-1.7845	-1.5211	56.1	-0.1611	4	0.2657	4	0.2657
-0.0684	-1.5094	15.0	0.4906	-0.6165	-0.8914	-1.9142	-1.4982	62.5	-0.3008	5	-1.2200	5	-1.2200
-0.7988	-1.4441	24.0	0.4906	-0.5707	-0.7196	-0.7196	-1.4410	69.7	-0.2919	6	0.0711	6	0.0711
-0.6518	-1.3379	33.0	0.4917	-0.5579	-0.6573	-0.6242	-1.4518	76.9	-0.2222	7	0.2816	7	0.2816
-0.5375	-0.9050	54.0	0.4586	-0.5248	-0.5911	-0.3262	-1.1538	83.4	-0.1960	8	-0.4845	8	-0.4845
-0.5130	-0.7335	65.0	0.5359	-0.5708	-0.5969	-0.8882	-0.8584	89.4	-0.2483	9	0.4376	9	0.4376
-0.5538	-0.7417	78.5	0.7973	-0.7973	-0.8148	-0.8322	-0.9804	95.4	-0.2670	10	0.0120	10	0.0120
-0.3170	-0.7417	79.5	0.7000	-0.6823	-0.7236	-0.7295	-0.7413	101.1	-0.1960	11	-0.7470	11	-0.7470
-0.8805	-0.8805	80.5	0.6882	-0.6528	-0.7118	-0.7295	-0.6823	101.1	-0.1960	12	-0.3001	12	-0.3001
-0.9181	-0.9181	81.3	0.7000	-0.6528	-0.7118	-0.7118	-0.7413	38.2	-0.3180	---BOTTOM---			
-0.8887	-0.8887	82.0	0.6882	-0.6184	-0.7118	-0.6381	-0.7825	43.4	-0.1178				
-0.9004	-0.9004	84.0	0.7118	-0.6587	-0.7177	-0.6351	-0.7061	50.4	-0.0308				
-0.3168	-0.3168	87.0	0.7236	-0.7295	-0.7059	-0.8880	-0.6764	56.1	-0.1178				
-0.8764	-0.8764	89.0	0.8179	-0.7896	-0.7966	-0.7612	-0.8218	62.5	-0.1528				
-0.8909	-0.8909	93.0	0.8534	-0.7825	-0.8108	-0.3569	-0.9669	69.7	-0.1960				
-0.6928	-0.6928	96.0	0.7966	-0.7470	-0.8038	-0.8250	-0.9669	76.9	-0.2136				
-0.93.0	100.0	100.0	0.9548	-0.6264	-0.6264	-0.8179	-0.9385	83.4	-0.2398				
-0.6840	-0.6840	98.0	0.2957	-0.4234	-0.3880	-0.2745	-0.2106	89.4	-0.2659				
-0.8845	-0.8845	98.0	0.5937	-0.7143	-0.6433	-0.5724	-0.3809	96.4	-0.1352				
-0.2833	-0.2833	84.0	0.5937	-0.7143	-0.6433	-0.5724	-0.3809	101.1	-0.3790				
-0.8845	-0.8845	73.5	0.5345	-0.6007	-0.5676	-0.3690	-0.2035						
-0.2833	-0.2833	74.0	0.2697	-0.3359	-0.3359	-0.2035	-0.2035						
-0.2833	-0.2833	75.0	0.2697	-0.3359	-0.3359	-0.2035	-0.2035						
-0.6494	-0.6494	33.0	0.2035	-0.2697	-0.3028	-0.3028	-0.3028						
-0.50.0	0.7888	50.0	0.7888	-0.50.0	0.7888	-0.50.0	0.7888						
-0.6876	-0.6876	24.0	0.6876	-0.2652	-0.3224	-0.3453	-0.2423						
-0.3283	-0.3283	10.0	0.2079	-0.2995	-0.4255	-0.4484	-0.4021						
-0.2629	-0.2629	5.0	0.2308	-0.3339	-0.4484	-0.5056	-0.4352						
-0.3038	-0.3038	10.0	0.3038	-0.3038	-0.3038	-0.3038	-0.3038						
-0.2629	-0.2629	5.0	0.2629	-0.3201	-0.3568	-0.4598	-0.4352						
-0.50.5	0.6050	5.5	0.6050	-0.50.5	0.6050	-0.50.5	0.6050						

TABLE A8. RUN 76, BC1W6V, DELT-45, CMJ-O.5, (BN/5)-1

SPLA-2C		PARALLEL NIVE		WING		BP = 2		BP = 6		BP = 12		BP = 16		BP = 22		FUSELAGE		MISC	
76	2	CLARO =	0.9376	CDARO =	0.6986	DLCL =	0.1844	DWLC =	0.4560										
ALPHA	PTOT	PTOT	0	VEL	YAW	H/C	CMUC	CMJW	CMJW										
-0.01	2132.84	2108.68	26.89	148.62	0.01	2.66	0.225	0.537	0.752										
BETA	CL	CD	CM	CROLL	CN	CV	CHTR	CHTR	CHTR										
-0.01	1.58	0.27	-0.81	0.00	-0.01	0.03	1.05	-0.30											
CANARD		BP=3.375		BP=10.125		XX/C		CP		XX/C		CP		XX/C		CP		XX/C	
0.0	0.2425	-1.0811	0.0	-0.4580	-0.8811	-0.8835	-3.0697												
2.5	-0.5517	-1.4006	2.5	0.6802	0.612	0.9578	-1.8410												
5.0	-0.5152	-0.9442	5.0	0.5266	0.4626	-1.0219	-1.4058												
10.0	-0.0679	-0.7708	10.0	0.2953	0.1811	-0.9707	-1.0603												
15.0	-0.5394	-0.7982	15.0	0.1427	0.0147	-1.0347	-0.9067												
25.0	-0.5243	-0.6612	24.0	-0.0749	-0.2028	-0.7916	-0.8044												
35.0	-0.5334	-0.6612	33.0	-0.2209	-0.3319	-0.8869	-0.8128												
50.0	-0.6795	-0.6795	54.0	-0.6279	-0.7018	-0.8869	-0.8128												
56.0	-0.8073	-0.9442	55.0	-1.0162	-1.1136	-1.1428	-1.1089												
65.0	-1.1633	-1.4098	78.5	-3.1593	-3.2370	-2.9351	-1.5912												
76.0	-0.3783	-3.0712	79.5	-21.9119	-22.1030	-13.5233	-3.9870												
79.0	-4.4770	-4.8879	80.5	-22.2814	-20.1788	-14.3670	-29.1210												
80.5	-22.1755	-19.2103	81.3	-21.7538	44.1829	-14.9663	-21.2591												
81.0	-19.4605	-18.4194	82.0	-19.0783	17.1675	-14.6503	-11.3520												
82.0	-14.4592	-16.1591	84.0	0.0183	-5.3062	-13.7342	-10.1759												
84.0	-0.3243	-0.0447	87.0	0.4071	-1.0426	-2.7164	-5.2731												
87.0	0.0447	-1.5032	89.0	-0.7837	-0.6172	0.6910	-3.3047												
89.0	-0.9382		93.0	-0.6330	-0.6172	-0.2604	-0.5300												
93.0	-0.7824		96.0	-0.3330	-0.7123	-0.3873	-0.7123												
96.0	-0.3343		100.0	-0.3555	-0.2287	-0.1336	-0.0701												
100.0	1.2047		96.0	0.4135	0.2391	0.3342	0.4214												
96.0	0.6495		84.0	0.3580	0.2708	0.2312	0.4848												
84.0	1.2047		73.5	0.1492	0.1492	0.2602	0.3712												
73.0	0.6495		54.0	-0.1468	-0.0728	-0.0358	0.1492												
50.0	0.7859		33.0	-0.2949	-0.3319	-0.2949	-0.0728												
35.0	0.6598		24.0	-0.3308	-0.3180	-0.3436	-0.1388												
25.0	0.3612		10.0	-0.4716	-0.3948	-0.3948	-0.1900												
10.0	0.2425		5.0	-0.4588	-0.3308	-0.4588	-0.2540												
5.0	0.0964		2.5	-0.4332	-0.3692	-0.5228	-0.0749												
2.5	0.1786																		
FUSELAGE		XLOC		CP		XLOC		CP		XLOC		CP		XLOC		CP		XLOC	
38.2	-0.3243	38.2	-0.3243	38.2	-0.3243	38.2	-0.3243	38.2	-0.3243	38.2	-0.3243	38.2	-0.3243	38.2	-0.3243	38.2	-0.3243	38.2	-0.3243
43.4	-0.3538	43.4	-0.3538	43.4	-0.3538	43.4	-0.3538	43.4	-0.3538	43.4	-0.3538	43.4	-0.3538	43.4	-0.3538	43.4	-0.3538	43.4	-0.3538
50.4	-0.2174	50.4	-0.2174	50.4	-0.2174	50.4	-0.2174	50.4	-0.2174	50.4	-0.2174	50.4	-0.2174	50.4	-0.2174	50.4	-0.2174	50.4	-0.2174
56.1	-0.1103	56.1	-0.1103	56.1	-0.1103	56.1	-0.1103	56.1	-0.1103	56.1	-0.1103	56.1	-0.1103	56.1	-0.1103	56.1	-0.1103	56.1	-0.1103
62.5	-0.3733	62.5	-0.3733	62.5	-0.3733	62.5	-0.3733	62.5	-0.3733	62.5	-0.3733	62.5	-0.3733	62.5	-0.3733	62.5	-0.3733	62.5	-0.3733
69.7	-0.3733	69.7	-0.3733	69.7	-0.3733	69.7	-0.3733	69.7	-0.3733	69.7	-0.3733	69.7	-0.3733	69.7	-0.3733	69.7	-0.3733	69.7	-0.3733
76.9	-0.1687	76.9	-0.1687	76.9	-0.1687	76.9	-0.1687	76.9	-0.1687	76.9	-0.1687	76.9	-0.1687	76.9	-0.1687	76.9	-0.1687	76.9	-0.1687
83.4	-0.2272	83.4	-0.2272	83.4	-0.2272	83.4	-0.2272	83.4	-0.2272	83.4	-0.2272	83.4	-0.2272	83.4	-0.2272	83.4	-0.2272	83.4	-0.2272
89.4	-0.3733	89.4	-0.3733	89.4	-0.3733	89.4	-0.3733	89.4	-0.3733	89.4	-0.3733	89.4	-0.3733	89.4	-0.3733	89.4	-0.3733	89.4	-0.3733
95.4	-0.3538	95.4	-0.3538	95.4	-0.3538	95.4	-0.3538	95.4	-0.3538	95.4	-0.3538	95.4	-0.3538	95.4	-0.3538	95.4	-0.3538	95.4	-0.3538
101.1	-0.2759	101.1	-0.2759	101.1	-0.2759	101.1	-0.2759	101.1	-0.2759	101.1	-0.2759	101.1	-0.2759	101.1	-0.2759	101.1	-0.2759	101.1	-0.2759
101.1	-0.2366	101.1	-0.2366	101.1	-0.2366	101.1	-0.2366	101.1	-0.2366	101.1	-0.2366	101.1	-0.2366	101.1	-0.2366	101.1	-0.2366	101.1	-0.2366

TABLE A8. (Continued)

RUN: SEQ										PAGE 140										
76	4	GLAERO =	1.1080	CDAERO =	0.7649	WING / CANARD	DCLC =	0.1868	DWLC =	0.4819	BJEPR = 8.1914									
ALPHA	PTOT	PSTAT	2106.04	27.57	150.58	0.01	2.65	0.218	0.514	0.732	M3T RN									
3.99	2133.61	2106.04	27.57	150.58	0.01	2.65	0.218	0.514	0.732	801.7388	0.100513E+07									
BETA	CL	CD	0.43	-0.49	-0.02	-0.01	0.06	1.26	-0.29	0.64	CLTR COTR									
-0.01	1.76	0.43	-0.49	-0.02	-0.01	0.06	1.26	-0.29	0.64	1.22	0.64									
CANARD										FUSELAGE										
BP=3.375 BP=10.125										---TOP---										
X/C										XLOC CP										
BP=2 BP=5 BP=12 BP=16 BP=22										NO. CP										
0.0	-1.0737	-4.7686	0.0	-0.4096	-0.4596	-1.2959	CP	-1.6205	CP	38.2	-0.3957	1	-0.5870							
2.5	-1.3853	-2.2757	2.5	0.6265	0.5141	-1.0837	CP	-1.3458	CP	43.4	-0.3957	2	-0.1539							
5.0	-0.8867	-1.7503	5.0	0.4766	0.3393	-1.1836	CP	-1.0962	CP	50.4	-0.2827	3	-0.8757							
10.0	-0.0675	-1.2695	10.0	0.2145	0.1147	-1.4082	CP	-0.9589	CP	56.1	-0.1392	4	0.0626							
15.0	-0.7976	-1.2072	15.0	0.0772	-0.0726	-1.3583	CP	-0.8840	CP	62.8	-0.4147	5	-0.9479							
20.0	-0.7175	-0.9490	20.0	-0.1475	-0.2598	-1.2709	CP	-0.8965	CP	69.7	-0.4052	6	-0.1178							
25.0	-0.6730	-0.8599	25.0	-0.2983	-0.4065	-1.2727	CP	-0.9840	CP	76.9	-0.2057	7	0.1813							
30.0	-0.7887	-0.7887	30.0	-0.6592	-0.6953	-1.1283	CP	-0.8400	CP	83.4	-0.2437	8	-1.0560							
35.0	-0.9134	-1.1182	35.0	-1.0418	-1.0988	-1.3078	CP	-1.5643	CP	89.4	-0.3672	9	-0.7313							
40.0	-1.2784	-1.6079	40.0	-3.1414	-3.2270	-2.9513	CP	-3.3412	CP	95.4	-0.3767	10	0.8772							
45.0	-0.4059	-3.2552	45.0	-20.7942	-21.0387	-12.9401	CP	-30.3645	CP	101.1	-0.3007	11	-0.0121							
50.0	-4.5372	-4.9826	50.0	-21.5913	-19.0846	-12.9143	CP	-18.6950	CP	101.1	-0.3007	12	-0.3755							
55.0	-21.0771	-15.9415	55.0	-31.3277	-35.4838	-14.4310	CP	-10.9991	CP	38.2	0.1649									
60.0	-19.5539	-15.4042	60.0	-19.2003	-17.2594	-14.4310	CP	-8.4217	CP	43.4	0.2218									
65.0	-15.9707	-15.0252	65.0	-0.6702	-6.3520	-14.0389	CP	-1.6407	CP	50.4	0.1174									
70.0	-0.5673	-0.5673	70.0	-0.4353	-0.9594	-2.9133	CP	-1.2551	CP	56.1	0.1459									
75.0	0.2554	-2.2294	75.0	-0.6848	-0.6462	0.4828	CP	-1.7907	CP	62.8	0.0033									
80.0	0.5222	-0.5222	80.0	-0.6385	-0.6594	-0.2982	CP	-0.8457	CP	69.7	-0.0917									
85.0	-0.7473	-0.7473	85.0	-0.6771	-0.6694	-0.5920	CP	-1.1179	CP	76.9	-0.0252									
90.0	-0.3577	0.7824	90.0	-0.2441	-0.0121	-0.1281	CP	-0.3369	CP	83.4	0.1174									
95.0	1.5520	-0.0632	95.0	0.6143	0.3050	0.2653	CP	0.2586	CP	89.4	0.2313									
100.0	0.5779	-0.5449	100.0	0.3978	0.3746	0.2895	CP	0.4442	CP	95.4	0.1459									
105.0	1.5520	-0.0632	105.0	0.2070	0.2791	0.2431	CP	0.3153	CP	101.1	-0.2532									
110.0	0.5779	0.5449	110.0	-0.0096	0.0265	0.0987	CP	0.1709	CP											
115.0	0.5734	0.5734	115.0	0.2261	-0.2261	-0.0457	CP	0.0265	CP											
120.0	0.7728	0.5734	120.0	-0.2723	-0.3347	-0.1250	CP	0.0148	CP											
125.0	0.7338	0.5738	125.0	-0.3847	-0.3223	-0.3472	CP	0.0397	CP											
130.0	0.4133	-1.2339	130.0	-0.6093	-0.4471	-0.4346	CP	0.0273	CP											
135.0	0.3064	0.2708	135.0	-0.5095	-0.3971	-0.5095	CP	0.1022	CP											
140.0	0.2263	0.2619	140.0	-0.5095	-0.3971	-0.5095	CP	0.1022	CP											
145.0	0.4311	0.5469	145.0	-0.5095	-0.3971	-0.5095	CP	0.1022	CP											

PAGE 142

A-234

TABLE A9. RUN 77. BC1W6V, DELP=45, CMJ=1.0, (BN/B)=1

PAGE 143

RUN:SEQ												BASEPR = 9.1914												PAGE 149																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																											
77 2												CLAERO = 1.0790 CDAERO = 0.8478 DCLC = 0.3621 DMLC = 0.8896												HOT																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																			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TABLE A9. (Continued)

RUN:SEQ		CLAERO =		PROPULSIVE		WING /		CANARD		PRESSURES		BASEPR =		PAGE	
77	4	PTOT	1.2778	COAERO =	0.9521	DCLC =	0.3803	CMUJ	CMUT			8.1914		14	
ALPHA	4.02	PSTAT	2120.15	VEL	13.67	YAW	H/C	CMUJ	CMUT			87.5090		0.708407E+06	
BETA	-0.01	CL	2.59	CM	-0.75	CROLL	CN	CV	CNTR			CLTR		0.70	
		CD	0.27		-0.75		-0.00	0.02	1.54			1.50		0.70	
***** CANARD *****														***** FUSELAGE*****	
BP=3.375 BP=10.125														BP = 22	
XX/C	0.0	CP	-4.9231	XX/C	0.0	CP	-0.4881	BP = 12	BP = 16	CP	CP	XLOC	CP	NO. CP	
0.0	-1.7811		-3.2713	2.5	0.5840		-0.4881	-1.4398	-1.6412	-5.4422	-5.4422	38.2	-0.4926	1 -0.5264	
2.5	-1.6195		-2.7506	5.0	0.7250		0.7250	-1.3391	-1.4398	-2.9753	-2.9753	43.4	-0.4926	2 -0.5264	
5.0	-1.0270		-1.2938	10.0	0.5740		0.5236	-1.4901	-1.2635	-2.1950	-2.1950	50.4	-0.3010	3 -1.1086	
10.0	-0.0574		-1.4938	15.0	0.3222		0.1712	-1.6160	-1.1629	-1.5908	-1.5908	58.1	-0.1668	4 -0.1625	
15.0	-0.9193		-1.2963	20.0	0.01460		-0.0301	-1.6412	-1.1126	-1.2636	-1.2636	62.5	-0.4842	5 -1.1086	
20.0	-0.8295		-1.1188	25.0	0.01057		-0.2819	-1.4901	-1.1814	-1.126	-1.126	69.7	-0.4734	6 -0.2353	
25.0	-0.8295		-1.1188	30.0	0.02353		0.4536	-1.3269	-1.1814	-1.0258	-1.0258	76.9	-0.2435	7 -0.1754	
30.0	-0.7936		-1.0270	35.0	0.07447		-0.8175	-1.2541	-0.8903	-1.3997	-1.3997	83.4	-0.2818	8 -1.0585	
35.0	-0.7936		-1.0270	40.0	0.12397		-1.3547	-1.4508	-2.1785	-1.9294	-1.9294	89.4	-0.3776	9 -0.5978	
40.0	-1.1168		-1.3143	45.0	0.18561		-4.4010	-4.0753	-5.2823	-6.2756	-6.2756	95.4	-0.4159	10 -0.8927	
45.0	-1.5656		-1.9427	50.0	0.0561		-4.4010	-4.0753	-5.2823	-6.2756	-6.2756	101.1	-0.3993	11 0.0195	
50.0	-0.4884		-4.2229	55.0	0.5536		-54.3411	-38.0883	-61.6645	-10.7795	-10.7795	---BOTTOM---			
55.0	-5.9107		-7.0236	60.0	45.2296		-47.4594	-36.0293	-33.3055	-9.6612	-9.6612	38.2	0.1781	12 -0.3236	
60.0	-37.5962		-35.8330	65.0	38.8444		115.4746	-34.3169	-9.4186	-3.9492	-3.9492	43.4	0.2356		
65.0	-20.0468		-27.3826	70.0	20.8118		-0.9941	-31.1540	-2.1088	-3.2881	-3.2881	50.4	0.0431		
70.0	-6.3603		-17.4155	75.0	0.0428		0.0428	-5.2971	-2.1088	-3.2881	-3.2881	56.1	0.0431		
80.0	-0.4988		-2.8874	80.0	0.15867		-2.1169	-1.9921	-3.2397	-4.3312	-4.3312	62.5	-0.2376		
85.0	-1.0330		0.7337	85.0	0.15867		-2.1169	-1.9921	-3.2397	-4.3312	-4.3312	69.7	-0.3776		
90.0	-1.7953		0.5692	90.0	0.10097		-1.3372	-1.1033	-1.2436	-4.7210	-4.7210	76.9	-0.3993		
95.0	-1.0481		0.4846	95.0	0.7602		-0.4171	-0.1833	-0.4640	-0.7758	-0.7758	83.4	-0.1477		
100.0	-0.2435		0.7337	100.0	0.1442		0.1754	0.2846	0.4717	0.4249	0.4249	89.4	-0.0135		
105.0	0.5692		0.5692		0.1910		0.1442	0.2378	0.4249	0.6276	0.6276	95.4	-0.1285		
110.0	0.6379		0.4846		0.0170		-0.0170	-0.0170	0.2013	0.3469	0.3469	101.1	-0.4734		
115.0	1.6725		0.5692		0.3080		-0.3080	-0.2353	-0.1625	-0.0170	-0.0170				
120.0	0.7528		0.4846		0.4536		-0.4536	-0.4536	-0.3080	-0.0897	-0.0897				
125.0	0.5995		0.5995		0.4077		-0.4833	-0.4581	-0.3071	-0.0554	-0.0554				
130.0	0.5889		0.5889		0.3826		-0.4581	-0.6594	-0.3574	0.2013	0.2013				
135.0	0.3914		-1.4220		0.3826		-0.3323	-0.7098	-0.3071	0.3469	0.3469				
140.0	0.3016		0.2478		5.0		-0.3826	-0.7098	-0.3071	0.3469	0.3469				
145.0	0.2118		0.2657		2.5		-0.4077	-0.7601	-0.2567	0.4197	0.4197				
150.0	0.5530		0.5530												
***** MISC *****															
BP=3.375 BP=10.125															
XX/C	0.0	CP	-4.9231	XX/C	0.0	CP	-0.4881	BP = 2	BP = 6	BP = 12	BP = 16				
0.0	-1.7811		-3.2713	2.5	0.5840		-0.4881		-1.4398	CP	CP				
2.5	-1.6195		-2.7506	5.0	0.7250		0.7250		-1.3391						
5.0	-1.0270		-1.2938	10.0	0.5740		0.5236		-1.4901						
10.0	-0.0574		-1.4938	15.0	0.3222		0.1712		-1.6160						
15.0	-0.9193		-1.2963	20.0	0.01460		-0.0301		-1.6412						
20.0	-0.8295		-1.1188	25.0	0.01057		-0.2819		-1.4901						
25.0	-0.8295		-1.1188	30.0	0.02353		0.4536		-1.3269						
30.0	-0.7936		-1.0270	35.0	0.07447		-0.8175		-1.2541						
35.0	-0.7936		-1.0270	40.0	0.12397		-1.3547		-1.4508						
40.0	-1.1168		-1.3143	45.0	0.18561		-4.4010		-4.0753						
45.0	-1.5656		-1.9427	50.0	0.0561		-4.4010		-4.0753						
50.0	-0.4884		-4.2229	55.0	0.5536		-54.3411		-38.0883						
55.0	-5.9107		-7.0236	60.0	45.2296		-47.4594		-36.0293						
60.0	-37.5962		-35.8330	65.0	38.8444		115.4746		-34.3169						
65.0	-20.0468		-27.3826	70.0	20.8118		-0.9941		-31.1540						
70.0	-6.3603		-17.4155	75.0	0.0428		0.0428		-5.2971						
80.0	-0.4988		-2.8874	80.0	0.15867		-2.1169		-1.9921						
85.0	-1.0330		0.7337	85.0	0.15867		-2.1169		-1.9921						
90.0	-1.7953		0.5692	90.0	0.10097		-1.3372		-1.1033						
95.0	-1.0481		0.4846	95.0	0.7602		-0.4171		-0.1833						
100.0	-0.2435		0.7337	100.0	0.1442		0.1754		0.2846						
105.0	0.5692		0.5692		0.1910		0.1442		0.2378						
110.0	0.6379		0.4846		0.0170		-0.0170		-0.0170						
115.0	1.6725		0.5692		0.3080		-0.3080		-0.2353						
120.0	0.7528		0.4846		0.4536		-0.4536		-0.3080						
125.0	0.5995		0.5995		0.4077		-0.4833		-0.4581						
130.0	0.5889		0.5889		0.3826		-0.4581		-0.6594						
135.0	0.3914		-1.4220		0.3826		-0.3323		-0.7098						
140.0	0.3016		0.2478		5.0		-0.3826		-0.7098						
145.0	0.2118		0.2657		2.5		-0.4077		-0.7601						
150.0	0.5530		0.5530												

TABLE A9. (Concluded)

RUN: SEQ		CLAERO =		PROPLUSIVE		WING / CANARD		PRESSURES		BASEPR = 9.1914		PAGE 147	
77	B	PLOT	PSTAY	CD	CM	CRGLL	CM	CV	CMTR	HGT	RN		
ALPHA	11.98	2133.82	2120.94	12.88	102.86	0.01	2.62	0.468	1.088	85.5867	0.88833E+05		
BETA	-0.01	3.46	0.90	-0.79	0.01	-0.01	0.00	2.45	-0.34	CLTR	CDTR		
										2.26	1.19		
X/C		BP=3.375		BP=10.125		BP=2		BP=6		BP=12		BP=16	
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP
0.0	-10.3360	0.0	-3.6480	0.0	-0.4681	-0.3078	-2.3848	-4.2347	-5.7841	38.2	-0.7270	38.2	-0.7270
2.5	-4.2387	2.5	-3.8196	2.5	0.4936	0.0127	-1.6168	-2.7658	-5.3567	43.4	-0.6864	43.4	-0.6864
5.0	-2.3524	5.0	-3.8577	5.0	0.3333	0.1208	-1.5901	-2.3648	-6.0896	50.4	-0.4424	50.4	-0.4424
10.0	-0.0849	10.0	-3.8767	10.0	0.0652	-0.3612	-1.6188	-1.9008	-4.2080	56.1	-0.2798	56.1	-0.2798
15.0	-1.7428	15.0	-4.3149	15.0	-0.1208	-0.5218	-1.8037	-1.7770	-2.8456	62.5	-0.8488	62.5	-0.8488
20.0	-1.4187	20.0	-4.7723	20.0	-0.3880	-0.7352	-1.4572	-1.6702	-2.1777	69.7	-0.8285	69.7	-0.8285
25.0	-1.3044	25.0	-3.7052	25.0	-0.5435	-0.7752	-1.9338	-1.7020	-2.1936	76.9	-0.3408	76.9	-0.3408
30.0	-1.3997	30.0	-1.0758	30.0	-0.9296	-1.0841	-2.0881	-0.8207	-2.3198	83.4	-0.3816	83.4	-0.3816
35.0	-1.5140	35.0	-1.7236	35.0	-1.3777	-1.5404	-2.4147	-2.7807	-2.9026	89.4	-0.5036	89.4	-0.5036
40.0	-1.9713	40.0	-4.6389	40.0	-4.3259	-4.8342	-5.2205	-6.3998	-8.6751	95.4	-0.4831	95.4	-0.4831
45.0	-0.6375	45.0	-7.8306	45.0	79.5	-4.2599	-57.4971	-42.4493	-78.0784	101.1	-0.4018	101.1	-0.4018
50.0	-6.6777	50.0	-7.8306	50.0	80.5	-49.2309	-50.6612	-40.3855	-42.9956	101.1	-0.4018	101.1	-0.4018
55.0	-39.5196	55.0	-40.0698	55.0	81.3	-36.8653	-106.9150	-38.2545	-16.9212	101.1	-0.4018	101.1	-0.4018
60.0	-21.0749	60.0	-31.0749	60.0	82.0	-16.3298	-2.9876	-34.2243	-7.3613	101.1	-0.4018	101.1	-0.4018
65.0	-8.2612	65.0	-19.6445	65.0	84.0	4.5912	0.4372	-0.4568	-1.7498	101.1	-0.4018	101.1	-0.4018
70.0	-0.6632	70.0	-3.7159	70.0	87.0	-0.3880	-4.3631	-2.6892	-3.7980	101.1	-0.4018	101.1	-0.4018
75.0	-1.4334	75.0	-0.7978	75.0	89.0	-1.5776	-2.6892	-3.6656	-4.8240	101.1	-0.4018	101.1	-0.4018
80.0	-2.1707	80.0	0.7978	80.0	93.0	-1.3488	-1.7624	-2.6237	-4.8240	101.1	-0.4018	101.1	-0.4018
85.0	-1.3981	85.0	0.7978	85.0	96.0	-1.3322	-1.9610	-1.5804	-5.0557	101.1	-0.4018	101.1	-0.4018
90.0	-0.4831	90.0	0.7978	90.0	100.0	-0.5875	-0.4386	0.0082	-0.1076	101.1	-0.4018	101.1	-0.4018
95.0	1.7941	95.0	-0.6864	95.0	98.0	0.6536	0.4054	0.3392	0.4385	101.1	-0.4018	101.1	-0.4018
100.0	0.6555	100.0	0.4319	100.0	84.0	0.4882	0.3889	0.3061	0.3658	101.1	-0.4018	101.1	-0.4018
	1.7941		-0.6864		73.5	0.2288	0.3061	0.3061	0.3833	101.1	-0.4018	101.1	-0.4018
	0.6555		0.4319		54.0	-0.0801	-0.0601	0.1516	0.1516	101.1	-0.4018	101.1	-0.4018
	0.8385		0.5742		33.0	0.3118	-0.3118	-0.1573	-0.0029	101.1	-0.4018	101.1	-0.4018
	0.8106		0.5248		24.0	-0.3345	-0.3612	-0.2276	0.0127	101.1	-0.4018	101.1	-0.4018
	0.5058		-1.8951		10.0	-0.3612	-0.3612	-0.4681	-0.1475	101.1	-0.4018	101.1	-0.4018
	0.4676		0.3343		5.0	-0.3612	-0.3612	-0.6016	-0.1475	101.1	-0.4018	101.1	-0.4018
	0.4105		0.4295		2.5	-0.3612	-0.3078	-0.7619	-0.2544	101.1	-0.4018	101.1	-0.4018
	0.5529		0.3343							101.1	-0.4018	101.1	-0.4018

TABLE A10. RUN 79, BC1W6V, DELF=48, CMJ=2.0, (BN/B)=1

RUN: SEQ										PROPLULSIVE										WING / CANARD										PRESSURES										BASEPR = 8.1914										PAGE 148																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																													
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TABLE A10. (Concluded)

PAGE 150

RUN: SEQ										BASEPR = 8.1914									
79 11										HGT MN									
ALPHA										87.3492 0.490614E+06									
12.00										CLTR									
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TABLE A11. (Continued)

RUN: SEQ		PROPULSIVE				WING / CANARD		PRESSURES		BASEPR = 8.1904		PAGE 255	
142	4	CLAERO =	CDAERO =	0.2423	DCLC =	0.0	CMWC	CMUT	CMUT	HOT	BN		
ALPHA	PTOT	PTSTAT	Q	VEL	YAW	H/C	CMWC	CMUT	CMUT				
4.06	2107.23	2076.83	30.40	162.06	0.0	2.66	0.0	0.0	0.0	86.9181	0.100239E+07		
BETA	CL	CD	CROLL	CN			CY	CNTR	CMTR	CLTR	CDTR		
0.0	0.70	0.24	-0.37	0.00	-0.00		0.01	0.71	-0.37	0.70	0.24		
***** CANARD *****													
%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP
0.0	-0.2437	-0.2276	0.0	-0.0529	-0.5510	-1.4328	-1.6379	-2.5324	38.2	-0.0773	1	-0.4404	
2.5	-0.2276	-0.2276	2.5	-0.2114	-0.8341	-1.0948	-1.2416	-1.5360	43.4	-0.0601	2	0.1816	
5.0	-0.2357	-0.2195	5.0	-0.4831	-0.6303	-0.8567	-0.9926	-1.1511	50.4	-0.0601	3	0.5059	
10.0	-0.2195	-0.2114	10.0	-0.4831	-0.5397	-0.7322	-0.7661	-0.8227	56.1	-0.0687	4	0.1816	
15.0	-0.2276	-0.2195	15.0	-0.3378	-0.4718	-0.6303	-0.6529	-0.6755	62.5	-0.1032	5	-0.4404	
25.0	-0.2276	-0.2114	24.0	-0.3685	-0.4038	-0.5057	-0.4944	-0.5067	69.7	-0.1849	6	0.0179	
35.0	-0.2276	-0.2114	33.0	-0.3749	-0.4077	-0.4404	-0.4732	-0.4732	76.9	-0.1635	7	0.5091	
50.0	-0.2195	-0.2195	54.0	-0.3749	-0.3749	-0.4404	-0.2788	-0.4404	83.4	-0.1483	8	0.2825	
55.0	-0.2195	-0.2276	55.0	-0.4479	-0.4738	-0.4996	-0.5169	-0.5255	89.4	-0.2066	9	-0.0871	
65.0	-0.2276	-0.2195	78.5	-0.7324	-0.7324	-0.7486	-0.7927	-0.9047	96.4	-0.2497	10	0.5181	
76.0	-0.2437	-0.2357	78.5	-0.6207	-0.5799	-0.6616	-0.7140	-0.8423	101.1	-0.2066	11	0.2425	
79.0	-0.2276	-0.2276	80.5	-0.5799	-0.5391	-0.6499	-0.7189	-0.8210	---	---BOTTOM---	12	-0.0621	
80.5	-0.2243	-0.2068	81.3	-0.5683	47.6347	-0.8499	-0.7257	-0.8598	38.2	-0.0342			
81.0	-0.2243	-0.2068	82.0	-0.5799	-0.9881	-0.6616	-0.7062	-0.8598	43.4	-0.0089			
82.0	-0.2128	-0.2010	84.0	-0.5741	-0.8424	-0.6616	-0.7062	-0.8531	50.4	-0.0286			
84.0	-0.2068	-0.2068	87.0	-0.5741	-0.6033	-0.6849	-0.7140	-0.8481	56.1	0.0347			
87.0	-0.2068	-0.2068	89.0	-0.6693	-0.6593	-0.7325	-0.7956	-0.9148	62.5	0.0951			
89.0	-0.1980	-0.1980	93.0	-0.7184	-0.6693	-0.7255	-0.2485	-0.9259	69.7	0.1296			
93.0	-0.2068	-0.2068	96.0	-0.6974	-0.6334	-0.7255	-0.7956	-0.9428	76.9	0.1594			
96.0	-0.2068	-0.1980	100.0	-0.6132	-0.5922	-0.5992	-0.7886	-0.9274	83.4	0.1985			
0.0	-0.1980	-0.1980	96.0	0.3407	0.3758	0.4777	0.3477	0.2215	89.4	0.2416			
0.0	-0.1980	-0.1980	84.0	0.7055	0.7125	0.6704	0.6073	0.5181	93.4	0.1468			
84.0	-0.1980	-0.1980	73.5	0.5745	-0.1785	0.6072	0.6072	0.4762	101.1	-0.3186			
73.0	-0.1980	-0.1980	54.0	0.2144	0.2798	0.3125	0.3125	0.1816					
50.0	-0.1807	-0.2068	33.0	0.1489	0.1489	0.1816	0.1816	0.1161					
35.0	-0.2276	-0.2276	24.0	0.1170	0.1509	0.1849	0.2418	0.1170					
25.0	-0.2276	-0.2195	10.0	0.2075	0.2302	0.2528	0.3208	0.2768					
10.0	-0.2276	-0.2195	5.0	0.2276	0.2981	0.3774	0.4113	0.3780					
5.0	-0.2357	-0.2195	2.5	0.3660	0.4113	0.4680	0.5019	0.4762					
2.5	-0.2276	-0.2276											

TABLE A11. (Concluded)

RUN: SEQ										PAGE 260									
142	6	CLARO	1.0886	CDAERO	0.4181	WING / CANARD	PRESSURES	BASEPR	8.1904										
ALPHA	PTOT	PSTAT	Q	VEL	VAM	H/C	CMJC	CMUT	RG										
11.98	2107.09	2076.91	30.17	161.60	0.0	2.65	0.0	0.0	86.8355	0.998939E+06									
BETA	CL	CD	CM	CROLL	CN	CY	CNTR	CNTR	CLTR	CDTR									
0.0	1.08	0.42	-0.46	0.01	0.00	0.00	1.14	-0.45	1.08	0.42									
***** CANARD *****										***** FUSELAGE*****									
BP=3.375 BP=10.125										-----TOP-----									
X/C	CP	X/C	CP	X/C	CP	X/C	CP	X/C	CP	XLOC	CP	NO.	CP	**MISC.**					
0.0	-0.2764	-0.2684	0.0	-2.8887	-5.6604	-8.0252	-2.3412	-1.4058	38.2	-0.1019	1	-0.6812							
2.5	-0.2684	-0.2684	2.5	-0.2310	-2.1700	-4.4397	-2.4210	-1.4400	43.4	-0.0832	2	0.3413							
5.0	-0.2684	-0.2684	5.0	-1.1663	-1.5769	-2.6832	-2.3069	-1.4172	50.4	-0.1279	3	-1.4068							
10.0	-0.2603	-0.2603	10.0	-0.9496	-1.2119	-1.3373	-2.3866	-1.3930	56.1	-0.1627	4	0.3083							
15.0	-0.2603	-0.2603	15.0	-0.8241	-0.9724	-1.1663	-2.2042	-1.3487	62.5	-0.2234	5	-1.1429							
20.0	-0.2684	-0.2684	20.0	-0.6758	-0.7556	-0.9810	-1.7023	-1.2917	69.7	-0.3016	6	0.0774							
25.0	-0.2684	-0.2684	25.0	-0.5822	-0.6812	-0.7801	-1.2089	-1.2749	76.9	-0.2689	7	0.5063							
30.0	-0.2766	-0.2766	30.0	-0.5163	-0.5493	-0.5822	-0.1784	-1.1100	83.4	-0.2081	8	-0.2923							
35.0	-0.2603	-0.2603	35.0	-0.5534	-0.5796	-0.6056	-0.5447	-1.0136	89.4	-0.2756	9	0.0098							
40.0	-0.2766	-0.2684	40.0	-0.8138	-0.8052	-0.8226	-0.8573	-0.9982	95.4	-0.2321	10	0.5274							
45.0	-0.2684	-0.2684	45.0	-0.6496	-0.6437	-0.7612	-0.8728	-1.0020	101.1	-0.1827	11	0.0844							
50.0	-0.2678	-0.2678	50.0	-0.6261	-0.6144	-0.7612	-0.8376	-0.2602	-----BOTTOM-----										
55.0	-0.2603	-0.2603	55.0	-0.6085	-0.6085	-0.7671	-0.8435	-0.9982	38.2	0.0197									
60.0	-0.2603	-0.2603	60.0	-0.6026	-0.6026	-0.7201	-0.8870	-0.9844	43.4	0.0644									
65.0	-0.2443	-0.2443	65.0	-0.6203	-0.6261	-0.7316	-0.8611	-0.9727	50.4	0.0110									
70.0	-0.2561	-0.2561	70.0	-0.6672	-0.6672	-0.7436	-0.8258	-0.9727	56.1	0.1328									
75.0	-0.2495	-0.2495	75.0	-0.7304	-0.7163	-0.8152	-0.9353	-1.0080	62.5	0.2107									
80.0	-0.2495	-0.2495	80.0	-0.7799	-0.7304	-0.8152	-0.9353	-1.0080	69.7	0.2802									
85.0	-0.2495	-0.2495	85.0	-0.7658	-0.6951	-0.8081	-0.9212	-0.9777	76.9	0.2715									
90.0	-0.2495	-0.2495	90.0	-0.6597	-0.5962	-0.6527	-0.8717	-0.2852	83.4	0.2889									
95.0	-0.2495	-0.2495	95.0	-0.3367	-0.4356	-0.3720	-0.3508	0.1883	89.4	0.3082									
100.0	-0.2495	-0.2495	100.0	0.7112	0.7606	0.6829	0.6264	0.4285	95.4	0.1873									
105.0	-0.2495	-0.2495	105.0	0.5051	-0.2524	0.6381	0.6061	0.4402	101.1	-0.3190									
110.0	-0.2495	-0.2495	110.0	0.3413	0.3413	0.3742	0.3413	0.2093											
115.0	-0.2495	-0.2495	115.0	0.3413	0.3413	0.3413	0.3413	0.1764											
120.0	-0.2684	-0.2684	120.0	0.3393	0.3507	0.3735	0.3964	0.2481											
125.0	-0.2684	-0.2684	125.0	0.4990	0.4876	0.5104	0.5333	0.4072											
130.0	-0.2603	-0.2603	130.0	0.6131	0.5789	0.5789	0.6017	0.4732											
135.0	-0.2684	-0.2684	135.0	2.5	0.6929	0.5447	0.5447	0.4732											
140.0	-0.2603	-0.2603	140.0																

TABLE A12. RUN 143, BW6V, DELF=45, CMU=0.5, (BN/B)=1

RUN: SEQ														PAGE 26													
143	1	CLARO =	0.2820	CDAERO =	0.0253	WING / CANARD		PRESSURES		BASEPR = 0.1904																	
ALPHA	PTOT	PSTAT	Q	VEL	YAW	H/C	CMAC	CMUW	CMUT	HOT	RM																
0.05	2107.23	2079.31	27.91	155.49	0.0	2.66	0.0	0.510	0.510	86.9365	0.957290E+06																
BETA	CL	CD	CM	CROLL	CN	CV	CNTR	CNTR	CDTR	CLTR	CDTR																
0.0	0.72	0.37	-0.80	0.00	-0.01	0.06	0.35	-0.53	0.35	0.54																	
..... CANARD														 FUSELAGE													
BP=3.375 BP=10.125														-----TOP-----													
%X/C	CP	%X/C	CP	BP = 2	BP = 6	BP = 12	BP = 16	BP = 22	CP	XLOC	CP	NO.	CP														
0.0	-0.4254	-0.4166	0.0	0.1611	-0.5170	-1.6330	-2.0089	-3.4267	-3.4267	38.2	-0.0987	1	-0.7112														
2.5	-0.4254	-0.4078	2.5	-0.4061	-0.8129	-1.4294	-1.7130	-1.8596	-1.8596	43.4	-0.0893	2	0.2865														
5.0	-0.4166	-0.4166	5.0	-0.4924	-0.8897	-0.9979	-1.2322	-1.8514	-1.8514	50.4	-0.1081	3	-0.9614														
10.0	-0.4254	-0.4166	10.0	-0.5540	-0.8650	-0.8992	-1.0349	-1.1828	-1.1828	56.1	-0.1174	4	0.2152														
15.0	-0.4254	-0.4078	15.0	-0.5047	-0.8280	-0.8280	-0.9362	-1.0595	-1.0595	62.5	-0.1644	5	-0.9257														
25.0	-0.4254	-0.4166	24.0	-0.5284	-0.8157	-0.7636	-0.8008	-0.9239	-0.9239	69.7	-0.2876	6	-0.0701														
35.0	-0.4078	-0.4166	33.0	-0.5592	-0.6761	-0.7831	-0.8544	-0.9257	-0.9257	78.9	-0.3052	7	0.2510														
50.0	-0.4254	-0.4254	54.0	-0.8188	-0.9257	-1.0683	-1.2466	-1.2466	-1.2466	83.4	-0.3239	8	-0.9102														
65.0	-0.4342	-0.4254	65.0	-1.2344	-1.3564	-1.4221	-1.5536	-1.7319	-1.7319	89.4	-0.4272	9	0.5740														
75.0	-0.4254	-0.4254	75.0	-3.2819	-3.5059	-3.1211	-4.0505	-5.8709	-5.8709	95.4	-0.4178	10	0.8697														
79.0	-0.4254	-0.4254	79.0	-15.8768	-18.2134	-9.5719	-19.1087	-37.0007	-37.0007	101.1	-0.3333	11	0.0294														
80.5	-0.4254	-0.4254	80.5	-17.1723	-17.1404	-9.1022	-16.9958	-0.0735	-0.0735	101.1	-0.3333	12	0.2914														
81.0	-0.4100	-0.4037	81.0	-17.6928	-16.1040	-10.7151	-17.3944	-7.4514	-7.4514	38.2	-0.0330																
82.0	-0.4037	-0.4164	82.0	-16.9183	-16.3977	-11.2665	-15.0443	-4.3893	-4.3893	43.4	-0.0142																
84.0	-0.4037	-0.4164	84.0	-7.8355	-8.4261	-11.5341	-9.2419	-3.9021	-3.9021	50.4	-0.0611																
87.0	-0.4164	-0.4164	87.0	0.0725	-2.1053	-7.4324	-3.6718	-3.2734	-3.2734	56.1	0.0515																
89.0	-0.3615	-0.3615	89.0	-0.3296	-0.4365	-3.2476	-1.5050	-2.9495	-2.9495	62.5	0.1078																
93.0	-0.3990	-0.4084	93.0	-0.6733	-0.4824	-0.3296	-0.4924	-3.5908	-3.5908	69.7	0.1735																
96.0	-0.3990	-0.4084	96.0	-0.8338	-0.4977	0.3120	-0.8109	-3.9532	-3.9532	76.8	0.2392																
100.0	-0.3990	-0.4084	100.0	0.0523	0.1975	0.0600	-0.0240	-0.4289	-0.4289	83.4	0.3143																
-0.4084	-0.4084	-0.4084	96.0	0.6570	0.7169	0.6787	0.6176	0.2204	0.2204	89.4	0.3813																
-0.4084	-0.4084	-0.4084	84.0	0.6534	0.6787	0.7474	0.6176	0.0862	0.0862	95.4	0.2111																
-0.3990	-0.3990	-0.3990	73.5	0.6073	-0.4266	0.6073	0.5717	0.1795	0.1795	101.1	-0.3427																
-0.4084	-0.4084	-0.4084	54.0	0.3578	0.4291	0.4291	0.3934	0.1082	0.1082																		
-0.4166	-0.4166	-0.4166	33.0	0.2152	0.2508	0.2865	0.2865	0.1062	0.1062																		
-0.4254	-0.4254	-0.4254	24.0	0.1734	0.1981	0.2598	0.2844	0.1241	0.1241																		
-0.4342	-0.4342	-0.4342	10.0	0.1558	0.2228	0.2844	0.3830	0.2665	0.2665																		
-0.4166	-0.4166	-0.4254	5.0	0.2598	0.2721	0.3830	0.4200	0.3934	0.3934																		
-0.4254	-0.4254	-0.4254	2.5	0.3707	0.3584	0.4693	0.5064	0.4291	0.4291																		
-0.4354	-0.4354	-0.4354	2.5																								

Force Data -
Use Run 313

Force Data -
Use Run 313

TABLE A12. (Continued)

[illegible]

Force Data -
Use Run 313

TABLE A13. RUN 144, BW6V, DELF=45, CMU=1.0, (BN/B)=1

RUN: SEQ										PAGE 266									
144	1	CLARO =	0.8342	CDAERO =	0.8265	WING / CANARD	PRESSURES			BASEPR =	0.1904								
ALPHA	0.07	PTO	2107.86	PSTAT	Q	VEL	YAW	H/C	CMUJ	CMUT	HGT	BN							
BETA	0.0	CL	1.71	CD	0.33	CROLL	0.02	CN	CY	CNTR	CLTR	COTR							
***** CANARD *****										***** FUSELAGE*****									
XX/C	0.0	CP	-0.4949	BP=3.375	BP=10.125	BP=2	BP=5	BP=12	BP=16	BP=22	XLCC	CP	NO.	CP	*****TOP*****				
2.5	-0.4949		-0.4949			XX/C	CP	CP	CP	CP	38.2	-0.1013	1	-0.8757					
5.0	-0.4949		-0.4949			2.5	-0.4718	-1.0459	-1.3954	-1.8197	43.4	-0.1013	2	0.2069					
10.0	-0.4949		-0.4771			5.0	-0.5717	-0.7214	-1.1458	-1.4703	50.4	-0.1393	3	-1.0923					
15.0	-0.4949		-0.4771			10.0	-0.5717	-0.7214	-0.9960	-1.1708	56.1	-0.1203	4	0.2069					
25.0	-0.4771		-0.4771			15.0	-0.5966	-0.7464	-0.9710	-1.0459	62.5	-0.1773	5	-1.0923					
35.0	-0.4949		-0.4771			24.0	-0.5966	-0.6965	-0.8463	-0.9461	69.7	-0.2913	6	-0.0818					
50.0	-0.4771		-0.4771			33.0	-0.6592	-0.7314	-0.9479	-1.0201	73.9	-0.3483	7	0.1658					
56.0	-0.5127		-0.4949			54.0	-0.9479	-1.0923	-1.3088	-0.2983	83.4	-0.3673	8	-1.0713					
65.0	-0.4771		-0.4771			78.5	-4.4527	-1.6594	-1.7735	-1.9065	89.4	-0.4813	9	0.6848					
75.0	-0.4949		-0.4949			79.5	-46.6094	-56.5970	-46.5456	-5.7829	95.4	-0.4433	10	0.8928					
79.0	-0.4771		-0.4771			80.5	-44.6885	-42.8561	-40.5809	-60.3503	101.1	-0.3673	11	-0.0971					
80.5	-0.5031		-0.5287			81.3	-27.5471	68.0077	-28.3188	-31.6609	*****BOTTOM*****								
81.0	-0.5031		-0.5159			82.0	-4.7576	7.1964	-17.1098	-1.9427	38.2	-0.0443	12	-0.3600					
82.0	-0.5159		-0.4902			84.0	0.9366	-3.0481	3.3788	-3.5494	43.4	-0.0063							
84.0	-0.4902					87.0	0.5159	-3.8836	-2.8296	-2.7525	50.4	-0.0823							
87.0	-0.5031					89.0	-2.1383	-3.5868	-3.4992	-3.9941	56.1	0.0507							
89.0	-0.4243		-0.4623			93.0	-1.5198	-1.3961	-1.8909	-0.6074	62.5	0.1077							
93.0	-0.4813					96.0	-1.5042	-1.4734	-0.9786	-1.1487	69.7	0.1648							
96.0	-0.4623		-0.4623			100.0	-0.5610	-0.4837	-0.3445	-0.6538	76.9	0.2408							
100.0	-0.4813		-0.4623			96.0	0.5679	0.6761	0.6452	0.5988	83.4	0.3168							
84.0	-0.4813		-0.4623			84.0	0.6297	0.7225	0.7380	0.5833	89.4	0.3548							
73.0	-0.4623		-0.4623			73.5	0.5678	-0.4427	0.6400	0.5678	95.4	0.1458							
50.0	-0.4623		-0.4623			54.0	0.3513	0.3513	0.4234	0.3513	101.1	-0.5003							
35.0	-0.4623		-0.4623			33.0	0.2069	0.2069	0.2069	0.2069									
25.0	-0.4949		-0.4771			24.0	0.1772	0.2021	0.2520	0.3020									
10.0	-0.4771		-0.4949			10.0	0.2021	0.2271	0.3020	0.4018									
5.0	-0.4949		-0.4771			5.0	0.2021	0.3269	0.4018	0.4517									
2.5	-0.4771		-0.4949			2.5	0.2770	0.3519	0.4767	0.4234									

Force Data -
Use Run 312

Force Data -
Use Run 312

TABLE A13. (Continued)

Force Data -
Use Run 312

TABLE A'3. (Concluded)

RUN: SEQ		PROPLUISIVE										WING / CANARD		PRESSURES		PAGE	
144 5		CLAERD = 1.0612 CDAERO = 1.0923 DCLC = 0.0										DCLC = 0.0		CMJW		270	
ALPHA		PSTAT										YAW		CMJW		RN	
11.99		0										H/C		CMJW		0.0102	
BETA		2094.76										0.0		0.0		1.062	
0.0		CD										CROLL		CN		CMTR	
		2.07										0.03		CY		1.39	
		0.76										-0.02		0.06		-0.87	
		0.0														0.94	

TABLE A14. RUN 145, BW6V, DELF-45, CMJ=2.0, (BN/B)=1

RUN: SEQ										PAGE 271									
145	1	CLAERO =	1.8058	COAERO =	1.1250	DCLC =	0.0	DWLC =	1.7854	BASEPR = 8.1904									
ALPHA	0.04	PTOT	2107.72	PSTAT	Q	VEL	YAW	H/C	CMJC	HGT									
BETA	0.0	CL	3.60	CD	CM	CROLL	CH	CY	CNTR	87.2267 0.470101E+06									
										CLTR									
										2.03 0.79									
***** CANARD *****										***** FUSELAGE *****									
BP=3.375	BP=10.125	BP = 2								BP = 12								BP = 22	
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP
0.0	-0.6671	0.0	-0.1457	0.0	-0.1780	0.0	-0.2632	0.0	-0.2941	0.0	-0.3619	0.0	-0.4248	0.0	-0.4877	0.0	-0.5506	0.0	-0.6135
2.5	-0.6304	2.5	-0.7135	2.5	-0.7966	2.5	-0.8797	2.5	-0.9628	2.5	-1.0459	2.5	-1.1290	2.5	-1.2121	2.5	-1.2952	2.5	-1.3783
5.0	-0.6671	5.0	-0.7135	5.0	-0.7966	5.0	-0.8797	5.0	-0.9628	5.0	-1.0459	5.0	-1.1290	5.0	-1.2121	5.0	-1.2952	5.0	-1.3783
10.0	-0.6671	10.0	-0.8168	10.0	-0.9000	10.0	-0.9832	10.0	-1.0664	10.0	-1.1496	10.0	-1.2328	10.0	-1.3160	10.0	-1.3992	10.0	-1.4824
15.0	-0.6671	15.0	-0.7650	15.0	-0.8482	15.0	-0.9314	15.0	-1.0146	15.0	-1.0978	15.0	-1.1810	15.0	-1.2642	15.0	-1.3474	15.0	-1.4306
20.0	-0.6671	20.0	-0.7650	20.0	-0.8482	20.0	-0.9314	20.0	-1.0146	20.0	-1.0978	20.0	-1.1810	20.0	-1.2642	20.0	-1.3474	20.0	-1.4306
25.0	-0.6671	25.0	-0.8012	25.0	-0.8844	25.0	-0.9676	25.0	-1.0508	25.0	-1.1340	25.0	-1.2172	25.0	-1.3004	25.0	-1.3836	25.0	-1.4668
30.0	-0.6671	30.0	-0.8012	30.0	-0.8844	30.0	-0.9676	30.0	-1.0508	30.0	-1.1340	30.0	-1.2172	30.0	-1.3004	30.0	-1.3836	30.0	-1.4668
35.0	-0.6671	35.0	-0.8374	35.0	-0.9206	35.0	-1.0038	35.0	-1.0870	35.0	-1.1702	35.0	-1.2534	35.0	-1.3366	35.0	-1.4198	35.0	-1.5030
40.0	-0.6671	40.0	-0.8736	40.0	-0.9568	40.0	-1.0400	40.0	-1.1232	40.0	-1.2064	40.0	-1.2896	40.0	-1.3728	40.0	-1.4560	40.0	-1.5392
45.0	-0.6671	45.0	-0.9098	45.0	-0.9930	45.0	-1.0762	45.0	-1.1594	45.0	-1.2426	45.0	-1.3258	45.0	-1.4090	45.0	-1.4922	45.0	-1.5754
50.0	-0.6671	50.0	-0.9460	50.0	-1.0292	50.0	-1.1124	50.0	-1.1956	50.0	-1.2788	50.0	-1.3620	50.0	-1.4452	50.0	-1.5284	50.0	-1.6116
55.0	-0.6671	55.0	-0.9822	55.0	-1.0654	55.0	-1.1486	55.0	-1.2318	55.0	-1.3150	55.0	-1.3982	55.0	-1.4814	55.0	-1.5646	55.0	-1.6478
60.0	-0.6671	60.0	-1.0184	60.0	-1.1016	60.0	-1.1848	60.0	-1.2680	60.0	-1.3512	60.0	-1.4344	60.0	-1.5176	60.0	-1.6008	60.0	-1.6840
65.0	-0.6671	65.0	-1.0546	65.0	-1.1378	65.0	-1.2210	65.0	-1.3042	65.0	-1.3874	65.0	-1.4706	65.0	-1.5538	65.0	-1.6370	65.0	-1.7202
70.0	-0.6671	70.0	-1.0908	70.0	-1.1740	70.0	-1.2572	70.0	-1.3404	70.0	-1.4236	70.0	-1.5068	70.0	-1.5900	70.0	-1.6732	70.0	-1.7564
75.0	-0.6671	75.0	-1.1270	75.0	-1.2102	75.0	-1.2934	75.0	-1.3766	75.0	-1.4598	75.0	-1.5430	75.0	-1.6262	75.0	-1.7094	75.0	-1.7926
80.0	-0.6671	80.0	-1.1632	80.0	-1.2464	80.0	-1.3296	80.0	-1.4128	80.0	-1.4960	80.0	-1.5792	80.0	-1.6624	80.0	-1.7456	80.0	-1.8288
85.0	-0.6671	85.0	-1.1994	85.0	-1.2826	85.0	-1.3658	85.0	-1.4490	85.0	-1.5322	85.0	-1.6154	85.0	-1.6986	85.0	-1.7818	85.0	-1.8650
90.0	-0.6671	90.0	-1.2356	90.0	-1.3188	90.0	-1.4020	90.0	-1.4852	90.0	-1.5684	90.0	-1.6516	90.0	-1.7348	90.0	-1.8180	90.0	-1.9012
95.0	-0.6671	95.0	-1.2718	95.0	-1.3550	95.0	-1.4382	95.0	-1.5214	95.0	-1.6046	95.0	-1.6878	95.0	-1.7710	95.0	-1.8542	95.0	-1.9374
100.0	-0.6671	100.0	-1.3080	100.0	-1.3912	100.0	-1.4744	100.0	-1.5576	100.0	-1.6408	100.0	-1.7240	100.0	-1.8072	100.0	-1.8904	100.0	-1.9736
105.0	-0.6671	105.0	-1.3442	105.0	-1.4274	105.0	-1.5106	105.0	-1.5938	105.0	-1.6770	105.0	-1.7602	105.0	-1.8434	105.0	-1.9266	105.0	-2.0098
110.0	-0.6671	110.0	-1.3804	110.0	-1.4636	110.0	-1.5468	110.0	-1.6300	110.0	-1.7132	110.0	-1.7964	110.0	-1.8796	110.0	-1.9628	110.0	-2.0460
115.0	-0.6671	115.0	-1.4166	115.0	-1.5000	115.0	-1.5832	115.0	-1.6664	115.0	-1.7496	115.0	-1.8328	115.0	-1.9160	115.0	-2.0000	115.0	-2.0832
120.0	-0.6671	120.0	-1.4528	120.0	-1.5362	120.0	-1.6194	120.0	-1.7026	120.0	-1.7858	120.0	-1.8690	120.0	-1.9522	120.0	-2.0354	120.0	-2.1186
125.0	-0.6671	125.0	-1.4890	125.0	-1.5724	125.0	-1.6556	125.0	-1.7388	125.0	-1.8220	125.0	-1.9052	125.0	-1.9884	125.0	-2.0716	125.0	-2.1548
130.0	-0.6671	130.0	-1.5252	130.0	-1.6086	130.0	-1.6918	130.0	-1.7750	130.0	-1.8582	130.0	-1.9414	130.0	-2.0246	130.0	-2.1078	130.0	-2.1910
135.0	-0.6671	135.0	-1.5614	135.0	-1.6448	135.0	-1.7280	135.0	-1.8112	135.0	-1.8944	135.0	-1.9776	135.0	-2.0608	135.0	-2.1440	135.0	-2.2272
140.0	-0.6671	140.0	-1.5976	140.0	-1.6810	140.0	-1.7642	140.0	-1.8474	140.0	-1.9306	140.0	-2.0138	140.0	-2.0970	140.0	-2.1802	140.0	-2.2634
145.0	-0.6671	145.0	-1.6338	145.0	-1.7172	145.0	-1.8004	145.0	-1.8836	145.0	-1.9668	145.0	-2.0500	145.0	-2.1332	145.0	-2.2164	145.0	-2.2996
150.0	-0.6671	150.0	-1.6700	150.0	-1.7534	150.0	-1.8366	150.0	-1.9198	150.0	-2.0030	150.0	-2.0862	150.0	-2.1694	150.0	-2.2526	150.0	-2.3358
155.0	-0.6671	155.0	-1.7062	155.0	-1.7896	155.0	-1.8728	155.0	-1.9560	155.0	-2.0392	155.0	-2.1224	155.0	-2.2056	155.0	-2.2888	155.0	-2.3720
160.0	-0.6671	160.0	-1.7424	160.0	-1.8258	160.0	-1.9090	160.0	-1.9922	160.0	-2.0754	160.0	-2.1586	160.0	-2.2418	160.0	-2.3250	160.0	-2.4082
165.0	-0.6671	165.0	-1.7786	165.0	-1.8620	165.0	-1.9452	165.0	-2.0284	165.0	-2.1116	165.0	-2.1948	165.0	-2.2780	165.0	-2.3612	165.0	-2.4444
170.0	-0.6671	170.0	-1.8148	170.0	-1.8982	170.0	-1.9814	170.0	-2.0646	170.0	-2.1478	170.0	-2.2310	170.0	-2.3142	170.0	-2.3974	170.0	-2.4806
175.0	-0.6671	175.0	-1.8510	175.0	-1.9344	175.0	-2.0176	175.0	-2.1008	175.0	-2.1840	175.0	-2.2672	175.0	-2.3504	175.0	-2.4336	175.0	-2.5168
180.0	-0.6671	180.0	-1.8872	180.0	-1.9706	180.0	-2.0538	180.0	-2.1370	180.0	-2.2202	180.0	-2.3034	180.0	-2.3866	180.0	-2.4698	180.0	-2.5530
185.0	-0.6671	185.0	-1.9234	185.0	-2.0068	185.0	-2.0900	185.0	-2.1732	185.0	-2.2564	185.0	-2.3396	185.0	-2.4228	185.0	-2.5060	185.0	-2.5892
190.0	-0.6671	190.0	-1.9596	190.0	-2.0430	190.0	-2.1262	190.0	-2.2094	190.0	-2.2926	190.0	-2.3758	190.0	-2.4590	190.0	-2.5422	190.0	-2.6254
195.0	-0.6671	195.0	-1.9958	195.0	-2.0792	195.0	-2.1624	195.0	-2.2456	195.0	-2.3288	195.0	-2.4120	195.0	-2.4952	195.0	-2.5784	195.0	-2.6616
200.0	-0.6671	200.0	-2.0320	200.0	-2.1154	200.0	-2.1986	200.0	-2.2818	200.0	-2.3650	200.0	-2.4482	200.0	-2.5314	200.0	-2.6146	200.0	-2.6978
205.0	-0.6671	205.0	-2.0682	205.0	-2.1516	205.0	-2.2348	205.0	-2.3180	205.0	-2.4012	205.0	-2.4844	205.0	-2.5676	205.0	-2.6508	205.0	-2.7340
210.0	-0.6671	210.0	-2.1044	210.0	-2.1878	210.0	-2.2710	210.0	-2.3542	210.0	-2.4374	210.0	-2.5206	210.0	-2.6038	210.0	-2.6870	210.0	-2.7702
215.0	-0.6671	215.0	-2.1406	215.0	-2.2240	215.0	-2.3072	215.0	-2.3904	215.0	-2.4736	215.0	-2.5568	215.0	-2.6400	215.0	-2.7232	215.0	-2.8064
220.0	-0.6671	220.0	-2.1768	220.0	-2.2602	220.0	-2.3434	220.0	-2.4266	220.0	-2.5098	220.0	-2.5930	220.0	-2.6762	220.0	-2.7594	220.0	-2.8426
225.0	-0.6671	225.0	-2.2130	225.0	-2.2964	225.0	-2.3796	225.0	-2.4628	225.0	-2.5460	225.0	-2.6292	225.0	-2.7124	225.0	-2.7956	225.0	-2.8788
230.0	-0.6671	230.0	-2.2492	230.0	-2.3326	230.0	-2.4158	230.0	-2.4990	230.0	-2.5822	230.0	-2.6654	230.0	-2.7486	230.0	-2.8318	230.0	-2.9150
235.0	-0.6671	235.0	-2.2854	235.0	-2.3688	235.0	-2.4520	235.0	-2.5352	235.0	-2.6184	235.0	-2.7016	235.0	-2.7848	235.0	-2.8680	235.0	-2.9512
240.0	-0.6671	240.0	-2.3216	240.0	-2.4050	240.0	-2.4882	240.0	-2.5714	240.0	-2.6546	240.0	-2.7378	240.0	-2.8210	240.0	-2.9042	240.0	-2.9874
245.0	-0.6671	245.0	-2.3578	245.0	-2.4412	245.0	-2.5244	245.0	-2.6076	245.0	-2.6908	245.0	-2.7740	245.0	-2.8572	245.0	-2.9404	245.0	-3.0236
250.0	-0.6671	250.0	-2.3940	250.0	-2.4774	250.0	-2.5606	250.0	-2.6438	250.0	-2.7270	250.0	-2.8102	250.0	-2.8934	250.0	-2.9766	250.0	-3.0598
255.0	-0.6671	255.0	-2.4302	255.0	-2.5136	255.0	-2.5968	255.0	-2.6800	255.0	-2.7632	255.0	-2.8464	255.0	-2.9296	255.0	-3.0128	255.0	-3.0960
260.0	-0.6671	260.0	-2.4664	260.0	-2.5498	260.0	-2.6330	260.0	-2.7162	260.0									

TABLE A14. (Continued)

PAGE 273

BASEPR =	8.1904
HGT	RN
87.0623	0.478439E+06
CLTR	CDTR
2.06	0.93

0019
CMUT
2.071
CMTR
-1.37

ESSURES
WLC = 1
CMUW
2.071
CNTR
2.11

ANARD P
0.0
CMUC
0.0
CV

WING /
DCLC -
W H/C 2.66
O CN

PULSIVE
 1.2786
 IEL
 6.93
 COLLE

PROF.
CDAERO
0
2 6.89
CM

1.7571
PSTAT
2:00.0
(CD

CLAERO
PTOT
2107.6
cl

```

RUN:SEQ
145 3
ALPHA
4.01
BETA

```

FUSELAGE		**NISC.***	
NO.	CP	NO.	CP
1	-0.1393	1	-1.1646
2	-0.1593	2	-0.4234
3	-0.2153	3	-0.7419
4	-0.2531	4	-0.2791
5	-0.3293	5	-2.0308
6	-0.4324	6	-2.0983
7	-0.5194	7	-0.0128
8	-0.5574	8	-1.3807
9	-0.6324	9	-1.0404
10	-0.5574	10	-0.9081
11	-0.5194	11	-0.1744
12	-0.5070	12	-0.4537

```

*****
BP = 22
CP
2.7434
2.5936
2.5437
2.5437
2.5437
-2.4439
-2.1751
-2.3194
-3.2178
-9.4128
85.5359

```

BP - 16
CP
3.8916
3.9915
3.9916
3.2426
-1.7949
-1.0960
-1.1646
-2.0308
-2.4197
-7.6645
24.0484

BP = 12 CP

UP - 6
CP
-3.6920
-1.7949
-1.5452
-1.2956
-1.1958
-1.1958
-1.1646
-1.4533
-2.1916
-6.6004
38.6717-

```

.....
BP = 2
CP
-1.4454
-0.6468
-1.1459
-1.0960
-1.0459
-0.9960
-1.0201
-1.3089
-1.9258
-5.9542
.....

```

.....	%X/C
0.0	0.0
2.5	2.5
5.0	5.0
10.0	10.0
15.0	15.0
24.0	24.0
33.0	33.0
54.0	54.0
65.0	65.0
78.5	78.5
79.5	79.5

CP
-0.6374
-0.6374
-0.6730
-0.6374
-0.6374
-0.6730
-0.6374
-0.6374
-0.6730
-0.6374

*** CANADA ***
 3.375
 CP
 0.6730
 0.6730
 0.6374
 0.6730
 0.6730
 0.6374
 0.6374
 0.6374
 0.6730
 0.6374

%x/c	B
0.0	0.0
2.5	0.0
5.0	0.0
10.0	0.0
15.0	0.0
25.0	0.0
35.0	0.0
50.0	0.0
56.0	0.0
65.0	0.0

Force Data -
Use Run 311

PAGE 278

Force Data -
Use Run 311

PAGE 276

[illegible]

TABLE A15. (Continued)

RUN:SEQ		CLAERO = 2.0941		CD AERO = 1.5607		WING / CANARD		PRESSURES		BASEPR = 8.1904		PAGE 278	
146 3		PSTAT		VEL		YAW		CMJC		HGT		RN	
ALPHA		2102.65		64.52		0.0		0.0		87.0072		0.402708E+08	
BETA		CL		CROLL		CN		CY		CLTP		CDTR	
0.0		4.77		0.04		0.01		-0.02		2.53		1.06	
***** CANARD *****		BP=3.375		BP=10.125		BP = 2		BP = 6		BP = 12		BP = 16	
X/C		CP		CP		CP		CP		CP		CP	
0.0	-0.7804	-0.7298	0.0	-1.8324	-4.1108	-5.9516	-4.1108	-4.1108	-4.1108	-4.1108	-4.1108	-4.1108	-4.1108
2.5	-0.7804	-0.7298	2.5	-0.7826	-1.2880	-4.6772	-3.7567	-3.7567	-3.7567	-3.7567	-3.7567	-3.7567	-3.7567
5.0	-0.7298	-0.6794	5.0	-1.2783	-1.7032	-4.0398	-3.7567	-3.7567	-3.7567	-3.7567	-3.7567	-3.7567	-3.7567
10.0	-0.7804	-0.7298	10.0	-1.2783	-1.4908	-1.7739	-3.8982	-3.8982	-3.8982	-3.8982	-3.8982	-3.8982	-3.8982
15.0	-0.7298	-0.7298	15.0	-1.2075	-1.4199	-1.4908	-3.9442	-3.9442	-3.9442	-3.9442	-3.9442	-3.9442	-3.9442
25.0	-0.7804	-0.7804	25.0	-1.0659	-1.2075	-1.4199	-1.4908	-1.4908	-1.4908	-1.4908	-1.4908	-1.4908	-1.4908
35.0	-0.7298	-0.7804	35.0	-1.0599	-1.0599	-1.4694	-1.4694	-1.4694	-1.4694	-1.4694	-1.4694	-1.4694	-1.4694
50.0	-0.7804	-0.7804	50.0	-1.4694	-1.4694	-1.4694	-1.4694	-1.4694	-1.4694	-1.4694	-1.4694	-1.4694	-1.4694
56.0	-0.7804	-0.7804	56.0	-2.1928	-2.5162	-2.6241	-2.6241	-2.6241	-2.6241	-2.6241	-2.6241	-2.6241	-2.6241
65.0	-0.7804	-0.7804	65.0	-6.8826	-7.5294	-8.1763	-8.1763	-8.1763	-8.1763	-8.1763	-8.1763	-8.1763	-8.1763
76.0	-0.7804	-0.8308	76.0	-189.8630	-177.6109	-174.6214	-103.8083	-101.1	-0.6296	-11	-0.3285	-12	-0.5917
79.0	-0.7804	-0.7992	79.0	-15.6035	-18.8487	-27.0163	0.1854	38.2	-0.0908	38.2	-0.0908	43.4	-0.0908
81.0	-0.6533	-0.8356	81.0	1.4616	212.6985	-4.8101	-7.5085	-20.3440	-20.3440	-20.3440	-20.3440	-20.3440	-20.3440
82.0	-0.7992	-0.7627	82.0	8.8637	-8.4201	9.5566	-8.6388	-10.4985	-10.4985	-10.4985	-10.4985	-10.4985	-10.4985
84.0	-0.7262	-0.7992	84.0	-7.1439	-6.8157	-7.3262	-6.3417	-7.3990	-7.3990	-7.3990	-7.3990	-7.3990	-7.3990
87.0	-0.6898	-0.7374	87.0	2.3003	-8.4565	-6.7062	-3.5339	-5.3938	-5.3938	-5.3938	-5.3938	-5.3938	-5.3938
89.0	-0.6835	-0.7374	89.0	-3.1362	-4.7593	-7.9179	-7.4790	-3.7063	-3.7063	-3.7063	-3.7063	-3.7063	-3.7063
93.0	-0.7374	-0.7374	93.0	-1.6883	-2.3465	-2.8728	-0.9426	-8.0932	-8.0932	-8.0932	-8.0932	-8.0932	-8.0932
95.0	-0.7374	-0.7374	95.0	-1.9555	-3.3117	-0.4601	-0.8549	-9.3655	-9.3655	-9.3655	-9.3655	-9.3655	-9.3655
100.0	-0.7374	-0.7374	100.0	-2.1710	-2.2587	-2.4780	-2.6536	-0.7233	-0.7233	-0.7233	-0.7233	-0.7233	-0.7233
96.0	-0.7513	-0.7913	96.0	0.5050	0.5928	0.4173	0.4173	0.2846	0.2846	0.2846	0.2846	0.2846	0.2846
99.0	-0.7374	-0.7913	99.0	0.6805	0.7682	0.7682	0.5928	-0.1969	-0.1969	-0.1969	-0.1969	-0.1969	-0.1969
84.0	-0.7374	-0.7913	84.0	0.7828	-0.6504	0.7828	0.5781	-0.0362	-0.0362	-0.0362	-0.0362	-0.0362	-0.0362
73.0	-0.7374	-0.7913	73.0	0.5781	0.3733	0.3733	0.3733	0.2410	0.2410	0.2410	0.2410	0.2410	0.2410
50.0	-0.7913	-0.7913	50.0	0.3733	0.3733	0.3733	0.3733	0.1686	0.1686	0.1686	0.1686	0.1686	0.1686
35.0	-0.7298	-0.7804	35.0	0.2795	0.2795	0.2795	0.2795	0.3503	0.3503	0.3503	0.3503	0.3503	0.3503
25.0	-0.7804	-0.7804	25.0	0.4211	0.4211	0.4211	0.4211	0.4919	0.4919	0.4919	0.4919	0.4919	0.4919
10.0	-0.7804	-0.7298	10.0	0.4919	0.4211	0.4211	0.4211	0.4919	0.4919	0.4919	0.4919	0.4919	0.4919
5.0	-0.7298	-0.7804	5.0	0.6335	0.4211	0.4211	0.4211	0.4211	0.4211	0.4211	0.4211	0.4211	0.4211
2.5	-0.7804	-0.7804	2.5	0.6335	0.4211	0.4211	0.4211	0.4211	0.4211	0.4211	0.4211	0.4211	0.4211

TABLE A18. (Concluded)

TABLE A16. (Continued)

RUN: SEQ										PROPLUSTIVE										WING / CANARD										PRESSURES										BASEPR = 8.1904										PAGE 283																																																																																									
147 3										CLAERO = 2.1577										CDERO = 1.7551										DCLC = 0.0										DWLC = 3.5317										BASEPR = 8.1904										PAGE 283																																																																															
ALPHA										PTOT										Q										VEL										YAW										H/C										CMJC										CMUW										CMUT										NOT										BASEPR = 8.1904										PAGE 283																													
4.01										2107.44										3.62										55.62										0.0										2.66										0.0										3.929										3.929										87.0204										0.347981E+08										BASEPR = 8.1904										PAGE 283																			
BETA										CL										CM										CROLL										CN										CY										CNTR										CMTR										CLTR										CDTR										BASEPR = 8.1904										PAGE 283																													
0.0										5.69										-3.88										0.08										0.01										-0.00										2.74										-1.70										2.67										1.11										BASEPR = 8.1904										PAGE 283																													
0.0										-0.8374										0.0										-1.6689										-3.9523										-4.6183										-4.0474										-2.9056										38.2										-0.1837										NO.										CP										MISC.										***									
2.8										-0.8374										2.5										-0.7174										-2.0495										-8.5232										-9.3814										-2.7154										43.4										-0.2362										2										0.4450																													
5.0										-0.8374										5.0										-1.2853										-1.5738										-4.0474										-3.4785										-2.5252										50.4										-0.1637										3										2.5813																													
10.0										-0.8374										10.0										-1.1932										-1.3834										-2.9056										-3.6670										-2.5252										58.1										-0.2362										4										0.1698																													
15.0										-0.8374										15.0										-1.0980										-1.1932										-1.5738										-3.4785										-2.7154										62.5										-0.3810										5										-2.3043																													
20.0										-0.8374										24.0										-1.0028										-1.1932										-1.2853										-1.8593										-2.5252										69.7										-0.4834										6										-0.3804																													
35.0										-0.8374										33.0										-1.2058										-1.4809										-1.4809										-1.4809										-2.5252										76.9										-0.5983										7										-0.1248																													
50.0										-0.8374										54.0										-1.7560										-1.7560										-2.0312										-5.3227										-2.8564										83.4										-0.5983										8										-1.8395																													
58.0										-0.8374										78.5										-7.4069										-8.1312										-8.7831										-9.2177										-11.6040										95.4										-0.7432										9										-1.2447																													
65.0										-0.8374										80.5										19.9555										-19.9752										-18.4071										-29.7247										0.2602										101.1										-0.5269										10										0.8773																													
70.0										-0.8374										81.3										-4.8882										311.3733										-6.5013										-11.0678										-11.0678										38.2										-0.0813										11										-0.2427																													
80.5										-0.8374										82.0										-8.7858										-9.6860										14.0771										-8.9799										-24.6296										43.4										-0.1837										12										0.5963																													
82.0										-0.8177										84.0										-8.4810										-7.7751										-8.5100										-6.9422										7.5791										50.4										0.1260																																																	
87.0										-0.8177										87.0										4.3267										-10.5190										-7.6770										-3.4146										5.0313										58.1										0.1884																																																	
89.0										-0.5983										89.0										-1.1309										-9.5478										-9.6152										-8.9667										-2.8362										62.5										0.2079																																																	
93.0										-0.7432										93.0										-1.4216										-2.4826										-3.1309										-1.0090										-8.5539										69.7										0.2079																																																	
96.0										-0.7432										96.0										-2.0898										-3.7795										-0.0658										-0.3018										-10.7352										76.9										0.3432																																																	
100.0										-0.6708										100.0										-2.9543										-3.1309										-3.3682										-3.5437										76.9										0.3432																																																											
96.0										-0.7432										96.0										0.4647										0.5826										0.3469										0.3469										89.4										0.2709																																																											
84.0										-0.6708										84.0										0.7005										0.8184										0.8184										0.6415										-0.3016										95.4										-0.0189																																																	
73.0										-0.7432										73.0										0.4450										-0.9306										0.7201										0.7201										-0.1053										101.1										-1.0329																																																	
50.0										-0.6708										50.0										0.1698										0.1698										0.4450										0.4450										0.1053																																																																					
35.0										-0.7696										35.0										0.8374										0.8374										0.6146										0.6146										0.0437																																																																					
25.0										-0.8374										25.0										0.5194										0.5194										0.5194										0.5194										0.7097										0.1698																																																											
10.0										-0.9053										10.0										0.8374										0.8374										0.8374										0.8374										0.8374										0.8374										0.8374																																																	
5.0										-0.8374										5.0										0.7097										0.7097										0.7097										0.7097										0.7097										0.7097										0.7097																																																	
2.5										-0.8374										2.5										0.6146										0.6146										0.6146										0.6146										0.6146										0.6146										0.6146																																																	

TABLE A16. (Concluded)

***** CANARD *****										***** FUSELAGE*****																	
BP=3.375 BP=10.125										-----TOP-----																	
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XLOC	CP	NO.	CP	*****MISC*****													
0.0	-0.9052	0.0	-0.9052	0.0	-0.9018	0.0	-0.9057	0.0	-0.9052	38.2	-0.3085	1	-1.7559														
2.5	-0.8373	2.5	-0.8373	2.5	-0.8125	2.5	-0.8125	2.5	-0.8125	43.4	-0.3085	2	0.4451														
5.0	-0.8373	5.0	-0.8373	5.0	-0.8373	5.0	-0.8373	5.0	-0.8373	50.4	-0.3085	3	-6.1578														
10.0	-0.8373	10.0	-0.8373	10.0	-0.8373	10.0	-0.8373	10.0	-0.8373	56.1	-0.4534	4	0.1699														
15.0	-0.9052	15.0	-0.9052	15.0	-0.9052	15.0	-0.9052	15.0	-0.9052	62.5	-0.8983	5	-4.5071														
20.0	-0.9052	20.0	-0.9052	20.0	-0.9052	20.0	-0.9052	20.0	-0.9052	66.7	-0.7431	6	-0.3802														
25.0	-0.9052	25.0	-0.9052	25.0	-0.9052	25.0	-0.9052	25.0	-0.9052	76.9	-0.7431	7	-0.3805														
30.0	-0.9052	30.0	-0.9052	30.0	-0.9052	30.0	-0.9052	30.0	-0.9052	83.4	-0.6707	8	-2.0588														
35.0	-0.9052	35.0	-0.9052	35.0	-0.9052	35.0	-0.9052	35.0	-0.9052	89.4	-0.7431	9	-1.7751														
40.0	-0.9052	40.0	-0.9052	40.0	-0.9052	40.0	-0.9052	40.0	-0.9052	101.1	-0.8983	10	0.8774														
45.0	-0.9052	45.0	-0.9052	45.0	-0.9052	45.0	-0.9052	45.0	-0.9052	---BOTTOM---																	
50.0	-0.9052	50.0	-0.9052	50.0	-0.9052	50.0	-0.9052	50.0	-0.9052	38.2	-0.0613	11	-0.4194														
55.0	-0.9052	55.0	-0.9052	55.0	-0.9052	55.0	-0.9052	55.0	-0.9052	43.4	-0.0188	12	-0.8320														
60.0	-0.9052	60.0	-0.9052	60.0	-0.9052	60.0	-0.9052	60.0	-0.9052	50.4	-0.1637																
65.0	-0.9052	65.0	-0.9052	65.0	-0.9052	65.0	-0.9052	65.0	-0.9052	56.1	0.1261																
70.0	-0.9052	70.0	-0.9052	70.0	-0.9052	70.0	-0.9052	70.0	-0.9052	62.5	0.1984																
75.0	-0.9052	75.0	-0.9052	75.0	-0.9052	75.0	-0.9052	75.0	-0.9052	69.7	0.3433																
80.0	-0.9052	80.0	-0.9052	80.0	-0.9052	80.0	-0.9052	80.0	-0.9052	76.9	0.4158																
85.0	-0.9052	85.0	-0.9052	85.0	-0.9052	85.0	-0.9052	85.0	-0.9052	83.4	0.4158																
90.0	-0.9052	90.0	-0.9052	90.0	-0.9052	90.0	-0.9052	90.0	-0.9052	89.4	0.4158																
95.0	-0.9052	95.0	-0.9052	95.0	-0.9052	95.0	-0.9052	95.0	-0.9052	95.4	0.4158																
100.0	-0.9052	100.0	-0.9052	100.0	-0.9052	100.0	-0.9052	100.0	-0.9052	101.1	-1.1777																
105.0	-0.9052	105.0	-0.9052	105.0	-0.9052	105.0	-0.9052	105.0	-0.9052																		
110.0	-0.9052	110.0	-0.9052	110.0	-0.9052	110.0	-0.9052	110.0	-0.9052																		
115.0	-0.9052	115.0	-0.9052	115.0	-0.9052	115.0	-0.9052	115.0	-0.9052																		
120.0	-0.9052	120.0	-0.9052	120.0	-0.9052	120.0	-0.9052	120.0	-0.9052																		
125.0	-0.9052	125.0	-0.9052	125.0	-0.9052	125.0	-0.9052	125.0	-0.9052																		
130.0	-0.9052	130.0	-0.9052	130.0	-0.9052	130.0	-0.9052	130.0	-0.9052																		
135.0	-0.9052	135.0	-0.9052	135.0	-0.9052	135.0	-0.9052	135.0	-0.9052																		
140.0	-0.9052	140.0	-0.9052	140.0	-0.9052	140.0	-0.9052	140.0	-0.9052																		
145.0	-0.9052	145.0	-0.9052	145.0	-0.9052	145.0	-0.9052	145.0	-0.9052																		
150.0	-0.9052	150.0	-0.9052	150.0	-0.9052	150.0	-0.9052	150.0	-0.9052																		
155.0	-0.9052	155.0	-0.9052	155.0	-0.9052	155.0	-0.9052	155.0	-0.9052																		
160.0	-0.9052	160.0	-0.9052	160.0	-0.9052	160.0	-0.9052	160.0	-0.9052																		
165.0	-0.9052	165.0	-0.9052	165.0	-0.9052	165.0	-0.9052	165.0	-0.9052																		
170.0	-0.9052	170.0	-0.9052	170.0	-0.9052	170.0	-0.9052	170.0	-0.9052																		
175.0	-0.9052	175.0	-0.9052	175.0	-0.9052	175.0	-0.9052	175.0	-0.9052																		
180.0	-0.9052	180.0	-0.9052	180.0	-0.9052	180.0	-0.9052	180.0	-0.9052																		
185.0	-0.9052	185.0	-0.9052	185.0	-0.9052	185.0	-0.9052	185.0	-0.9052																		
190.0	-0.9052	190.0	-0.9052	190.0	-0.9052	190.0	-0.9052	190.0	-0.9052																		
195.0	-0.9052	195.0	-0.9052	195.0	-0.9052	195.0	-0.9052	195.0	-0.9052																		
200.0	-0.9052	200.0	-0.9052	200.0	-0.9052	200.0	-0.9052	200.0	-0.9052																		
205.0	-0.9052	205.0	-0.9052	205.0	-0.9052	205.0	-0.9052	205.0	-0.9052																		
210.0	-0.9052	210.0	-0.9052	210.0	-0.9052	210.0	-0.9052	210.0	-0.9052																		
215.0	-0.9052	215.0	-0.9052	215.0	-0.9052	215.0	-0.9052	215.0	-0.9052																		
220.0	-0.9052	220.0	-0.9052	220.0	-0.9052	220.0	-0.9052	220.0	-0.9052																		
225.0	-0.9052	225.0	-0.9052	225.0	-0.9052	225.0	-0.9052	225.0	-0.9052																		
230.0	-0.9052	230.0	-0.9052	230.0	-0.9052	230.0	-0.9052	230.0	-0.9052																		
235.0	-0.9052	235.0	-0.9052	235.0	-0.9052	235.0	-0.9052	235.0	-0.9052																		
240.0	-0.9052	240.0	-0.9052	240.0	-0.9052	240.0	-0.9052	240.0	-0.9052																		
245.0	-0.9052	245.0	-0.9052	245.0	-0.9052	245.0	-0.9052	245.0	-0.9052																		
250.0	-0.9052	250.0	-0.9052	250.0	-0.9052	250.0	-0.9052	250.0	-0.9052																		
255.0	-0.9052	255.0	-0.9052	255.0	-0.9052	255.0	-0.9052	255.0	-0.9052																		
260.0	-0.9052	260.0	-0.9052	260.0	-0.9052	260.0	-0.9052	260.0	-0.9052																		
265.0	-0.9052	265.0	-0.9052	265.0	-0.9052	265.0	-0.9052	265.0	-0.9052																		
270.0	-0.9052	270.0	-0.9052	270.0	-0.9052	270.0	-0.9052	270.0	-0.9052																		
275.0	-0.9052	275.0	-0.9052	275.0	-0.9052	275.0	-0.9052	275.0	-0.9052																		
280.0	-0.9052	280.0	-0.9052	280.0	-0.9052	280.0	-0.9052	280.0	-0.9052																		
285.0	-0.9052	285.0	-0.9052	285.0	-0.9052	285.0	-0.9052	285.0	-0.9052																		
290.0	-0.9052	290.0	-0.9052	290.0	-0.9052	290.0	-0.9052	290.0	-0.9052																		
295.0	-0.9052	295.0	-0.9052	295.0	-0.9052	295.0	-0.9052	295.0	-0.9052																		
300.0	-0.9052	300.0	-0.9052	300.0	-0.9052	300.0	-0.9052	300.0	-0.9052																		
305.0	-0.9052	305.0	-0.9052	305.0	-0.9052	305.0	-0.9052	305.0	-0.9052																		
310.0	-0.9052	310.0	-0.9052	310.0	-0.9052	310.0	-0.9052	310.0	-0.9052																		
315.0	-0.9052	315.0	-0.9052	315.0	-0.9052	315.0	-0.9052	315.0	-0.9052																		
320.0	-0.9052	320.0	-0.9052	320.0	-0.9052	320.0	-0.9052	320.0	-0.9052																		
325.0	-0.9052	325.0	-0.9052	325.0	-0.9052	325.0	-0.9052	325.0	-0.9052																		
330.0	-0.9052	330.0	-0.9052	330.0	-0.9052	330.0	-0.9052	330.0	-0.9052																		
335.0	-0.9052	335.0	-0.9052	335.0	-0.9052	335.0	-0.9052	335.0	-0.9052																		
340.0	-0.9052	340.0	-0.9052	340.0	-0.9052	340.0	-0.9052	340.0	-0.9052																		
345.0	-0.9052	345.0	-0.9052	345.0	-0.9052	345.0	-0.9052	345.0	-0.9052																		
350.0	-0.9052	350.0	-0.9052	350.0	-0.9052	350.0	-0.9052	350.0	-0.9052																		
355.0	-0.9052	355.0	-0.9052	355.0	-0.9052	355.0	-0.9052	355.0	-0.9052																		
360.0	-0.9052	360.0	-0.9052	360.0	-0.9052	360.0	-0.9052	360.0	-0.9052																		
365.0	-0.9052	365.0	-0.9052	365.0	-0.9052	365.0	-0.9052	365.0	-0.9052																		
370.0	-0.9052	370.0	-0.9052	370.0	-0.9052	370.0	-0.9052	370.0	-0.9052																		
375.0	-0.9052	375.0	-0.9052	375.0	-0.9052	375.0	-0.9052	375.0	-0.9052																		
380.0	-0.9052	380.0	-0.9052	380.0	-0.9052	380.0	-0.9052	380.0	-0.9052																		
385.0	-0.9052	385.0	-0.9052	385.0	-0.9052	385.0	-0.9052	385.0	-0.9052																		
390.0	-0.9052	390.0	-0.9052	390.0	-0.9052	390.0	-0.9052	390.0	-0.9052																		
395.0	-0.9052	395.0	-0.9052	395.0	-0.9052	395.0	-0.9052	395.0	-0.9052																		
400.0	-0.9052	400.0	-0.9052	400.0	-0.9052	400.0	-0.9052	400.0	-0.9052																		
405.0	-0.9052	405.0	-0.9052	405.0	-0.9052	405.0	-0.9052	405.0	-0.9052																		
410.0	-0.9052	410.0	-0.9052	410.0	-0.9052	410.0	-0.9052	410.0	-0.9052																		
415.0	-0.9052	415.0	-0.9052	415.0	-0.9052	415.0	-0.9052	415.0	-0.9052																		
420.0	-0.9052	420.0	-0.9052	420.0	-0.9052	420.0	-0.9052	420.0	-0.9052																		
425.0	-0.9052	425.0	-0.9052	425.0	-0.9052	425.0	-0.9052	425.0	-0.9052																		
430.0	-0.9052	430.0	-0.9052	430.0	-0.9052	430.0	-0.9052	430.0	-0.9052																		
435.0	-0.9052	435.0	-0.9052	435.0	-0.9052	435.0	-0.9052	435.0	-0.9052																		
440.0	-0.9052	440.0	-0.9052	440.0	-0.9052	440.0	-0.9052	440.0	-0.9052																		
445.0	-0.9052	445.0	-0.9052	445.0	-0.9052	445.0	-0.9052	445.0	-0.9052																		
450.0	-0.9052	450.0	-0.9052	450.0	-0.9052	450.0	-0.9052	450.0	-0.9052																		
455.0	-0.9052	455.0	-0.9052	455.0	-0.9052	455.0	-0.9052	455.0	-0.9052																		
460.0	-0.9052	460.0	-0.9052	460.0	-0.9052	460.0	-0.9052	460.0	-0.9052																		
465.0	-0.9052	465.0	-0.9052	465.0	-0.9052	465.0	-0.9052	465.0	-0.9052																		
470.0	-0.9052	470.0	-0.9052	470.0	-0.9052	470.0	-0.9052	470.0	-0.9052																		
475.0	-0.9052	475.0	-0.9052	475.0	-0.9052	475.0	-0.9052	475.0	-0.9052																		
480.0	-0.9052	480.0	-0.9052	480.0	-0.9052	480.0	-0.9052	480.0	-0.9052																		
485.0	-0.9052	485.0	-0.9052	485.0	-0.9052	485.0	-0.9052	485.0	-0.9052																		
490.0	-0.9052	490.0	-0.9052	490.0	-0.9052	490.0	-0.9052	490.0	-0.9052																		
4																											

TABLE A17. RUN 148, BW6V, DELF=45, CMJ=2.0, (BN/B)=1

RUN: SEQ										PROPLUISIVE										WING / CANARD										PRESSURES										BASEPR = 8.1904										PAGE 286																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																			
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O.0										3.50										O.14										-2.42										O.04										O.01										O.01										2.08										-1.37										2.08										0.81																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																	
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TABLE A17. (Concluded)

RUN: SEQ										PAGE 280									
148	5	CLARO =	2.5817	CDARO =	1.7315	DELIC =	0.0	CMUC	1.9531	BASEPR =	8.1904	HGT	RM	87.1828	0.422238E+05	CLTR	CDTR	1.47	
ALPHA	12.02	PTOT	2107.02	VEL	87.38	YAW	0.0	H/C	2.053										
BETA	0.0	CL	4.53	CM	-2.83	CROLL	0.06	CV	3.17										
		CD	1.10																
***** CANARD *****										***** FUSELAGE *****									
BP=3.375	BP=10.125	CP		BP = 2	BP = 6	BP = 12	BP = 16	BP = 22		----	----	----	----	----	----	----	----	----	
XX/C	0.0	CP	-0.7125	XX/C	CP	CP	CP	CP		XLOC	CP								
0.0	-0.6662		-0.7125	0.0	-6.4538	-7.3508	-5.2872	-3.9268	-3.4730	38.2	-0.2847	1	-1.2505						
2.5	-0.6200		-0.7125	2.5	-0.5373	-7.8781	-5.8434	-4.1209	-3.5378	43.4	-0.3340	2	0.4357						
5.0	-0.6200		-0.7125	5.0	-2.2419	-6.1843	-5.4169	-4.4449	-3.6028	50.4	-0.3833	3	8.7472						
10.0	-0.6662		-0.7583	10.0	-1.8532	-1.3998	-7.3608	-5.2224	-3.6028	56.1	-0.4820	4	0.2484						
15.0	-0.7125		-0.7125	15.0	-1.5939	-1.5939	-6.3240	-5.8112	-3.7870	62.5	-0.6298	5	3.8735						
20.0	-0.7125		-0.7125	20.0	-1.3998	-1.4844	-1.5939	-5.8484	-4.0861	69.7	-0.7288	6	0.3137						
25.0	-0.7125		-0.7125	25.0	-1.2508	-1.4378	-1.2508	-4.2484	-4.4357	76.9	-0.7779	7	0.2468						
30.0	-0.7125		-0.7125	30.0	-1.4378	-1.6252	-1.6252	-2.5820	-6.4967	83.4	-0.8793	8	0.8926						
35.0	-0.7125		-0.7586	35.0	-2.0405	-2.3564	-2.2578	-1.9124	-6.3819	89.4	-0.7268	9	1.8713						
40.0	-0.7125		-0.7125	40.0	-6.3819	-7.0918	-7.8317	-8.0783	-10.2880	95.4	-0.8793	10	0.7977						
45.0	-0.6662		-0.7125	45.0	-108.9434	-73.7099	-74.7792	-78.9833	-101.1	101.1	-0.8793	11	0.4072						
50.0	-0.6662		-0.7125	50.0	-12.2822	-12.6492	-19.0229	-28.1330	-0.1367										
55.0	-0.6038		-0.6038	55.0	-6.7100	217.8481	-9.8784	-13.2184	-19.2883	38.2	-0.0371								
60.0	-0.6708		-0.7039	60.0	0.1870	-7.0769	3.0332	-11.0811	-13.1498	43.4	-0.0371								
65.0	-0.8040		-0.6038	65.0	-6.1427	-6.2762	-7.4108	-8.9101	-7.1103	50.4	-0.0308								
70.0	-0.8705		-0.7039	70.0	0.7643	-6.7433	-6.4784	-4.2408	-7.1103	56.1	0.2088								
75.0	-0.7039		-0.6753	75.0	-2.5347	-3.8895	-6.8103	-7.0709	-8.9088	62.5	0.3072								
80.0	-0.7286		-0.7286	80.0	-1.4107	-2.1333	-3.0168	-0.8487	-8.5582	69.7	0.3598								
85.0	-0.7286		-0.7286	85.0	-1.5114	-2.6953	-1.1298	-1.6918	-8.3558	73.0	0.3072								
90.0	-0.7286		-0.7286	90.0	-0.8289	-1.3706	-1.5713	-1.8522	-0.6882	83.4	0.3072								
95.0	-0.7286		-0.7286	95.0	0.5161	0.7169	0.5563	0.4760	-0.1663	89.4	0.3072								
100.0	-0.7286		-0.7286	100.0	0.6366	0.8373	0.7972	0.5984	-0.1262	95.4	0.3072								
105.0	-0.7286		-0.7286	105.0	0.6231	-0.6884	0.6231	0.6231	0.1264	101.1	-0.8766								
110.0	-0.7286		-0.7286	110.0	0.4357	0.4357	0.4357	0.4357	0.1264										
115.0	-0.7286		-0.7286	115.0	0.4357	0.4357	0.4357	0.4357	0.1264										
120.0	-0.7286		-0.7286	120.0	0.4795	0.4795	0.4795	0.4795	0.1595										
125.0	-0.7586		-0.7586	125.0	0.6091	0.6091	0.6091	0.6091	0.2484										
130.0	-0.7586		-0.7586	130.0	0.6091	0.6091	0.6091	0.6091	0.2484										
135.0	-0.7125		-0.7125	135.0	0.7387	0.7387	0.7387	0.7387	0.2484										
140.0	-0.6662		-0.6662	140.0	2.5	0.4147	0.2203	0.0907	-0.1264										
145.0	-0.7125		-0.7125	145.0															
150.0	-0.7586		-0.7586	150.0															
155.0	-0.7125		-0.7125	155.0															
160.0	-0.7586		-0.7586	160.0															
165.0	-0.7125		-0.7125	165.0															
170.0	-0.7586		-0.7586	170.0															
175.0	-0.7125		-0.7125	175.0															
180.0	-0.7586		-0.7586	180.0															
185.0	-0.7125		-0.7125	185.0															
190.0	-0.7586		-0.7586	190.0															
195.0	-0.7125		-0.7125	195.0															
200.0	-0.7586		-0.7586	200.0															
205.0	-0.7125		-0.7125	205.0															
210.0	-0.7586		-0.7586	210.0															
215.0	-0.7125		-0.7125	215.0															
220.0	-0.7586		-0.7586	220.0															
225.0	-0.7125		-0.7125	225.0															
230.0	-0.7586		-0.7586	230.0															
235.0	-0.7125		-0.7125	235.0															
240.0	-0.7586		-0.7586	240.0															
245.0	-0.7125		-0.7125	245.0															
250.0	-0.7586		-0.7586	250.0															
255.0	-0.7125		-0.7125	255.0															
260.0	-0.7586		-0.7586	260.0															
265.0	-0.7125		-0.7125	265.0															
270.0	-0.7586		-0.7586	270.0															
275.0	-0.7125		-0.7125	275.0															
280.0	-0.7586		-0.7586	280.0															
285.0	-0.7125		-0.7125	285.0															
290.0	-0.7586		-0.7586	290.0															
295.0	-0.7125		-0.7125	295.0															
300.0	-0.7586		-0.7586	300.0															
305.0	-0.7125		-0.7125	305.0															
310.0	-0.7586		-0.7586	310.0															
315.0	-0.7125		-0.7125	315.0															
320.0	-0.7586		-0.7586	320.0															
325.0	-0.7125		-0.7125	325.0															
330.0	-0.7586		-0.7586	330.0															
335.0	-0.7125		-0.7125	335.0															
340.0	-0.7586		-0.7586	340.0															
345.0	-0.7125		-0.7125	345.0															
350.0	-0.7586		-0.7586	350.0															
355.0	-0.7125		-0.7125	355.0															
360.0	-0.7586		-0.7586	360.0															
365.0	-0.7125		-0.7125	365.0															
370.0	-0.7586		-0.7586	370.0															
375.0	-0.7125		-0.7125	375.0															
380.0	-0.7586		-0.7586	380.0															
385.0	-0.7125		-0.7125	385.0															
390.0	-0.7586		-0.7586	390.0															
395.0	-0.7125		-0.7125	395.0															
400.0	-0.7586		-0.7586	400.0															
405.0	-0.7125		-0.7125	405.0															
410.0	-0.7586		-0.7586	410.0															
415.0	-0.7125		-0.7125	415.0															
420.0	-0.7586		-0.7586	420.0															
425.0	-0.7125		-0.7125	425.0															

TABLE A18. RUN 149, BWV, DELP=45, CMU=1.0, (BN/B)=1

TUN:SEQ										PAGE 281									
149	1	CLARO =	1.5773	CDAERO =	0.8964	WING / CANARD	PRESSURES	BASEPR =	8.1904										
ALPHA	PTOT	PSTAT	2106.52	VEL	VAV	H/C	CMU	HOT	RM										
BETA	CL	CD	2.48	0.37	-1.66	0.03	0.01	0.02	1.91	CLTR	CDTR	CMTR	1.91	0.67					
0.0	2.48	0.37	-1.66	0.03	0.01	0.02	1.91	1.91	0.67										
***** CANARD *****										***** FUSELAGE *****									
BP=3.375		BP=10.125		BP=2		BP=6		BP=12		BP=18		BP=22		KLOC		CP		MISC...	
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP
0.0	-0.5274	0.0	-0.5274	0.0	-0.0389	0.0	-0.2980	-2.2415	-2.9642	-3.3429	-3.9823	-3.0189	38.2	-0.0873	1	-1.0630	1	-1.0630	
2.5	-0.5274	2.5	-0.5274	2.5	-0.4924	-1.0107	-1.5936	-1.9823	-1.9823	-3.0189	-3.9823	-3.0189	43.4	-0.1367	2	0.2483	2	0.2483	
5.0	-0.5274	5.0	-0.5274	5.0	-0.5872	-0.7518	-1.1402	-1.3984	-1.3984	-1.9823	-3.0189	-1.9823	50.4	-0.1867	3	-1.2503	3	-1.2503	
10.0	-0.5274	10.0	-0.5274	10.0	-0.6219	-0.7518	-1.0754	-1.0754	-1.0754	-1.9823	-3.0189	-1.9823	56.1	-0.2367	4	0.2483	4	0.2483	
15.0	-0.5274	15.0	-0.5274	15.0	-0.6219	-0.6887	-0.9459	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	62.5	-0.2867	5	-1.2503	5	-1.2503	
20.0	-0.5274	20.0	-0.5274	20.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	68.7	-0.3367	6	-0.3136	6	-0.3136	
25.0	-0.5274	25.0	-0.5274	25.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	75.9	-0.3867	7	0.1147	7	0.1147	
30.0	-0.5274	30.0	-0.5274	30.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	83.4	-0.4367	8	-1.0893	8	-1.0893	
35.0	-0.5274	35.0	-0.5274	35.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	89.4	-0.4867	9	0.0881	9	0.0881	
40.0	-0.5274	40.0	-0.5274	40.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	95.4	-0.5367	10	0.9773	10	0.9773	
45.0	-0.5274	45.0	-0.5274	45.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	101.1	-0.5867	11	-0.1281	11	-0.1281	
50.0	-0.5274	50.0	-0.5274	50.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	107.1	-0.6367	12	0.3670	12	0.3670	
55.0	-0.5274	55.0	-0.5274	55.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	113.1	-0.6867					
60.0	-0.5274	60.0	-0.5274	60.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	119.1	-0.7367					
65.0	-0.5274	65.0	-0.5274	65.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	125.1	-0.7867					
70.0	-0.5274	70.0	-0.5274	70.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	131.1	-0.8367					
75.0	-0.5274	75.0	-0.5274	75.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	137.1	-0.8867					
80.0	-0.5274	80.0	-0.5274	80.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	143.1	-0.9367					
85.0	-0.5274	85.0	-0.5274	85.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	149.1	-0.9867					
90.0	-0.5274	90.0	-0.5274	90.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	155.1	-1.0367					
95.0	-0.5274	95.0	-0.5274	95.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	161.1	-1.0867					
100.0	-0.5274	100.0	-0.5274	100.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	167.1	-1.1367					
105.0	-0.5274	105.0	-0.5274	105.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	173.1	-1.1867					
110.0	-0.5274	110.0	-0.5274	110.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	179.1	-1.2367					
115.0	-0.5274	115.0	-0.5274	115.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	185.1	-1.2867					
120.0	-0.5274	120.0	-0.5274	120.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	191.1	-1.3367					
125.0	-0.5274	125.0	-0.5274	125.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	197.1	-1.3867					
130.0	-0.5274	130.0	-0.5274	130.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	203.1	-1.4367					
135.0	-0.5274	135.0	-0.5274	135.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	209.1	-1.4867					
140.0	-0.5274	140.0	-0.5274	140.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	215.1	-1.5367					
145.0	-0.5274	145.0	-0.5274	145.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	221.1	-1.5867					
150.0	-0.5274	150.0	-0.5274	150.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	227.1	-1.6367					
155.0	-0.5274	155.0	-0.5274	155.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	233.1	-1.6867					
160.0	-0.5274	160.0	-0.5274	160.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	239.1	-1.7367					
165.0	-0.5274	165.0	-0.5274	165.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	245.1	-1.7867					
170.0	-0.5274	170.0	-0.5274	170.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	251.1	-1.8367					
175.0	-0.5274	175.0	-0.5274	175.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	257.1	-1.8867					
180.0	-0.5274	180.0	-0.5274	180.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	263.1	-1.9367					
185.0	-0.5274	185.0	-0.5274	185.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	269.1	-1.9867					
190.0	-0.5274	190.0	-0.5274	190.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	275.1	-2.0367					
195.0	-0.5274	195.0	-0.5274	195.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	281.1	-2.0867					
200.0	-0.5274	200.0	-0.5274	200.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	287.1	-2.1367					
205.0	-0.5274	205.0	-0.5274	205.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	293.1	-2.1867					
210.0	-0.5274	210.0	-0.5274	210.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	299.1	-2.2367					
215.0	-0.5274	215.0	-0.5274	215.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	305.1	-2.2867					
220.0	-0.5274	220.0	-0.5274	220.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	311.1	-2.3367					
225.0	-0.5274	225.0	-0.5274	225.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	317.1	-2.3867					
230.0	-0.5274	230.0	-0.5274	230.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	323.1	-2.4367					
235.0	-0.5274	235.0	-0.5274	235.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	329.1	-2.4867					
240.0	-0.5274	240.0	-0.5274	240.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	335.1	-2.5367					
245.0	-0.5274	245.0	-0.5274	245.0	-0.6219	-0.7518	-0.8811	-0.8811	-0.8811	-1.9823	-3.0189	-1.9823	341.1	-2.5867					
25																			

TABLE A10. (Continued)

TABLE A10. (Concluded)

TABLE A19. (Continued)

RUN: SEQ										BASEPR = 8.1916										PAGE 444																																							
187	4	CLAEPO	0.7208	CDAEPO	0.2474	DLCL	0.0	DMCL	0.0	NET	86.3498	0.106767E+07	CLTR	0.72	0.25																																												
ALPHA	4.01	PTOT	2118.26	PSTAT	2088.08	VEL	157.01	YAW	H/C	CRUC	CMW	CMUT	CMTR	0.73	-0.38																																												
BETA	0.0	CL	0.72	CD	0.25	CM	-0.36	CRULL	0.00	CM	0.01	0.73	-0.38																																														
***** CANARD *****																																																											
BP=3.375										BP=10.125										BP=6										BP=12										BP=16										BP=22									
XX/C										XX/C										XX/C										XX/C										XX/C										XX/C									
0.0										0.0										0.0										0.0										0.0										0.0									
-0.2275										-0.2193										-0.2193										-0.2193										-0.2193										-0.2193									
2.5										2.5										2.5										2.5										2.5										2.5									
-0.2193										-0.2193										-0.2193										-0.2193										-0.2193										-0.2193									
0.0										0.0										0.0										0.0										0.0										0.0									
-0.2112										-0.2112										-0.2112										-0.2112										-0.2112										-0.2112									
5.0										5.0										5.0										5.0										5.0										5.0									
-0.2193										-0.2193										-0.2193										-0.2193										-0.2193										-0.2193									
10.0										10.0										10.0										10.0										10.0										10.0									
-0.2275										-0.2193										-0.2193										-0.2193										-0.2193										-0.2193									
15.0										15.0										15.0										15.0										15.0										15.0									
-0.2275										-0.2193										-0.2193										-0.2193										-0.2193										-0.2193									
25.0										25.0										25.0										25.0										25.0										25.0									
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35.0										35.0										35.0										35.0										35.0										35.0									
-0.2193										-0.2193										-0.2193										-0.2193										-0.2193										-0.2193									
50.0										50.0										50.0										50.0										50.0										50.0									
-0.2193										-0.2193										-0.2193										-0.2193										-0.2193										-0.2193									
55.0										55.0										55.0										55.0										55.0										55.0									
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65.0										65.0										65.0										65.0										65.0										65.0									
-0.2193										-0.2193										-0.2193										-0.2193										-0.2193										-0.2193									
75.0										75.0										75.0										75.0										75.0										75.0									
-0.2193										-0.2193										-0.2193										-0.2193										-0.2193										-0.2193									
79.0										79.0										79.0										79.0										79.0										79.0									
-0.2112										-0.2193										-0.2193										-0.2193										-0.2193										-0.2193									
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-0.1375										-0.1975										-0.1975										-0.1975										-0.1975										-0.1975									
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84.0										84.0										84.0										84.0										84.0										84.0									
-0.2034										-0.2034										-0.2034										-0.2034										-0.2034										-0.2034									
87.0										87.0										87.0										87.0										87.0										87.0									
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89.0										89.0										89.0										89.0										89.0										89.0									
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93.0										93.0										93.0										93.0										93.0										93.0									
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96.0										96.0										96.0										96.0										96.0										96.0									
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100.0										100.0										100.0										100.0										100.0										100.0									
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96.0										96.0										96.0										96.0										96.0										96.0									
-0.2149										-0.2149										-0.2149										-0.2149										-0.2149										-0.2149									
84.0										84.0										84.0										84.0										84.0										84.0									
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73.0										73.0										73.0										73.0										73.0										73.0									
-0.2149										-0.2149										-0.2149										-0.2149										-0.2149										-0.2149									
50.0										50.0										50.0										50.0										50.0										50.0									
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35.0										35.0										35.0										35.0										35.0										35.0									
-0.2112										-0.2112										-0.2112										-0.2112										-0.2112										-0.2112									
25.0										25.0										25.0										25.0										25.0										25.0									
-0.2193										-0.2193										-0.2193										-0.2193										-0.2193										-0.2193									
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5.0										5.0										5.0										5.0										5.0										5.0									
-0.2193										-0.2193										-0.2193										-0.2193										-0.2193										-0.2193									
2.5										2.5										2.5										2.5										2.5										2.5									
-0.2112										-0.2193										-0.2193										-0.2193										-0.2193										-0.2193									
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69.7										69.7										69.7										69.7										69.7										69.7									
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75.9										75.9										75.9										75.9										75.9										75.9									
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-0.0490										-0.0490										-0.0490										-0.0490										-0.0490										-0.0490									
69.7										69.7										69.7										69.7										69.7										69.7									
-0.1328										-0.1328										-0.1328										-0.1328										-0.1328										-0.1328									
75.9										75.9										75.9										75.9										75.9										75.9									
-0.1498										-0.1498										-0.1498										-0.1498										-0.1498										-0.1498									
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101.1										101.1										101.1										101.1										101.1										101.1									
-0.3018										-0.3018										-0.3018										-0.3018										-0.3018										-0.3018									
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XLOC										XLOC										XLOC										XLOC										XLOC										XLOC									
38.2										38.2										38.2										38.2										38.2										38.2									
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43.4										43.4										43.4										43.4										43.4										43.4									
-0.0673										-0.0673										-0.0673										-0.0673										-0.0673										-0.0673									
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-0.0760										-0.0760										-0.0760										-0.0760										-0.0760										-0.0760									
56.1										56.1										56.1										56.1										56.1										56.1									
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-0.1020										-0.1020										-0.1020										-0.1020										-0.1020										-0.1020									
69.7										69.7										69.7										69.7										69.7										69.7									
-0.1715										-0.1715										-0.1715										-0.1715										-0.1715										-0.1715									
75.9										75.9										75.9										75.9										75.9										75.9									
-0.1628										-0.1628										-0.1628										-0.1628										-0.1628										-0.1628									
82.4										82.4										82.4										82.4										82.4										82.4									
-0.1348										-0.1348										-0.1348										-0.1348										-0.1348										-0.1348									
89.4										89.4										89.4										89.4										89.4										89.4									
-0.2149										-0.2149										-0.2149										-0.2149										-0.2149										-0.2149									
94.1										94.1										94.1										94.1										94.1										94									

TABLE A19. (Concluded)

RUN:SEQ														PROPELLANTIVE WING / CANARD PRESSURES														BASEPR = 8.1916														PAGE 446																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																			
187 6														CLARO = 1.1278														CDARO = 0.4261														DLCL = 0.0														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC														CHWC											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TABLE A20. RUN 188, BWGV, DELF=4R J=0.5, (BN/B)=0.5

RUN: SEQ		CANARD		PROPLUSIVE		WING / CANARD		PRESSURES		BASEPR = 8.1916		PAGE 447	
188	1	CLAERO =	0.4560	CD AERO =	0.3093	DCLC =	0.0	DMLC =	0.4294	HGT	87.7681	0.105144E+07	BN
ALPHA	PTOT	PSTAT	0	VEL	YAV	M/C	CMJC	CMJM	CMJT	CLTR	0.63	0.22	CDTR
BETA	CL	CD	0.89	0.06	0.04	0.00	-0.05	0.63	-0.40				
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
CANARD		PROPLUSIVE		WING		PRESSURES		FUSELAGE		MISC		Force Data - Use	
BP=3.375 BP=10.125		BP=2 BP=6 BP=12 BP=18 BP=22		XLOC		XLOC		XLOC		XLOC		Run 222	
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP		
0.0	-0.3398	0.0	0.4567	0.3753	0.0033	-0.3687	-0.3571	38.2	-0.0766	1	-0.4422		
2.5	-0.3233	2.5	0.3106	-0.4850	-0.7756	-0.7873	-0.7873	43.4	-0.0889	2	0.0956		
5.0	-0.3398	5.0	0.2641	-0.4385	-0.5431	-0.6361	-0.7640	50.4	-0.0878	3	-0.5094		
10.0	-0.3316	10.0	-0.3571	-0.4734	-0.5664	-0.5431	-0.6245	56.1	-0.0878	4	0.1628		
15.0	-0.3316	15.0	0.3571	-0.4385	-0.4966	-0.5315	-0.5848	62.5	-0.0858	5	-0.4088		
25.0	-0.3398	24.0	-0.3687	-0.4152	-0.4385	-0.4850	-0.4734	69.7	-0.1474	6	0.0284		
35.0	-0.3233	33.0	0.3414	-0.4086	-0.4758	-0.5094	-0.4422	76.9	-0.1740	7	0.4846		
50.0	-0.3150	54.0	0.5094	-0.5430	-0.6102	-0.1397	2.7808	83.4	-0.1851	8	-0.4012		
56.0	-0.3150	65.0	-0.6873	-0.8112	-0.8023	-0.8377	-0.7935	89.4	-0.2802	9	-0.1420		
65.0	-0.3067	78.5	-0.8112	-1.9706	-1.7316	-1.4042	-1.4681	95.4	-0.3067	10	0.6358		
76.0	-0.3233	79.5	7.8810	-11.4611	-1.2958	-1.1820	-1.5532	101.1	-0.2536	11	0.3225		
79.0	-0.3067	80.5	-7.6415	-11.1378	-1.3137	-1.1840	-0.2960			12	-0.0328		
80.5	-0.3439	81.3	-7.6476	46.7475	-1.3916	-1.1581	-1.4514	38.2	-0.0412				
81.0	-0.3439	82.0	-7.6297	-12.2153	-1.3616	-1.1840	-1.4155	43.4	-0.0147				
82.0	-0.3379	84.0	-8.1025	-11.5148	-1.3556	-1.1581	-1.3916	50.4	-0.0689				
84.0	-0.3559	87.0	-8.3052	-11.0241	-1.3856	-1.1820	-1.4035	56.1	0.0207				
87.0	-0.3499	89.0	-8.4457	-9.9784	-1.4527	-1.3374	-1.4527	62.5	0.0561				
89.0	-0.3156	92.0	-7.1133	-2.6915	-1.3519	-0.3940	-1.5247	69.7	0.0738				
93.0	-0.3244	96.0	-5.3776	-0.7685	-1.2654	-1.3014	-1.5175	76.9	0.1093				
96.0	-0.3156	100.0	-2.6050	-1.0782	-1.0082	-1.2008	-0.3148	83.4	0.1624				
100.0	-0.3156	96.0	0.4054	0.4830	0.2974	0.2757	0.1389	89.4	0.2068				
96.0	-0.3156	94.0	0.6214	0.6574	0.7006	0.5710	0.4414	95.4	0.0207				
94.0	-0.3156	73.5	0.5328	-0.3078	0.5682	0.5662	0.3881	101.1	-0.4749				
73.0	-0.3244	54.0	0.1964	0.2300	0.2972	0.2972	0.1628						
50.0	-0.3156	33.0	0.0956	0.0956	0.0956	0.1628	0.0620						
35.0	-0.3067	24.0	0.0149	0.0265	0.0963	0.1312	0.0498						
25.0	-0.3067	10.0	0.0814	0.0730	0.1196	0.1428	0.1964						
10.0	-0.3067	5.0	0.0814	0.0847	0.1428	0.2242	0.3309						
5.0	-0.3482	2.5	0.1196	0.1428	0.2939	0.3288	0.3309						
2.5	-0.3398												

TABLE A20. (Concluded)

RUN: SEQ		CLAERO =		PROPLUSIVE		WING / CANARD		PRESSURES		BASEPR =		PAGE	
188 5		PSTAT 0		VEL		YAW H/C		CMJC		HGT RN		451	
ALPHA		2118.83		2089.55		29.27		155.13		87.1025		0.1042	
BETA		CL		CD		CROLL		CN		CLTR		CDTR	
0.0		1.20		0.32		-0.63		0.03		0.91		0.42	
CANARD		BP=3.375		BP=10.125		BP=2		BP=6		BP=12		BP=16	
XX/C		CP		CP		CP		CP		CP		CP	
0.0	-0.3693	-0.3693	0.0	-3.1890	-5.8704	-9.2576	-4.1852	-2.0954	38.2	-0.1125	1	-0.8724	
2.5	-0.3525	-0.3776	2.5	-0.3078	-2.5071	-3.6947	-3.8594	-2.0130	43.4	-0.1125	2	0.3856	
5.0	-0.3525	-0.3609	5.0	-1.2839	-1.7308	-3.2362	-3.7087	-2.0248	50.4	-0.1483	3	-2.3345	
10.0	-0.3609	-0.3776	10.0	-1.0957	-1.3309	-1.9190	-3.7087	-1.9895	58.1	-0.1931	4	0.3176	
15.0	-0.3776	-0.3609	15.0	-0.9899	-1.0722	-1.4720	-3.2362	-1.9190	62.5	-0.2647	5	-1.6544	
20.0	-0.3609	-0.3860	20.0	-0.8135	-0.8958	-1.1428	-1.6349	-1.8601	69.7	-0.3453	6	0.0116	
35.0	-0.3609	-0.3860	35.0	-0.7024	-0.8384	-0.8404	-0.8044	-1.9264	76.9	-0.3453	7	0.3274	
50.0	-0.3776	-0.3776	50.0	-0.7024	-0.7364	-0.8724	0.1138	2.3577	83.4	-0.5094	8	-0.8455	
56.0	-0.3776	-0.3776	56.0	-0.8018	-0.9899	-1.0436	-0.9888	-1.6702	89.4	-0.3811	9	-0.4157	
65.0	-0.3776	-0.3693	65.0	-0.7075	-1.8224	-2.4760	-2.1895	-2.0731	95.4	-0.3542	10	0.7499	
76.0	-0.3776	-0.3776	76.0	-6.0757	-9.3730	-1.4853	-2.0970	-2.6298	101.1	-0.2826	11	-0.0308	
79.0	-0.3525	-0.3776	79.0	-6.6830	-9.2343	-1.4914	-1.7275	-0.3528	---BOTTOM---		12	-0.2991	
80.5	-0.3468	-0.3407	80.5	-6.1362	36.8308	-1.8729	-1.6730	-2.1515	38.2	0.0128			
81.0	-0.3407	-0.3347	81.0	-6.0314	-10.3208	-1.7094	-1.5883	-2.0788	43.4	0.0486			
82.0	-0.3468	-0.3589	82.0	-6.2937	-9.2186	-1.6004	-1.7215	-1.9537	50.4	0.0039			
84.0	-0.3347	-0.3347	84.0	-6.6934	-9.3761	-1.6367	-1.6367	-1.8184	58.1	0.1382			
87.0	-0.3539	-0.3539	87.0	-6.8048	-8.5517	-1.7270	-1.7270	-1.7853	62.5	0.2188			
89.0	-0.3353	-0.3353	89.0	-5.9015	-4.8888	-1.5449	-0.4375	-1.7124	69.7	0.2814			
93.0	-0.3542	-0.3542	93.0	-5.1802	-2.6866	-1.3773	-1.5230	-1.6250	76.9	0.2904			
96.0	-0.3453	-0.3453	96.0	-5.8088	-1.3700	-1.1661	-1.1879	-0.3720	83.4	0.3083			
100.0	-0.3542	-0.3542	100.0	0.4002	0.4877	0.3201	0.3420	0.0724	89.4	0.3262			
96.0	-0.3453	-0.3453	96.0	0.7052	0.8062	0.7062	0.6188	0.3420	95.4	0.1829			
84.0	-0.3542	-0.3542	84.0	0.6236	-0.2624	0.6236	0.6236	0.3516	101.1	-0.2468			
73.0	-0.3453	-0.3453	73.0	0.3516	0.3856	0.3856	0.3516	0.1476					
50.0	-0.3721	-0.3542	50.0	0.3516	0.3516	0.3516	0.3516	0.1816					
35.0	-0.3525	-0.3776	35.0	0.3273	0.3861	0.4214	0.4214	0.2567					
25.0	-0.3609	-0.3609	25.0	0.5155	0.5155	0.5390	0.5507	0.4196					
10.0	-0.3609	-0.3693	10.0	0.6213	0.5978	0.5625	0.5978	0.4876					
5.0	-0.3525	-0.3609	5.0	0.7036	0.5743	0.4096	0.4684	0.3856					
2.5	-0.3776	-0.3893	2.5										

Force Data - Use
Run 222

TABLE A21. RUN 189, BW6V, DELF=48, CMU=1.0, (BN/B)N=0.5

RUN: SEQ										PROPLUSIVE										WING / CANARD										PRESSURES										BASEPR = 8.1916										PAGE 455									
189 1 CLAERO = 0.8210 CDAERO = 0.5816										Q VEL YAW H/C CMUC										DWLC = 0.9058										HGT RN										56.5633 0.723852E+06																			
ALPHA PTOT 2119.11 2105.10 14.01 107.02 0.0 2.65 0.0										CM CROLL CN										CMUT										CLTR CDTR										0.98 0.39																			
BETA CL CD										CROLL CN										CMUT										CLTR CDTR										0.98 0.39																			
0.0 1.53 0.06 -1.08 0.01 0.01 -0.01										CROLL CN										CMUT										CLTR CDTR										0.98 0.39																			
BP=3.375 BP=10.125										BP=2 BP=6 BP=12 BP=16 BP=22										BP=22										BP=22										BP=22																			
X/C CP										X/C CP										X/C CP										X/C CP										X/C CP										X/C CP									
-0.4372 -0.4197 -0.4032 -0.4372 -0.4197 -0.4032 -0.4372 -0.4197 -0.4032 -0.4372										0.0 0.4341 0.3604 -0.0818 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058																			
0.0 0.4372 -0.4032 -0.4197 -0.4032 -0.4197 -0.4032 -0.4197 -0.4032 -0.4197										0.0 0.4341 0.3604 -0.0818 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058																			
0.0 0.4372 -0.4032 -0.4197 -0.4032 -0.4197 -0.4032 -0.4197 -0.4032 -0.4197										0.0 0.4341 0.3604 -0.0818 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058																			
0.0 0.4372 -0.4032 -0.4197 -0.4032 -0.4197 -0.4032 -0.4197 -0.4032 -0.4197										0.0 0.4341 0.3604 -0.0818 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058																			
0.0 0.4372 -0.4032 -0.4197 -0.4032 -0.4197 -0.4032 -0.4197 -0.4032 -0.4197										0.0 0.4341 0.3604 -0.0818 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058																			
0.0 0.4372 -0.4032 -0.4197 -0.4032 -0.4197 -0.4032 -0.4197 -0.4032 -0.4197										0.0 0.4341 0.3604 -0.0818 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058																			
0.0 0.4372 -0.4032 -0.4197 -0.4032 -0.4197 -0.4032 -0.4197 -0.4032 -0.4197										0.0 0.4341 0.3604 -0.0818 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058																			
0.0 0.4372 -0.4032 -0.4197 -0.4032 -0.4197 -0.4032 -0.4197 -0.4032 -0.4197										0.0 0.4341 0.3604 -0.0818 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058 -0.8650 -0.4257 -1.1134 -1.3058										-0.4257 -1.1134 -1.3058 -0.8650 -																			

Force Data - Use
Run 223

Table A21. (Concluded)

Force Data - Use
Run 223

TABLE A22. RUN 190, BW6V, DELF=45, CMU-2.0, (BN/B)W=0.5

RUN: SEQ										PAGE 456																					
190	1	CLAERO =	0.3952	COAERO =	C.8036	DCLC =	0.0	WING / CANARD	PRESSURES	BASEPR =	8.1916	HGT	RM																		
ALPHA	0.05	PTOT	2119.25	PSTAT	0	VEL	77.35	YAW	H/C	CMUJ	86.2393	0.528544E+06	CLTR	COTR																	
BETA	0.0	CL	2.14	CD	-0.20	CM	-1.54	CHOLL	CN	CY	1.09	0.43																			
***** CANARD *****										***** FUSELAGE *****																					
BP=3.375 BP=10.125										NO. CP																					
XX/C	0.0	-0.5630	-0.5630	CP	0.0	0.3982	0.0702	CP	-0.3048	-0.6327	-0.7731	38.2	-0.1697	1	-0.4828																
2.5	-0.5296	-0.5630	-0.5630	CP	2.5	-0.4921	-0.5389	CP	-0.9137	-1.1480	-1.2417	43.4	-0.1341	2	0.1948																
5.0	-0.5296	-0.5630	-0.5630	CP	5.0	-0.3983	-0.4921	CP	-0.7731	-0.8199	-0.9806	50.4	-0.1341	3	-0.9182																
10.0	-0.5296	-0.5630	-0.5630	CP	10.0	-0.3983	-0.5389	CP	-0.6795	-0.7731	-0.9806	56.1	-0.1697	4	0.1948																
15.0	-0.5296	-0.5630	-0.5630	CP	15.0	-0.3983	-0.4921	CP	-0.6327	-0.8199	-0.9806	62.5	-0.1697	5	-0.4828																
20.0	-0.5630	-0.5630	-0.5630	CP	20.0	-0.4452	-0.4921	CP	-0.5857	-0.5389	-0.6327	69.7	-0.2411	6	-0.0764																
25.0	-0.5296	-0.5630	-0.5630	CP	25.0	-0.4928	-0.4928	CP	-0.4828	-0.8182	-0.4828	76.9	-0.2768	7	0.2236																
30.0	-0.5630	-0.5630	-0.5630	CP	30.0	-0.6182	-0.7537	CP	-0.7537	-1.8374	-1.8374	83.4	-0.2768	8	-0.8212																
35.0	-0.5296	-0.5630	-0.5630	CP	35.0	-0.9544	-1.4895	CP	-1.1328	-1.0814	-0.9188	89.4	-0.3837	9	-0.6181																
40.0	-0.5296	-0.5630	-0.5630	CP	40.0	-0.3837	-3.5225	CP	-3.5225	-1.5908	-1.8108	95.4	-0.4850	10	0.7460																
45.0	-0.5630	-0.5630	-0.5630	CP	45.0	-24.2531	-38.0062	CP	-5.0728	-1.3572	-2.1052	101.1	-0.4194	11	0.1858																
50.0	-0.5296	-0.5630	-0.5630	CP	50.0	-22.4196	-37.3542	CP	-3.7940	-1.2807	-0.5609																				
55.0	-0.4888	-0.5630	-0.5630	CP	55.0	-23.0947	-39.4912	CP	-3.1725	-1.3087	-2.0087	38.2	-0.0628	12	-0.2408																
60.0	-0.5127	-0.5630	-0.5630	CP	60.0	-23.0716	-38.9467	CP	-2.9254	-1.3572	-1.7914	43.4	-0.0628																		
65.0	-0.5609	-0.5630	-0.5630	CP	65.0	-24.8560	-37.6917	CP	-2.4670	-1.2848	-1.6708	50.4	-0.1341																		
70.0	-0.4644	-0.5630	-0.5630	CP	70.0	-25.7013	-35.2552	CP	-1.4537	-1.4054	-1.5984	56.1	-0.0271																		
75.0	-0.5368	-0.5630	-0.5630	CP	75.0	-26.0430	-31.0343	CP	-1.3727	-1.4597	-1.8881	62.5	0.0442																		
80.0	-0.4907	-0.5630	-0.5630	CP	80.0	-23.0825	-8.5705	CP	-1.1985	-0.5600	-1.8951	69.7	0.0442																		
85.0	-0.5265	-0.5630	-0.5630	CP	85.0	-17.2486	-0.9083	CP	-1.0824	-1.4307	-1.7790	76.9	0.0442																		
90.0	-0.5265	-0.5630	-0.5630	CP	90.0	-9.0929	-2.8238	CP	-0.9954	-1.3436	-0.5020	83.4	0.0799																		
95.0	-0.4907	-0.5630	-0.5630	CP	95.0	0.2527	0.3687	CP	0.2336	0.2336	0.0495	89.4	0.0799																		
100.0	-0.5265	-0.5630	-0.5630	CP	100.0	0.5139	0.6009	CP	0.6380	0.5719	0.4268	95.4	-0.2768																		
105.0	-0.5265	-0.5630	-0.5630	CP	105.0	0.6009	-0.4828	CP	0.6009	0.6009	0.4854	101.1	-0.8118																		
110.0	-0.4907	-0.5630	-0.5630	CP	110.0	0.3700	0.1945	CP	0.3300	0.3300	0.1945																				
115.0	-0.4907	-0.5630	-0.5630	CP	115.0	0.0591	0.0591	CP	0.1945	0.1945	0.0591																				
120.0	-0.5630	-0.5630	-0.5630	CP	120.0	0.0234	0.0702	CP	0.0234	0.1170	-0.0235																				
125.0	-0.5296	-0.5630	-0.5630	CP	125.0	0.1170	0.0224	CP	0.1170	0.2108	0.1945																				
130.0	-0.5630	-0.5630	-0.5630	CP	130.0	0.0702	0.0702	CP	0.2108	0.3045	0.3300																				
135.0	-0.5296	-0.5630	-0.5630	CP	135.0	2.5	0.1170	CP	0.2576	0.3513	0.3300																				
140.0	-0.5630	-0.5630	-0.5630	CP	140.0	2.5	0.1170	CP	0.2576	0.3513	0.3300																				

Force Data - Use
Run 223

Force Data - Use
Run 223

TABLE A22. (Continued)

PROPELLSIVE WING / CANARD PRESSURES										PAGE 458	
BASEPR = 8.1916										BASEPR = 8.1916	
HMT										HMT	
88.0241 0.529777E+08										88.0241 0.529777E+08	
CLTR										CLTR	
1.25 0.50										1.25 0.50	
COTR										COTR	
0.0										0.0	
2.33										2.33	
0.06										0.06	
-1.57										-1.57	
0.02										0.02	
0.01										0.01	
-0.03										-0.03	
1.25										1.25	
-0.74										-0.74	
COTR										COTR	
1.25										1.25	
0.50										0.50	
0.0										0.0	
2.33										2.33	
0.06										0.06	
-1.57										-1.57	
0.02										0.02	
0.01										0.01	
-0.03										-0.03	
1.25										1.25	
-0.74										-0.74	
COTR										COTR	
1.25										1.25	
0.50										0.50	
0.0										0.0	
2.33										2.33	
0.06										0.06	
-1.57										-1.57	
0.02										0.02	
0.01										0.01	
-0.03										-0.03	
1.25										1.25	
-0.74										-0.74	
COTR										COTR	
1.25										1.25	
0.50										0.50	
0.0										0.0	
2.33										2.33	
0.06										0.06	
-1.57										-1.57	
0.02										0.02	
0.01										0.01	
-0.03										-0.03	
1.25										1.25	
-0.74										-0.74	
COTR										COTR	
1.25										1.25	
0.50										0.50	
0.0										0.0	
2.33										2.33	
0.06										0.06	
-1.57										-1.57	
0.02										0.02	
0.01										0.01	
-0.03										-0.03	
1.25										1.25	
-0.74										-0.74	
COTR										COTR	
1.25										1.25	
0.50										0.50	
0.0										0.0	
2.33										2.33	
0.06										0.06	
-1.57										-1.57	
0.02										0.02	
0.01										0.01	
-0.03										-0.03	
1.25										1.25	
-0.74										-0.74	
COTR										COTR	
1.25										1.25	
0.50										0.50	
0.0										0.0	
2.33										2.33	
0.06										0.06	
-1.57										-1.57	
0.02										0.02	
0.01										0.01	
-0.03										-0.03	
1.25										1.25	
-0.74										-0.74	
COTR										COTR	
1.25										1.25	
0.50										0.50	
0.0										0.0	
2.33										2.33	
0.06										0.06	
-1.57										-1.57	
0.02										0.02	
0.01										0.01	
-0.03										-0.03	

TABLE A22. (Concluded)

RUN: SEQ		PROPLUSIVE				WING / CANARD		PRESSURES		PAGE	
190	5	CLAERO =	0.8367	CD AERO =	0.9784	DCLC =	0.0	CMJC	CMUW	CMUT	BASEPR = 9.1916
	ALPHA	PTOT	PSTAT	Q	VEL	YAW	H/C				HJT RN
12.02		2119.40	2112.16	7.23	76.73	0.0	2.68	0.0	2.065	2.065	87.5690 0.521881E+06
	BETA	CL	CD	CM	CRULL	CN		CY	CNTR	CLTR	CDTR
0.0		2.80	0.34	-1.68	0.04	0.00		-0.05	-0.82	1.62	0.75

CANARD				WING				FUSELAGE				MISC.			
BP=3.375		BP=10.125		BP=6		BP=12		BP=16		EP=22		TOP		BOT	
%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP
0.0	-0.5655	-0.5994	0.0	-3.2869	-6.3797	-3.9055	-2.2403	-1.7645	38.2	-0.2001	1	-0.9308			
2.5	-0.5994	-0.5955	2.5	-0.4798	-2.7636	-3.6676	-2.2879	-1.7168	43.4	-0.1638	2	0.3074			
5.0	-0.5655	-0.5955	5.0	-1.3838	-2.0024	-3.5260	-2.0975	-1.7168	50.4	-0.2001	3	-1.8936			
10.0	-0.5655	-0.5994	10.0	-1.1459	-1.4314	-3.0491	-2.1460	-1.6217	56.1	-0.2363	4	0.3074			
15.0	-0.5315	-0.5655	15.0	-0.6334	-1.2411	-2.6208	-2.3830	-1.7645	62.5	-0.2449	5	-1.4809			
20.0	-0.5655	-0.5994	20.0	-0.9080	-1.0607	-1.3838	-2.1450	-1.6693	68.7	-0.4836	6	0.0322			
25.0	-0.5655	-0.5994	25.0	-0.7930	-1.0683	-0.9308	-2.1687	-1.6184	75.9	-0.4173	7	0.1110			
30.0	-0.5994	-0.5994	30.0	-0.9308	-0.9308	-1.0683	-1.2058	-1.4977	83.4	-0.4173	8	-0.0890			
35.0	-0.5655	-0.5994	35.0	-1.2142	-1.9387	-1.4677	-1.1418	-1.4315	89.4	-0.4536	9	-0.8616			
40.0	-0.5655	-0.5994	40.0	11.7889	-2.5323	-5.1261	-1.8663	-1.2866	95.4	-0.4173	10	0.7005			
45.0	-0.5655	-0.5994	45.0	25.0248	-37.9617	-5.8897	-2.0426	-1.3324	101.1	-0.3812	11	0.1405			
50.0	-0.5655	-0.5994	50.0	23.3841	-36.4426	-4.2670	-1.6999	-0.5484			12	-0.4784			
55.0	-0.5655	-0.5994	55.0	23.5058	122.7427	-3.5620	-1.5526	-1.3813	38.2	0.0173					
60.0	-0.5239	-0.5239	60.0	23.8261	-37.7903	-3.8028	-1.5036	-1.3324	43.4	0.0636					
65.0	-0.5239	-0.5239	65.0	24.9033	-37.1530	-3.7289	-1.2833	-1.3079	50.4	-0.0914					
70.0	-0.5484	-0.5484	70.0	25.5087	-34.4341	-1.9204	-1.2833	-1.2833	56.1	0.0897					
75.0	-0.5484	-0.5484	75.0	26.7693	-30.1891	-1.9817	-1.3921	-1.3038	62.5	0.1984					
80.0	-0.5622	-0.5622	80.0	24.0677	-8.4964	-1.3627	-0.6554	-1.3627	68.7	0.2708					
85.0	-0.5622	-0.5622	85.0	18.9884	-1.8932	-1.2448	-1.3038	-1.3038	75.9	0.2708					
90.0	-0.5622	-0.5622	90.0	9.7628	-3.1605	-1.0680	-1.2448	-0.5963	83.4	0.2346					
95.0	-0.5622	-0.5622	95.0	0.4352	0.4647	0.2584	0.2289	0.0226	89.4	0.1984					
100.0	-0.5622	-0.5622	100.0	0.6710	0.8184	0.7594	0.6710	0.4352	95.4	-0.1638					
0.0	-0.5985	-0.5985	0.0	0.6710	0.8184	0.7594	0.6710	0.4352	101.1	-0.8158					
2.5	-0.5985	-0.5985	2.5	0.5925	-0.5180	0.5825	0.7201	0.4450							
5.0	-0.5985	-0.5985	5.0	0.3074	0.3074	0.3074	0.3074	0.1698							
7.5	-0.5985	-0.5985	7.5	0.3074	0.3074	0.3074	0.3074	0.1698							
10.0	-0.5985	-0.5985	10.0	0.3767	0.4243	0.3767	0								

Force Data - Use
Run 223

A-275

[illegible]

TABLE A23. (Concluded)

RUN:SEQ										PAGE 495													
216	7	CLARO =	1.2267	CDARO =	0.4785	DCLC =	0.0	WING / CANARD	PRESSURES														
ALPHA	11.99	PTOT	2146.20	VEL	20.23	YAW	128.57	H/C	CMJC	CMW	CMUT												
BETA	0.0	CL	1.23	CD	0.48	CROLL	0.00	CM	CV	CNTR	1.21	CNTR	CNTR										
														BASEPR = 8.1924									
														HGT IN									
														87.6630 0.882648E+06									
														CLTR CDTR									
														1.13 0.48									
														..MISC..									
														NO. CP									
														1 - 0.5757									
														2 0.2606									
														3 - 1.0184									
														4 0.2606									
														5 - 1.3828									
														6 0.0839									
														7 0.1342									
														8 - 0.6142									
														9 0.4083									
														10 - 0.0766									
														11 - 0.8461									
														12 - 0.3718									
														..FPU..									
														XLOC CP									
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TABLE A24. RUN 217, BC1W6V, DELF=45, CMU=1.0, (BN/B)V=0.5

RUN: SEQ										PAGE 488									
217	1	CLAERO =	0.5873	CD AERO =	0.7072	DEL C =	0.5351	DEL C =	0.5015	BASEPR =	8.1924								
		PLOT	0	VEL	W/V	H/C	CMU	CMU	CMU	HGT	IN								
		2146.70	2138.78	7.91	80.19	0.0	2.65	0.683	1.041	88.8000	0.541223E+08								
		BETA	0.0	CD	CROLL	CM	CV	CNTR	CNTR	CLTR	COTR								
		2.02	-0.19	-0.44	-0.01	0.01	0.08	0.93	-0.10	0.93	0.46								
***** CANARD *****										***** FUSELAGE *****									
BP=3.375		BP=10.125		BP = 2		BP = 6		BP = 12		BP = 16		BP = 22		***** TOP *****		***** BOTTOM *****		***** NTSC *****	
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	KLDC	CP	KLDC	CP	MD.	CP
0.0	0.1920	-1.2969	0.0	-0.8290	-0.8290	-0.8290	-0.8290	-0.8290	-0.8290	-0.8290	-0.8290	-0.8290	-0.8290	38.2	-0.4888	38.2	-0.4888	1	-0.2594
2.5	-0.7898	-2.0416	2.5	-0.3938	0.9116	0.9116	0.9116	0.9116	0.9116	0.9116	0.9116	0.9116	0.9116	43.4	-0.4888	43.4	-0.4888	2	-0.7625
5.0	-0.6766	-1.1109	5.0	0.7375	0.7375	0.7375	0.7375	0.7375	0.7375	0.7375	0.7375	0.7375	0.7375	50.4	-0.3929	50.4	-0.3929	3	-0.6367
10.0	-0.2113	-1.0799	10.0	-0.3503	0.3459	0.3459	0.3459	0.3459	0.3459	0.3459	0.3459	0.3459	0.3459	58.1	-0.0942	58.1	-0.0942	4	-0.1336
15.0	-0.7386	-1.0178	15.0	-0.3894	0.2153	0.2153	0.2153	0.2153	0.2153	0.2153	0.2153	0.2153	0.2153	62.5	-0.0811	62.5	-0.0811	5	-0.9110
20.0	-0.6456	-0.8937	20.0	0.0848	-0.0457	-0.0457	-0.0457	-0.0457	-0.0457	-0.0457	-0.0457	-0.0457	-0.0457	69.7	-0.0942	69.7	-0.0942	6	-0.1336
35.0	-0.7076	-0.8937	35.0	-0.0078	-0.2594	-0.2594	-0.2594	-0.2594	-0.2594	-0.2594	-0.2594	-0.2594	-0.2594	76.9	-0.1608	76.9	-0.1608	7	0.2708
50.0	-0.8937	-0.8937	50.0	-0.5110	-0.6367	-0.6367	-0.6367	-0.6367	-0.6367	-0.6367	-0.6367	-0.6367	-0.6367	83.4	-0.1936	83.4	-0.1936	8	-0.7285
65.0	-1.0485	-1.0485	65.0	-0.8890	-1.2865	-1.2865	-1.2865	-1.2865	-1.2865	-1.2865	-1.2865	-1.2865	-1.2865	89.4	-0.2594	89.4	-0.2594	9	-0.4300
76.0	-1.4831	-1.4831	76.0	-0.3923	-4.6311	-4.6311	-4.6311	-4.6311	-4.6311	-4.6311	-4.6311	-4.6311	-4.6311	96.4	-0.3923	96.4	-0.3923	10	0.8388
79.0	-8.6637	-7.8426	79.0	-0.4284	78.5	78.5	78.5	78.5	78.5	78.5	78.5	78.5	78.5	101.1	-0.2923	101.1	-0.2923	11	0.1830
80.5	-13.3559	-15.8238	80.5	-0.6637	80.5	80.5	80.5	80.5	80.5	80.5	80.5	80.5	80.5	---	---	---	---	12	-0.1604
81.0	-7.8916	-15.8238	81.0	-0.8937	81.0	81.0	81.0	81.0	81.0	81.0	81.0	81.0	81.0	---	---	---	---		
82.0	-5.6971	-9.5711	82.0	-0.8937	82.0	82.0	82.0	82.0	82.0	82.0	82.0	82.0	82.0	---	---	---	---		
84.0	-1.2403	-8.5711	84.0	-0.8167	-1.1064	-1.1064	-1.1064	-1.1064	-1.1064	-1.1064	-1.1064	-1.1064	-1.1064	38.2	0.1378	38.2	0.1378		
87.0	-1.5543	-8.5711	87.0	-0.5690	-2.5844	-2.5844	-2.5844	-2.5844	-2.5844	-2.5844	-2.5844	-2.5844	-2.5844	43.4	0.1707	43.4	0.1707		
89.0	-2.1474	-3.4390	89.0	-0.2742	-4.5928	-4.5928	-4.5928	-4.5928	-4.5928	-4.5928	-4.5928	-4.5928	-4.5928	50.4	0.0081	50.4	0.0081		
93.0	-1.0877	-3.4390	93.0	-0.8074	-2.5133	-2.5133	-2.5133	-2.5133	-2.5133	-2.5133	-2.5133	-2.5133	-2.5133	56.1	-0.1936	56.1	-0.1936		
96.0	-0.0811	0.7005	96.0	-0.0230	-1.0759	-1.0759	-1.0759	-1.0759	-1.0759	-1.0759	-1.0759	-1.0759	-1.0759	62.5	-0.5910	62.5	-0.5910		
100.0	1.2304	-1.0846	100.0	-1.2387	-1.0230	-1.0230	-1.0230	-1.0230	-1.0230	-1.0230	-1.0230	-1.0230	-1.0230	69.7	-0.8903	69.7	-0.8903		
96.0	0.5880	-1.0846	96.0	0.0852	0.0282	0.0282	0.0282	0.0282	0.0282	0.0282	0.0282	0.0282	0.0282	76.9	-0.5910	76.9	-0.5910		
84.0	1.2304	-1.0846	84.0	-0.0552	-0.0526	-0.0526	-0.0526	-0.0526	-0.0526	-0.0526	-0.0526	-0.0526	-0.0526	83.4	-0.4284	83.4	-0.4284		
73.0	0.5880	0.5018	73.0	-0.1336	-0.3852	-0.3852	-0.3852	-0.3852	-0.3852	-0.3852	-0.3852	-0.3852	-0.3852	89.4	-0.1936	89.4	-0.1936		
50.0	0.7658	0.6674	50.0	-0.5110	-0.5110	-0.5110	-0.5110	-0.5110	-0.5110	-0.5110	-0.5110	-0.5110	-0.5110	95.4	-0.1274	95.4	-0.1274		
35.0	0.6864	0.5953	35.0	-0.7625	-0.3852	-0.3852	-0.3852	-0.3852	-0.3852	-0.3852	-0.3852	-0.3852	-0.3852	101.1	-0.4888	101.1	-0.4888		
10.0	0.2541	-1.4211	10.0	-0.6884	-0.7854	-0.7854	-0.7854	-0.7854	-0.7854	-0.7854	-0.7854	-0.7854	-0.7854	---	---	---	---		
5.0	0.2230	0.1920	5.0	-0.6113	-0.6984	-0.6984	-0.6984	-0.6984	-0.6984	-0.6984	-0.6984	-0.6984	-0.6984	---	---	---	---		
2.5	0.0369	0.1300	2.5	-0.6549	-0.6984	-0.6984	-0.6984	-0.6984	-0.6984	-0.6984	-0.6984	-0.6984	-0.6984	---	---	---	---		
	0.0890	0.4091		-0.6984	-0.7854	-0.7854	-0.7854	-0.7854	-0.7854	-0.7854	-0.7854	-0.7854	-0.7854	---	---	---	---		

TABLE A24. (Continued)

RUN:SEQ		CLAERO = 0.6140		PROPULSIVE		WING / CANARD		PRESSURES		BASEPR = 8.1934		PAGE 500	
217	4	PTOT	PSTAT	Q	VEL	YAW	H/C	CMAC	CMUW	HGT	MD	CP	
4.08	BETA	2146.84	2128.93	7.91	80.16	0.0	3.87	0.634	1.032	87.4453	0.841983E+06	CLTR	CDTR
0.0		CL	CD	CM	CROLL	CN		CV	CNTR	CLTR	CDTR		
		2.08	-0.10	-0.28	0.02	0.00	0.03	0.97	0.09	0.94	0.47		
***** CANARD *****													
BP=3.375		BP=10.125		CP	CP	XX/C	BP = 2	BP = 8	BP = 12	BP = 16	BP = 22	***** FUSELAGE *****	
0.0	0.0	-3.7783	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2.8	2.8	-3.2504	2.8	0.3087	0.6983	-0.9188	-0.8548	-2.0470	36.2	-0.4918	36.2	-0.4918	1 - 0.3831
5.0	5.0	-3.2504	5.0	0.6939	0.9504	-0.9188	-0.7418	-1.9598	43.4	-0.4884	43.4	-0.4884	2 - 0.8843
10.0	10.0	-2.4112	10.0	0.3502	0.3459	-0.8288	-0.6983	-1.2928	50.4	-0.2898	50.4	-0.2898	3 - 0.8813
18.0	18.0	-1.8139	18.0	0.3024	0.1718	-0.7418	-0.6983	-0.9188	56.1	-0.0942	56.1	-0.0942	4 - 0.2593
26.0	26.0	-1.0486	24.0	0.0022	-0.1327	-0.7418	-0.6983	-0.8288	62.6	-0.0811	62.6	-0.0811	5 - 0.6366
38.0	38.0	-1.0787	32.0	0.1335	-0.2893	-0.8288	-0.8288	-0.8288	68.7	-0.0811	68.7	-0.0811	6 - 0.2593
50.0	50.0	-1.0486	54.0	0.0109	-0.8109	-0.9882	-1.2300	-0.9882	76.9	-0.1273	76.9	-0.1273	7 - 0.3247
65.0	65.0	-1.1759	78.8	-0.1604	-4.6636	-0.9882	-1.2300	-0.9882	89.4	-0.1604	89.4	-0.1604	8 - 0.6985
76.0	76.0	-4.5846	78.8	0.1144	-115.4320	-3.4385	-1.8159	-1.8159	95.4	-0.3268	95.4	-0.3268	9 - 0.4838
84.80	84.80	-6.0687	80.8	88.7848	-41.6552	4.0817	-1.2406	-1.2406	101.1	-0.3268	101.1	-0.3268	10 - 0.7290
13.4882	13.4882	-28.6687	81.3	21.0103	142.4148	-0.7258	-2.9871	-2.9871	101.1	-0.3268	101.1	-0.3268	11 - 0.2978
81.0	81.0	-15.9288	82.0	-6.8303	142.4148	-0.7258	-2.9871	-2.9871	101.1	-0.3268	101.1	-0.3268	12 - 0.1604
32.0	32.0	-9.8610	84.0	-0.1421	-5.9690	-2.4048	-1.3077	-1.3077	38.2	0.1707	38.2	0.1707	
84.0	84.0	-1.3501	87.0	-0.8152	-4.8902	-1.9571	-1.3077	-1.3077	43.4	0.2368	43.4	0.2368	
37.0	37.0	-1.8959	89.0	-2.2086	-2.7746	-1.6427	-1.3077	-1.3077	50.4	0.0714	50.4	0.0714	
39.0	39.0	-3.7033	93.0	-0.9151	-1.1578	-1.1036	-1.3077	-1.3077	54.1	-0.1273	54.1	-0.1273	
33.0	33.0	-1.1207	96.0	-0.1216	-1.0787	-0.8841	-1.3077	-1.3077	58.8	-0.4818	58.8	-0.4818	
86.0	86.0	-0.0611	100.0	-1.0787	-1.1307	-0.8841	-1.3077	-1.3077	69.7	-0.6971	69.7	-0.6971	
30.0	30.0	-0.7998	96.0	-0.0795	-0.1085	-0.1085	-1.3077	-1.3077	76.9	-0.6240	76.9	-0.6240	
30.0	30.0	-1.0876	84.0	0.0283	-0.1085	0.3518	-0.8088	0.7020	95.4	-0.1604	95.4	-0.1604	
0.6011	0.4687	-1.0876	73.5	0.1338	-0.3851	-0.0077	0.4954	0.4954	101.1	-0.5248	101.1	-0.5248	
1.7269	0.4687	73.5	0.1338	-0.3851	-0.0077	0.4954	0.4954	0.4954	101.1	-0.5248	101.1	-0.5248	
4.0	0.7005	33.0	-0.7624	-0.6366	-0.5109	-0.8883	-0.8366	-0.1335					
0.8329	0.5953	24.0	-0.6548	-0.6983	-0.7418	-0.8883	-0.8366	-0.1335					
0.7193	0.5953	10.0	-0.6112	-0.7418	-0.7852	-0.8883	-0.8366	-0.1335					
0.2230	0.3161	5.0	-0.5677	-0.7418	-0.7852	-0.8883	-0.8366	-0.1335					
0.1920	0.4402	2.5	-0.6548	-0.6548	-0.7418	-0.8883	-0.8366	-0.1335					
2.5	0.5332	0.5332											

TABLE A24. (Concluded)

RUN: SEQ		CLARO =		PROPULSIVE		WING / CANARD		PRESSURES		BASEPR = 8.1924		PAGE 503	
217 6		PTOT		Q		YAW		CMUN		HGT		RN	
ALPHA		2139.12		7.57		78.41		0.02		87.1714		0.530347E+06	
BETA		CL		CD		CROLL		CN		CLTR		CDTR	
0.0		2.89		0.42		0.02		-0.01		1.83		0.85	
BP-3.375		BP-10.125		BP = 2		BP = 6		BP = 12		BP = 16		BP = 22	
XX/C		CP		XX/C		CP		CP		CP		CP	
0.0	-7.5192	-3.4361	0.0	-0.6782	-0.4965	-1.5419	-1.5873	-4.9055	38.2	-0.6916	1	-0.9677	
2.5	-8.0052	-3.6953	2.5	-0.4965	0.3672	-1.3601	-1.3147	-3.6781	43.4	-0.6916	2	-0.5734	
5.0	-3.4361	-3.5981	5.0	0.5944	0.2782	-1.4509	-1.1783	-3.1328	50.4	-0.3902	3	-0.9677	
10.0	-0.3251	-3.8573	10.0	-0.4965	0.0035	-1.6328	-1.1329	-1.8600	55.1	-0.2785	4	0.0837	
15.0	-1.6861	-4.0842	15.0	0.0944	-0.1783	-1.5873	-1.0873	-1.2237	62.5	-0.1381	5	-1.0990	
20.0	-1.3946	-4.6999	20.0	-0.0874	-0.3601	-1.5419	-1.1329	-0.9964	69.7	-0.1727	6	0.0837	
25.0	-1.2649	-3.8573	25.0	-0.3106	-0.4420	-1.4932	-1.3618	-0.9677	76.9	-0.2418	7	-0.2072	
30.0	-1.3621		30.0	-0.5734	-0.7047	-1.3618	-1.3978	-0.9677	83.4	-0.2785	8	-1.7277	
35.0	-1.4918	-1.8566	35.0	-1.0029	-1.4872	-1.6256	-1.6948	-1.2451	89.4	-0.3456	9	-1.6151	
40.0	-1.9454	-1.6214	40.0	-0.4148	-4.4622	-4.0471	-3.0785	-1.7840	95.4	-0.4148	10	0.5812	
45.0	-1.5843	-4.5054	45.0	-0.5843	-51.0683	-6.9499	-2.9733	-0.5170	101.1	-0.3110	11	0.0743	
50.0	-0.5843	-8.6858	50.0	-0.5843	-51.0683	-6.9499	-2.9733	-0.5170	101.1	-0.3110	12	-0.7423	
55.0	-7.6812	-31.6987	55.0	-0.3015	139.2278	-3.8621	-2.3182	-1.6164	38.2	0.2425			
60.0	-14.6464	-17.9673	60.0	-0.1495	0.5590	-3.4879	-2.3182	-1.6164	43.4	0.2770			
65.0	-8.8915	-11.5349	65.0	-0.2363	-5.9207	-2.8094	-1.8971	-1.7334	50.4	0.1041			
70.0	-6.6926		70.0	-0.0784	-5.8973	-2.2247	-1.8866	-1.7802	56.1	0.0003			
75.0	-1.5930		75.0	-0.1078	-3.3608	-2.0092	-1.7840	-1.8403	62.5	-0.3456			
80.0	-2.0843	-4.6428	80.0	-0.1462	-1.4462	-1.4179	-0.3577	-1.8122	69.7	-0.5186			
85.0	-2.6288		85.0	-0.1671	-1.5306	-1.1083	-1.3336	-0.5732	76.9	-0.4148			
90.0	-1.4872		90.0	-0.8830	-1.3053	-0.7140	-0.9674	-0.5732	83.4	-0.2073			
95.0	-0.3110	0.8997	95.0	0.3278	0.1583	0.2151	0.4122	0.2714	89.4	0.0895			
100.0	2.1797	-1.1759	100.0	0.1870	0.2433	0.2714	0.6938	0.7220	95.4	-0.0343			
105.0	0.6576	0.4134	105.0	0.0837	-0.5734	0.3465	0.4779	0.7407	101.1	-0.5878			
110.0	0.6576	-1.1759	110.0	-0.3105	-0.5734	-0.1791	0.6337	0.2151					
115.0	0.8305	0.4154	115.0	-0.5734	-0.4420	-0.3105	-0.3105	0.0837					
120.0	0.8305	0.6576	120.0	-0.5734	-0.4420	-0.5734	-0.3105	0.1399					
125.0	0.8091	0.5174	125.0	-0.5874	-0.6328	-0.6328	-0.1783	0.3485					
130.0	0.3878	-1.9130	130.0	-0.4965	-0.5419	-0.8600	-0.3601	0.4779					
135.0	0.4526	0.3230	135.0	-0.4965	-0.5419	-0.8600	-0.3601	0.4779					
140.0	0.3878	0.4202	140.0	-0.5419	-0.5419	-0.8600	-0.3601	0.4779					
145.0	0.5498	0.2258	145.0	-0.5419	-0.5419	-0.8600	-0.3601	0.4779					

TABLE A25. RUN 218, BC1W8V, DELF=45, CMU-2.0. (BM/S)W=0.5

CANARD										WING										FUSELAGE										MISC.									
BP=3.375 BP=10.125										BP=2 BP=6 BP=12 BP=16 BP=22										TOP										BOTTOM									
XX/C										XX/C										XX/C										XX/C									
CP										CP										CP										CP									
-0.1384										-0.1384										-0.1384										-0.1384									
-0.9829										-0.9829										-0.9829										-0.9829									
-1.6463										-1.6463										-1.6463										-1.6463									
-0.2891										-0.2891										-0.2891										-0.2891									
-0.9622										-0.9622										-0.9622										-0.9622									
-0.9019										-0.9019										-0.9019										-0.9019									
-0.8822										-0.8822										-0.8822										-0.8822									
-1.1038										-1.1038										-1.1038										-1.1038									
-1.2848										-1.2848										-1.2848										-1.2848									
-1.8275										-1.8275										-1.8275										-1.8275									
-0.4400										-0.4400										-0.4400										-0.4400									
-5.6860										-5.6860										-5.6860										-5.6860									
-10.3328										-10.3328										-10.3328										-10.3328									
-47.1900										-47.1900										-47.1900										-47.1900									
-25.7275										-25.7275										-25.7275										-25.7275									
-14.8860										-14.8860										-14.8860										-14.8860									
-1.8661										-1.8661										-1.8661										-1.8661									
-1.5613										-1.5613										-1.5613										-1.5613									
-2.9203										-2.9203										-2.9203										-2.9203									
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TABLE A25. (Continued)

RUM:SEQ		CLAERO =		PROPLUISIVE		WING / CANARD		PRESSURES		BASEPR = 8.1924		PAGE 507	
218	3	PTOT	PSTAT	Q	VEL	YAW	H/C	CMAC	CMUT	HGT	RM		
ALPHA	4.08	2147.33	2143.38	3.96	58.62	0.0	2.66	1.257	3.325	87.0961	0.383628E+08		
BETA	0.0	CL	CD	CM	CROLL	CN	CY	CNTR	CMTR	CLTR	CDTR		
		3.41	-0.63	-0.66	-0.02	0.02	0.03	1.16	0.03	1.12	0.52		
BP=3.375 BP=10.125		CANARD		BP = 2		BP = 6		BP = 12		BP = 16		BP = 22	
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP
0.0	-2.4881	-3.7908	0.0	-1.0154	-0.8414	-1.0154	-0.8414	-1.0154	-0.8414	-1.0154	-0.8414	-1.0154	-0.8414
2.5	-2.0538	-3.2948	2.5	-0.4064	0.9859	0.0287	-0.8804	0.0287	-0.8804	0.0287	-0.8804	0.0287	-0.8804
5.0	-1.4335	-3.7287	5.0	0.8988	0.8988	0.1453	-0.4934	0.1453	-0.4934	0.1453	-0.4934	0.1453	-0.4934
10.0	-0.3189	-3.1705	10.0	-0.3194	0.5508	-0.1453	-0.4934	-0.1453	-0.4934	-0.1453	-0.4934	-0.1453	-0.4934
15.0	-1.1854	-2.9223	15.0	0.5508	0.2897	-0.2323	-0.4934	-0.2323	-0.4934	-0.2323	-0.4934	-0.2323	-0.4934
20.0	-0.9992	-1.3718	20.0	0.2027	-0.0683	-0.4934	-0.4934	-0.4934	-0.4934	-0.4934	-0.4934	-0.4934	-0.4934
25.0	-0.9992	-1.3718	25.0	0.2027	-0.0683	-0.4934	-0.4934	-0.4934	-0.4934	-0.4934	-0.4934	-0.4934	-0.4934
30.0	-1.0813	-1.3094	30.0	0.5235	-0.5235	-1.0266	-1.0266	-1.0266	-1.0266	-1.0266	-1.0266	-1.0266	-1.0266
35.0	-1.3094	-1.7436	35.0	-0.7780	-1.0266	-1.0266	-1.0266	-1.0266	-1.0266	-1.0266	-1.0266	-1.0266	-1.0266
40.0	-1.4335	-2.5802	40.0	-1.0008	-1.7955	-1.1332	-1.1332	-1.1332	-1.1332	-1.1332	-1.1332	-1.1332	-1.1332
45.0	-1.9297	-5.7759	45.0	1.6480	-6.6930	-3.9809	-1.6630	-3.9809	-1.6630	-3.9809	-1.6630	-3.9809	-1.6630
50.0	-0.5030	-10.4906	50.0	228.7833	-6.0446	-1.3875	-2.0144	-1.3875	-2.0144	-1.3875	-2.0144	-1.3875	-2.0144
55.0	-8.8165	-48.6767	55.0	281.0090	-3.4026	-1.4323	-1.7009	-1.4323	-1.7009	-1.4323	-1.7009	-1.4323	-1.7009
60.0	-21.8523	-26.0180	60.0	-0.1337	-0.0441	-3.2236	-1.3875	-3.2236	-1.3875	-3.2236	-1.3875	-3.2236	-1.3875
65.0	-12.5379	-14.8664	65.0	-3.7610	-10.2988	-2.7310	-1.4323	-2.7310	-1.4323	-2.7310	-1.4323	-2.7310	-1.4323
70.0	-8.7763	-1.6114	70.0	-0.2232	-8.1942	-1.8354	-1.4771	-1.8354	-1.4771	-1.8354	-1.4771	-1.8354	-1.4771
75.0	-1.3875	-4.8416	75.0	-3.3801	-4.3502	-1.6013	-1.7092	-1.6013	-1.7092	-1.6013	-1.7092	-1.6013	-1.7092
80.0	-2.8551	0.7872	80.0	-1.0624	-1.4397	-1.3319	-0.5772	-1.3319	-0.5772	-1.3319	-0.5772	-1.3319	-0.5772
85.0	-1.1332	-2.2590	85.0	-1.6554	-2.5717	-1.1163	-1.4397	-1.1163	-1.4397	-1.1163	-1.4397	-1.1163	-1.4397
90.0	0.5885	-2.3590	90.0	-2.4638	-0.4655	-0.1461	0.3390	-0.1461	0.3390	-0.1461	0.3390	-0.1461	0.3390
95.0	7.0782	-2.3590	95.0	-0.4095	-0.4156	0.1234	0.8242	0.1234	0.8242	0.1234	0.8242	0.1234	0.8242
100.0	0.3898	0.3898	100.0	-0.7750	-0.5235	-0.5235	0.2312	-0.5235	0.2312	-0.5235	0.2312	-0.5235	0.2312
105.0	0.6547	0.7209	105.0	-1.2781	-1.2781	-1.2781	-0.7750	-1.2781	-0.7750	-1.2781	-0.7750	-1.2781	-0.7750
110.0	0.7376	0.4895	110.0	-0.7544	-1.0154	-0.9284	-0.6674	-0.9284	-0.6674	-0.9284	-0.6674	-0.9284	-0.6674
115.0	0.1794	-1.8877	115.0	-0.7544	-0.9284	-0.9284	-0.5804	-0.9284	-0.5804	-0.9284	-0.5804	-0.9284	-0.5804
120.0	0.3034	0.0654	120.0	-0.6874	-0.8414	-0.8414	-0.7544	-0.8414	-0.7544	-0.8414	-0.7544	-0.8414	-0.7544
125.0	0.1174	0.1174	125.0	-0.7544	-0.8414	-0.8414	-0.7544	-0.8414	-0.7544	-0.8414	-0.7544	-0.8414	-0.7544
130.0	0.3655	0.3655	130.0	-0.7544	-0.8414	-0.8414	-0.7544	-0.8414	-0.7544	-0.8414	-0.7544	-0.8414	-0.7544

TABLE A28. (Concluded)

RUN: SEQ												PROPLUSTRIVE												WING / CANARD												PRESSURES												BASEPR = 8.1924												PAGE 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TABLE A26. (Continued)

RUN: SEQ										PAGE 578									
240	4	CLARO =	0.3608	CDARO =	0.0643	WING / CANARD		PRESSURES		BASEPR = 8.1914									
ALPHA	4.03	PTOT	2139.13	PSTAT	30.06	VEL	H/C	CMAC	CMUT	HOT	RN								
BETA	-0.01	CL	0.36	CD	0.06	CM	0.01	CN	0.00	CLTR	CDTR								
						ROLL	0.00												
							-0.08												

TABLE A26. (Concluded)

RUN:SEQ										PAGE 50									
240	10	CLAE0 =	0.8610	CDAE0 =	0.1890	WING / CANARD	PRESSURES			BASEPR =	8.1914								
ALPHA	PTOT	PSTAT	Q	VEL	YAW	H/C	CMC	CMC	CMUT	HGT	RN								
12.07	2138.92	2103.86	30.06	158.25	0.01	2.67	0.0	0.0	0.0	#7.2350	0.103002E+07								
BETA	CL	CD	CM	CROLL	CN	CY	CNTR	CNTR	CNTR	CLTR	CDTR								
-0.01	0.86	0.19	-0.01	0.00	-0.00	0.01	0.86	-0.01	-0.01	0.83	0.21								
***** CANARD *****																			
BP=3.375		BP=10.125		BP=2		BP=6		BP=12		BP=16		BP=22		FUSELAGE		TOP		MISC	
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XLOC	CP	NO.	CP		
0.0	-3.8222	0.0	-0.4792	-1.6817	-3.7772	-3.4911	-1.4412	-3.4911	-1.4412	38.2	-0.2397	1	-0.4916	38.2	-0.2397	1	-0.4916		
2.5	-2.0330	2.5	-0.1700	-1.1778	-1.9336	-3.1934	-1.2923	-3.1934	-1.2923	43.4	-0.1874	2	0.1704	43.4	-0.1874	2	0.1704		
5.0	-1.3712	5.0	-0.6510	-0.9030	-1.3038	-3.0673	-1.3038	-3.0673	-1.3038	50.4	-0.1351	3	-0.7898	50.4	-0.1351	3	-0.7898		
10.0	-0.0396	10.0	-0.1586	-0.7312	-0.9831	-1.3381	-1.2236	-1.3381	-1.2236	56.1	-0.1251	4	0.1042	56.1	-0.1251	4	0.1042		
15.0	-0.8892	15.0	-0.5450	-0.6396	-0.8342	-0.7641	-1.1435	-0.7641	-1.1435	62.5	-0.1525	5	-0.8227	62.5	-0.1525	5	-0.8227		
25.0	-0.6278	24.0	-0.4792	-0.5031	-0.6052	-0.5708	-1.0518	-0.5708	-1.0518	69.7	-0.2048	6	-0.0613	69.7	-0.2048	6	-0.0613		
35.0	-0.4971	33.0	-0.4254	-0.4916	-0.5247	-0.4916	-0.7234	-0.4916	-0.7234	76.9	-0.1961	7	0.5582	76.9	-0.1961	7	0.5582		
50.0	-0.3827	54.0	-0.3261	-0.3592	-0.3923	-0.4314	-0.6842	-0.4314	-0.6842	83.4	-0.1961	8	0.0901	83.4	-0.1961	8	0.0901		
58.0	-0.3416	55.0	-0.3353	-0.3617	-0.4314	-0.4140	-0.7888	-0.4140	-0.7888	89.4	-0.1961	9	0.2858	89.4	-0.1961	9	0.2858		
65.0	-0.3634	78.5	-0.3268	-0.5970	-0.4750	-0.4227	82.4834	-0.4227	82.4834	101.1	-0.1812	10	0.1681	101.1	-0.1812	10	0.1681		
76.0	-0.1948	78.5	-0.5235	-0.5235	-0.5058	22.3770	52.4834	-0.5058	52.4834	---	---	11	-0.0163	---	---	11	-0.0163		
79.0	-0.4807	80.5	-0.5412	-0.5177	-0.2817	-0.5825	-0.7713	-0.2817	-0.7713	---	---	12	-0.0305	---	---	12	-0.0305		
80.5	-0.4941	81.3	-0.5471	36.0757	-0.3053	-0.2817	-0.6238	-0.3053	-0.6238	38.2	0.0567			38.2	0.0567				
81.0	-0.4823	82.0	-0.4882	-0.8261	-0.3230	-0.3525	-0.6120	-0.3230	-0.6120	43.4	0.0567			43.4	0.0567				
82.0	-0.4587	84.0	-0.2582	-0.3289	-0.3751	-0.3448	-0.6759	-0.3751	-0.6759	50.4	-0.0130			50.4	-0.0130				
84.0	-0.2081	87.0	-0.2935	-0.3112	-0.3820	-0.3448	-0.6759	-0.3820	-0.6759	56.1	0.0918			56.1	0.0918				
87.0	-0.2346	89.0	-0.3213	-0.3355	-0.3852	-0.3852	-0.6759	-0.3852	-0.6759	62.5	0.1177			62.5	0.1177				
89.0	-0.2135	93.0	-0.2504	-0.2433	-0.2859	-0.2078	-0.6476	-0.2859	-0.6476	69.7	0.1351			69.7	0.1351				
93.0	-0.1674	96.0	-0.2078	-0.1868	-0.2007	-0.2220	-0.6476	-0.2007	-0.6476	76.9	0.1177			76.9	0.1177				
96.0	-0.1438	100.0	-0.1724	-0.1085	-0.0873	-0.1298	-0.2007	-0.0873	-0.2007	83.4	0.0828			83.4	0.0828				
100.0	1.7825		0.0972	0.1539	0.1610	0.1397	-0.0092	0.1610	-0.0092	89.4	0.0741			89.4	0.0741				
95.0	0.1003	84.0	0.1965	0.2249	0.2390	0.1894	0.0617	0.2390	0.0617	95.4	0.0854			95.4	0.0854				
81.0	1.7825	73.5	0.1042	-0.1606	0.1373	0.1373	0.0711	0.1373	0.0711	101.1	-0.0566			101.1	-0.0566				
73.0	0.1003	54.0	0.1042	0.0711	0.0711	0.0380	-0.0282	0.0711	-0.0282										
50.0	0.2223	33.0	0.1373	-0.1937	0.1704	0.1704	0.0380	0.1704	0.0380										
35.0	0.0667	24.0	0.1735	0.1850	0.2079	0.2308	0.1048	0.2079	0.1048										
25.0	0.0421	10.0	0.2995	0.3224	0.3682	0.4140	0.3029	0.3682	0.3029										
10.0	0.1320	5.0	0.3567	0.4025	0.4827	0.5170	0.4353	0.4827	0.4353										
5.0	0.1076	2.5	0.4483	0.4713	0.4942	0.5365	0.4684	0.4942	0.4684										
2.5	0.5650																		

TABLE A27. RUN 241, BC1WGV, DELF-O, CMU-O.5, (BN/S)W-O.5

RUN: SEQ										PAGE 583															
241	1	CLARENO =	0.2014	CUAERO =	0.1068	DCLC =	0.0444	DMLC =	0.1389	BASEPR =	8.1914														
ALPHA	0.03	PTOT	2138.99	VEL	2117.82	YAW	2.67	H/C	0.536	HST	87.2368	BN													
BETA	-0.01	CD	-0.66	CH	-0.22	CROLL	0.01	CH	0.23	CLTR	0.23	CDTR	0.04												
***** CANARD *****										***** FUSELAGE *****															
BP=3.375 EP=10.125										-----TOP-----															
*****										*****															
XX/C	0.0	0.2238	0.3151	CP	0.0	0.4402	0.4082	CP	0.4883	0.5234	0.5685	CP	0.5234	0.5685	CP	0.5234	0.5685	CP	0.5234						
2.5	-0.0052	-0.0052	-0.0052	CP	2.5	0.0715	0.1837	CP	0.0247	-0.1049	-0.0728	CP	-0.1049	-0.0728	CP	-0.1049	-0.0728	CP	-0.1049						
5.0	-0.1310	-0.1081	-0.1081	CP	5.0	0.2639	0.0875	CP	0.0875	-0.1630	-0.1208	CP	-0.1630	-0.1208	CP	-0.1630	-0.1208	CP	-0.1630						
10.0	-0.1310	-0.1996	-0.1996	CP	10.0	-0.0247	-0.0728	CP	0.1890	-0.2011	-0.1690	CP	-0.2011	-0.1690	CP	-0.2011	-0.1690	CP	-0.2011						
15.0	-0.2340	-0.2110	-0.2110	CP	15.0	-0.0668	-0.1209	CP	0.2011	-0.2011	-0.1690	CP	-0.2011	-0.1690	CP	-0.2011	-0.1690	CP	-0.2011						
25.0	-0.2340	-0.2225	-0.2225	CP	25.0	-0.1209	-0.1850	CP	0.1850	-0.1850	-0.1530	CP	-0.1850	-0.1530	CP	-0.1850	-0.1530	CP	-0.1850						
35.0	-0.1768	-0.1996	-0.1996	CP	35.0	-0.1573	-0.2036	CP	0.2036	-0.2963	-0.2500	CP	-0.2963	-0.2500	CP	-0.2963	-0.2500	CP	-0.2963						
50.0	-0.2110	-0.2110	-0.2110	CP	50.0	-0.2036	-0.2963	CP	0.2963	1.9746	-0.2036	CP	-0.2036	-0.2036	CP	-0.2036	-0.2036	CP	-0.2036						
56.0	-0.2484	-0.2484	-0.2484	CP	56.0	-0.2555	-0.3287	CP	0.3287	-0.3531	-0.3043	CP	-0.3531	-0.3043	CP	-0.3531	-0.3043	CP	-0.3531						
65.0	-0.3026	-0.3026	-0.3026	CP	65.0	-0.6983	-1.1951	CP	0.6094	-0.4385	-0.3778	CP	-0.4385	-0.3778	CP	-0.4385	-0.3778	CP	-0.4385						
76.0	-0.1424	-0.6918	-0.6918	CP	76.0	21.4527	25.2014	CP	-3.1882	-3.0031	73.1638	CP	-3.0031	73.1638	CP	-3.0031	73.1638	CP	-3.0031						
79.0	-1.0803	-1.1146	-1.1146	CP	80.5	18.7895	-11.2100	CP	-0.2867	-0.3693	-1.0876	CP	-0.3693	-1.0876	CP	-0.3693	-1.0876	CP	-0.3693						
80.5	-16.5437	-22.3315	-22.3315	CP	81.3	-3.3673	84.3519	CP	-0.3693	-0.2536	-0.3032	CP	-0.2536	-0.3032	CP	-0.2536	-0.3032	CP	-0.2536						
82.0	2.4380	7.6818	7.6818	CP	82.0	-0.0307	-0.7325	CP	-0.3857	-0.2784	-0.2289	CP	-0.2784	-0.2289	CP	-0.2784	-0.2289	CP	-0.2784						
84.0	1.6371	-0.3940	-0.3940	CP	84.0	-3.3828	-1.5664	CP	-0.4883	-0.3362	-0.2619	CP	-0.3362	-0.2619	CP	-0.3362	-0.2619	CP	-0.3362						
87.0	0.6298	-0.6298	-0.6298	CP	87.0	-0.2949	-1.6985	CP	-0.5013	-0.3362	-0.2797	CP	-0.3362	-0.2797	CP	-0.3362	-0.2797	CP	-0.3362						
89.0	1.4059	-0.9022	-0.9022	CP	89.0	-1.0841	-0.6273	CP	-0.5280	-0.3790	-0.2698	CP	-0.3790	-0.2698	CP	-0.3790	-0.2698	CP	-0.3790						
93.0	0.1950	0.3790	0.3790	CP	93.0	-0.3194	-0.1009	CP	-0.3551	-0.1705	-0.2698	CP	-0.1705	-0.2698	CP	-0.1705	-0.2698	CP	-0.1705						
96.0	1.0602	0.2936	0.2936	CP	96.0	-0.4088	-0.3959	CP	-0.3959	-0.2003	-0.2400	CP	-0.2003	-0.2400	CP	-0.2003	-0.2400	CP	-0.2003						
100.0	3.3442	-1.3781	-1.3781	CP	100.0	-1.2430	-1.2132	CP	-0.1009	-0.0811	-0.1407	CP	-0.0811	-0.1407	CP	-0.0811	-0.1407	CP	-0.0811						
96.0	-0.0858	-0.0359	-0.0359	CP	96.0	-0.0977	0.1076	CP	0.1771	0.1374	0.1275	CP	0.1374	0.1275	CP	0.1374	0.1275	CP	0.1374						
84.0	3.3442	-1.3781	-1.3781	CP	73.5	-0.1109	0.1671	CP	0.0281	0.0281	0.0745	CP	0.0281	0.0745	CP	0.0281	0.0745	CP	0.0281						
73.0	-0.0959	-0.0359	-0.0359	CP	54.0	-0.1109	-0.1573	CP	-0.1573	-0.1109	-0.1109	CP	-0.1109	-0.1109	CP	-0.1109	-0.1109	CP	-0.1109						
50.0	0.0862	0.1106	0.1106	CP	33.0	-0.1573	-0.0182	CP	-0.0182	-0.1573	-0.1573	CP	-0.1573	-0.1573	CP	-0.1573	-0.1573	CP	-0.1573						
35.0	-0.0280	-0.0395	-0.0395	CP	24.0	-0.1209	-0.1369	CP	-0.0888	-0.0728	-0.0888	CP	-0.0728	-0.0888	CP	-0.0728	-0.0888	CP	-0.0728						
25.0	-0.2225	-0.3483	-0.3483	CP	10.0	-0.1049	-0.1369	CP	-0.1049	-0.1049	-0.2036	CP	-0.1049	-0.2036	CP	-0.1049	-0.2036	CP	-0.1049						
10.0	-0.1538	-0.2225	-0.2225	CP	5.0	-0.1209	-0.1690	CP	-0.1690	-0.1209	-0.0408	CP	-0.0408	-0.1109	CP	-0.0408	-0.1109	CP	-0.0408						
5.0	-0.2568	-0.2797	-0.2797	CP	2.5	-0.2171	-0.2492	CP	-0.2492	-0.2171	-0.1209	CP	-0.1209	-0.0646	CP	-0.1209	-0.0646	CP	-0.1209						
2.5	-0.4855	-0.4855	-0.4855	CP	2.5	-0.2171	-0.2492	CP	-0.2492	-0.2171	-0.1209	CP	-0.1209	-0.0646	CP	-0.1209	-0.0646	CP	-0.1209						

TABLE A27.

[illegible]

TABLE A27. (Concluded)

PROPELLSIVE WING / CANARD PRESSURES									
CLARO = 0.9571	COAERO = 0.2288	DCLC = 0.1012	DWLC = 0.2529						
PTOT	PSTAT	Q	VEL	YAW	H/C	CMUC	CMUN	CMUT	
2136.85	2117.71	21.13	132.85	0.01	2.67	0.266	0.956	0.825	
BETA	CL	CM	CM	CM	CM	CM	CM	CM	
-0.01	1.31	-0.52	-0.08	0.01	-0.01	0.00	1.02	-0.03	
241	5	CLARO = 0.9571	COAERO = 0.2288	DCLC = 0.1012	DWLC = 0.2529				
ALPHA	PTOT	PSTAT	Q	VEL	YAW	H/C	CMUC	CMUN	CMUT
12.06	2136.85	2117.71	21.13	132.85	0.01	2.67	0.266	0.956	0.825
BETA	CL	CM	CM	CM	CM	CM	CM	CM	CM
-0.01	1.31	-0.52	-0.08	0.01	-0.01	0.00	1.02	-0.03	

TABLE A29. RUN 256. 8W6V. DELF-O. CMU-O. (8W/8)W-O.5

RUN:SEQ										PAGE 588									
256	CLARO		CDARO																
ALPHA	PLOT	Q	VEL	YAW	H/C	CMUC	CMUW	CMUT	CMUW	CMUT	CMUW	CMUT	CMUW	CMUT	CMUW	CMUT	CMUW	CMUT	CMUW
3.59	21417.40	21119.00298.34	202.744512.43	-2.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
BETA	CL	CD	CM	CMUW	CMUW	CMUW	CMUW	CMUW	CMUW	CMUW	CMUW	CMUW	CMUW	CMUW	CMUW	CMUW	CMUW	CMUW	CMUW
12.43	20558.70		18760.30	0.00	-0.00	0.00	-0.00	0.00	-0.00	0.00	-0.00	0.00	-0.00	0.00	-0.00	0.00	-0.00	0.00	0.00
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TABLE A28. (Continued)

RUN: SEQ													
256	4												
ALPHA	0.01	CLAERO = 0.1397	CDAERO = 0.0376	WING / CANARD	PRESSURES		BASPR = 8.1914		PAGE 599				
BETA	-0.01	PTOT	PSTAT	VEL	YAW	H/C	CHLW	CHLIT	HQT	BN			
		2141.82	2111.98	29.83	160.07	0.01	2.67	0.0	87.1731	0.987642E+06			
		CL	CD	CM	CROLL	CN	CV	CNTR	CLTR	CDTR			
		0.14	0.04	-0.11	0.01	-0.00	0.01	0.12	0.12	0.08			
***** CANARD *****													
XX/C	0.0	CP	BP=3.375	BP=10.125									
0.0	-0.1774	-0.1692	0.0	0.5489	0.5605	0.4682	0.5258	0.5028	CP	XLDC	CP		
2.5	-0.1692	-0.1774	2.5	-0.1433	-0.1202	-0.1087	-0.1316	-0.1433	CP	38.2	0.9437	1	-0.2353
5.0	-0.1692	-0.1692	5.0	-0.1316	-0.1548	-0.1895	-0.1684	-0.2358	CP	43.4	0.9728	2	-0.1353
10.0	-0.1692	-0.1774	10.0	-0.1778	-0.2358	-0.2587	-0.2240	-0.2471	CP	50.4	0.9728	3	-0.2687
15.0	-0.1692	-0.1692	15.0	-0.2125	-0.2125	-0.2125	-0.2125	-0.2358	CP	56.1	0.9437	4	-0.1656
20.0	-0.1692	-0.1692	20.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP	62.5	0.9437	5	-0.2353
25.0	-0.1692	-0.1692	25.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP	68.7	0.9437	6	-0.1656
30.0	-0.1692	-0.1692	30.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP	76.9	0.9728	7	-0.2161
35.0	-0.1692	-0.1692	35.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP	83.4	0.9437	8	-0.2018
40.0	-0.1692	-0.1692	40.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP	89.4	0.9728	9	-0.2018
45.0	-0.1692	-0.1692	45.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP	98.4	0.9437	10	-0.2018
50.0	-0.1692	-0.1692	50.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP	101.1	0.9437	11	-0.2018
55.0	-0.1692	-0.1692	55.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
60.0	-0.1692	-0.1692	60.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
65.0	-0.1692	-0.1692	65.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
70.0	-0.1692	-0.1692	70.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
75.0	-0.1692	-0.1692	75.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
80.0	-0.1692	-0.1692	80.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
85.0	-0.1692	-0.1692	85.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
90.0	-0.1692	-0.1692	90.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
95.0	-0.1692	-0.1692	95.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
100.0	-0.1692	-0.1692	100.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
105.0	-0.1692	-0.1692	105.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
110.0	-0.1692	-0.1692	110.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
115.0	-0.1692	-0.1692	115.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
120.0	-0.1692	-0.1692	120.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
125.0	-0.1692	-0.1692	125.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
130.0	-0.1692	-0.1692	130.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
135.0	-0.1692	-0.1692	135.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
140.0	-0.1692	-0.1692	140.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
145.0	-0.1692	-0.1692	145.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
150.0	-0.1692	-0.1692	150.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
155.0	-0.1692	-0.1692	155.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
160.0	-0.1692	-0.1692	160.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
165.0	-0.1692	-0.1692	165.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
170.0	-0.1692	-0.1692	170.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
175.0	-0.1692	-0.1692	175.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
180.0	-0.1692	-0.1692	180.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
185.0	-0.1692	-0.1692	185.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
190.0	-0.1692	-0.1692	190.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
195.0	-0.1692	-0.1692	195.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
200.0	-0.1692	-0.1692	200.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
205.0	-0.1692	-0.1692	205.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
210.0	-0.1692	-0.1692	210.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
215.0	-0.1692	-0.1692	215.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
220.0	-0.1692	-0.1692	220.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
225.0	-0.1692	-0.1692	225.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
230.0	-0.1692	-0.1692	230.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
235.0	-0.1692	-0.1692	235.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
240.0	-0.1692	-0.1692	240.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
245.0	-0.1692	-0.1692	245.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
250.0	-0.1692	-0.1692	250.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
255.0	-0.1692	-0.1692	255.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
260.0	-0.1692	-0.1692	260.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
265.0	-0.1692	-0.1692	265.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
270.0	-0.1692	-0.1692	270.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
275.0	-0.1692	-0.1692	275.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
280.0	-0.1692	-0.1692	280.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
285.0	-0.1692	-0.1692	285.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
290.0	-0.1692	-0.1692	290.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
295.0	-0.1692	-0.1692	295.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
300.0	-0.1692	-0.1692	300.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
305.0	-0.1692	-0.1692	305.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
310.0	-0.1692	-0.1692	310.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
315.0	-0.1692	-0.1692	315.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
320.0	-0.1692	-0.1692	320.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
325.0	-0.1692	-0.1692	325.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
330.0	-0.1692	-0.1692	330.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
335.0	-0.1692	-0.1692	335.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
340.0	-0.1692	-0.1692	340.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
345.0	-0.1692	-0.1692	345.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
350.0	-0.1692	-0.1692	350.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
355.0	-0.1692	-0.1692	355.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
360.0	-0.1692	-0.1692	360.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
365.0	-0.1692	-0.1692	365.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
370.0	-0.1692	-0.1692	370.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
375.0	-0.1692	-0.1692	375.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
380.0	-0.1692	-0.1692	380.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
385.0	-0.1692	-0.1692	385.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
390.0	-0.1692	-0.1692	390.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
395.0	-0.1692	-0.1692	395.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
400.0	-0.1692	-0.1692	400.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
405.0	-0.1692	-0.1692	405.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
410.0	-0.1692	-0.1692	410.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
415.0	-0.1692	-0.1692	415.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
420.0	-0.1692	-0.1692	420.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
425.0	-0.1692	-0.1692	425.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
430.0	-0.1692	-0.1692	430.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
435.0	-0.1692	-0.1692	435.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
440.0	-0.1692	-0.1692	440.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
445.0	-0.1692	-0.1692	445.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
450.0	-0.1692	-0.1692	450.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
455.0	-0.1692	-0.1692	455.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
460.0	-0.1692	-0.1692	460.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
465.0	-0.1692	-0.1692	465.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
470.0	-0.1692	-0.1692	470.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
475.0	-0.1692	-0.1692	475.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
480.0	-0.1692	-0.1692	480.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
485.0	-0.1692	-0.1692	485.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
490.0	-0.1692	-0.1692	490.0	-0.2020	-0.2020	-0.2020	-0.2020	-0.2358	CP				
495.0	-0.1692	-0.1692	495.0	-0.2020	-0.2020	-0.2020	-0.2020</						

TABLE A28. (Continued)

RUN:SEQ												
256	7	CLAERO = 0.3291										
ALPHA	4.02	PTOT	2142.10	PSTAT	2112.04	Q	VEL	YAW	H/C	CMC	CMW	CMJT
BETA	-0.01	CL	0.33	CD	0.06	CM	160.76	CROLL	CN	CV	CNTR	CNTR
							-0.13	0.01	-0.00	0.01	0.32	-0.13
***** CANARD *****												
BP=3.375 BP=10.125												
CP												
%X/C	0.0	-0.1825	-0.1825	0.0	0.2342	-0.2009	-0.9473	CP	-0.9430	CP	-0.4528	CP
2.5	-0.1825	-0.1743	2.5	-0.1780	-0.7376	-0.9338	-0.7963	1.1513	-1.1513	43.4	0.9926	1
5.0	-0.1825	-0.1743	5.0	-0.1825	-0.5101	-0.9475	-0.8590	-0.7849	50.4	1.0013	3	2
10.0	-0.1743	-0.1743	10.0	-0.1591	-0.4643	-0.9017	-0.9330	-0.9673	56.1	0.9752	4	3
15.0	-0.1743	-0.1743	15.0	-0.3727	-0.4071	-0.4872	-0.1986	-0.4528	62.5	0.9639	5	4
25.0	-0.1743	-0.1825	25.0	-0.3040	-0.3498	-0.3841	-0.3841	-0.3612	69.7	0.9939	6	5
35.0	-0.1743	-0.1661	35.0	-0.2898	-0.2898	-0.3229	-0.3560	-0.3229	76.8	0.9926	7	6
50.0	-0.1825	-0.1743	50.0	-0.2567	-0.2567	1.0344	-0.2898	83.4	0.9926	8	7	
56.0	-0.1743	-0.1743	56.0	0.9926	0.9752	0.9752	0.9668	89.4	1.0013	9	8	
65.0	-0.1743	-0.1743	65.0	0.9839	0.9839	0.9752	0.9678	95.4	1.0013	10	9	
76.0	-0.1743	-0.1661	76.0	0.9839	0.9839	0.9752	0.9678	101.1	0.9839	11	10	
79.0	-0.1743	-0.1580	79.0	0.9839	0.9839	0.9752	0.9678	101.1	0.9839	12	11	
80.0	-0.1716	-0.1716	80.0	0.4840	-0.4722	-0.4722	21.9435	53.4298	38.2	0.9752	13	12
81.0	-0.1598	-0.1716	81.0	-0.4663	36.5669	-0.2482	-0.2601	-0.3720	38.2	0.9752	14	13
82.0	-0.1775	-0.1775	82.0	-0.3956	0.7552	-0.2836	-0.2836	-0.3013	43.4	0.9839	15	14
87.0	-0.1657	-0.1657	87.0	-0.2070	-0.2306	-0.2188	-0.3190	-0.3308	50.4	0.9485	16	15
87.0	0.9839	0.9839	87.0	-0.2365	-0.3718	-0.3484	-0.3249	-0.1834	56.1	0.9926	17	16
89.0	0.9752	0.9752	89.0	-0.2755	-0.2897	-0.3535	-0.3606	-0.3748	62.5	0.9926	18	17
93.0	0.9926	0.9926	93.0	-0.3187	-0.2258	-0.2613	-0.1974	-0.1904	69.7	0.9639	19	18
96.0	0.9839	0.9839	96.0	-0.1833	-0.1833	-0.1833	-0.2116	-0.3393	76.8	0.9839	20	19
100.0	0.9839	0.9839	100.0	-0.1407	-0.1052	-0.0911	-0.1123	-0.1974	83.4	0.9839	21	20
100.0	0.9839	0.9839	100.0	-0.0834	0.1288	0.1501	0.1430	0.1005	89.4	1.0013	22	21
101.0	0.9839	0.9839	101.0	0.1714	0.1005	0.1974	0.1856	1.3418	95.4	0.9839	23	22
101.0	0.9839	0.9839	101.0	0.0413	-0.1574	0.0744	0.0744	0.1075	101.1	0.9752	24	23
101.0	0.9839	0.9839	101.0	-0.0249	-0.0912	-0.0580	-0.0580	-0.0912	101.1	0.9752	25	24
101.0	0.9839	0.9839	101.0	0.0082	-0.1574	0.0082	0.0082	-0.0912	101.1	0.9752	26	25
101.0	0.9839	0.9839	101.0	-0.0177	-0.0043	-0.0043	-0.0043	-0.0979	101.1	0.9752	27	26
101.0	0.9839	0.9839	101.0	0.0510	0.0739	0.0853	0.0853	0.0744	101.1	0.9752	28	27
101.0	0.9839	0.9839	101.0	5.0	0.1540	0.1655	0.1655	0.1834	101.1	0.9752	29	28
101.0	0.9839	0.9839	101.0	2.5	0.2342	0.2342	0.2342	0.3028	101.1	0.9752	30	29
101.0	0.9839	0.9839	101.0	-0.1651	-0.1651	-0.1651	-0.1651	-0.1651	101.1	0.9752	31	30
101.0	0.9839	0.9839	101.0	-0.1825	-0.1825	-0.1825	-0.1825	-0.1825	101.1	0.9752	32	31
101.0	0.9839	0.9839	101.0	-0.1825	-0.1825	-0.1825	-0.1825	-0.1825	101.1	0.9752	33	32

TABLE A28. (Concluded)

PROPLUSTIVE WING / CANARD PRESSURES										BASEPR = 8.1914		PAGE 603	
CLAERO = 0.7415 CDAERO = 0.1727 DCLC = 0.0 DMCL = 0.0										HGT RM			
PTOT 2142.17 PSTAT 2112.00 30.17 161.13 0.01 2.72 0.0 CMUT										88.9847 0.990759E+06			
ALPHA 11.93 0.01 0.74 0.17 -0.20 0.00 -0.00 0.01 0.75 -0.20										CLTR CDR			
BETA -0.01 0.74 0.17 -0.20 0.00 -0.00 0.01 0.75 -0.20										0.72 0.21			
CANARD										FUSELAGE		MISC	
BP=3.375 BP=10.125										TOP		BOTTOM	
XX/C CP										XLOC CP		MD. CP	
0.0	-0.2191	-0.2191	0.0	-2.3072	-4.2694	-5.9119	-3.1628	-1.4403	-1.4403	38.2	1.0098	1	-0.5822
2.5	-0.2110	-0.2110	2.5	-0.1741	-1.9422	-2.4898	-2.5128	-1.3376	-1.3376	43.4	1.0098	2	0.2084
5.0	-0.2191	-0.2110	5.0	-1.0410	-1.5201	-1.7027	-2.3528	-1.3376	-1.3376	50.4	1.0098	3	-1.0438
10.0	-0.2110	-0.2110	10.0	-0.1855	-1.0638	-1.2920	-2.2388	-1.2578	-1.2578	56.1	1.0098	4	0.1104
15.0	-0.2029	-0.2110	15.0	-0.7444	-0.8588	-1.0824	-1.6884	-1.2692	-1.2692	62.5	1.0098	5	-0.9450
20.0	-0.2029	-0.2110	20.0	-0.5619	-0.8304	-0.7788	-1.2350	-1.1095	-1.1095	69.7	1.0098	6	-0.0875
25.0	-0.2029	-0.2110	25.0	-0.4803	-0.5162	-0.6811	-0.8192	-0.7141	-0.7141	76.9	1.0098	7	-0.2429
30.0	-0.2110	-0.2110	30.0	-0.3513	-0.3843	-0.4832	-0.9019	-0.7141	-0.7141	83.4	1.0098	8	-0.2358
35.0	-0.2110	-0.2110	35.0	-0.0098	0.9922	1.0183	1.0008	0.9922	0.9922	89.4	1.0098	9	-0.2287
40.0	-0.2191	-0.2110	40.0	0.9835	1.0008	1.0098	0.9922	0.9922	0.9922	95.4	1.0098	10	-0.2358
45.0	-0.2191	-0.2110	45.0	-0.5317	-0.5259	-0.5259	25.2176	53.2330	53.2330	101.1	1.0098	11	-0.2358
50.0	-0.2191	-0.2110	50.0	-0.5376	-0.5435	-0.3282	-0.6608	-0.7807	-0.7807	107.1	1.0098	12	-0.2287
55.0	-0.2208	-0.2110	55.0	-0.2792	-0.2792	-0.3438	-0.2616	-0.6022	-0.6022	113.2	0.9835		
60.0	-0.1970	-0.2110	60.0	-0.4908	-0.7960	-0.3438	-0.3088	-0.6374	-0.6374	119.4	0.9822		
65.0	-0.1912	-0.2110	65.0	-0.2558	-0.2910	-0.2675	-0.2675	-0.6318	-0.6318	125.6	0.9822		
70.0	0.9835	1.0098	70.0	-0.2792	-0.3277	-0.3791	-0.3556	-0.2088	-0.2088	131.8	0.9822		
75.0	0.9835	1.0098	75.0	-0.2570	-0.2711	-0.2923	-0.2287	-0.2429	-0.2429	138.0	0.9822		
80.0	0.9835	1.0098	80.0	-0.2146	-0.2004	-0.2146	-0.2711	-0.6315	-0.6315	144.2	0.9822		
85.0	0.9835	1.0098	85.0	-0.1581	-0.1227	-0.1227	-0.1934	-0.0379	-0.0379	150.4	0.9822		
90.0	0.9835	1.0098	90.0	0.1105	0.1529	0.1388	0.1176	1.2051	1.2051	156.6	0.9822		
95.0	0.9835	1.0098	95.0	0.2165	0.1458	0.2429	0.1670	0.0875	0.0875	162.8	0.9822		
100.0	0.9835	1.0098	100.0	0.1104	-0.1864	0.1764	0.1434	0.0444	0.0444	169.0	0.9822		
105.0	0.9835	1.0098	105.0	0.1104	0.0774	0.0774	0.0444	0.0444	0.0444	175.2	0.9822		
110.0	0.9835	1.0098	110.0	0.2094	-0.2194	0.1784	0.1784	0.0444	0.0444	181.4	0.9822		
115.0	0.9835	1.0098	115.0	0.2352	0.2024	0.2138	0.2366	0.0789	0.0789	187.6	0.9822		
120.0	0.9835	1.0098	120.0	0.3735	0.3883	0.4181	0.4181	0.3083	0.3083	193.8	0.9822		
125.0	0.9835	1.0098	125.0	0.4876	0.5104	0.5560	0.5560	0.4732	0.4732	200.0	0.9822		
130.0	0.9835	1.0098	130.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	206.2	0.9822		
135.0	0.9835	1.0098	135.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	212.4	0.9822		
140.0	0.9835	1.0098	140.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	218.6	0.9822		
145.0	0.9835	1.0098	145.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	224.8	0.9822		
150.0	0.9835	1.0098	150.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	231.0	0.9822		
155.0	0.9835	1.0098	155.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	237.2	0.9822		
160.0	0.9835	1.0098	160.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	243.4	0.9822		
165.0	0.9835	1.0098	165.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	249.6	0.9822		
170.0	0.9835	1.0098	170.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	255.8	0.9822		
175.0	0.9835	1.0098	175.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	262.0	0.9822		
180.0	0.9835	1.0098	180.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	268.2	0.9822		
185.0	0.9835	1.0098	185.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	274.4	0.9822		
190.0	0.9835	1.0098	190.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	280.6	0.9822		
195.0	0.9835	1.0098	195.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	286.8	0.9822		
200.0	0.9835	1.0098	200.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	293.0	0.9822		
205.0	0.9835	1.0098	205.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	299.2	0.9822		
210.0	0.9835	1.0098	210.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	305.4	0.9822		
215.0	0.9835	1.0098	215.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	311.6	0.9822		
220.0	0.9835	1.0098	220.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	317.8	0.9822		
225.0	0.9835	1.0098	225.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	324.0	0.9822		
230.0	0.9835	1.0098	230.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	330.2	0.9822		
235.0	0.9835	1.0098	235.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	336.4	0.9822		
240.0	0.9835	1.0098	240.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	342.6	0.9822		
245.0	0.9835	1.0098	245.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	348.8	0.9822		
250.0	0.9835	1.0098	250.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	355.0	0.9822		
255.0	0.9835	1.0098	255.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	361.2	0.9822		
260.0	0.9835	1.0098	260.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	367.4	0.9822		
265.0	0.9835	1.0098	265.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	373.6	0.9822		
270.0	0.9835	1.0098	270.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	379.8	0.9822		
275.0	0.9835	1.0098	275.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	386.0	0.9822		
280.0	0.9835	1.0098	280.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	392.2	0.9822		
285.0	0.9835	1.0098	285.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	398.4	0.9822		
290.0	0.9835	1.0098	290.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	404.6	0.9822		
295.0	0.9835	1.0098	295.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	410.8	0.9822		
300.0	0.9835	1.0098	300.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	417.0	0.9822		
305.0	0.9835	1.0098	305.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	423.2	0.9822		
310.0	0.9835	1.0098	310.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	429.4	0.9822		
315.0	0.9835	1.0098	315.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	435.6	0.9822		
320.0	0.9835	1.0098	320.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	441.8	0.9822		
325.0	0.9835	1.0098	325.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	448.0	0.9822		
330.0	0.9835	1.0098	330.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	454.2	0.9822		
335.0	0.9835	1.0098	335.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	460.4	0.9822		
340.0	0.9835	1.0098	340.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	466.6	0.9822		
345.0	0.9835	1.0098	345.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	472.8	0.9822		
350.0	0.9835	1.0098	350.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	479.0	0.9822		
355.0	0.9835	1.0098	355.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	485.2	0.9822		
360.0	0.9835	1.0098	360.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	491.4	0.9822		
365.0	0.9835	1.0098	365.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	497.6	0.9822		
370.0	0.9835	1.0098	370.0	0.6359	0.5560	0.5216	0.5216	0.5082	0.5082	503.8	0.9822		</

TABLE A29. (Continued)

RUN:SEQ		CLAERO =		PROPLUSIVE		WING / CANARD		PRESSURES		BASEPR = 8.1914		PAGE 608	
257	5	PSTAT	0.3762	CD AERO	0.1635	DLCL	0.0	CMUC	0.1669	HOT	87.1404	0.968135E+08	
ALPHA	2141.89	VEL	185.29	W/C	0.01	2.66	0.0	CV	0.511	CLTR	0.40	0.07	
BETA	CL	0.54	-0.32	CM	-0.21	CROLL	0.01	CV	0.41	CMTR	-0.19		
-0.01													
***** CANARD *****													
BP=3.375		BP=10.125		BP=2		BP=6		BP=12		BP=16		BP=22	
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP
0.0	-0.2405	0.0	-0.2318	0.0	-0.2220	0.0	-0.1313	0.0	-0.4724	0.0	-0.5334	0.0	-0.7527
2.5	-0.2405	2.5	-0.2318	2.5	-0.2410	2.5	-0.8136	2.5	-1.0936	2.5	-1.0936	2.5	-1.1790
5.0	-0.2405	5.0	-0.2318	5.0	-0.4724	5.0	-0.6952	5.0	-0.6674	5.0	-0.7039	5.0	-0.8867
10.0	-0.2492	10.0	-0.2405	10.0	-0.2288	10.0	-0.5334	10.0	-0.6187	10.0	-0.6430	10.0	-0.8430
15.0	-0.2405	15.0	-0.2318	15.0	-0.4115	15.0	-0.4237	15.0	-0.5212	15.0	-0.5455	15.0	-0.5455
20.0	-0.2405	20.0	-0.2231	20.0	-0.3384	20.0	-0.3750	20.0	-0.4359	20.0	-0.4359	20.0	-0.4481
25.0	-0.2405	25.0	-0.2231	25.0	-0.3384	25.0	-0.3750	25.0	-0.4359	25.0	-0.4359	25.0	-0.4481
30.0	-0.2405	30.0	-0.2405	30.0	-0.3384	30.0	-0.3750	30.0	-0.4359	30.0	-0.4359	30.0	-0.4481
35.0	-0.2405	35.0	-0.2405	35.0	-0.3384	35.0	-0.3750	35.0	-0.4359	35.0	-0.4359	35.0	-0.4481
40.0	-0.2405	40.0	-0.2318	40.0	-0.3384	40.0	-0.3750	40.0	-0.4359	40.0	-0.4359	40.0	-0.4481
45.0	-0.2405	45.0	-0.2318	45.0	-0.3384	45.0	-0.3750	45.0	-0.4359	45.0	-0.4359	45.0	-0.4481
50.0	-0.2405	50.0	-0.2318	50.0	-0.3384	50.0	-0.3750	50.0	-0.4359	50.0	-0.4359	50.0	-0.4481
55.0	-0.2405	55.0	-0.2318	55.0	-0.3384	55.0	-0.3750	55.0	-0.4359	55.0	-0.4359	55.0	-0.4481
60.0	-0.2405	60.0	-0.2318	60.0	-0.3384	60.0	-0.3750	60.0	-0.4359	60.0	-0.4359	60.0	-0.4481
65.0	-0.2405	65.0	-0.2318	65.0	-0.3384	65.0	-0.3750	65.0	-0.4359	65.0	-0.4359	65.0	-0.4481
70.0	-0.2405	70.0	-0.2318	70.0	-0.3384	70.0	-0.3750	70.0	-0.4359	70.0	-0.4359	70.0	-0.4481
75.0	-0.2405	75.0	-0.2318	75.0	-0.3384	75.0	-0.3750	75.0	-0.4359	75.0	-0.4359	75.0	-0.4481
80.0	-0.2405	80.0	-0.2318	80.0	-0.3384	80.0	-0.3750	80.0	-0.4359	80.0	-0.4359	80.0	-0.4481
85.0	-0.2405	85.0	-0.2318	85.0	-0.3384	85.0	-0.3750	85.0	-0.4359	85.0	-0.4359	85.0	-0.4481
90.0	-0.2405	90.0	-0.2318	90.0	-0.3384	90.0	-0.3750	90.0	-0.4359	90.0	-0.4359	90.0	-0.4481
95.0	-0.2405	95.0	-0.2318	95.0	-0.3384	95.0	-0.3750	95.0	-0.4359	95.0	-0.4359	95.0	-0.4481
100.0	-0.2405	100.0	-0.2318	100.0	-0.3384	100.0	-0.3750	100.0	-0.4359	100.0	-0.4359	100.0	-0.4481
105.0	-0.2405	105.0	-0.2318	105.0	-0.3384	105.0	-0.3750	105.0	-0.4359	105.0	-0.4359	105.0	-0.4481
110.0	-0.2405	110.0	-0.2318	110.0	-0.3384	110.0	-0.3750	110.0	-0.4359	110.0	-0.4359	110.0	-0.4481
115.0	-0.2405	115.0	-0.2318	115.0	-0.3384	115.0	-0.3750	115.0	-0.4359	115.0	-0.4359	115.0	-0.4481
120.0	-0.2405	120.0	-0.2318	120.0	-0.3384	120.0	-0.3750	120.0	-0.4359	120.0	-0.4359	120.0	-0.4481
125.0	-0.2405	125.0	-0.2318	125.0	-0.3384	125.0	-0.3750	125.0	-0.4359	125.0	-0.4359	125.0	-0.4481
130.0	-0.2405	130.0	-0.2318	130.0	-0.3384	130.0	-0.3750	130.0	-0.4359	130.0	-0.4359	130.0	-0.4481
135.0	-0.2405	135.0	-0.2318	135.0	-0.3384	135.0	-0.3750	135.0	-0.4359	135.0	-0.4359	135.0	-0.4481
140.0	-0.2405	140.0	-0.2318	140.0	-0.3384	140.0	-0.3750	140.0	-0.4359	140.0	-0.4359	140.0	-0.4481
145.0	-0.2405	145.0	-0.2318	145.0	-0.3384	145.0	-0.3750	145.0	-0.4359	145.0	-0.4359	145.0	-0.4481
150.0	-0.2405	150.0	-0.2318	150.0	-0.3384	150.0	-0.3750	150.0	-0.4359	150.0	-0.4359	150.0	-0.4481
155.0	-0.2405	155.0	-0.2318	155.0	-0.3384	155.0	-0.3750	155.0	-0.4359	155.0	-0.4359	155.0	-0.4481
160.0	-0.2405	160.0	-0.2318	160.0	-0.3384	160.0	-0.3750	160.0	-0.4359	160.0	-0.4359	160.0	-0.4481
165.0	-0.2405	165.0	-0.2318	165.0	-0.3384	165.0	-0.3750	165.0	-0.4359	165.0	-0.4359	165.0	-0.4481
170.0	-0.2405	170.0	-0.2318	170.0	-0.3384	170.0	-0.3750	170.0	-0.4359	170.0	-0.4359	170.0	-0.4481
175.0	-0.2405	175.0	-0.2318	175.0	-0.3384	175.0	-0.3750	175.0	-0.4359	175.0	-0.4359	175.0	-0.4481
180.0	-0.2405	180.0	-0.2318	180.0	-0.3384	180.0	-0.3750	180.0	-0.4359	180.0	-0.4359	180.0	-0.4481
185.0	-0.2405	185.0	-0.2318	185.0	-0.3384	185.0	-0.3750	185.0	-0.4359	185.0	-0.4359	185.0	-0.4481
190.0	-0.2405	190.0	-0.2318	190.0	-0.3384	190.0	-0.3750	190.0	-0.4359	190.0	-0.4359	190.0	-0.4481
195.0	-0.2405	195.0	-0.2318	195.0	-0.3384	195.0	-0.3750	195.0	-0.4359	195.0	-0.4359	195.0	-0.4481
200.0	-0.2405	200.0	-0.2318	200.0	-0.3384	200.0	-0.3750	200.0	-0.4359	200.0	-0.4359	200.0	-0.4481
205.0	-0.2405	205.0	-0.2318	205.0	-0.3384	205.0	-0.3750	205.0	-0.4359	205.0	-0.4359	205.0	-0.4481
210.0	-0.2405	210.0	-0.2318	210.0	-0.3384	210.0	-0.3750	210.0	-0.4359	210.0	-0.4359	210.0	-0.4481
215.0	-0.2405	215.0	-0.2318	215.0	-0.3384	215.0	-0.3750	215.0	-0.4359	215.0	-0.4359	215.0	-0.4481
220.0	-0.2405	220.0	-0.2318	220.0	-0.3384	220.0	-0.3750	220.0	-0.4359	220.0	-0.4359	220.0	-0.4481
225.0	-0.2405	225.0	-0.2318	225.0	-0.3384	225.0	-0.3750	225.0	-0.4359	225.0	-0.4359	225.0	-0.4481
230.0	-0.2405	230.0	-0.2318	230.0	-0.3384	230.0	-0.3750	230.0	-0.4359	230.0	-0.4359	230.0	-0.4481
235.0	-0.2405	235.0	-0.2318	235.0	-0.3384	235.0	-0.3750	235.0	-0.4359	235.0	-0.4359	235.0	-0.4481
240.0	-0.2405	240.0	-0.2318	240.0	-0.3384	240.0	-0.3750	240.0	-0.4359	240.0	-0.4359	240.0	-0.4481
245.0	-0.2405	245.0	-0.2318	245.0	-0.3384	245.0	-0.3750	245.0	-0.4359	245.0	-0.4359	245.0	-0.4481
250.0	-0.2405	250.0	-0.2318	250.0	-0.3384	250.0	-0.3750	250.0	-0.4359	250.0	-0.4359	250.0	-0.4481
255.0	-0.2405	255.0	-0.2318	255.0	-0.3384	255.0	-0.3750	255.0	-0.4359	255.0	-0.4359	255.0	-0.4481
260.0	-0.2405	260.0	-0.2318	260.0	-0.3384	260.0	-0.3750	260.0	-0.4359	260.0	-0.4359	260.0	-0.4481
265.0	-0.2405	265.0	-0.2318	265.0	-0.3384	265.0	-0.3750	265.0	-0.4359	265.0	-0.4359	265.0	-0.4481
270.0	-0.2405	270.0	-0.2318	270.0	-0.3384	270.0	-0.3750	270.0	-0.4359	270.0	-0.4359	270.0	-0.4481
275.0	-0.2405	275.0	-0.2318	275.0	-0.3384	275.0	-0.3750	275.0	-0.4359	275.0	-0.4359	275.0	-0.4481
280.0	-0.2405	280.0	-0.2318	280.0	-0.3384	280.0	-0.3750	280.0	-0.4359	280.0	-0.4359	280.0	-0.4481
285.0	-0.2405	285.0	-0.2318	285.0	-0.3384	285.0	-0.3750	285.0	-0.4359	285.0	-0.4359	285.0	-0.4481
290.0	-0.2405	290.0	-0.2318	290.0	-0.3384	290.0	-0.3750	290.0	-0.4359	290.0	-0.4359	290.0	-0.4481
295.0	-0.2405	295.0	-0.2318	295.0	-0.3384	295.0	-0.3750	295.0	-0.4359	295.0	-0.4359	295.0	-0.4481
300.0	-0.2405	300.0	-0.2318	300.0	-0.3384	300.0	-0.3750	300.0	-0.4359	300.0	-0.4359	300.0	-0.4481
305.0	-0.2405	305.0	-0.2318	305.0	-0.3384	305.0	-0.3750	305.0	-0.4359	305.0	-0.4359	305.0	-0.4481
310.0	-0.2405	310.0	-0.2318	310.0	-0.3384	310.0	-0.3750	310.0	-0.4359	310.0	-0.4359	310.0	-0.4481
315.0	-0.2405	315.0	-0.2318	315.0	-0.3384	315.0	-0.3750	315.0	-0.4359	315.0	-0.4359	315.0	-0.4481
320.0	-0.2405	320.0	-0.2318	320.0	-0.3384	320.0	-0.3750	320.0	-0.4359	320.0	-0.4359	320.0	-0.4481
325.0	-0.2405	325.0	-0.2318	325.0	-0.3384	325.0	-0.3750	325.0	-0.4359	325.0	-0.4359	325.0	-0.4481
330.0	-0.2405	330.0	-0.2318	330.0	-0.3384	330.0	-0.3750	330.0	-0.4359	330.0	-0.4359	330.0	-0.4481
335.0	-0.2405	335.0	-0.2318	335.0	-0.3384	335.0	-0.3750	335.0	-0.4359	335.0	-0.4359	335.0	-0.4481
340.0	-0.2405	340.0	-0.2318	340.0	-0.3384	340.0	-0.3750	340.0	-0.4359	340.0	-0.4359	340.0	-0.4481
345.0	-0.2405	345.0	-0.2318	345.0	-0.3384	345.0	-0.3750	345.0	-0.4359	345.0	-0.4359	345.0	-0.4481
350.0	-0.2405	350.0</											

TABLE A29.

PROPULSIVE										WING / CANARD										PRESSURES										BASEPR = 8.1914										PAGE 808																																																											
CLARO = 0.7438										DCLC = 0.0										DWLC = 0.2501										BASEPR = 8.1914										PAGE 808																																																											
PTOT										VEL										YAW										H/C										CMWC										CMUT										HGT										RN																													
2141.96										27.91										184.36										0.01										2.71										0.0										0.558										0.558										88.5055										0.902044E+08									
BETA										CN										CROLL										CN										CY										CNR										CNR										CDTR										O.18																			
-0.01										-0.19										-0.28										0.00										-0.00										0.02										-0.26										0.80										0.18																			

CANARD										WING										FUSELAGE										MISC.									
BP=3.375 BP=10.125										BP = 2 BP = 6 BP = 12 BP = 16 BP = 22										----TOP----										---BOTTOM---									
X/C										X/C										X/C										X/C									
CP										CP										CP										CP									
-0.2805										-0.2805										-0.2805										-0.2805									
-0.2717										-0.2717										-0.2717										-0.2717									
-0.2805										-0.2805										-0.2805										-0.2805									
-0.2805										-0.2805										-0.2805										-0.2805									
-0.2805										-0.2805										-0.2805										-0.2805									
-0.2717										-0.2717										-0.2717										-0.2717									
-0.2805										-0.2805										-0.2805										-0.2805									
-0.2805										-0.2805										-0.2805										-0.2805									
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-0.2805										-0.2805										-0.2805										-0.2805									
-0.2805										-0.2805										-0.2805										-0.2805									
-0.2805										-0.2805										-0.2805										-0.2805									
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-0.2805										-0.2805										-0.2805										-0.2805									
-0.2805										-0.2805										-0.2805										-0.2805									
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-0.2805										-0.2805										-0.2805										-0.2805									
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-0.2805										-0.2805										-0.2805										-0.2805									
-0.2805										-0.2805										-0.2805										-0.2805									
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-0.2805										-0.2805										-0.2805										-0.2805									
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-0.2805										-0.2805										-0.2805										-0.2805									
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-0.2805										-0.2805										-0.2805										-0.2805									
-0.2805										-0.2805										-0.2805										-0.2805									

TABLE A30. RUN 259, BM6V, DELF=0, CMU=1.0, (BM/B)V=0.5

RIN: SEQ													
256	1	CLAERO = 0.1478											
ALPHA	-0.01	PTOT	PSTAT	O	VEL	YAW	H/C	CMAC	CMW	DMLC	= 0.2681		BASEPR = 9.1814
BETA	-0.01	2142.38	2126.48	15.93	116.37	0.01	2.68	0.0	1.037	CMUT	1.037		HGT RN
		CL	CD	CM	CROLL	CH	CV		CNTR	0.22	-0.18		87.1184 0.728632E+06
		0.42	-0.68	-0.23	0.00	-0.00	0.01		0.22				CLTR CDTR
***** CANARD *****													
BP=3.375 BP=10.125													
XX/C	CP												
0.0	-0.2588	-0.2434	0.0	0.5289	0.5605	0.4857	0.4641	0.5288	38.2	1.0370	..MISC...		
2.5	-0.2588	-0.2434	2.5	-0.2487	-0.1191	-0.2919	-0.2371	0.2055	43.4	1.0370	NO.	CP	
5.0	-0.2588	-0.2434	5.0	-0.1407	-0.1838	-0.2919	-0.2055	-0.3135	50.4	1.0370	2	-0.2449	
10.0	-0.2434	-0.3204	10.0	-0.2371	-0.3351	-0.3135	-0.2919	-0.3135	53.1	1.0370	3	-0.1825	
15.0	-0.2588	-0.3204	15.0	-0.2487	-0.3351	-0.2703	-0.2371	-0.3135	53.1	1.0370	4	-0.3074	
25.0	-0.2434	-0.2896	24.0	-0.2487	-0.2919	-0.2487	-0.2055	-0.2919	62.5	1.0370	5	-0.1825	
35.0	-0.2434	-0.2588	33.0	-0.2487	-0.3074	-0.3074	-0.3074	-0.2449	69.7	1.0370	6	-0.2449	
50.0	-0.2434	-0.2588	54.0	-0.3074	-0.3074	-0.4323	-0.1298	-0.2449	76.9	1.0370	7	-0.1200	
58.0	-0.2434	-0.2588	65.0	1.0205	1.0205	-0.4323	1.0634	-0.2449	83.4	1.0370	8	-0.2805	
65.0	-0.2434	-0.2434	78.5	1.0205	1.0205	-0.4323	1.0634	-0.2449	89.4	1.0370	9	-0.2805	
76.0	-0.2434	-0.2434	79.5	60.6012	64.2924	-0.2635	-0.2635	-0.2635	95.4	1.0370	10	-0.2805	
79.0	-0.2588	-0.2434	80.5	38.5878	38.1010	-0.3302	-0.2857	-0.2301	101.1	1.0370	11	-0.2805	
80.5	-0.2190	-0.2078	81.3	31.8701	81.5814	-0.3302	-0.2857	-0.2301	101.1	1.0370	12	-0.2805	
81.0	-0.2412	-0.1987	82.0	5.0623	5.6470	-0.3302	-0.2857	-0.2301	101.1	1.0370			
82.0	-0.2301	-0.2190	84.0	5.9228	5.4007	-0.2746	-0.3302	-0.2301	101.1	1.0370			
84.0	-0.1856	-0.1856	87.0	8.2781	-1.7201	-0.4414	-0.3302	-0.2301	101.1	1.0370			
87.0	-0.1957	-0.1957	89.0	3.3448	-0.4848	-0.4946	-0.4410	-0.2079	101.1	1.0370			
89.0	1.0370	1.0370	93.0	0.5491	0.3618	-0.4277	-0.3302	-0.2079	101.1	1.0370			
93.0	1.0370	1.0370	98.0	-0.2136	0.3474	-0.3208	-0.2672	-0.2672	101.1	1.0370			
98.0	1.0370	1.0370	100.0	-2.0334	-2.1137	-0.1868	-0.1333	-0.2939	101.1	1.0370			
1.0205	1.0370	1.0370	96.0	-0.0664	0.0664	0.0808	0.0942	-0.2672	101.1	1.0370			
0.9876	1.0370	1.0370	96.0	-0.0664	0.0664	0.0808	0.0942	-0.2672	101.1	1.0370			
0.9876	1.0370	1.0370	84.0	0.0674	0.0674	0.0808	0.0942	-0.2672	101.1	1.0370			
0.9876	1.0370	1.0370	73.5	-0.2449	-0.2449	-0.0876	-0.1343	-0.2672	101.1	1.0370			
0.9876	1.0370	1.0370	54.0	-0.1200	-0.1200	-0.1825	-0.2672	-0.2672	101.1	1.0370			
1.0041	1.0370	1.0370	33.0	-0.1200	-0.1200	-0.1825	-0.2672	-0.2672	101.1	1.0370			
1.0041	1.0370	1.0370	24.0	-0.1407	-0.1407	-0.1623	-0.0975	-0.1825	101.1	1.0370			
1.0041	1.0370	1.0370	10.0	-0.0759	-0.1191	-0.1407	-0.0327	-0.1825	101.1	1.0370			
1.0041	1.0370	1.0370	5.0	-0.0543	-0.1191	-0.0975	-0.0543	-0.1200	101.1	1.0370			
1.0041	1.0370	1.0370	2.5	-0.0975	-0.1191	-0.0543	-0.0543	-0.1200	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2280	101.1	1.0370			
1.0041	1.0370	1.0370	0.0	-0.2280	-0.2280	-0.2280	-0.2280	-0.2					

TABLE A30. (Continued)

RUN:SEQ		CLAERO = 0.3138		CD AERO = 0.3774		WING / CANARD		PRESSURES		BASEPR = 8.1914		PAGE 611	
258	3	PTOT	PSTAT	O	VEL	YAW	H/C	CMUC	CMUM	HOT	RM		
4.01	2142.38	2128.03	14.35	110.36	0.01	2.67	0.0	1.154	1.154	87.1726	0.692496E+06		
BETA	CL	CD	CM	CROLL	CN	CY	CNTR	CMTR		CLTR	CDTR		
-0.01	0.89	-0.71	-0.27	0.00	-0.00	0.01	0.42	-0.22		0.41	0.06		
***** CANARD *****													
BP=3.375		BP=10.125		BP = 2		BP = 6		BP = 12		BP = 16		BP = 22	
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP
0.0	-0.2621	0.0	-0.2621	0.0	-0.1639	-0.1238	-0.2437	-0.3397	-0.4356	38.2	1.0215	1	-0.3834
2.5	-0.2791	2.5	-0.2791	2.5	-0.2917	-0.6274	-0.9871	-1.0351	-0.9392	43.4	1.0033	2	-0.1081
5.0	-0.2791	5.0	-0.2621	5.0	-0.5075	-0.8795	-0.7473	-0.7713	-0.7473	50.4	1.0033	3	-0.4527
10.0	-0.2621	10.0	-0.2621	10.0	-0.2677	-0.5315	-0.6753	-0.6274	-0.6274	56.1	0.9850	4	-0.1081
15.0	-0.2449	15.0	-0.2791	15.0	-0.4596	-0.4396	-0.5555	-0.5315	-0.5075	62.5	1.0033	5	-0.3834
25.0	-0.2621	25.0	-0.2621	24.0	-0.3636	-0.4116	-0.4596	-0.3878	-0.4356	69.7	1.0033	6	-0.1081
35.0	-0.2621	35.0	-0.2621	33.0	-0.3141	-0.3834	-0.3834	-0.4527	-0.3834	76.9	1.0215	7	-0.3041
50.0	-0.2621	50.0	-0.2621	54.0	-0.3141	-0.3834	-0.3834	0.1713	-0.3834	83.4	1.0398	8	-0.3041
56.0	-0.2621	56.0	-0.2621	65.0	0.9850	0.9850	1.0215	1.0215	1.0033	89.4	1.0033	9	-0.3041
65.0	-0.2449	65.0	-0.2621	78.5	1.0033	1.0033	1.0033	1.0215	1.0033	96.4	1.0215	10	-0.3041
76.0	-0.2791	76.0	-0.2621	79.5	68.1872	71.7132	-6.9839	35.3208	110.9315	101.1	1.0215	11	-0.3041
78.0	-0.2791	78.0	-0.2621	80.5	-43.0048	-42.1898	-0.3547	-0.7867	-1.8503	---	---	12	-0.2892
80.5	-0.2682	80.5	-0.2435	81.3	35.2344	87.3406	-0.4040	-0.3300	-0.3300	38.2	1.0033		
81.0	-0.2558	81.0	-0.2558	82.0	4.2622	-9.1807	-0.4410	-0.3300	-0.3300	43.4	1.0033		
82.0	-0.2558	82.0	-0.2558	84.0	-4.7616	-5.9467	-0.2806	-0.4040	-0.3547	50.4	1.0215		
84.0	-0.2806	84.0	-0.2435	87.0	9.2371	-1.7496	-0.5151	-0.3916	-0.2958	56.1	1.0033		
87.0	-0.2435	87.0	-0.2435	89.0	-3.8843	-0.3753	-0.5417	-0.4972	-0.4378	62.5	0.9850		
89.0	1.0033	89.0	1.0033	93.0	0.5130	0.4685	-0.4080	-0.2892	-0.3041	68.7	1.0033		
93.0	0.9850	93.0	0.9850	96.0	-0.2149	-0.3189	-0.3189	-0.3189	-0.3932	76.9	0.9850		
96.0	0.9850	96.0	0.9850	100.0	-2.2650	-2.4136	-0.1852	-0.2000	-0.2892	83.4	1.0033		
100.0	1.0033	100.0	1.0033	96.0	-0.0813	-0.0515	0.0376	0.0970	0.0525	89.4	1.0033		
96.0	0.9850	96.0	0.9850	84.0	0.0970	0.0079	-0.2892	0.1416	0.2159	95.4	1.0033		
84.0	0.9850	84.0	1.0033	73.5	-0.2447	-0.2447	0.0326	-0.0367	0.1713	101.1	1.0215		
73.0	1.0033	73.0	1.0033	54.0	-0.1081	-0.1061	-0.1061	-0.1081	-0.1754				
50.0	0.9850	50.0	1.0215	33.0	-0.0367	-0.2447	-0.1061	-0.0367	-0.1754				
35.0	-0.2791	35.0	-0.2791	24.0	-0.0518	-0.0998	-0.0759	-0.0518	-0.1238				
25.0	-0.2621	25.0	-0.2621	10.0	0.0440	0.0440	0.0440	0.0920	0.0326				
10.0	-0.2791	10.0	-0.2621	5.0	0.0920	0.0920	0.1160	0.1879	0.1713				
5.0	-0.2621	5.0	-0.2621	2.5	0.1879	0.2119	0.2359	0.2838	0.2406				
2.5	-0.2621	2.5	-0.2621										

TABLE A30. (Concluded)

TABLE A31. RUN 259, 8W6V, DELF=0, CMU=2.0, (BN/B)W=0.5

RUN: SEQ		PROPELLSIVE										WING / CANARD PRESSURES										PRESSURES										BASEPR = 8.1914										PAGE 615																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																													
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TABLE A31. (Continued)

PROPLUSTIVE WING / CANARD PRESSURES										PAGE 617	
CLARO = 0.3381 CDAERO = 0.4439 DCLC = 0.0										BASEPR = 8.1914	
PTOT ALPHA 4.07										HGT BN	
BETA -0.01										87.8526 0.486398E+06	
CL 1.03										CLTR CDR	
CD -1.55										0.46 0.06	
PROPLUSTIVE WING / CANARD PRESSURES Q VEL YAW H/C CMJC 7.01 76.89 0.01 2.69 0.0 CM CROLL CN CY -0.38 0.00 -0.00 0.02 0.46 -0.28											
CANARD BP=3.375 BP=10.125										FUSELAGE ----TOP----	
XX/C CP 0.0 -0.3319 2.5 -0.3319 5.0 -0.3319 10.0 -0.3319 15.0 -0.3319 20.0 -0.3319 25.0 -0.3319 30.0 -0.3319 35.0 -0.3319 40.0 -0.3319 45.0 -0.3319 50.0 -0.3319 55.0 -0.3319 60.0 -0.3319 65.0 -0.3319 70.0 -0.3319 75.0 -0.3319 80.0 -0.3319 85.0 -0.3319 90.0 -0.3319 95.0 -0.3319 100.0 -0.3319 105.0 -0.3319 110.0 -0.3319 115.0 -0.3319 120.0 -0.3319										XLOC CP 38.2 0.9589 43.4 1.0363 50.4 0.9889 56.1 0.9615 62.5 0.9415 69.7 0.9589 76.9 0.9889 83.4 0.9589 89.4 1.0363 95.4 0.9889 101.1 0.9889 106.1 0.9889 111.1 0.9889 116.1 0.9889 121.1 0.9889	
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TABLE A31. (Concluded)

[illegible]

TABLE A32. RUN 262, BWV, DELF=0, CMU=0, (BM/B)V=0.25

[illegible]

TABLE A32.

RUN: SEQ														
262	8	CLARO =		0.3290	CDAERO =	0.0612	DCLC =	0.0	WING / CANARD		PRESSURES		BASEPR =	8.1914
ALPHA	4.07	PTOT	0	VEL	VAV	H/C	CMAC	CMUT	CMUT	CMUT	CMUT	CMUT	87.4208	0.101824E+07
BETA	-0.01	CL	CD	CM	CROLL	CN	CY	CNTR	CNTR	CNTR	CNTR	CNTR	CLTR	CDTR
		0.33	0.06	-0.13	0.01	-0.00	0.01	0.33	-0.13	0.32	0.09	0.09		
***** CANARD *****														
BP=3.375 BP=10.125														
XX/C	0.0	CP	XX/C	CP	BP = 2	BP = 6	BP = 12	BP = 16	BP = 22	***** FUSELAGE*****				
-0.1743	-0.1661	0.0	0.2342	0.0166	-0.1898	-0.2582	-0.3384	38.2	-0.0851	***** TOP*****				
-0.1580	-0.1661	2.5	-0.1851	-0.6131	-0.8207	-0.7963	-0.8536	43.4	-0.0620	XLOC CP				
-0.1743	-0.1743	5.0	-0.4185	-0.5428	-0.6246	-0.6818	-0.7276	50.4	-0.0620	3 -0.3560				
-0.1661	-0.1743	10.0	-0.1666	-0.4524	-0.5444	-0.5444	-0.5444	56.1	-0.0707	4 -0.0580				
-0.1743	-0.1743	15.0	-0.3498	-0.3841	-0.4414	-0.4298	-0.4643	62.5	-0.0794	5 -0.3229				
-0.1580	-0.1580	24.0	-0.2811	-0.3154	-0.3727	-0.3612	-0.3841	69.7	-0.1317	6 -0.1243				
-0.1743	-0.1743	33.0	-0.2567	-0.2598	-0.2598	-0.2598	-0.2598	76.9	-0.1143	7 -0.2045				
-0.1661	-0.1661	54.0	-0.2336	-0.2336	-0.2336	-0.2336	-0.2336	83.4	-0.0881	8 -0.1974				
-0.1661	-0.1661	65.0	-0.2450	-0.2799	-0.3222	-0.3222	-0.3222	89.4	-0.1579	9 -0.1974				
-0.1661	-0.1661	76.0	-0.2169	-0.4890	-0.3845	-0.4108	-0.3522	95.4	-0.1840	10 -0.1974				
-0.1580	-0.1580	79.5	-0.4251	-0.4863	2.5574	4.3021	53.4597	101.1	-0.1491	11 -0.1974				
-0.1480	-0.1480	80.5	-0.4486	-0.4545	-0.2482	-0.2718	-0.8494	101.1	-0.1491	12 -0.1974				
-0.1480	-0.1480	81.3	-0.4310	51.2608	-0.2188	-0.2188	-0.3284	38.2	-0.0633	--- BOTTOM ---				
-0.1539	-0.1539	82.0	-0.3720	-0.7492	-0.2385	-0.2385	-0.2541	43.4	-0.0010					
-0.1579	-0.1579	84.0	-0.2129	-0.2129	-0.2482	-0.2482	-0.2954	50.4	-0.0794					
-0.1480	-0.1480	87.0	-0.2246	-0.2482	-0.3308	-0.3013	-0.1598	56.1	-0.0010					
-0.1598	-0.1598	89.0	-0.2684	-0.2967	-0.3606	-0.3677	-0.3535	62.5	-0.0252					
-0.1579	-0.1579	93.0	-0.2045	-0.2329	-0.2471	-0.1974	-0.1904	69.7	0.0252					
-0.1666	-0.1666	96.0	-0.1691	-0.1762	-0.1833	-0.2045	-0.3180	76.9	0.0077					
-0.1666	-0.1666	100.0	-0.1407	-0.1052	-0.0768	-0.1052	-0.1904	83.4	-0.0010					
-0.1666	-0.1666	96.0	-0.0934	0.1359	0.1572	0.1572	0.1005	89.4	0.0077					
-0.1666	-0.1666	84.0	0.1643	0.1147	0.1572	0.1572	0.1714	95.4	0.0077					
-0.1666	-0.1666	73.5	0.0413	-0.1574	0.0744	0.0744	0.1737	101.1	-0.0794					
-0.1666	-0.1666	54.0	-0.0249	-0.0580	-0.0580	-0.0580	-0.0912	-0.0912	-0.0912					
-0.1579	-0.1666	33.0	-0.0249	-0.1905	-0.0580	-0.0580	-0.0249	-0.0912	-0.0912					
-0.1743	-0.1661	24.0	-0.0177	-0.0292	-0.0063	-0.0063	-0.0635	-0.0635	-0.0635					
-0.1580	-0.1661	10.0	0.0853	0.0853	0.1082	0.1082	0.0744	0.0744	0.0744					
-0.1661	-0.1661	5.0	0.1540	0.1655	0.2113	0.2113	0.1737	0.1737	0.1737					
-0.1661	-0.1661	2.5	0.2227	0.2571	0.3143	0.3143	0.2914	0.2914	0.2914					

TABLE A32.
(Concluded)

TABLE A33. RUN 265. BWV, DELF-O, CMU-O.5, (BW/B)V-O.25

RUN:SEQ										PAGE 625									
265	2	CLARO =	0.1823	CDARO =	0.1163	WING / CANARD	PRESSURES												
ALPHA	PTOT	0	VEL	VAM	H/C	CMUC	CMJW	CMJW	CMJW	CMJW	CMJW	CMJW	CMJW	CMJW	CMJW	CMJW	CMJW	CMJW	CMJW
-0.04	2139.20	2121.91	17.29	120.66	0.01	2.66	0.0	0.495	0.495	0.495	0.495	0.495	0.495	0.495	0.495	0.495	0.495	0.495	0.495
BETA	CL	CD	CM	CROLL	CN	CV	CNTR	CNTR	CNTR	CNTR	CNTR	CNTR	CNTR	CNTR	CNTR	CNTR	CNTR	CNTR	CNTR
-0.01	0.31	-0.36	-0.19	0.00	-0.00	0.00	0.21	-0.16	0.21	-0.16	0.21	-0.16	0.21	-0.16	0.21	-0.16	0.21	-0.16	0.21
***** CANARD *****										***** WING *****									
BP=3:375 BP=10.125										BP=2 BP=6 BP=12 BP=16 BP=22									
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP
0.0	-0.2348	0.0	0.5228	0.0	0.5428	0.0	0.4830	0.0	0.5030	0.0	0.5030	0.0	0.5030	0.0	0.5030	0.0	0.5030	0.0	0.5030
2.5	-0.2206	2.5	-0.2137	2.5	-0.1340	2.5	-0.1340	2.5	-0.2733	2.5	-0.2733	2.5	-0.2733	2.5	-0.2733	2.5	-0.2733	2.5	-0.2733
5.0	-0.2064	5.0	-0.1738	5.0	-0.1839	5.0	-0.1839	5.0	-0.3131	5.0	-0.3131	5.0	-0.3131	5.0	-0.3131	5.0	-0.3131	5.0	-0.3131
10.0	-0.2064	10.0	-0.2137	10.0	-0.2534	10.0	-0.2534	10.0	-0.3131	10.0	-0.3131	10.0	-0.3131	10.0	-0.3131	10.0	-0.3131	10.0	-0.3131
15.0	-0.2206	15.0	-0.1937	15.0	-0.2336	15.0	-0.2336	15.0	-0.2932	15.0	-0.2932	15.0	-0.2932	15.0	-0.2932	15.0	-0.2932	15.0	-0.2932
20.0	-0.2348	20.0	-0.2137	20.0	-0.2137	20.0	-0.2137	20.0	-0.2733	20.0	-0.2733	20.0	-0.2733	20.0	-0.2733	20.0	-0.2733	20.0	-0.2733
25.0	-0.2064	25.0	-0.2079	25.0	-0.2079	25.0	-0.2079	25.0	-0.2658	25.0	-0.2658	25.0	-0.2658	25.0	-0.2658	25.0	-0.2658	25.0	-0.2658
30.0	-0.2206	30.0	-0.2658	30.0	-0.2658	30.0	-0.2658	30.0	-0.3131	30.0	-0.3131	30.0	-0.3131	30.0	-0.3131	30.0	-0.3131	30.0	-0.3131
35.0	-0.2206	35.0	-0.3227	35.0	-0.3227	35.0	-0.3227	35.0	-0.3781	35.0	-0.3781	35.0	-0.3781	35.0	-0.3781	35.0	-0.3781	35.0	-0.3781
40.0	-0.2064	40.0	1.3036	40.0	0.8812	40.0	0.8812	40.0	0.8812	40.0	0.8812	40.0	0.8812	40.0	0.8812	40.0	0.8812	40.0	0.8812
45.0	-0.2206	45.0	0.9839	45.0	0.9839	45.0	0.9839	45.0	0.9839	45.0	0.9839	45.0	0.9839	45.0	0.9839	45.0	0.9839	45.0	0.9839
50.0	-0.2064	50.0	79.5 55.7785	50.0	58.2278	50.0	58.2278	50.0	58.2278	50.0	58.2278	50.0	58.2278	50.0	58.2278	50.0	58.2278	50.0	58.2278
55.0	-0.2206	55.0	80.5 38.5876	55.0	42.7276	55.0	42.7276	55.0	42.7276	55.0	42.7276	55.0	42.7276	55.0	42.7276	55.0	42.7276	55.0	42.7276
60.0	-0.2090	60.0	81.3 26.3187	60.0	92.3598	60.0	92.3598	60.0	92.3598	60.0	92.3598	60.0	92.3598	60.0	92.3598	60.0	92.3598	60.0	92.3598
65.0	-0.2284	65.0	82.0 5.5107	65.0	0.1987	65.0	0.1987	65.0	0.1987	65.0	0.1987	65.0	0.1987	65.0	0.1987	65.0	0.1987	65.0	0.1987
70.0	-0.1884	70.0	84.0 0.3730	70.0	-2.4230	70.0	-2.4230	70.0	-2.4230	70.0	-2.4230	70.0	-2.4230	70.0	-2.4230	70.0	-2.4230	70.0	-2.4230
75.0	-0.2192	75.0	87.0 10.5130	75.0	-1.9310	75.0	-1.9310	75.0	-1.9310	75.0	-1.9310	75.0	-1.9310	75.0	-1.9310	75.0	-1.9310	75.0	-1.9310
80.0	-0.2115	80.0	89.0 5.0671	80.0	-0.9850	80.0	-0.9850	80.0	-0.9850	80.0	-0.9850	80.0	-0.9850	80.0	-0.9850	80.0	-0.9850	80.0	-0.9850
85.0	-0.2115	85.0	93.0 0.2730	85.0	-0.6396	85.0	-0.6396	85.0	-0.6396	85.0	-0.6396	85.0	-0.6396	85.0	-0.6396	85.0	-0.6396	85.0	-0.6396
90.0	-0.2115	90.0	96.0 0.1094	90.0	-0.7506	90.0	-0.7506	90.0	-0.7506	90.0	-0.7506	90.0	-0.7506	90.0	-0.7506	90.0	-0.7506	90.0	-0.7506
95.0	-0.2266	95.0	100.0 -1.9469	95.0	-1.3179	95.0	-1.3179	95.0	-1.3179	95.0	-1.3179	95.0	-1.3179	95.0	-1.3179	95.0	-1.3179	95.0	-1.3179
100.0	-0.2266	100.0	96.0 -0.0477	100.0	0.0385	100.0	0.0385	100.0	0.0385	100.0	0.0385	100.0	0.0385	100.0	0.0385	100.0	0.0385	100.0	0.0385
105.0	-0.2266	105.0	84.0 0.1003	105.0	0.1003	105.0	0.1003	105.0	0.1003	105.0	0.1003	105.0	0.1003	105.0	0.1003	105.0	0.1003	105.0	0.1003
110.0	-0.2266	110.0	73.5 -0.1504	110.0	-0.2079	110.0	-0.2079	110.0	-0.2079	110.0	-0.2079	110.0	-0.2079	110.0	-0.2079	110.0	-0.2079	110.0	-0.2079
115.0	-0.2266	115.0	54.0 -0.0928	115.0	-0.0928	115.0	-0.0928	115.0	-0.0928	115.0	-0.0928	115.0	-0.0928	115.0	-0.0928	115.0	-0.0928	115.0	-0.0928
120.0	-0.2266	120.0	33.0 -0.0928	120.0	-0.0928	120.0	-0.0928	120.0	-0.0928	120.0	-0.0928	120.0	-0.0928	120.0	-0.0928	120.0	-0.0928	120.0	-0.0928
125.0	-0.2206	125.0	24.0 -0.1340	125.0	-0.1340	125.0	-0.1340	125.0	-0.1340	125.0	-0.1340	125.0	-0.1340	125.0	-0.1340	125.0	-0.1340	125.0	-0.1340
130.0	-0.2064	130.0	10.0 -0.0842	130.0	-0.0842	130.0	-0.0842	130.0	-0.0842	130.0	-0.0842	130.0	-0.0842	130.0	-0.0842	130.0	-0.0842	130.0	-0.0842
135.0	-0.2206	135.0	5.0 -0.0345	135.0	-0.0345	135.0	-0.0345	135.0	-0.0345	135.0	-0.0345	135.0	-0.0345	135.0	-0.0345	135.0	-0.0345	135.0	-0.0345
140.0	-0.2206	140.0	2.5 -0.0345	140.0	-0.1141	140.0	-0.1141	140.0	-0.1141	140.0	-0.1141	140.0	-0.1141	140.0	-0.1141	140.0	-0.1141	140.0	-0.1141
145.0	-0.2064	145.0																	
150.0	-0.2206	150.0																	
155.0	-0.2206	155.0																	
160.0	-0.2206	160.0																	
165.0	-0.2206	165.0																	
170.0	-0.2206	170.0																	
175.0	-0.2206	175.0																	
180.0	-0.2206	180.0																	
185.0	-0.2206	185.0																	
190.0	-0.2206	190.0																	
195.0	-0.2206	195.0																	
200.0	-0.2206	200.0																	
205.0	-0.2206	205.0																	
210.0	-0.2206	210.0																	
215.0	-0.2206	215.0																	
220.0	-0.2206	220.0																	
225.0	-0.2206	225.0																	
230.0	-0.2206	230.0																	
235.0	-0.2206	235.0																	
240.0	-0.2206	240.0																	
245.0	-0.2206	245.0																	
250.0	-0.2206	250.0																	
255.0	-0.2206	255.0																	
260.0	-0.2206	260.0																	
265.0	-0.2206	265.0																	
270.0	-0.2206	270.0																	
275.0	-0.2206	275.0																	
280.0	-0.2206	280.0																	
285.0	-0.2206	285.0																	
290.0	-0.2206	290.0																	
295.0	-0.2206	295.0																	
300.0	-0.2206	300.0																	
305.0	-0.2206	305.0																	
310.0	-0.2206	310.0																	
315.0	-0.2206	315.0																	
320.0	-0.2206	320.0																	
325.0	-0.2206	325.0																	
330.0	-0.2206	330.0																	
335.0	-0.2206	335.0																	
340.0	-0.2206	340.0																	
345.0	-0.2206	345.0																	

TABLE A33.

PAGE 027

BASEPR = 8.1804
HGT RM
97.6337 0.768174E+08
CLTR COTR
0.40 0.08

PRO	PRESSURES		
DWLC	DWLC =	0.1613	
	CMUW	CMUT	
.0	0.404	0.494	
CY	CNTR	CNTR	
0.00	0.40	-0.19	

PROPLUSIVE		WING /	
RO =	0.1431	DCLC =	
VEL	YAW	H/C	
29	120.74	0.01	2.98
CM	CROLL	CN	
23	0.00	-0.00	

CLAURO	0.3653
PTOT	PSTAT
2139.20	2121.9
CL	CD
BETA	0.22

●●FUSELAGE●●	NO.	CP	●●MISC.●●●
-----TOP-----	KLOC	CP	
	38.2	-0.0903	1 -0.3508
	43.4	-0.0900	2 -0.0323
	50.4	-0.0850	3 -0.3808
	58.1	-0.0781	4 -0.0353
	62.6	-0.0903	5 -0.3230
	69.7	-0.0509	6 -0.0518
	78.9	-0.1808	7 -0.2327
	83.4	-0.1208	8 -0.2080
	89.4	-0.1118	9 -0.2204
	95.4	-0.2268	10 -0.2452
	01.1	-0.1984	11 -0.2327
-----BOTTOM----			12 -0.2304

%C	BP = 2	BP = 6	BP = 12	BP = 16	BP = 22
	CP	CP	CP	CP	CP
0.0	0.1845	-0.0544	-0.3729	-0.2137	-0.5122
2.5	0.1738	-0.6913	-1.0297	-0.9899	-0.9501
5.0	0.4326	-0.5122	-0.6316	-0.6515	-0.7710
10.0	0.1639	-0.4525	-0.5719	-0.5122	-0.5520
15.0	0.3729	-0.3729	-0.4923	-0.3729	-0.4525
20.0	0.2733	-0.3932	-0.3928	-0.3131	-0.3729
24.0	0.2733	-0.3230	-0.3808	-0.3808	-0.3230
33.0	0.3230	-0.3230	-0.3230	1.0581	-0.3230
44.0	0.3230	-0.3230	0.4084	0.3781	-0.3030
55.0	0.3933	0.7266	0.4084	-0.4691	-0.4368
78.5	1.4086	-0.9842	7.2736	7.0888	92.3714
79.5	55.9219	58.5356	7.2736	7.0888	92.3714
80.5	-36.7102	-43.3707	-0.3627	-0.3432	-1.3877
81.3	26.5577	92.3714	-0.2704	-0.2294	-0.3525
82.0	6.3102	-0.3525	-0.2910	-0.2500	-0.3115
84.0	0.2318	-2.2488	-0.3012	-0.3217	-0.3012
87.0	11.9917	-1.9413	-0.3432	-0.3432	-0.1884
89.0	-5.9427	-0.9973	-0.4053	-0.4053	-0.3807
93.0	0.4580	-0.6273	-0.2943	-0.2327	-0.2050
96.0	-0.1094	0.7260	-0.2204	-0.2327	-0.3150
100.0	-1.9716	-1.3673	-0.1217	-0.1340	-0.2204
96.0	-0.10107	0.0756	0.1373	0.1495	0.1250
84.0	0.1496	0.1250	-0.2204	0.1990	1.2395
73.5	-0.1504	-0.2079	0.1374	0.0798	0.3100
94.0	-0.0353	-0.0353	-0.0353	-0.0928	-0.0928
33.0	0.0423	-0.1504	0.0353	-0.0353	-0.0928
24.0	0.0251	0.0352	0.0053	0.0451	-0.0146
10.0	0.1446	0.1446	0.1446	0.1845	0.0798
5.0	0.2442	0.2243	0.2243	0.3036	0.1948
2.5	0.3238	0.2840	0.3437	0.3835	0.2525

***** CANARD *****	CP	CP
BP=3.975 BP=10.125	-0.2206	-0.2206
0.0	-0.2206	-0.2206
2.5	-0.2206	-0.2206
5.0	-0.2206	-0.2206
10.0	-0.2348	-0.2064
15.0	-0.2206	-0.2064
25.0	-0.2206	-0.2206
35.0	-0.2206	-0.2064
50.0	-0.2206	-0.2064
65.0	-0.2206	-0.2064
80.0	-0.1922	-0.2206
78.0	-0.2064	-0.2206
80.5	-0.2090	-0.2192
81.0	-0.1834	-0.1884
82.0	-0.2090	-0.1987
84.0	-0.2192	
87.0	-0.2090	
89.0	-0.2115	-0.2115
93.0	-0.2115	-0.2115
96.0	-0.1984	-0.2115
00.0	-0.1984	-0.2115
96.0	-0.1984	-0.2115
84.0	-0.1984	-0.2115
73.0	-0.1984	-0.2115
87.0	-0.2115	-0.2115
50.0	-0.2115	-0.2115
35.0	-0.2064	-0.2064
25.0	-0.2206	-0.2064
10.0	-0.2064	-0.2206
5.0	-0.2348	-0.2206
2.5	-0.2064	-0.2206

TABLE A33. (Concluded)

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RUN:SEQ 265 8
ALPHA 12.04
BETA -0.01
CLAERO = 0.7406
PTOT 2139.13
PSTAT 2121.73
CD 0.97
CDAERO = 0.2860
VEL 17.40
CM 121.23
CROLL 0.00
DCLC = 0.0
H/C 2.73
CN -0.00
WING / CANARD PRESSURES
BP = 2 BP = 6 BP = 12 BP = 16 BP = 22
XX/C CP CP CP CP
-0.2558 -0.2416 -0.2558 -0.2558 -0.2558
2.5 -0.2558 2.5 -0.2363 -1.8083 -5.7835 -2.7773 -1.4722
5.0 -0.2558 5.0 -1.0371 -1.8083 -2.4609 -2.5202 -1.2151
10.0 -0.2558 10.0 -0.2558 10.0 -0.2460 -0.9778 -1.6304 -2.4807 -1.2348
15.0 -0.2558 15.0 -0.2558 15.0 -0.6811 -0.7997 -1.2151 -2.1643 -1.2348
20.0 -0.2558 20.0 -0.2558 20.0 -0.5229 -0.6416 -0.8196 -1.6304 -1.1857
25.0 -0.2558 25.0 -0.2558 25.0 -0.4867 -0.4867 -0.6010 -0.8196 -1.1162
30.0 -0.2558 30.0 -0.2558 30.0 -0.3773 -0.4295 -0.4867 -0.6010 -0.8196
35.0 -0.2558 35.0 -0.2558 35.0 -0.4603 -0.7764 -0.5084 -0.4151 -0.7011
40.0 -0.2558 40.0 -0.2558 40.0 -1.4364 -1.0322 -0.5204 -0.5084 -0.7011
45.0 -0.2558 45.0 -0.2558 45.0 -56.2874 58.8117 7.3344 7.3545 91.7658
50.0 -0.2558 50.0 -0.2558 50.0 -36.5782 -43.6660 -0.4157 -0.3342 -1.3832
55.0 -0.2558 55.0 -0.2558 55.0 -24.6975 81.3078 -0.3546 -0.3528 -0.6398
60.0 -0.2558 60.0 -0.2558 60.0 -7.8228 87.0 -1.0573 -0.3750 -0.6295
65.0 -0.2558 65.0 -0.2558 65.0 -12.8821 -87.0 -2.1572 -0.3648 -0.6907
70.0 -0.2558 70.0 -0.2558 70.0 -8.8051 -89.0 -0.8051 -0.4565 -0.3546
75.0 -0.2558 75.0 -0.2558 75.0 -0.6323 89.0 -0.6323 -0.4460 -0.2324
80.0 -0.2558 80.0 -0.2558 80.0 -0.1274 96.0 -0.1274 -0.3357 -0.7033
85.0 -0.2558 85.0 -0.2558 85.0 -1.9285 100.0 -1.9285 -0.2621 -0.2744
90.0 -0.2558 90.0 -0.2558 90.0 -0.0441 96.0 -0.0441 -0.2621 -0.2621
95.0 -0.2558 95.0 -0.2558 95.0 -0.2034 84.0 -0.2034 -0.2621 -0.2621
100.0 -0.2558 100.0 -0.2558 100.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
105.0 -0.2558 105.0 -0.2558 105.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
110.0 -0.2558 110.0 -0.2558 110.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
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165.0 -0.2558 165.0 -0.2558 165.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
170.0 -0.2558 170.0 -0.2558 170.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
175.0 -0.2558 175.0 -0.2558 175.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
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185.0 -0.2558 185.0 -0.2558 185.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
190.0 -0.2558 190.0 -0.2558 190.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
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205.0 -0.2558 205.0 -0.2558 205.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
210.0 -0.2558 210.0 -0.2558 210.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
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255.0 -0.2558 255.0 -0.2558 255.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
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265.0 -0.2558 265.0 -0.2558 265.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
270.0 -0.2558 270.0 -0.2558 270.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
275.0 -0.2558 275.0 -0.2558 275.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
280.0 -0.2558 280.0 -0.2558 280.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
285.0 -0.2558 285.0 -0.2558 285.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
290.0 -0.2558 290.0 -0.2558 290.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
295.0 -0.2558 295.0 -0.2558 295.0 -0.0885 84.0 -0.0885 -0.2621 -0.2621
300.0 -0.2558 300.0 -0.2558 300.0 -0.0885 84.0 -0.
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TABLE A34. (Continued)

PROPULSIVE										WING / CANARD										PRESSURES										BASEPR = 8.1904										PAGE 632																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																							
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TABLE A34. (Concluded)

TABLE A35. RUN 267, BW6V, DELP-O, CMJ-2-O, (RM/S)W-0.25

PROPLULSIVE										WING / CANARD PRESSURES									
CLAERO = 0.1452 CDAERO = 0.3717 DCLC = 0.0										DMLC = 0.5354									
PTOT 2139.69										CMJW CMUT									
CL 0.01										2.067 2.067									
BETA -0.01										CROLL CN CV CNTR CNTR									
0.68 -1.72										0.01 0.00 -0.00 0.26 -0.25									
CANARD										WING									
BP-3.375 BP-10.125										BP = 2 BP = 6 BP = 12 BP = 16 BP = 22									
XX/C CP										XX/C CP									
0.0	-0.3198	-0.3198	0.0	0.6892	0.6892	0.5848	0.5001	0.5001	0.5001	0.5001	0.5001	0.5001	0.5001	0.5001	0.5001	0.5001	0.5001	0.5001	0.5001
2.5	-0.2595	-0.2595	2.5	-0.2612	-0.0920	-0.3457	-0.2612	-0.0074	-0.0074	-0.2612	-0.0074	-0.0074	-0.0074	-0.0074	-0.0074	-0.0074	-0.0074	-0.0074	-0.0074
5.0	-0.2595	-0.1991	5.0	-0.0920	-0.0920	-0.2612	-0.2612	-0.1768	-0.1768	-0.2612	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768
10.0	-0.2595	-0.2595	10.0	-0.2612	-0.0920	-0.2612	-0.0920	-0.0920	-0.0920	-0.2612	-0.0920	-0.0920	-0.0920	-0.0920	-0.0920	-0.0920	-0.0920	-0.0920	-0.0920
15.0	-0.1991	-0.2595	15.0	-0.1768	-0.1768	-0.3457	-0.3457	-0.0920	-0.0920	-0.1768	-0.0920	-0.0920	-0.0920	-0.0920	-0.0920	-0.0920	-0.0920	-0.0920	-0.0920
20.0	-0.3198	-0.3198	20.0	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768	-0.1768
25.0	-0.3198	-0.3198	25.0	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596
30.0	-0.3198	-0.3198	30.0	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596	-0.4596
35.0	-0.2595	-0.2595	35.0	-0.5375	-1.8893	-0.4731	-0.4731	-0.4731	-0.4731	-0.5375	-0.4731	-0.4731	-0.4731	-0.4731	-0.4731	-0.4731	-0.4731	-0.4731	-0.4731
40.0	-0.2595	-0.2595	40.0	2.7112	-1.9537	-0.6019	-0.6019	-0.6019	-0.6019	2.7112	-0.6019	-0.6019	-0.6019	-0.6019	-0.6019	-0.6019	-0.6019	-0.6019	-0.6019
45.0	-0.2595	-0.2595	45.0	78.5	239.2819	34.2393	37.2004	389.1824	389.1824	78.5	34.2393	37.2004	389.1824	389.1824	389.1824	389.1824	389.1824	389.1824	389.1824
50.0	-0.2595	-0.2595	50.0	79.5228	239.2819	34.2393	37.2004	389.1824	389.1824	79.5228	239.2819	34.2393	37.2004	389.1824	389.1824	389.1824	389.1824	389.1824	389.1824
55.0	-0.2595	-0.2595	55.0	81.3122	312.1912	-0.4733	-0.4733	-0.4733	-0.4733	81.3122	312.1912	-0.4733	-0.4733	-0.4733	-0.4733	-0.4733	-0.4733	-0.4733	-0.4733
60.0	-0.2595	-0.2595	60.0	82.0	12.4618	-0.2555	-0.2555	-0.2555	-0.2555	82.0	12.4618	-0.2555	-0.2555	-0.2555	-0.2555	-0.2555	-0.2555	-0.2555	-0.2555
65.0	-0.2595	-0.2595	65.0	84.0	-1.2572	-1.9977	-0.2555	-0.2555	-0.2555	84.0	-1.2572	-1.9977	-0.2555	-0.2555	-0.2555	-0.2555	-0.2555	-0.2555	-0.2555
70.0	-0.2595	-0.2595	70.0	87.0	-28.5624	-8.8320	-0.2555	-0.2555	-0.2555	87.0	-28.5624	-8.8320	-0.2555	-0.2555	-0.2555	-0.2555	-0.2555	-0.2555	-0.2555
75.0	-0.2595	-0.2595	75.0	89.0	13.1118	-3.3416	-0.5121	-0.4597	-0.4597	89.0	13.1118	-3.3416	-0.5121	-0.4597	-0.4597	-0.4597	-0.4597	-0.4597	-0.4597
80.0	-0.2595	-0.2595	80.0	93.0	2.1603	-2.1366	-0.3549	-0.3025	-0.3025	93.0	2.1603	-2.1366	-0.3549	-0.3025	-0.3025	-0.3025	-0.3025	-0.3025	-0.3025
85.0	-0.2595	-0.2595	85.0	96.0	0.5359	-2.7851	-0.3025	-0.3025	-0.3025	96.0	0.5359	-2.7851	-0.3025	-0.3025	-0.3025	-0.3025	-0.3025	-0.3025	-0.3025
90.0	-0.2595	-0.2595	90.0	100.0	-8.4857	-4.8468	-0.1453	-0.0920	-0.0920	100.0	-8.4857	-4.8468	-0.1453	-0.0920	-0.0920	-0.0920	-0.0920	-0.0920	-0.0920
95.0	-0.2595	-0.2595	95.0	96.0	-0.3025	-0.1453	0.1167	0.1167	0.1167	96.0	-0.3025	-0.1453	0.1167	0.1167	0.1167	0.1167	0.1167	0.1167	0.1167
100.0	-0.2595	-0.2595	100.0	84.0	0.0119	0.0119	-0.3025	0.1691	0.1691	84.0	0.0119	0.0119	-0.3025	0.1691	0.1691	0.1691	0.1691	0.1691	0.1691
	-0.3444	-0.3444		72.5	-0.2151	-0.2151	-0.4596	0.0285	0.0285	72.5	-0.2151	-0.2151	-0.4596	0.0285	0.0285	0.0285	0.0285	0.0285	0.0285
	-0.2800	-0.2800		54.0	-0.2151	-0.2151	-0.4596	-0.2151	-0.2151	54.0	-0.2151	-0.2151	-0.4596	-0.2151	-0.2151	-0.2151	-0.2151	-0.2151	-0.2151
	-0.2800	-0.2800		33.0	-0.2151	-0.2151	-0.4596	-0.2151	-0.2151	33.0	-0.2151	-0.2151	-0.4596	-0.2151	-0.2151	-0.2151	-0.2151	-0.2151	-0.2151
	-0.3198	-0.3198		24.0	0.0772	-0.0920	0.0920	0.0772	0.0772	24.0	0.0772	-0.0920	0.0920	0.0772	0.0772	0.0772	0.0772	0.0772	0.0772
	-0.2595	-0.2595		10.0	-0.0074	-0.0920	0.0920	-0.0074	-0.0074	10.0	-0.0074	-0.0920	0.0920	-0.0074	-0.0074	-0.0074	-0.0074	-0.0074	-0.0074
	-0.2595	-0.2595		5.0	0.2463	0.0772	-0.0074	0.1617	0.1617	5.0	0.2463	0.0772	-0.0074	0.1617	0.1617	0.1617	0.1617	0.1617	0.1617
	-0.2595	-0.2595		2.5	-0.0074	-0.0074	0.2463	0.1617	0.1617	2.5	-0.0074	-0.0074	0.2463	0.1617	0.1617	0.1617	0.1617	0.1617	0.1617

BASEPR = 8.1904
HGT RM
86.9890 0.371825E+06
CLTR CDTR
0.26 0.04

---TOP---
XLOC CP
38.2 -0.0869
43.4 -0.0869
50.4 -0.0869
56.1 -0.0869
62.5 -0.0225
68.7 -0.0869
76.9 -0.1512
83.4 -0.1512
89.4 -0.2151
95.4 -0.2151
101.1 -0.2151
---BOTTOM---
XLOC CP
38.2 -0.0869
43.4 -0.0869
50.4 -0.1512
56.1 -0.0869
62.5 -0.0869
68.7 -0.0869
76.9 -0.0869
83.4 -0.1512
89.4 -0.0869
95.4 -0.1512
101.1 -0.2156

---MISC---
NO. CP
1 -0.4596
2 -0.2151
3 -0.4596
4 -0.2151
5 -0.2151
6 -0.2151
7 -0.3549
8 -0.3025
9 -0.3025
10 -0.3025
11 -0.3025
12 -0.3025

TABLE A38. (Continued)

TABLE A35. (Concluded)

RUN:SEQ		PROPLULSIVE										WING / CANARD PRESSURES										PAGE	
267	5	CLAERO =	0.6999	CDAERO =	0.4505	DCLC =	0.0	CMJC	0.0	DWLC =	0.9673											8.1904	
ALPHA	12.00	PTOT	2139.62	PSTAT	2135.67	VEL	57.76	YAW	0.01	H/C	2.130											89.0825 0.386055E+06	
BETA	-0.01	CL	1.67	CD	-1.45	CM	-0.48	CROLL	0.00	CN	0.01											CLTR COTR	
																						0.87 0.24	
CANARD		WING										FUSELAGE										MISC.	
BP=3.375 BP=10.125		BP = 2 BP = 6 BP = 12 BP = 16 BP = 22										TOP										NO. CP	
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP		
0.0	-0.4416	0.0	-0.4416	0.0	-0.4416	0.0	-0.4416	0.0	-0.4416	0.0	-0.4416	0.0	-0.4416	0.0	-0.4416	0.0	-0.4416	0.0	-0.4416	0.0	-0.4416	1	-0.5233
2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2	0.2314
5.0	-0.4416	5.0	-0.4416	5.0	-0.4416	5.0	-0.4416	5.0	-0.4416	5.0	-0.4416	5.0	-0.4416	5.0	-0.4416	5.0	-0.4416	5.0	-0.4416	5.0	-0.4416	3	-1.2777
10.0	-0.3174	10.0	-0.3174	10.0	-0.3174	10.0	-0.3174	10.0	-0.3174	10.0	-0.3174	10.0	-0.3174	10.0	-0.3174	10.0	-0.3174	10.0	-0.3174	10.0	-0.3174	4	0.2314
15.0	-0.4416	15.0	-0.4416	15.0	-0.4416	15.0	-0.4416	15.0	-0.4416	15.0	-0.4416	15.0	-0.4416	15.0	-0.4416	15.0	-0.4416	15.0	-0.4416	15.0	-0.4416	5	-1.0262
25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	6	-0.0202
35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	7	-0.4694
50.0	-0.3795	50.0	-0.3795	50.0	-0.3795	50.0	-0.3795	50.0	-0.3795	50.0	-0.3795	50.0	-0.3795	50.0	-0.3795	50.0	-0.3795	50.0	-0.3795	50.0	-0.3795	8	-0.4694
65.0	-0.4416	65.0	-0.4416	65.0	-0.4416	65.0	-0.4416	65.0	-0.4416	65.0	-0.4416	65.0	-0.4416	65.0	-0.4416	65.0	-0.4416	65.0	-0.4416	65.0	-0.4416	9	-0.4694
75.0	-0.4416	75.0	-0.4416	75.0	-0.4416	75.0	-0.4416	75.0	-0.4416	75.0	-0.4416	75.0	-0.4416	75.0	-0.4416	75.0	-0.4416	75.0	-0.4416	75.0	-0.4416	10	-0.4694
80.5	-0.4029	80.5	-0.4029	80.5	-0.4029	80.5	-0.4029	80.5	-0.4029	80.5	-0.4029	80.5	-0.4029	80.5	-0.4029	80.5	-0.4029	80.5	-0.4029	80.5	-0.4029	11	-0.4155
81.0	-0.2238	81.0	-0.2238	81.0	-0.2238	81.0	-0.2238	81.0	-0.2238	81.0	-0.2238	81.0	-0.2238	81.0	-0.2238	81.0	-0.2238	81.0	-0.2238	81.0	-0.2238	12	-0.4155
84.0	-0.3581	84.0	-0.3581	84.0	-0.3581	84.0	-0.3581	84.0	-0.3581	84.0	-0.3581	84.0	-0.3581	84.0	-0.3581	84.0	-0.3581	84.0	-0.3581	84.0	-0.3581		
87.0	-0.3133	87.0	-0.3133	87.0	-0.3133	87.0	-0.3133	87.0	-0.3133	87.0	-0.3133	87.0	-0.3133	87.0	-0.3133	87.0	-0.3133	87.0	-0.3133	87.0	-0.3133		
89.0	-0.4047	89.0	-0.4047	89.0	-0.4047	89.0	-0.4047	89.0	-0.4047	89.0	-0.4047	89.0	-0.4047	89.0	-0.4047	89.0	-0.4047	89.0	-0.4047	89.0	-0.4047		
93.0	-0.4047	93.0	-0.4047	93.0	-0.4047	93.0	-0.4047	93.0	-0.4047	93.0	-0.4047	93.0	-0.4047	93.0	-0.4047	93.0	-0.4047	93.0	-0.4047	93.0	-0.4047		
96.0	-0.3385	96.0	-0.3385	96.0	-0.3385	96.0	-0.3385	96.0	-0.3385	96.0	-0.3385	96.0	-0.3385	96.0	-0.3385	96.0	-0.3385	96.0	-0.3385	96.0	-0.3385		
100.0	-0.4047	100.0	-0.4047	100.0	-0.4047	100.0	-0.4047	100.0	-0.4047	100.0	-0.4047	100.0	-0.4047	100.0	-0.4047	100.0	-0.4047	100.0	-0.4047	100.0	-0.4047		
96.0	-0.4047	96.0	-0.4047	96.0	-0.4047	96.0	-0.4047	96.0	-0.4047	96.0	-0.4047	96.0	-0.4047	96.0	-0.4047	96.0	-0.4047	96.0	-0.4047	96.0	-0.4047		
73.0	-0.3385	73.0	-0.3385	73.0	-0.3385	73.0	-0.3385	73.0	-0.3385	73.0	-0.3385	73.0	-0.3385	73.0	-0.3385	73.0	-0.3385	73.0	-0.3385	73.0	-0.3385		
50.0	-0.4047	50.0	-0.4047	50.0	-0.4047	50.0	-0.4047	50.0	-0.4047	50.0	-0.4047	50.0	-0.4047	50.0	-0.4047	50.0	-0.4047	50.0	-0.4047	50.0	-0.4047		
35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	35.0	-0.5036	35.0	-0.5036		
25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	25.0	-0.4416	25.0	-0.4416		
10.0	-0.3795	10.0	-0.3795	10.0	-0.3795	10.0	-0.3795	10.0	-0.3795	10.0	-0.3795	10.0	-0.3795	10.0	-0.3795	10.0	-0.3795	10.0	-0.3795	10.0	-0.3795		
5.0	-0.3795	5.0	-0.3795	5.0	-0.3795	5.0	-0.3795	5.0	-0.3795	5.0	-0.3795	5.0	-0.3795	5.0	-0.3795	5.0	-0.3795	5.0	-0.3795	5.0	-0.3795		
2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2.5	-0.3795	2.5	-0.3795		

TABLE A36. (Continued)

RUN: SEQ		CLAERO = 0.3537		CD AERO = 0.3537		PROPLULSIVE		WING / CANARD		PRESSURES		BASEPR = 8.1804		PAGE 942	
271 4		PTOT		PSTAT		Q		VEL		VAV		HGT		RM	
4.02		2139.13		2109.07		30.06		160.44		0.01		86.9525		0.996487E+06	
BETA		CL		CD		CM		CROLL		CN		CLTR		CDTR	
-0.01		0.35		0.08		-0.07		0.00		-0.00		0.35		0.11	
***** CANARD *****		BP=3.375		BP=10.125		***** WING *****		BP = 2		BP = 6		BP = 12		BP = 16	
XX/C		CP		CP		XX/C		CP		CP		CP		CP	
0.0	0.3610	0.1241	0.0	0.4599	0.3340	0.0	0.4599	0.3340	-0.0095	-0.4102	-0.5705	-0.4102	-0.5705	-0.4102	-0.5705
2.5	-0.5375	-0.8152	2.5	-0.2042	-0.4217	2.5	-0.2042	-0.4217	-0.7652	-0.7766	-0.9713	-0.7652	-0.7766	-0.9713	-0.9713
5.0	-0.4477	-0.6845	5.0	-0.2385	-0.3988	5.0	-0.2385	-0.3988	-0.5019	-0.6278	-0.8965	-0.5019	-0.6278	-0.8965	-0.8965
10.0	0.9062	-0.5048	10.0	-0.1927	-0.3873	10.0	-0.1927	-0.3873	-0.4675	-0.4789	-0.5133	-0.4675	-0.4789	-0.5133	-0.5133
15.0	-0.4231	-0.4395	15.0	-0.2958	-0.3186	15.0	-0.2958	-0.3186	-0.4217	-0.4560	-0.4446	-0.4217	-0.4560	-0.4446	-0.4446
25.0	-0.3415	-0.3495	25.0	-0.2495	-0.3072	25.0	-0.2495	-0.3072	-0.3415	-0.3415	-0.3645	-0.3415	-0.3415	-0.3645	-0.3645
35.0	-0.2435	-0.2353	35.0	-0.2267	-0.2598	35.0	-0.2267	-0.2598	-0.2929	-0.2929	-0.2929	-0.2929	-0.2929	-0.2929	-0.2929
50.0	-0.2516	-0.2190	50.0	-0.1936	-0.2598	50.0	-0.1936	-0.2598	-0.2929	-0.2929	-0.2929	-0.2929	-0.2929	-0.2929	-0.2929
56.0	-0.2190	-0.2680	56.0	-0.2598	-0.3004	56.0	-0.2598	-0.3004	-0.3353	-0.3179	-0.3179	-0.3353	-0.3179	-0.3179	-0.3179
65.0	-0.1945	-0.3496	65.0	-0.4347	-0.4046	65.0	-0.4347	-0.4046	-0.3789	-0.3789	-0.3789	-0.3789	-0.3789	-0.3789	-0.3789
76.0	-0.4395	-0.4347	76.0	-0.4347	-0.4046	76.0	-0.4347	-0.4046	-0.3789	-0.3789	-0.3789	-0.3789	-0.3789	-0.3789	-0.3789
79.0	-0.4395	-0.4347	79.0	-0.4347	-0.4046	79.0	-0.4347	-0.4046	-0.3789	-0.3789	-0.3789	-0.3789	-0.3789	-0.3789	-0.3789
80.5	-0.4347	-0.4347	80.5	-0.4347	-0.4046	80.5	-0.4347	-0.4046	-0.3789	-0.3789	-0.3789	-0.3789	-0.3789	-0.3789	-0.3789
81.0	-0.4288	-0.4288	81.0	-0.4288	-0.4288	81.0	-0.4288	-0.4288	-0.4288	-0.4288	-0.4288	-0.4288	-0.4288	-0.4288	-0.4288
82.0	-0.4111	-0.4111	82.0	-0.4111	-0.4111	82.0	-0.4111	-0.4111	-0.4111	-0.4111	-0.4111	-0.4111	-0.4111	-0.4111	-0.4111
84.0	-0.1753	-0.1753	84.0	-0.1753	-0.1753	84.0	-0.1753	-0.1753	-0.1753	-0.1753	-0.1753	-0.1753	-0.1753	-0.1753	-0.1753
87.0	-0.1576	-0.1576	87.0	-0.1576	-0.1576	87.0	-0.1576	-0.1576	-0.1576	-0.1576	-0.1576	-0.1576	-0.1576	-0.1576	-0.1576
89.0	-0.1523	-0.1523	89.0	-0.1523	-0.1523	89.0	-0.1523	-0.1523	-0.1523	-0.1523	-0.1523	-0.1523	-0.1523	-0.1523	-0.1523
93.0	-0.1349	-0.1349	93.0	-0.1349	-0.1349	93.0	-0.1349	-0.1349	-0.1349	-0.1349	-0.1349	-0.1349	-0.1349	-0.1349	-0.1349
96.0	-0.1000	-0.1000	96.0	-0.1000	-0.1000	96.0	-0.1000	-0.1000	-0.1000	-0.1000	-0.1000	-0.1000	-0.1000	-0.1000	-0.1000
100.0	0.6930	0.6930	100.0	0.6930	0.6930	100.0	0.6930	0.6930	0.6930	0.6930	0.6930	0.6930	0.6930	0.6930	0.6930
96.0	0.1091	0.1091	96.0	0.1091	0.1091	96.0	0.1091	0.1091	0.1091	0.1091	0.1091	0.1091	0.1091	0.1091	0.1091
84.0	0.6930	0.6930	84.0	0.6930	0.6930	84.0	0.6930	0.6930	0.6930	0.6930	0.6930	0.6930	0.6930	0.6930	0.6930
73.0	0.1091	0.1091	73.0	0.1091	0.1091	73.0	0.1091	0.1091	0.1091	0.1091	0.1091	0.1091	0.1091	0.1091	0.1091
50.0	0.1786	0.1786	50.0	0.1786	0.1786	50.0	0.1786	0.1786	0.1786	0.1786	0.1786	0.1786	0.1786	0.1786	0.1786
35.0	0.0016	0.0016	35.0	0.0016	0.0016	35.0	0.0016	0.0016	0.0016	0.0016	0.0016	0.0016	0.0016	0.0016	0.0016
25.0	-0.1209	-0.1209	25.0	-0.1209	-0.1209	25.0	-0.1209	-0.1209	-0.1209	-0.1209	-0.1209	-0.1209	-0.1209	-0.1209	-0.1209
10.0	-0.0883	-0.0883	10.0	-0.0883	-0.0883	10.0	-0.0883	-0.0883	-0.0883	-0.0883	-0.0883	-0.0883	-0.0883	-0.0883	-0.0883
5.0	-0.1454	-0.1454	5.0	-0.1454	-0.1454	5.0	-0.1454	-0.1454	-0.1454	-0.1454	-0.1454	-0.1454	-0.1454	-0.1454	-0.1454
2.5	0.0996	0.0996	2.5	0.0996	0.0996	2.5	0.0996	0.0996	0.0996	0.0996	0.0996	0.0996	0.0996	0.0996	0.0996

TABLE A36. (Concluded)

RUN: SEQ										PAGE 644									
271	6	CLARO =	0.8522	CDAERO =	0.2007	WING / CANARD	PRESSURES	BASEPR =	8.1904										
ALPHA	12.07	PTOT	2138.99	PSTAT	2108.93	VEL	H/C	CMJC	CMW	CMUT									
BETA	-0.01	CL	0.85	CD	0.20	CROLL	CM	CY	CNTR	CMTR									

TABLE A37. RUN 272, BC1W6V, DELF-O, CMJ-O.5, (BN/B)W-O.25

RUN: SEQ										PAGE 645									
272	1	CLAERO	=	0.2138	CDAERO	=	0.1794	DCLC	=	0.0491	DWLC	=	0.1273	BASEPR = 8.1904					
ALPHA	0.03	PTOT	2138.77	PSTAT	0	VEL	126.58	YAW	H/C	CMJC	CMJW	CMJW	CMJW	HGT	RM	87.0914 0.787667E+08			
BETA	-0.01	CL	0.39	CD	-0.57	CM	-0.19	CROLL	CN	CV	CNTR	CNTR	CNTR	CLTR	CDTR	0.22 0.15			
***** CANARD *****										***** FUSELAGE *****									
X/C		BP=3.375		BP=10.125		BP=2		BP=6		BP=12		BP=16		BP=22		***** TOP *****			
CP		CP		CP		CP		CP		CP		CP		CP		***** BOTTOM *****			
0.0	0.4001	0.0	0.5179	0.0	0.2683	0.0	0.3234	0.0	0.4334	0.0	0.4885	0.0	0.4885	0.0	0.4885	XLOC	CP	NO.	CP
2.5	-0.0448	2.5	-0.1365	2.5	-0.3187	2.5	-0.3050	2.5	-0.0819	2.5	-0.1903	2.5	-0.2821	2.5	-0.2821	38.2	-0.1568	1	-0.2708
5.0	-0.1234	5.0	-0.1888	5.0	-0.4518	5.0	-0.1768	5.0	-0.1553	5.0	-0.2086	5.0	-0.2454	5.0	-0.2454	43.4	-0.1429	2	-0.1117
10.0	0.8844	10.0	0.2150	10.0	-0.3004	10.0	-0.0352	10.0	-0.2637	10.0	-0.2454	10.0	-0.2821	10.0	-0.2821	50.4	-0.0731	3	-0.2178
15.0	-0.2673	15.0	-0.2542	15.0	-0.0436	15.0	-0.1536	15.0	-0.2454	15.0	-0.2454	15.0	-0.2821	15.0	-0.2821	56.1	-0.0581	4	-0.1117
20.0	-0.2412	20.0	-0.2281	20.0	-0.1720	20.0	-0.2066	20.0	-0.2454	20.0	-0.2454	20.0	-0.2821	20.0	-0.2821	62.5	-0.0462	5	-0.2178
25.0	-0.2281	25.0	-0.2281	25.0	-0.1647	25.0	-0.2178	25.0	-0.2178	25.0	-0.2178	25.0	-0.2178	25.0	-0.2178	69.7	-0.0731	6	-0.1647
30.0	-0.2542	30.0	-0.2542	30.0	-0.1647	30.0	-0.2178	30.0	-0.2178	30.0	-0.2178	30.0	-0.2178	30.0	-0.2178	76.9	-0.0581	7	-0.3618
35.0	-0.2804	35.0	-0.2804	35.0	-0.3106	35.0	-0.1478	35.0	-0.2708	35.0	-0.2708	35.0	-0.2708	35.0	-0.2708	83.4	-0.0731	8	-0.3618
40.0	-0.3851	40.0	-0.3851	40.0	-0.4374	40.0	-1.3717	40.0	-0.3943	40.0	-0.3244	40.0	-0.2821	40.0	-0.2821	89.4	-0.1568	9	-0.5391
45.0	-0.3066	45.0	-0.3066	45.0	-0.7778	45.0	-1.3717	45.0	-0.6177	45.0	-0.4840	45.0	-0.3683	45.0	-0.3683	95.4	-0.2367	10	-0.3618
50.0	-1.1835	50.0	-1.2489	50.0	-1.2489	50.0	-1.2489	50.0	-1.2489	50.0	-1.2489	50.0	-1.2489	50.0	-1.2489	101.1	-0.2127	11	-0.3618
55.0	-17.6854	55.0	-25.5552	55.0	-25.5552	55.0	-25.5552	55.0	-25.5552	55.0	-25.5552	55.0	-25.5552	55.0	-25.5552	---	---	12	-0.3504
60.0	0.3220	60.0	6.4630	60.0	6.4630	60.0	6.4630	60.0	6.4630	60.0	6.4630	60.0	6.4630	60.0	6.4630	---	---	---	---
65.0	0.3031	65.0	-0.6890	65.0	-0.6890	65.0	-0.6890	65.0	-0.6890	65.0	-0.6890	65.0	-0.6890	65.0	-0.6890	---	---	---	---
70.0	0.2086	70.0	0.2086	70.0	0.2086	70.0	0.2086	70.0	0.2086	70.0	0.2086	70.0	0.2086	70.0	0.2086	---	---	---	---
75.0	1.5123	75.0	1.5123	75.0	1.5123	75.0	1.5123	75.0	1.5123	75.0	1.5123	75.0	1.5123	75.0	1.5123	---	---	---	---
80.0	0.2341	80.0	0.2341	80.0	0.2341	80.0	0.2341	80.0	0.2341	80.0	0.2341	80.0	0.2341	80.0	0.2341	---	---	---	---
85.0	0.4715	85.0	0.4715	85.0	0.4715	85.0	0.4715	85.0	0.4715	85.0	0.4715	85.0	0.4715	85.0	0.4715	---	---	---	---
90.0	1.1977	90.0	1.1977	90.0	1.1977	90.0	1.1977	90.0	1.1977	90.0	1.1977	90.0	1.1977	90.0	1.1977	---	---	---	---
95.0	0.3878	95.0	-1.5812	95.0	-1.5812	95.0	-1.5812	95.0	-1.5812	95.0	-1.5812	95.0	-1.5812	95.0	-1.5812	---	---	---	---
100.0	-0.0671	100.0	-0.0452	100.0	-0.0452	100.0	-0.0452	100.0	-0.0452	100.0	-0.0452	100.0	-0.0452	100.0	-0.0452	---	---	---	---
105.0	0.3078	105.0	-1.5812	105.0	-1.5812	105.0	-1.5812	105.0	-1.5812	105.0	-1.5812	105.0	-1.5812	105.0	-1.5812	---	---	---	---
110.0	-0.0871	110.0	-0.0452	110.0	-0.0452	110.0	-0.0452	110.0	-0.0452	110.0	-0.0452	110.0	-0.0452	110.0	-0.0452	---	---	---	---
115.0	0.0945	115.0	0.0945	115.0	0.0945	115.0	0.0945	115.0	0.0945	115.0	0.0945	115.0	0.0945	115.0	0.0945	---	---	---	---
120.0	-0.0448	120.0	-0.0710	120.0	-0.0710	120.0	-0.0710	120.0	-0.0710	120.0	-0.0710	120.0	-0.0710	120.0	-0.0710	---	---	---	---
125.0	-0.2019	125.0	-0.3851	125.0	-0.3851	125.0	-0.3851	125.0	-0.3851	125.0	-0.3851	125.0	-0.3851	125.0	-0.3851	---	---	---	---
130.0	-0.1888	130.0	-0.2019	130.0	-0.2019	130.0	-0.2019	130.0	-0.2019	130.0	-0.2019	130.0	-0.2019	130.0	-0.2019	---	---	---	---
135.0	-0.2673	135.0	-0.2673	135.0	-0.2673	135.0	-0.2673	135.0	-0.2673	135.0	-0.2673	135.0	-0.2673	135.0	-0.2673	---	---	---	---
140.0	-0.3066	140.0	-0.3066	140.0	-0.3066	140.0	-0.3066	140.0	-0.3066	140.0	-0.3066	140.0	-0.3066	140.0	-0.3066	---	---	---	---
145.0	2.5	145.0	2.5	145.0	2.5	145.0	2.5	145.0	2.5	145.0	2.5	145.0	2.5	145.0	2.5	---	---	---	---

TABLE A37. (Continued)

TABLE A37. (Concluded)

RUN: SEQ															PAGE 649														
272	13	CLARO =	0.9372	CDARO =	0.3358	WING / CANARD	PRESSURES	BASEPR =	8.1904	HGT	89.2004	0.770235E+06	CLTR	0.97	0.22														
ALPHA	12.14	PTOT	2138.35	PSTAT	2120.38	17.97	123.92	0.01	2.73	0.290	0.506	0.797	CMUT	-0.03															
BETA	-0.01	CL	1.28	CD	-0.38	CM	-0.08	-0.00	-0.01	0.02	0.99	-0.03																	
***** CANARD *****																													
XX/C	0.0	BP = 2	BP = 6	BP = 12	BP = 16	BP = 22																							
CP	-2.3869	CP	-0.4271	CP	-0.2816	CP	-3.1546	CP	-1.6606	CP	-1.4499	CP	-1.3925	CP	-1.3268	CP	-1.2733	CP	-1.2392										
5.0	-1.9770	5.0	-0.3007	5.0	-0.6648	5.0	-1.1826	5.0	-0.9902	5.0	-0.8753	5.0	-0.8178	5.0	-0.7655	5.0	-0.7228	5.0	-0.6896										
10.0	-1.8813	10.0	-0.3773	10.0	-0.6838	10.0	-0.8178	10.0	-0.6041	10.0	-0.5144	10.0	-0.4383	10.0	-0.3688	10.0	-0.3088	10.0	-0.2588										
15.0	-1.7447	15.0	-0.5306	15.0	-0.8838	15.0	-0.6071	15.0	-0.4934	15.0	-0.3939	15.0	-0.3136	15.0	-0.2440	15.0	-0.1845	15.0	-0.1342										
25.0	-1.7993	25.0	-0.5497	25.0	-0.8971	25.0	-0.6041	25.0	-0.4934	25.0	-0.3939	25.0	-0.3136	25.0	-0.2440	25.0	-0.1845	25.0	-0.1342										
35.0	-1.4031	35.0	-0.5488	35.0	-0.8971	35.0	-0.6041	35.0	-0.4934	35.0	-0.3939	35.0	-0.3136	35.0	-0.2440	35.0	-0.1845	35.0	-0.1342										
50.0	-0.5559	50.0	-0.5144	50.0	-0.7623	50.0	-0.5280	50.0	-0.4186	50.0	-0.3388	50.0	-0.2744	50.0	-0.2244	50.0	-0.1845	50.0	-0.1446										
65.0	-0.6104	65.0	-0.5144	65.0	-0.7623	65.0	-0.5280	65.0	-0.4186	65.0	-0.3388	65.0	-0.2744	65.0	-0.2244	65.0	-0.1845	65.0	-0.1446										
76.0	-0.3920	76.0	-0.5144	76.0	-0.7623	76.0	-0.5280	76.0	-0.4186	76.0	-0.3388	76.0	-0.2744	76.0	-0.2244	76.0	-0.1845	76.0	-0.1446										
79.0	-1.2391	79.0	-0.5144	79.0	-0.7623	79.0	-0.5280	79.0	-0.4186	79.0	-0.3388	79.0	-0.2744	79.0	-0.2244	79.0	-0.1845	79.0	-0.1446										
80.5	-19.3366	80.5	-0.5144	80.5	-0.7623	80.5	-0.5280	80.5	-0.4186	80.5	-0.3388	80.5	-0.2744	80.5	-0.2244	80.5	-0.1845	80.5	-0.1446										
81.0	1.1598	81.0	-0.5144	81.0	-0.7623	81.0	-0.5280	81.0	-0.4186	81.0	-0.3388	81.0	-0.2744	81.0	-0.2244	81.0	-0.1845	81.0	-0.1446										
82.0	0.5875	82.0	-0.5144	82.0	-0.7623	82.0	-0.5280	82.0	-0.4186	82.0	-0.3388	82.0	-0.2744	82.0	-0.2244	82.0	-0.1845	82.0	-0.1446										
84.0	0.0748	84.0	-0.5144	84.0	-0.7623	84.0	-0.5280	84.0	-0.4186	84.0	-0.3388	84.0	-0.2744	84.0	-0.2244	84.0	-0.1845	84.0	-0.1446										
87.0	1.4555	87.0	-0.5144	87.0	-0.7623	87.0	-0.5280	87.0	-0.4186	87.0	-0.3388	87.0	-0.2744	87.0	-0.2244	87.0	-0.1845	87.0	-0.1446										
89.0	0.1416	89.0	-0.5144	89.0	-0.7623	89.0	-0.5280	89.0	-0.4186	89.0	-0.3388	89.0	-0.2744	89.0	-0.2244	89.0	-0.1845	89.0	-0.1446										
93.0	0.3749	93.0	-0.5144	93.0	-0.7623	93.0	-0.5280	93.0	-0.4186	93.0	-0.3388	93.0	-0.2744	93.0	-0.2244	93.0	-0.1845	93.0	-0.1446										
96.0	1.1184	96.0	-0.5144	96.0	-0.7623	96.0	-0.5280	96.0	-0.4186	96.0	-0.3388	96.0	-0.2744	96.0	-0.2244	96.0	-0.1845	96.0	-0.1446										
100.0	0.8560	100.0	-0.5144	100.0	-0.7623	100.0	-0.5280	100.0	-0.4186	100.0	-0.3388	100.0	-0.2744	100.0	-0.2244	100.0	-0.1845	100.0	-0.1446										
84.0	-0.0042	84.0	-0.5144	84.0	-0.7623	84.0	-0.5280	84.0	-0.4186	84.0	-0.3388	84.0	-0.2744	84.0	-0.2244	84.0	-0.1845	84.0	-0.1446										
73.0	0.8560	73.0	-0.5144	73.0	-0.7623	73.0	-0.5280	73.0	-0.4186	73.0	-0.3388	73.0	-0.2744	73.0	-0.2244	73.0	-0.1845	73.0	-0.1446										
50.0	-0.0042	50.0	-0.5144	50.0	-0.7623	50.0	-0.5280	50.0	-0.4186	50.0	-0.3388	50.0	-0.2744	50.0	-0.2244	50.0	-0.1845	50.0	-0.1446										
35.0	0.0863	35.0	-0.5144	35.0	-0.7623	35.0	-0.5280	35.0	-0.4186	35.0	-0.3388	35.0	-0.2744	35.0	-0.2244	35.0	-0.1845	35.0	-0.1446										
25.0	0.0316	25.0	-0.5144	25.0	-0.7623	25.0	-0.5280	25.0	-0.4186	25.0	-0.3388	25.0	-0.2744	25.0	-0.2244	25.0	-0.1845	25.0	-0.1446										
10.0	0.1546	10.0	-0.5144	10.0	-0.7623	10.0	-0.5280	10.0	-0.4186	10.0	-0.3388	10.0	-0.2744	10.0	-0.2244	10.0	-0.1845	10.0	-0.1446										
5.0	0.1408	5.0	-0.5144	5.0	-0.7623	5.0	-0.5280	5.0	-0.4186	5.0	-0.3388	5.0	-0.2744	5.0	-0.2244	5.0	-0.1845	5.0	-0.1446										
2.5	0.5782	2.5	-0.5144	2.5	-0.7623	2.5	-0.5280	2.5	-0.4186	2.5	-0.3388	2.5	-0.2744	2.5	-0.2244	2.5	-0.1845	2.5	-0.1446										
***** FUSELAGE *****																													
XX/C	0.0	BP = 2	BP = 6	BP = 12	BP = 16	BP = 22																							
CP	-2.3869	CP	-0.4271	CP	-0.2816	CP	-3.1546	CP	-1.6606	CP	-1.4499	CP	-1.3925	CP	-1.3268	CP	-1.2733	CP	-1.2392										
5.0	-1.9770	5.0	-0.3007	5.0	-0.6648	5.0	-1.1826	5.0	-0.9902	5.0	-0.8753	5.0	-0.8178	5.0	-0.7655	5.0	-0.7228	5.0	-0.6896										
10.0	-1.8813	10.0	-0.3773	10.0	-0.6838	10.0	-0.8178	10.0	-0.6041	10.0	-0.5144	10.0	-0.4383	10.0	-0.3688	10.0	-0.3088	10.0	-0.2588										
15.0	-1.7447	15.0	-0.5306	15.0	-0.8838	15.0	-0.6071	15.0	-0.4934	15.0	-0.3939	15.0	-0.3136	15.0	-0.2440	15.0	-0.1845	15.0	-0.1342										
25.0	-1.7993	25.0	-0.5497	25.0	-0.8971	25.0	-0.6041	25.0	-0.4934	25.0	-0.3939	25.0	-0.3136	25.0	-0.2440	25.0	-0.1845	25.0	-0.1342										
35.0	-1.4031	35.0	-0.5488	35.0	-0.8971	35.0	-0.6041	35.0	-0.4934	35.0	-0.3939	35.0	-0.3136	35.0	-0.2440	35.0	-0.1845	35.0	-0.1342										
50.0	-0.5559	50.0	-0.5144	50.0	-0.7623	50.0	-0.5280	50.0	-0.4186	50.0	-0.3388	50.0	-0.2744	50.0	-0.2244	50.0	-0.1845	50.0	-0.1446										
65.0	-0.6104	65.0	-0.5144	65.0	-0.7623	65.0	-0.5280	65.0	-0.4186	65.0	-0.3388	65.0	-0.2744	65.0	-0.2244	65.0	-0.1845	65.0	-0.1446										
76.0	-0.3920	76.0	-0.5144	76.0	-0.7623	76.0	-0.5280	76.0	-0.4186	76.0	-0.3388	76.0	-0.2744	76.0	-0.2244	76.0	-0.1845	76.0	-0.1446										
79.0	-1.2391	79.0	-0.5144	79.0	-0.7623	79.0	-0.5280	79.0	-0.4186	79.0	-0.3388	79.0	-0.2744	79.0	-0.2244	79.0	-0.1845	79.0	-0.1446										
80.5	-19.3366	80.5	-0.5144	80.5	-0.7623	80.5	-0.5280	80.5	-0.4186	80.5	-0.3388	80.5	-0.2744	80.5	-0.2244	80.5	-0.1845	80.5	-0.1446										
81.0	1.1598	81.0	-0.5144	81.0	-0.7623	81.0	-0.5280	81.0	-0.4186	81.0	-0.3388	81.0	-0.2744	81.0	-0.2244	81.0	-0.1845	81.0	-0.1446										
82.0	0.5875	82.0	-0.5144	82.0	-0.7623	82.0	-0.5280	82.0	-0.4186	82.0	-0.3388	82.0	-0.2744	82.0	-0.2244	82.0	-0.1845	82.0	-0.1446										
84.0	0.0748	84.0	-0.5144	84.0	-0.7623	84.0	-0.5280	84.0	-0.4186	84.0	-0.3388	84.0	-0.2744	84.0	-0.2244	84.0	-0.1845	84.0	-0.1446										
87.0	1.4555	87.0	-0.5144	87.0	-0.7623	87.0	-0.5280	87.0	-0.4186	87.0	-0.3388	87.0	-0.2744	87.0	-0.2244	87.0	-0.1845	87.0	-0.1446										
89.0	0.1416	89.0	-0.5144	89.0	-0.7623	89.0	-0.5280	89.0	-0.4186	89.0	-0.3388	89.0	-0.2744	89.0	-0.2244	89.0	-0.1845	89.0	-0.1446										
93.0	0.3749	93.0	-0.5144	93.0	-0.7623	93.0	-0.5280	93.0	-0.4186	93.0	-0.3388	93.0	-0.2744	93.0	-0.2244	93.0	-0.1845	93.0	-0.1446										
96.0	1.1184	96.0	-0.5144	96.0	-0.7623	96.0	-0.5280	96.0	-0.4186	96.0	-0.3388	96.0	-0.2744	96.0	-0.2244	96.0	-0.1845	96.0	-0.1446										
100.0	0.8560	100.0	-0.5144	100.0	-0.7623	100.0	-0.5280	100.0	-0.4186	100.0	-0.3388	100.0	-0.2744	100.0	-0.2244	100.0	-0.1845	100.0	-0.1446										
84.0	-0.0042	84.0	-0.5144	84.0	-0.7623	84.0	-0.5280	84.0	-0.4186	84.0	-0.3388	84.0	-0.2744	84.0	-0.2244	84.0	-0.1845	84.0	-0.1446										
73.0	0.8560	73.0	-0.5144	73.0	-0.7623	73.0	-0.5280	73.0	-0.4186	73.0	-0.3388	73.0	-0.2744	73.0	-0.2244	73.0	-0.1845	73.0	-0.1446										
50.0	-0.0042	50.0	-0.5144	50.0	-0.7623	50.0	-0.5280	50.0	-0.4186	50.0	-0.3388	50.0	-0.2744	50.0	-0.2244	50.0	-0.1845	50.0	-0.1446										
35.0	0.0863	35.0	-0.5144	35.0	-0.7623	35.0	-0.5280	35.0	-0.4186	35.0	-0.3388	35.0	-0.2744	35.0	-0.2244	35.0	-0.1845	35.0	-0.1446										
25.0	0.0316	25.0	-0.5144	25.0	-0.7623	25.0	-0.5280	25.0	-0.4186	25.0	-0.3388	25.0	-0.2744	25.0	-0.2244	25.0	-0.1845	25.0	-0.1446										
10.0	0.1546	10.0	-0.5144	10.0	-0.7623	10.0	-0.5280	10.0	-0.4186	10.0	-0.3388	10.0	-0.2744	10.0	-0.2244	10.0	-0.1845	10.0	-0.1446										
5.0	0.1408	5.0	-0.5144	5.0	-0.7623	5.0	-0.5280	5.0	-0.4186	5.0	-0.3388	5.0	-0.2744	5.0	-0.2244	5.0	-0.1845	5.0	-0.1446										

TABLE A38. RUN 273, BC1W6V, DELF=0, CMU=1.0, (BN/8)W=0.25

PROPULSIVE										WING / CANARD PRESSURES										BASEPR = 8.1904										PAGE 850																																																																																																													
CDAERO = 0.2216										DCLC = 0.1037										DMLC = 0.2683										HOT																																																																																																													
PSTAT										VEL										YAW										H/C										CMUW										CMUT																																																																																									
2128.35										9.04										87.76										0.01										2.66										0.594										1.033																																																																															
BETA										CL										CM										CIVOLL										CN										CV										CMTR										O.08																																																																					
-0.01										-0.30										0.00										-0.00										0.02										0.24										-0.20																																																																															

TABLE A33. (Continued)

RUN: SEQ											
273	3	CLAERO = 0.4296		CDALERO = 0.3226		DCLC = 0.1441		DMLC = 0.3350		BASEPR = 8.1904	
ALPHA		PTOT		Q		VEL		YAW		H/C	
4.02	2138.35	2129.31		0.04		87.73		0.01		2.66	
BETA	CL	CD		CROLL		CN		CY		CMTR	
-0.01	0.91	-1.23		-0.25		0.00		-0.01		0.47	
***** CANARD *****											
BP=3.375		BP=10.125		BP=2		BP=6		BP=12		BP=16	
CP		CP		CP		CP		CP		CP	
0.4633	-0.0797	0.0	-0.0974	0.2451	0.1690	-0.3258	-0.4019	-0.3258	-0.4019	-0.3258	-0.4019
-0.8771	-1.0300	2.5	-0.4400	0.5877	0.5923	-0.7825	-1.0109	-0.7825	-1.0109	-0.7825	-1.0109
5.0	-0.5685	5.0	1.1967	0.2832	-0.5161	-0.6303	-0.8206	-0.6303	-0.8206	-0.6303	-0.8206
10.0	2.7712	10.0	-0.6771	-0.1736	-0.5541	-0.5161	-0.6683	-0.5541	-0.6683	-0.5161	-0.6683
15.0	-0.5685	15.0	-0.1355	-0.3258	-0.5161	-0.4400	-0.5841	-0.5161	-0.4400	-0.5841	-0.5841
20.0	-0.8771	20.0	-0.5142	-0.4019	-0.4780	-0.3639	-0.4400	-0.4780	-0.3639	-0.4400	-0.4400
25.0	-0.4870	25.0	-0.3784	-0.3141	-0.5342	-0.4242	-0.3141	-0.5342	-0.4242	-0.3141	-0.3141
30.0	-0.4327	30.0	-0.3141	-0.4242	-0.5342	-0.4242	-0.3141	-0.5342	-0.4242	-0.3141	-0.3141
35.0	-0.4599	35.0	-0.4712	-0.9026	-0.8581	-0.4422	-0.4422	-0.8581	-0.4422	-0.4422	-0.4422
40.0	-0.8771	40.0	2.1073	-2.3832	-0.8767	-0.5871	-0.5001	-0.8767	-0.5871	-0.5001	-0.5001
45.0	-0.4870	45.0	75.5131	9177	136.5406	5.0245	26.1734	176.6027	101.1	-0.3263	176.6027
50.0	-1.2744	50.0	80.586	2232	-91.7430	-0.3656	-0.6401	-2.7374	-2.7374	-0.3263	-2.7374
55.0	-1.8719	55.0	81.316	9874	150.0442	-0.4245	-0.4048	-0.4245	-0.4048	-0.4245	-0.4048
60.0	-39.2922	60.0	82.066	9818	-13.8111	-0.4441	-0.4441	-0.4441	-0.4441	-0.4441	-0.4441
65.0	18.1176	65.0	84.0	4.9657	0.8104	-0.6989	-0.8753	-0.6989	-0.8753	-0.6989	-0.8753
70.0	-1.2281	70.0	87.0	-9.9307	-4.3836	-0.8753	-0.8753	-0.8753	-0.8753	-0.8753	-0.8753
75.0	3.3977	75.0	89.0	-22.3634	-2.1300	-0.8801	-0.8801	-0.8801	-0.8801	-0.8801	-0.8801
80.0	0.7167	80.0	93.0	7.0434	-1.2339	-0.8208	-0.8208	-0.8208	-0.8208	-0.8208	-0.8208
85.0	-2.2384	85.0	96.0	1.4544	-1.5641	-0.4321	-0.2906	-0.4321	-0.2906	-0.4321	-0.2906
90.0	0.3320	90.0	100.0	-3.6628	-2.5309	-0.2199	-0.1727	-0.2199	-0.1727	-0.2199	-0.1727
95.0	0.7746	95.0	96.0	-0.1963	-0.0312	0.1103	0.0631	0.1103	0.0631	0.1103	0.0631
100.0	-3.1075	100.0	98.0	0.6631	0.0159	-0.5029	0.1574	-0.5029	0.1574	-0.5029	0.1574
105.0	-0.1814	105.0	94.0	-0.0940	-0.5342	0.1261	-0.0940	0.1261	-0.0940	0.1261	-0.0940
110.0	-3.1075	110.0	73.0	-0.0940	-0.5342	0.1261	-0.0940	0.1261	-0.0940	0.1261	-0.0940
115.0	-0.2683	115.0	54.0	-0.0940	-0.5342	-0.0940	-0.0940	-0.0940	-0.0940	-0.0940	-0.0940
120.0	0.0214	120.0	33.0	-0.0940	-0.5342	-0.0940	-0.0940	-0.0940	-0.0940	-0.0940	-0.0940
125.0	-0.0797	125.0	24.0	-0.0940	-0.5342	-0.0940	-0.0940	-0.0940	-0.0940	-0.0940	-0.0940
130.0	-0.2155	130.0	10.0	-0.0974	-0.0974	-0.0593	-0.0593	-0.0593	-0.0593	-0.0593	-0.0593
135.0	-0.1884	135.0	5.0	-0.1736	-0.1355	0.0168	0.0168	0.0168	0.0168	0.0168	0.0168
140.0	-0.1884	140.0	2.5	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
145.0	0.2155	145.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
150.0	0.0561	150.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
155.0	0.0561	155.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
160.0	0.0561	160.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
165.0	0.0561	165.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
170.0	0.0561	170.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
175.0	0.0561	175.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
180.0	0.0561	180.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
185.0	0.0561	185.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
190.0	0.0561	190.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
195.0	0.0561	195.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
200.0	0.0561	200.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
205.0	0.0561	205.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
210.0	0.0561	210.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
215.0	0.0561	215.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
220.0	0.0561	220.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
225.0	0.0561	225.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
230.0	0.0561	230.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
235.0	0.0561	235.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
240.0	0.0561	240.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
245.0	0.0561	245.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
250.0	0.0561	250.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
255.0	0.0561	255.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
260.0	0.0561	260.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
265.0	0.0561	265.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
270.0	0.0561	270.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
275.0	0.0561	275.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
280.0	0.0561	280.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
285.0	0.0561	285.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
290.0	0.0561	290.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
295.0	0.0561	295.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
300.0	0.0561	300.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
305.0	0.0561	305.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
310.0	0.0561	310.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
315.0	0.0561	315.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
320.0	0.0561	320.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
325.0	0.0561	325.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
330.0	0.0561	330.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
335.0	0.0561	335.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
340.0	0.0561	340.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
345.0	0.0561	345.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
350.0	0.0561	350.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
355.0	0.0561	355.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
360.0	0.0561	360.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
365.0	0.0561	365.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
370.0	0.0561	370.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
375.0	0.0561	375.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
380.0	0.0561	380.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
385.0	0.0561	385.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
390.0	0.0561	390.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
395.0	0.0561	395.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
400.0	0.0561	400.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
405.0	0.0561	405.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
410.0	0.0561	410.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
415.0	0.0561	415.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
420.0	0.0561	420.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
425.0	0.0561	425.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
430.0	0.0561	430.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
435.0	0.0561	435.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	0.0548
440.0	0.0561	440.0	0.0	-0.2877	-0.2496	0.0548	0.0548	0.0548	0.0548	0.0548	

TABLE A38. (Concluded)

RUN: SEQ										PROPLUSIVE										WING / CANARD PRESSURES										BASEPR = 8.1904										PAGE 884									
273	6	CLAERO = 0.9809 CDAERO = 0.4274 DCLC = 0.2187 DWLC = 0.4573										HGT										89.2749 0.548478E+05										RN																	
ALPHA	12.06	PTOT 2136.26										VEL										CLTR 1.03										CDTR 0.22																	
BETA	-0.01	CL 1.66										CM																																					
		CD -1.01										CROLL																																					
		CN -0.16										CN																																					
		CY -0.00										CY																																					
		CNTR -0.01										CNTR																																					
		CMTR -0.05										CMTR																																					

TABLE A39. RUN 274, BC1W6V, DELF-O, CMU=2.0, (BN/6)W=0.25

RUN:SEQ										PAGE 655									
274	1	CLARO	-1.0788	CDARO	-0.3775	DCLC	-0.2193	DMLC	-1.8754	BASEPR	-8.1904								
ALPHA	0.01	PTOT	2138.21	PSTAT	4.29	VEL	60.38	YAW	H/C	CMUW	87.0442	BN	0.378549E+06						
BETA	0.01	CL	1.02	CD	-2.70	CM	-0.48	CROLL	CN	CY	CLTR	CDTR	0.04						
***** CANARD *****										***** FUSELAGE *****									
BP=3.375 BP=10.125										BP=2 BP=5 BP=12 BP=16 BP=22									
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP
0.0	0.3153	0.0	0.3724	0.0	-1.9637	0.0	-0.8419	0.0	0.2800	0.0	0.4403	0.0	0.3601	0.0	0.3889	0.0	0.3407	0.0	0.3889
2.5	-0.1992	2.5	-0.2564	2.5	-0.8419	2.5	-0.6840	2.5	0.4403	2.5	-0.2809	2.5	-0.5213	2.5	-0.1572	2.5	-0.3407	2.5	-0.1572
5.0	-0.3136	5.0	-0.4279	5.0	3.1648	5.0	1.5621	5.0	-0.2008	5.0	-0.3611	5.0	-0.6015	5.0	-0.3889	5.0	-0.2797	5.0	-0.3889
10.0	3.5735	10.0	3.5735	10.0	-0.8419	10.0	-0.4045	10.0	-0.2809	10.0	-0.2809	10.0	-0.5213	10.0	-0.1572	10.0	-0.1577	10.0	-0.1572
15.0	-0.4851	15.0	-0.5422	15.0	-0.2008	15.0	-0.3611	15.0	-0.5213	15.0	-0.3611	15.0	-0.6015	15.0	-0.0967	15.0	-0.0967	15.0	-0.0967
25.0	-0.4279	25.0	-0.4851	25.0	0.5213	25.0	0.5213	25.0	-0.6015	25.0	-0.3611	25.0	-0.5213	25.0	-0.1577	25.0	-0.1577	25.0	-0.1577
35.0	-0.4279	35.0	-0.5994	35.0	0.3889	35.0	0.3889	35.0	-0.3889	35.0	-0.3889	35.0	-0.5213	35.0	-0.7861	35.0	-0.7861	35.0	-0.7861
50.0	-0.5422	50.0	-0.6566	50.0	0.3889	50.0	-0.6205	50.0	-0.6205	50.0	-0.6205	50.0	-0.3889	50.0	-0.3889	50.0	-0.3407	50.0	-0.3889
56.0	-0.5994	56.0	-0.6566	56.0	0.3889	56.0	-0.6205	56.0	-0.6205	56.0	-0.6205	56.0	-0.3889	56.0	-0.3889	56.0	-0.3407	56.0	-0.3889
65.0	-0.8280	65.0	-0.8852	65.0	0.3889	65.0	-0.6205	65.0	-0.6205	65.0	-0.6205	65.0	-0.3889	65.0	-0.3889	65.0	-0.3407	65.0	-0.3889
76.0	-0.7709	76.0	-1.9141	76.0	0.3889	76.0	-0.6205	76.0	-0.6205	76.0	-0.6205	76.0	-0.3889	76.0	-0.3889	76.0	-0.3407	76.0	-0.3889
79.0	-2.7717	79.0	-3.1146	79.0	0.3889	79.0	-0.6205	79.0	-0.6205	79.0	-0.6205	79.0	-0.3889	79.0	-0.3889	79.0	-0.3407	79.0	-0.3889
80.5	-72.9447	80.5	-112.1469	80.5	0.3889	80.5	-0.6205	80.5	-0.6205	80.5	-0.6205	80.5	-0.3889	80.5	-0.3889	80.5	-0.3407	80.5	-0.3889
81.0	-0.9383	81.0	21.1795	81.0	0.3889	81.0	-0.6205	81.0	-0.6205	81.0	-0.6205	81.0	-0.3889	81.0	-0.3889	81.0	-0.3407	81.0	-0.3889
82.0	1.3726	82.0	-3.3316	82.0	0.3889	82.0	-0.6205	82.0	-0.6205	82.0	-0.6205	82.0	-0.3889	82.0	-0.3889	82.0	-0.3407	82.0	-0.3889
84.0	0.9599	84.0	0.9599	84.0	0.3889	84.0	-0.6205	84.0	-0.6205	84.0	-0.6205	84.0	-0.3889	84.0	-0.3889	84.0	-0.3407	84.0	-0.3889
87.0	7.7273	87.0	7.7273	87.0	0.3889	87.0	-0.6205	87.0	-0.6205	87.0	-0.6205	87.0	-0.3889	87.0	-0.3889	87.0	-0.3407	87.0	-0.3889
89.0	2.0380	89.0	-2.9633	89.0	0.3889	89.0	-0.6205	89.0	-0.6205	89.0	-0.6205	89.0	-0.3889	89.0	-0.3889	89.0	-0.3407	89.0	-0.3889
93.0	2.7090	93.0	2.7090	93.0	0.3889	93.0	-0.6205	93.0	-0.6205	93.0	-0.6205	93.0	-0.3889	93.0	-0.3889	93.0	-0.3407	93.0	-0.3889
96.0	5.5757	96.0	5.5757	96.0	0.3889	96.0	-0.6205	96.0	-0.6205	96.0	-0.6205	96.0	-0.3889	96.0	-0.3889	96.0	-0.3407	96.0	-0.3889
100.0	-0.2187	100.0	-0.2187	100.0	0.3889	100.0	-0.6205	100.0	-0.6205	100.0	-0.6205	100.0	-0.3889	100.0	-0.3889	100.0	-0.3407	100.0	-0.3889
96.0	-0.6456	96.0	-0.6456	96.0	0.3889	96.0	-0.6205	96.0	-0.6205	96.0	-0.6205	96.0	-0.3889	96.0	-0.3889	96.0	-0.3407	96.0	-0.3889
84.0	-0.2187	84.0	-0.2187	84.0	0.3889	84.0	-0.6205	84.0	-0.6205	84.0	-0.6205	84.0	-0.3889	84.0	-0.3889	84.0	-0.3407	84.0	-0.3889
73.0	-0.6456	73.0	-0.6456	73.0	0.3889	73.0	-0.6205	73.0	-0.6205	73.0	-0.6205	73.0	-0.3889	73.0	-0.3889	73.0	-0.3407	73.0	-0.3889
50.0	-0.2187	50.0	-0.2187	50.0	0.3889	50.0	-0.6205	50.0	-0.6205	50.0	-0.6205	50.0	-0.3889	50.0	-0.3889	50.0	-0.3407	50.0	-0.3889
35.0	-0.3136	35.0	-0.3136	35.0	0.3889	35.0	-0.6205	35.0	-0.6205	35.0	-0.6205	35.0	-0.3889	35.0	-0.3889	35.0	-0.3407	35.0	-0.3889
25.0	-0.4851	25.0	-0.4851	25.0	0.3889	25.0	-0.6205	25.0	-0.6205	25.0	-0.6205	25.0	-0.3889	25.0	-0.3889	25.0	-0.3407	25.0	-0.3889
10.0	-0.3707	10.0	-0.3707	10.0	0.3889	10.0	-0.6205	10.0	-0.6205	10.0	-0.6205	10.0	-0.3889	10.0	-0.3889	10.0	-0.3407	10.0	-0.3889
5.0	-0.4279	5.0	-0.4279	5.0	0.3889	5.0	-0.6205	5.0	-0.6205	5.0	-0.6205	5.0	-0.3889	5.0	-0.3889	5.0	-0.3407	5.0	-0.3889
2.5	-0.2564	2.5	-0.2564	2.5	0.3889	2.5	-0.6205	2.5	-0.6205	2.5	-0.6205	2.5	-0.3889	2.5	-0.3889	2.5	-0.3407	2.5	-0.3889
***** TOP *****										***** BOTTOM *****									
38.2	-0.3407	38.2	-0.3407	38.2	-0.3407	38.2	-0.3407	38.2	-0.3407	38.2	-0.3407	38.2	-0.3407	38.2	-0.3407	38.2	-0.3407	38.2	-0.3407
43.4	-0.3407	43.4	-0.3407	43.4	-0.3407	43.4	-0.3407	43.4	-0.3407	43.4	-0.3407	43.4	-0.3407	43.4	-0.3407	43.4	-0.3407	43.4	-0.3407
50.4	-0.2797	50.4	-0.2797	50.4	-0.2797	50.4	-0.2797	50.4	-0.2797	50.4	-0.2797	50.4	-0.2797	50.4	-0.2797	50.4	-0.2797	50.4	-0.2797
56.1	-0.1577	56.1	-0.1577	56.1	-0.1577	56.1	-0.1577	56.1	-0.1577	56.1	-0.1577	56.1	-0.1577	56.1	-0.1577	56.1	-0.1577	56.1	-0.1577
62.5	-0.0967	62.5	-0.0967	62.5	-0.0967	62.5	-0.0967	62.5	-0.0967	62.5	-0.0967	62.5	-0.0967	62.5	-0.0967	62.5	-0.0967	62.5	-0.0967
69.7	-0.1577	69.7	-0.1577	69.7	-0.1577	69.7	-0.1577	69.7	-0.1577	69.7	-0.1577	69.7	-0.1577	69.7	-0.1577	69.7	-0.1577	69.7	-0.1577
76.9	-0.1577	76.9	-0.1577	76.9	-0.1577	76.9	-0.1577	76.9	-0.1577	76.9	-0.1577	76.9	-0.1577	76.9	-0.1577	76.9	-0.1577	76.9	-0.1577
83.4	-0.2187	83.4	-0.2187	83.4	-0.2187	83.4	-0.2187	83.4	-0.2187	83.4	-0.2187	83.4	-0.2187	83.4	-0.2187	83.4	-0.2187	83.4	-0.2187
89.4	-0.2187	89.4	-0.2187	89.4	-0.2187	89.4	-0.2187	89.4	-0.2187	89.4	-0.2187	89.4	-0.2187	89.4	-0.2187	89.4	-0.2187	89.4	-0.2187
101.1	-0.5236	101.1	-0.5236	101.1	-0.5236	101.1	-0.5236	101.1	-0.5236	101.1	-0.5236	101.1	-0.5236	101.1	-0.5236	101.1	-0.5236	101.1	-0.5236
***** MISC.										***** MISC.									
NO.	CP	NO.	CP	NO.	CP	NO.	CP	NO.	CP	NO.	CP	NO.	CP	NO.	CP	NO.	CP	NO.	CP
1	-0.3889	1	-0.3889	1	-0.3889	1	-0.3889	1	-0.3889	1	-0.3889	1	-0.3889	1	-0.3889	1	-0.3889	1	-0.3889
2	-0.1572	2	-0.1572	2	-0.1572	2	-0.1572	2	-0.1572	2	-0.1572	2	-0.1572	2	-0.1572	2	-0.1572	2	-0.1572
3	-0.3889	3	-0.3889	3	-0.3889	3	-0.3889	3	-0.3889	3	-0.3889	3	-0.3889	3	-0.3889	3	-0.3889	3	-0.3889
4	-0.1572	4	-0.1572	4	-0.1572	4	-0.1572	4	-0.1572	4	-0.1572	4	-0.1572	4	-0.1572	4	-0.1572	4	-0.1572
5	-0.3889	5	-0.3889	5	-0.3889	5	-0.3889	5	-0.3889	5	-0.3889	5	-0.3889	5	-0.3889	5	-0.3889	5	-0.3889
6	-0.1572	6	-0.1572	6	-0.1572	6	-0.1572	6	-0.1572	6	-0.1572	6	-0.1572	6	-0.1572	6	-0.1572	6	-0.1572
7	-0.7861	7	-0.7861	7	-0.7861	7	-0.7861	7	-0.7861	7	-0.7861	7	-0.7861	7	-0.7861	7	-0.7861	7	-0.7861
8	-0.7364	8	-0.7364	8	-0.7364	8	-0.7364	8	-0.7364	8	-0.7364	8	-0.7364	8	-0.7364	8	-0.7364	8	-0.7364
9	-0.7364	9	-0.7364	9	-0.7364	9	-0.7364	9	-0.7364	9	-0.7364	9	-0.7364	9	-0.7364	9	-0.7364	9	-0.7364
10	-0.6868	10	-0.6868	10	-0.6868	10	-0.6868	10	-0.6868	10	-0.6868	10	-0.6868	10	-0.6868	10	-0.6868	10	-0.6868
11	-0.7861	11	-0.7861	11	-0.7861	11	-0.7861	11	-0.7861	11	-0.7861	11	-0.7861	11	-0.7861	11	-0.7861	11	-0.7861
12	-0.7364	12	-0.7364	12	-0.7364	12	-0.7364	12	-0.7364	12	-0.7364	12	-0.7364	12	-0.7364	12	-0.7364	12	-0.7364

TABLE A39. (Continued)

RUN: SEQ		PROPLUSIVE										WING / CANARD										PRESSURES										BASEPR = 8.180J										PAGE 688																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																												
274	2	CLAERO	-1.1807	CDAERO	-0.3549	DCLC	0.1738	DMUC	0.1738	CP	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.2800	0.0405	0.1207	0.280

TABLE A39. (Concluded)

RUN: SEQ										PROPLULSIVE										WING / CANARD PRESSURES										BASEPR = 8.1904										PAGE 680									
274 6										CLAERO = -0.0779										DCLC = 0.4580										HOT										NM									
ALPHA										PTOT										Q										CMJC										CMUT									
12.08										2138.00										4.41										1.218										3.312									
BETA										CL										CM										CROLL										CMTR									
-0.01										2.37										-0.33										-0.01										1.14									
										CD										-0.01										0.03										-0.13									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
										CL										CM										CROLL										CMTR									
										2.37										-0.33										-0.01										1.14									
										-2.28										-0.01										0.03										-0.13									
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										CL										CM										CROLL										CMTR									

TABLE A40. RUN 277, BV6V, DELF=45, CMJ=0.0, (BN/B)W=0.25

RUN: SEQ										PAGE 661									
277	1	CLAE0	-	0.5209	COA0	-	0.2419	WING	/	CANARD	PRESSURES	BASEPR	=	5.1904					
ALPHA	PTOT	2132.40	PTAT	2103.34	VEL	30.06	180.15	YAW	H/C	CMJW	CMJUT	HGT		87.4810	O.100348E+07				
BETA	CL	0.52	CD	0.24	CM	-0.32	0.00	CROLL	CH	CV	CNTR	CLTR		0.52	O.30				
-0.01																			
CANARD										WING									
BP=3.375 BP=10.125										BP=2 BP=6 BP=12 BP=16 BP=22									
%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP
0.0	-0.2646	0.0	-0.2646	0.0	-0.2646	0.0	-0.2646	0.0	-0.2646	0.0	-0.2646	0.0	-0.2646	0.0	-0.2646	0.0	-0.2646	0.0	-0.2646
2.5	-0.2565	2.5	-0.2565	2.5	-0.2565	2.5	-0.2565	2.5	-0.2565	2.5	-0.2565	2.5	-0.2565	2.5	-0.2565	2.5	-0.2565	2.5	-0.2565
5.0	-0.2585	5.0	-0.2585	5.0	-0.2585	5.0	-0.2585	5.0	-0.2585	5.0	-0.2585	5.0	-0.2585	5.0	-0.2585	5.0	-0.2585	5.0	-0.2585
10.0	-0.2728	10.0	-0.2728	10.0	-0.2728	10.0	-0.2728	10.0	-0.2728	10.0	-0.2728	10.0	-0.2728	10.0	-0.2728	10.0	-0.2728	10.0	-0.2728
15.0	-0.2565	15.0	-0.2565	15.0	-0.2565	15.0	-0.2565	15.0	-0.2565	15.0	-0.2565	15.0	-0.2565	15.0	-0.2565	15.0	-0.2565	15.0	-0.2565
25.0	-0.2646	25.0	-0.2646	25.0	-0.2646	25.0	-0.2646	25.0	-0.2646	25.0	-0.2646	25.0	-0.2646	25.0	-0.2646	25.0	-0.2646	25.0	-0.2646
35.0	-0.2728	35.0	-0.2728	35.0	-0.2728	35.0	-0.2728	35.0	-0.2728	35.0	-0.2728	35.0	-0.2728	35.0	-0.2728	35.0	-0.2728	35.0	-0.2728
50.0	-0.2646	50.0	-0.2646	50.0	-0.2646	50.0	-0.2646	50.0	-0.2646	50.0	-0.2646	50.0	-0.2646	50.0	-0.2646	50.0	-0.2646	50.0	-0.2646
58.0	-0.2646	58.0	-0.2646	58.0	-0.2646	58.0	-0.2646	58.0	-0.2646	58.0	-0.2646	58.0	-0.2646	58.0	-0.2646	58.0	-0.2646	58.0	-0.2646
65.0	-0.2646	65.0	-0.2646	65.0	-0.2646	65.0	-0.2646	65.0	-0.2646	65.0	-0.2646	65.0	-0.2646	65.0	-0.2646	65.0	-0.2646	65.0	-0.2646
76.0	-0.2891	76.0	-0.2891	76.0	-0.2891	76.0	-0.2891	76.0	-0.2891	76.0	-0.2891	76.0	-0.2891	76.0	-0.2891	76.0	-0.2891	76.0	-0.2891
79.0	-0.2810	79.0	-0.2810	79.0	-0.2810	79.0	-0.2810	79.0	-0.2810	79.0	-0.2810	79.0	-0.2810	79.0	-0.2810	79.0	-0.2810	79.0	-0.2810
80.5	-0.2191	80.5	-0.2191	80.5	-0.2191	80.5	-0.2191	80.5	-0.2191	80.5	-0.2191	80.5	-0.2191	80.5	-0.2191	80.5	-0.2191	80.5	-0.2191
81.0	-0.2309	81.0	-0.2309	81.0	-0.2309	81.0	-0.2309	81.0	-0.2309	81.0	-0.2309	81.0	-0.2309	81.0	-0.2309	81.0	-0.2309	81.0	-0.2309
82.0	-0.2309	82.0	-0.2309	82.0	-0.2309	82.0	-0.2309	82.0	-0.2309	82.0	-0.2309	82.0	-0.2309	82.0	-0.2309	82.0	-0.2309	82.0	-0.2309
84.0	-0.2368	84.0	-0.2368	84.0	-0.2368	84.0	-0.2368	84.0	-0.2368	84.0	-0.2368	84.0	-0.2368	84.0	-0.2368	84.0	-0.2368	84.0	-0.2368
87.0	-0.2306	87.0	-0.2306	87.0	-0.2306	87.0	-0.2306	87.0	-0.2306	87.0	-0.2306	87.0	-0.2306	87.0	-0.2306	87.0	-0.2306	87.0	-0.2306
89.0	-0.2623	89.0	-0.2623	89.0	-0.2623	89.0	-0.2623	89.0	-0.2623	89.0	-0.2623	89.0	-0.2623	89.0	-0.2623	89.0	-0.2623	89.0	-0.2623
93.0	-0.2623	93.0	-0.2623	93.0	-0.2623	93.0	-0.2623	93.0	-0.2623	93.0	-0.2623	93.0	-0.2623	93.0	-0.2623	93.0	-0.2623	93.0	-0.2623
96.0	-0.2623	96.0	-0.2623	96.0	-0.2623	96.0	-0.2623	96.0	-0.2623	96.0	-0.2623	96.0	-0.2623	96.0	-0.2623	96.0	-0.2623	96.0	-0.2623
100.0	-0.2710	100.0	-0.2710	100.0	-0.2710	100.0	-0.2710	100.0	-0.2710	100.0	-0.2710	100.0	-0.2710	100.0	-0.2710	100.0	-0.2710	100.0	-0.2710
96.0	-0.2710	96.0	-0.2710	96.0	-0.2710	96.0	-0.2710	96.0	-0.2710	96.0	-0.2710	96.0	-0.2710	96.0	-0.2710	96.0	-0.2710	96.0	-0.2710
84.0	-0.2710	84.0	-0.2710	84.0	-0.2710	84.0	-0.2710	84.0	-0.2710	84.0	-0.2710	84.0	-0.2710	84.0	-0.2710	84.0	-0.2710	84.0	-0.2710
73.0	-0.2710	73.0	-0.2710	73.0	-0.2710	73.0	-0.2710	73.0	-0.2710	73.0	-0.2710	73.0	-0.2710	73.0	-0.2710	73.0	-0.2710	73.0	-0.2710
50.0	-0.2797	50.0	-0.2797	50.0	-0.2797	50.0	-0.2797	50.0	-0.2797	50.0	-0.2797	50.0	-0.2797	50.0	-0.2797	50.0	-0.2797	50.0	-0.2797
35.0	-0.2728	35.0	-0.2728	35.0	-0.2728	35.0	-0.2728	35.0	-0.2728	35.0	-0.2728	35.0	-0.2728	35.0	-0.2728	35.0	-0.2728	35.0	-0.2728
25.0	-0.2728	25.0	-0.2728	25.0	-0.2728	25.0	-0.2728	25.0	-0.2728	25.0	-0.2728	25.0	-0.2728	25.0	-0.2728	25.0	-0.2728	25.0	-0.2728
10.0	-0.2810	10.0	-0.2810	10.0	-0.2810	10.0	-0.2810	10.0	-0.2810	10.0	-0.2810	10.0	-0.2810	10.0	-0.2810	10.0	-0.2810	10.0	-0.2810
5.0	-0.2646	5.0	-0.2646	5.0	-0.2646	5.0	-0.2646	5.0	-0.2646	5.0	-0.2646	5.0	-0.2646	5.0	-0.2646	5.0	-0.2646	5.0	-0.2646
2.5	-0.2810	2.5	-0.2810	2.5	-0.2810	2.5	-0.2810	2.5	-0.2810	2.5	-0.2810	2.5	-0.2810	2.5	-0.2810	2.5	-0.2810	2.5	-0.2810
0.0	-0.2646	0.0	-0.2646	0.0	-0.2646	0.0	-0.2646	0.0	-0.2646	0.0	-0.2646	0.0	-0.2646	0.0	-0.2646	0.0	-0.2646	0.0	-0.2646

TABLE A40. (Continued)

RUN: SEQ		PROPELLSIVE										WING / CANARD										PRESSURES										BASEPR = 8.1904										PAGE 683																																							
277 3		CLAERO = 0.6921 CDAERO = 0.2946 DCLC = 0.0										BP = 2 BP = 6 BP = 12 BP = 16 BP = 22										FUSELAGE										NO. CP										NO. CP																																							
ALPHA		PTOT										VEL										YAW										H/C										CMUT										HOT										CLTR										CDTR									
4.05		2132.26										30.40										161.26										0.01										2.66										0.0										87.0177										0.100900E+07									
BETA		CL										CM										CROLL										CN										CV										CNTR										0.69										0.35									
-0.01		0.69										0.29										-0.35										0.00										-0.00										0.71										0.69										0.35									
0.0		-0.2599										0.0										-0.4151										-1.3435										-1.1552										-2.8833										38.2										-0.0857									
2.5		-0.2599										2.5										-0.2453										-1.0405										-1.2669										-1.6162										43.4										-0.0599									
5.0		-0.2680										8.0										-0.5057										-0.5963										-0.9019										-0.926										50.4										-0.0771									
10.0		-0.2599										10.0										-0.2566										-0.5623										-0.7661										-0.7661										56.1										-0.0857									
15.0		-0.2599										15.0										-0.4265										-0.5283										-0.6942										-0.6969										62.5										-0.1202									
20.0		-0.2680										24.0										-0.3812										-0.4378										-0.5170										-0.5810										69.7										-0.1719									
25.0		-0.2760										33.0										-0.3747										-0.4074										-0.4729										-0.5283										76.9										-0.1719									
50.0		-0.2599										54.0										-0.3420										-0.4074										-0.4729										-0.4729										83.4										-0.1633									
56.0		-0.2599										65.0										-0.3701										-0.4563										-0.5855										-0.5942										89.4										-0.2150									
65.0		-0.2680										78.5										-0.4658										-0.6631										-0.9044										-0.9388										95.4										-0.2687									
76.0		-0.2760										78.5										-0.5274										-0.5274										-0.9239										-0.7607										101.1										-0.2338									
79.0		-0.2599										80.5										-0.5099										-0.5168										-0.8772										-0.7198										101.1										-0.2338									
80.5		-0.2651										81.3										-0.5099										-0.5168										-0.8772										-0.7198										101.1										-0.2338									
81.0		-0.2476										82.0										-0.5316										-0.5316										-0.8656										-0.7432										101.1										-0.2338									
82.0		-0.2476										84.0										-0.5316										-0.5316										-0.8656										-0.7432										101.1										-0.2338									
84.0		-0.2356										87.0										-0.5333										-0.5624										-0.8714										-0.7316										101.1										-0.2338									
87.0		-0.2324										89.0										-0.6132										-0.6624										-0.9850										-0.8167										101.1										-0.2338									
89.0		-0.2581										93.0										-0.6132										-0.6624										-0.9850										-0.8167										101.1										-0.2338									
93.0		-0.2581										96.0										-0.6132										-0.6624										-0.9850										-0.8167										101.1										-0.2338									
96.0		-0.2409										100.0										-0.6132										-0.6624										-0.9850										-0.8167										101.1										-0.2338									
98.0		-0.2495										100.0										-0.6132										-0.6624										-0.9850										-0.8167										101.1										-0.2338									
99.0		-0.2495										100.0										-0.6132										-0.6624										-0.9850										-0.8167										101.1										-0.2338									
100.0		-0.2495										100.0										-0.6132										-0.6624										-0.9850										-0.8167										101.1										-0.2338									
101.1		-0.2495										101.1										-0.6132										-0.6624										-0.9850										-0.8167										101.1										-0.2338									
102.2		-0.2495										102.2										-0.6132										-0.6624										-0.9850										-0.8167										102.2										-0.2338									
103.3		-0.2495										103.3										-0.6132										-0.6624										-0.9850										-0.8167										103.3										-0.2338									
104.4		-0.2495										104.4										-0.6132										-0.6624										-0.9850										-0.8167										104.4										-0.2338									
105.5		-0.2495										105.5										-0.6132										-0.6624										-0.9850										-0.8167										105.5										-0.2338									
106.6		-0.2495										106.6										-0.6132										-0.6624										-0.9850										-0.8167										106.6										-0.2338									
107.7		-0.2495										107.7										-0.6132										-0.6624										-0.9850										-0.8167										107.7										-0.2338									
108.8		-0.2495										108.8										-0.6132										-0.6624										-0.9850										-0.8167										108.8										-0.2338									
109.9		-0.2495										109.9										-0.6132										-0.6624										-0.9850										-0.8167										109.9										-0.2338									
111.0		-0.2495										111.0										-0.6132										-0.6624										-0.9850										-0.8167										111.0										-0.2338									
112.1		-0.2495										112.1										-0.6132										-0.6624										-0.9850										-0.8167										112.1										-0.2338									
113.2		-0.2495										113.2										-0.6132										-0.6624										-0.9850										-0.8167										113.2										-0.2338									
114.3		-0.2495										114.3										-0.6132										-0.6624										-0.9850										-0.8167										114.3										-0.2338									
115.4		-0.2495										115.4										-0.6132										-0.6624										-0.9850										-0.8167										115.4										-0.2338									
116.5		-0.2495										116.5										-0.6132										-0.6624										-0.9850										-0.8167										116.5										-0.2338									
117.6		-0.2495										117.6										-0.6132										-0.6624										-0.9850										-0.8167										117.6										-0.2338									
118.7		-0.2495										118.7										-0.6132										-0.6624										-0.9850										-0.8167										118.7										-0.2338									
119.8		-0.2495										119.8										-0.6132										-0.6624										-0.9850										-0.8167										119.8										-0.2338									
120.9		-0.2495										120.9										-0.6132										-0.6624										-0.9850										-0.8167										120.9										-0.2338									
122.0		-0.2495										122.0										-0.6132										-0.6624										-0.9850										-0.8167										122.0										-0.2338									
123.1		-0.2495										123.1										-0.6132										-0.6624										-0.9850										-0.8167										123.1										-0.2338									
124.2		-0.2495										124.2										-0.6132										-0.6624										-0.9850										-0.8167										124.2										-0.2338									
125.3		-0.2495										125.3										-0.6132										-0.6624										-0.9850										-0.8167										125.3										-0.2338									
126.4		-0.2495										126.4										-0.6132										-0.6624										-0.9850										-0.8167										126.4										-0.2338									
127.5		-0.2495										127.5										-0.6132										-0.6624										-0.9850										-0.8167										127.5										-0.2338									
128.6		-0.2495										128.6										-0.6132										-0.6624										-0.9850										-0.8167										128.6										-0.2338									
129.7		-0.2495										129.7										-0.6132										-0.6624										-0.9850										-0.8167										129.7										-0.2338									
130.8		-0.2495										130.8										-0.6132										-0.6624										-0.9850										-0.8167										130.8										-0.2338									
131.9		-0.2495										131.9										-0.6132										-0.6624										-0.9850										-0.8167										131.9										-0.2338									
133.0		-0.2495										133.0										-0.6132										-0.6624										-0.9850										-0.8167										133.0										-0.2338									
134.1		-0.2495										134.1										-0.6132										-0.6624										-0.9850										-0.8167										134.1										-0.2338									
135.2		-0.2495										135.2										-0.6132										-0.6624										-0.9850										-0.8167										135.2										-0.2338									
136.3		-0.2495										136.3										-0.6132										-0.6624										-0.9850										-0.8167										136.3										-0.2338									
137.4		-0.2495										137.4										-0.6132										-0.6624										-0.9850										-0.8167										137.4										-0.2338									
138.5		-0.2495										138.5										-0.6132										-0.6624										-0.9850										-0.8167										138.5										-0.2338									
139.6		-0.2495										139.6										-0.6132										-0.6624										-0.9850										-0.8167										139.6										-0.2338									
140.7		-0.2495										140.7										-0.6132										-0.6624										-0.9850										-0.8167										140.7										-0.2338									
141.8		-0.2495										141.8										-0.6132										-0.6624										-0.9850										-0.8167										141.8										-0.2338									
142.9		-0.2495										142.9										-0.6132										-0.6624										-0.9850										-0.8167										142.9										-0.2338									
144.0		-0.2495										144.0										-0.6132										-0.6624										-0.9850										-0.8167										144.0										-0.2338									
145.1		-0.2495										145.1										-0.6132										-0.6624										-0.9850										-0.8167										145.1										-0.2338									
146.2		-0.2495										146.2										-0.6132										-0.6624										-0.9850										-0.8167										146.2										-0.2338									
147.3		-0.2495										147.3										-0.6132										-0.6624										-0.9850										-0.8167										147.3										-0.2338									
148.4		-0.2495										148.4										-0.6132										-0.6624										-0.9850										-0.8167										148.4										-0.2338									
149.5		-0.2495										149.5										-0.6132										-0.6624										-0.9850										-0.8167										149.5										-0.2338									
150.6		-0.2495										150.6										-0.6132										-0.6624										-0.9850										-0.8167										150.6										-0.2338									
151.7		-0.2495										151.7										-0.6132										-0.6624										-0.9850										-0.8167										151.7										-0.2338									
152.8		-0.2495										152.8										-0.6132										-0.6624										-0.9850										-0.8167										152.8										-0.2338									
153.9		-0.2495										153.9										-0.6132										-0.6624										-0.9850										-0.8167										153.9										-0.2338									
155.0		-0.2495										155.0										-0.6132										-0.6624										-0.9850										-0.8167										155.0										-0.2338									
156.1		-0.2495										156.1										-0.6132										-0.6624										-0.9850										-0.8167										156.1										-0.2338									
157.2		-0.2495										157.2										-0.6132										-0.6624										-0.9850										-0.8167										157.2										-0.2338									
158.3		-0.2495										158.3										-0.6132										-0.6624										-0.9850										-0.8167										158.3										-0.2338									
159.4		-0.2495										159.4										-0.6132										-0.6624										-0.9850										-0.8167										159.4										-0.2338									
160.5		-0.2495										160.5										-0.6132										-0.6624										-0.9850										-0.8167										160.5										-0.2338									
161.6		-0.2495										161.6										-0.6132										-0.6624										-0.9850										-0.8167										161.6										-0.2338									
162.7		-0.2495										162.7										-0.6132										-0.6624										-0.9850										-0.8167										162.7										-0.2338									
163.8		-0.2495										163.8										-0.6132										-0.6624										-0.9850										-0.8167										163.8										-0.2338									
164.9		-0.2495										164.9										-0.6132										-0.6624										-0.9850										-0.8167										164.9										-0.2338									
166.0		-0.2495										166.0										-0.6132										-0.6624										-0.9850										-0.8167										166.0										-0.2338									
167.1		-0.2495										167.1										-0.6132																																																											

TABLE A40. (Concluded)

RUN: SEQ		CLARO = 1.0858		PROPULSIVE		WING / CANARD		PRESSURES		BASEPR = 8.1904		PAGE 665	
277	B	PTOT	PTAT	Q	VEL	YAW	M/C	CMUW	CMUT	HOT	RN		
12.03		2133.12	2103.06	30.06	180.49	0.01	2.75	0.0	0.0	89.9482	0.988211E+08		
BETA	CL	CD	CM	CM	CM	CM	CM	CM	CM	CLTR	CDTR		
-0.01	1.08	0.48	-0.44	0.01	-0.00	0.00	1.17	-0.45		1.07	0.55		
***** CANARD *****													
BP=3.375		BP=10.125		BP=2		BP=6		BP=12		BP=15		BP=22	
%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP	%X/C	CP
-0.3088	-0.3006	0.0	-2.8148	-5.5511	-7.0052	-2.9063	-1.5895	-1.5437	38.2	-0.1087	1	-0.6901	
-0.3006	-0.3006	2.5	-0.2728	-2.2765	-2.6887	-2.7889	-1.5437	43.4	-0.1174	2	0.3360		
-0.3006	-0.3088	5.0	-1.2461	-1.8239	-2.0933	-2.7346	-1.5323	50.4	-0.1438	3	-1.6832		
-0.2925	-0.3088	10.0	-0.2843	-1.2576	-1.8124	-2.7117	-1.9208	56.1	-0.1959	4	0.2688		
-0.2925	-0.3006	15.0	-0.8453	-1.0066	-1.3605	-2.5171	-1.4521	62.5	-0.2482	5	-1.2860		
-0.3006	-0.2525	20.0	-0.6736	-0.7852	-1.0400	-1.3720	-1.4407	69.7	-0.3266	6	0.0381		
-0.3088	-0.3006	25.0	-0.6239	-0.6901	-0.8557	-0.9219	-1.4184	76.9	-0.3092	7	-0.3569		
-0.2925	-0.2925	30.0	-0.4915	-0.5577	-0.6901	-0.3029	-1.2860	83.4	-0.2589	8	-0.3498		
-0.3006	-0.3006	35.0	-0.4835	-0.5619	-0.7536	-0.6752	-1.1545	89.4	-0.3353	9	-0.3569		
-0.3006	-0.3170	40.0	-0.4142	-0.6403	-1.2852	-1.1981	-1.2068	95.4	-0.2743	10	-0.3498		
-0.3170	-0.3088	45.0	-0.5113	-0.5054	-1.4960	-1.3781	-1.3014	101.1	-0.2133	11	-0.3498		
-0.3088	-0.2932	50.0	-0.5173	-0.5113	-1.3781	-0.9889	-0.2873	101.1	-0.2133	12	-0.3427		
-0.2814	-0.2873	55.0	-0.4877	51.7582	-1.4428	-1.0184	-1.2012	38.2	0.0046				
-0.2755	-0.2873	60.0	-0.4937	-0.9248	-1.3427	-1.0361	-1.1540	43.4	0.0307				
-0.2814	-0.2814	65.0	-0.4996	-0.9467	-1.1776	-1.0184	-1.0822	50.4	-0.0390				
-0.2814	-0.2814	70.0	-0.5173	-0.5621	-1.1835	-1.0307	-0.2873	55.1	0.1092				
-0.2817	-0.2817	75.0	-0.6051	-0.6406	-1.1442	-1.0591	-1.1159	62.5	0.1876				
-0.3004	-0.3004	80.0	-0.5596	-0.6548	-0.8889	-0.3781	-0.3498	69.7	0.2488				
-0.3004	-0.3004	85.0	-0.5596	-0.6619	-0.8038	-0.9740	-1.0875	75.9	0.2488				
-0.3004	-0.3004	90.0	-0.5484	-0.6974	-0.7328	-0.9101	-0.3358	83.4	0.2747				
-0.2917	-0.3004	95.0	0.3241	0.4235	-0.3809	0.3450	0.1823	89.4	0.2634				
-0.3004	-0.3004	100.0	0.6646	0.7427	-0.3498	0.6150	0.4093	95.4	0.1701				

TABLE A41. RUN 280, BW6V, DELF-45, CMU=0.5, (BN/B)W=0.25

RUN: SEQ		PROPLUSIVE										WING / CANARD		PRESSURES		BASEPR = 8.1904		PAGE 666			
280	2	CLAERO = 0.7105		CDAERO = 0.4412		DCLC = 0.0		DMLC = 0.4631		HGT		BN		HGT		87.9400		0.581730E+06			
ALPHA	PTOT	PSTAT		Q		VEL		YAW		H/C		CMU		CMU		CMU		CLTR			
-0.01	2133.12	2122.94		10.17		93.10		0.01		2.69		0.0		0.935		0.935		0.81			
BETA	CL	CD		CM		CROLL		CN		CV		CNR		CNR		CNR		0.40			
-0.01	1.17	0.17		-0.78		0.01		-0.01		0.01		0.81		-0.51		0.81					
***** CANARD *****		***** WING *****										***** BP = 2		***** BP = 6		***** BP = 12		***** BP = 16		***** BP = 22	
BP=3.375 BP=10.125		XX/C		CP		XX/C		CP		XX/C		CP		XX/C		CP		XX/C			
-0.3489	-0.3489	0.0		0.5291		0.3336		0.0892		-0.2829		-0.6889		38.2		-0.0788		1			
-0.3489	-0.3489	2.5		-0.3844		-0.3844		-0.7227		-0.8243		-1.0811		43.4		-0.0788		2			
-0.3730	-0.3730	5.0		-0.3187		-0.3844		-0.6213		-0.7227		-0.8581		50.4		-0.0788		3			
-0.3489	-0.3489	10.0		-0.4183		-0.3844		-0.6213		-0.5874		-0.7227		56.1		-0.1046		4			
-0.3489	-0.3489	15.0		-0.3506		-0.4521		-0.6213		-0.4859		-0.6889		62.5		-0.0788		5			
-0.3247	-0.3247	24.0		-0.3844		-0.4183		-0.5536		-0.4521		-0.5874		69.7		-0.1819		6			
-0.3489	-0.3489	33.0		-0.3667		-0.3667		-0.6889		-0.4845		-0.5823		76.9		-0.2076		7			
-0.3489	-0.3489	50.0		-0.5823		-0.5823		-0.7999		-0.7999		-0.7999		83.4		-0.2076		8			
-0.3247	-0.3247	55.0		-0.7999		-1.2119		-0.7999		-0.7742		-0.7999		89.4		-0.3106		9			
-0.3247	-0.3247	65.0		-0.0531		-2.7828		-1.2634		-1.3922		-1.4953		95.4		-0.3106		10			
-0.3247	-0.3247	75.0		-0.3489		-0.3489		-1.2100		-1.3320		-1.5933		101.1		-0.2849		11			
-0.3247	-0.3247	80.5		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849		12			
-0.3247	-0.3247	81.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	82.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	83.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	84.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	85.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	86.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	87.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	88.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	89.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	90.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	91.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	92.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	93.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	94.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	95.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	96.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	97.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	98.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	99.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	100.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	101.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	102.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	103.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	104.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	105.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	106.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	107.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	108.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	109.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	110.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	111.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	112.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	113.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	114.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	115.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	116.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	117.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	118.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	119.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	120.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	121.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	122.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	123.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	124.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	125.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	126.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	127.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	128.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	129.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	130.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	131.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	132.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	133.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	134.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	135.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	136.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	137.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	138.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	139.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	140.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	141.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	142.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	143.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	144.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.3247	-0.3247	145.0		-0.3489		-0.3489		-1.9940		-1.3320		-1.3320		101.1		-0.2849					
-0.																					

TABLE A41. (Continued)

RUN: SEQ		CLAERO		PROPLULSIVE		WING / CANARD		PRESSURES		BASEPR = 9.1904		PAGE 668	
280	4	PTOT	PSTAT	Q	VEL	YAW	H/C	CMJC	CMUT	HGT	RN		
ALPHA	4.08	2133.19	2123.13	10.08	92.61	0.01	2.68	0.0	0.550	87.6534	0.578059E+06		
BETA	-0.01	1.37	0.27	-0.83	0.01	-0.01	0.01	0.01	1.01	CLTR	CDTR		
										0.98	0.47		
***** CANARD *****													
BP=3.875		BP=10.125		BP=2		BP=6		BP=12		BP=16		BP=22	
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP
0.0	-0.3628	0.0	-0.3628	0.0	-0.1250	0.0	-0.6040	-1.8015	-2.3489	-2.9647	-3.6015	-4.2015	-4.8015
2.5	-0.3383	2.5	-0.3383	2.5	-0.3303	2.5	-0.8778	-1.2540	-1.6620	-2.2857	-2.8578	-3.4328	-4.0078
5.0	-0.3383	5.0	-0.3383	5.0	-0.5698	5.0	-0.7066	-1.0145	-1.1172	-1.5278	-1.9378	-2.3478	-2.7578
10.0	-0.3383	10.0	-0.3383	10.0	-0.3303	10.0	-0.6040	-0.8778	-0.8778	-1.0830	-1.2880	-1.4930	-1.6980
15.0	-0.3383	15.0	-0.3383	15.0	-0.5358	15.0	-0.5698	-0.8093	-0.7408	-0.8436	-0.9466	-1.0496	-1.1526
20.0	-0.3383	20.0	-0.3383	20.0	-0.4672	20.0	-0.5358	-0.7066	-0.6383	-0.7408	-0.8436	-0.9466	-1.0496
25.0	-0.3383	25.0	-0.3383	25.0	-0.4797	25.0	-0.4797	-0.5786	-0.6775	-0.7764	-0.8753	-0.9742	-1.0731
30.0	-0.3628	30.0	-0.3628	30.0	-0.5786	30.0	-0.6775	-0.7764	-0.8753	-0.9742	-1.0731	-1.1720	-1.2709
35.0	-0.3628	35.0	-0.3628	35.0	-0.8710	35.0	-1.3137	-0.8970	-0.9231	-1.0002	-1.0773	-1.1544	-1.2315
40.0	-0.3628	40.0	-0.3628	40.0	-0.0897	40.0	-2.8501	-1.3137	-1.4338	-1.6002	-1.7673	-1.9344	-2.1015
45.0	-0.3628	45.0	-0.3628	45.0	-0.3584	45.0	-2.7556	-1.3040	-1.3392	-1.6388	-1.9384	-2.2380	-2.5376
50.0	-0.2821	50.0	-0.2821	50.0	-0.4918	50.0	-2.0440	-1.2884	-1.3392	-1.6388	-1.9384	-2.2380	-2.5376
55.0	-0.3173	55.0	-0.3173	55.0	-0.340402	55.0	-1.580378	-1.2511	-1.3216	-1.5807	-1.8607	-2.1407	-2.4207
60.0	-0.3173	60.0	-0.3173	60.0	-0.240501	60.0	-3.4259	-1.2159	-1.3392	-1.6036	-1.8607	-2.1407	-2.4207
65.0	-0.3173	65.0	-0.3173	65.0	1.0217	65.0	-1.8326	-1.1102	-1.3216	-1.6036	-1.8607	-2.1407	-2.4207
70.0	-0.3349	70.0	-0.3349	70.0	-0.0178	70.0	-1.6388	-1.3392	-1.3216	-1.6036	-1.8607	-2.1407	-2.4207
75.0	-0.2997	75.0	-0.2997	75.0	-1.4337	75.0	-1.7729	-1.4548	-1.4097	-0.3349	-1.7517	-2.0317	-2.3117
80.0	-0.3502	80.0	-0.3502	80.0	-0.6494	80.0	-1.5396	-1.4548	-0.4374	-0.3527	-0.6668	-0.9468	-1.2268
85.0	-0.3502	85.0	-0.3502	85.0	-0.2890	85.0	-1.3913	-1.4128	-1.5609	-1.8788	-2.1967	-2.5147	-2.8327
90.0	-0.3502	90.0	-0.3502	90.0	-0.8825	90.0	-1.4337	-1.2853	-1.3913	-0.3738	-0.6668	-0.9468	-1.2268
95.0	-0.3502	95.0	-0.3502	95.0	0.5377	95.0	0.3469	0.1349	0.1985	0.0077	0.2488	0.4988	0.7488
100.0	-0.3502	100.0	-0.3502	100.0	0.6013	100.0	0.7709	0.3950	0.6849	0.4741	0.4105	0.1138	0.149
105.0	-0.3502	105.0	-0.3502	105.0	0.6084	105.0	0.2819	0.7073	0.7073	0.7073	0.7073	0.7073	0.7073
110.0	-0.3502	110.0	-0.3502	110.0	0.3116	110.0	0.3116	0.3116	0.3116	0.3116	0.3116	0.3116	0.3116
115.0	-0.3502	115.0	-0.3502	115.0	0.1138	115.0	0.2819	0.2127	0.2127	0.2127	0.2127	0.2127	0.2127
120.0	-0.3241	120.0	-0.3241	120.0	0.2171	120.0	0.1829	0.1829	0.2856	0.0803	0.3116	0.3116	0.3116
125.0	-0.3628	125.0	-0.3628	125.0	0.2854	125.0	0.2513	0.2513	0.4224	0.4224	0.4224	0.4224	0.4224
130.0	-0.3628	130.0	-0.3628	130.0	0.3682	130.0	0.3540	0.4224	0.4908	0.3116	0.3116	0.3116	0.3116
135.0	-0.3871	135.0	-0.3871	135.0	2.5	135.0	0.4566	0.5251	0.5251	0.5251	0.5251	0.5251	0.5251
140.0	-0.3628	140.0	-0.3628	140.0		140.0							
***** FUSELAGE *****													
XLOC		XLOC		XLOC		XLOC		XLOC		XLOC		XLOC	
NO.	CP	NO.	CP	NO.	CP	NO.	CP	NO.	CP	NO.	CP	NO.	CP
1	-0.4797	1	-0.4797	1	-0.4797	1	-0.4797	1	-0.4797	1	-0.4797	1	-0.4797
2	0.2127	2	0.2127	2	0.2127	2	0.2127	2	0.2127	2	0.2127	2	0.2127
3	-0.6775	3	-0.6775	3	-0.6775	3	-0.6775	3	-0.6775	3	-0.6775	3	-0.6775
4	0.2127	4	0.2127	4	0.2127	4	0.2127	4	0.2127	4	0.2127	4	0.2127
5	-0.6775	5	-0.6775	5	-0.6775	5	-0.6775	5	-0.6775	5	-0.6775	5	-0.6775
6	0.0149	6	0.0149	6	0.0149	6	0.0149	6	0.0149	6	0.0149	6	0.0149
7	-0.4162	7	-0.4162	7	-0.4162	7	-0.4162	7	-0.4162	7	-0.4162	7	-0.4162
8	-0.3950	8	-0.3950	8	-0.3950	8	-0.3950	8	-0.3950	8	-0.3950	8	-0.3950
9	-0.4162	9	-0.4162	9	-0.4162	9	-0.4162	9	-0.4162	9	-0.4162	9	-0.4162
10	-0.3950	10	-0.3950	10	-0.3950	10	-0.3950	10	-0.3950	10	-0.3950	10	-0.3950
11	-0.3950	11	-0.3950	11	-0.3950	11	-0.3950	11	-0.3950	11	-0.3950	11	-0.3950
12	-0.3738	12	-0.3738	12	-0.3738	12	-0.3738	12	-0.3738	12	-0.3738	12	-0.3738

TABLE A41. (Concluded)

RUN: SEQ										PAGE 671									
280 7										BASEPR = 8.1904									
ALPHA										HGT									
12.07										90.0125 0.874659E+06									
BETA										CLTR									
-0.01										1.47									
1.89										0.78									
0.63										CMTR									
-0.99										-0.71									
0.01										1.60									
0.01										-0.01									
0.01										0.00									
0.01										0.00									
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TABLE A42. RUN 281. BW6V, DELF=45, CMU=1.0, (BN/B)W=0.25

RUN: SEQ										PAGE 672									
281	ALPHA	PTOT	CLAERO	0.6447	COAERO	0.5116	WING / CANARD	PRESSURES		BASEPR	8.1904								
		PSTAT	0	VEL	YAW	H/C	CMUW	CMUW	CMUW	HGT	87.4083	0.397499E+06							
	BETA	CD	CL	CM	CROLL	CN	CV	CNTR	CNTR	CLTR	0.86	0.42							
			1.65	-0.07	-1.13	0.01	-0.02	0.03	0.86										
***** CANARD *****										***** FUSELAGE *****									
BP=3.375 BP=10.125										---TOP---									
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP
0.0	-0.3852	0.0	0.4311	0.3586	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	38.2	-0.1477	38.2	-0.1477	38.2	-0.1477	38.2	-0.1477	38.2	-0.1477
2.5	-0.3852	2.5	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	43.4	-0.1477	43.4	-0.1477	43.4	-0.1477	43.4	-0.1477	43.4	-0.1477
5.0	-0.3852	5.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	50.4	-0.1477	50.4	-0.1477	50.4	-0.1477	50.4	-0.1477	50.4	-0.1477
10.0	-0.3852	10.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	56.1	-0.2028	56.1	-0.2028	56.1	-0.2028	56.1	-0.2028	56.1	-0.2028
15.0	-0.3852	15.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	62.8	-0.2028	62.8	-0.2028	62.8	-0.2028	62.8	-0.2028	62.8	-0.2028
20.0	-0.3852	20.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	69.7	-0.3132	69.7	-0.3132	69.7	-0.3132	69.7	-0.3132	69.7	-0.3132
25.0	-0.3852	25.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	76.9	-0.3132	76.9	-0.3132	76.9	-0.3132	76.9	-0.3132	76.9	-0.3132
30.0	-0.3852	30.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	83.4	-0.3132	83.4	-0.3132	83.4	-0.3132	83.4	-0.3132	83.4	-0.3132
35.0	-0.3852	35.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	89.4	-0.3684	89.4	-0.3684	89.4	-0.3684	89.4	-0.3684	89.4	-0.3684
40.0	-0.3852	40.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684
45.0	-0.3852	45.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684
50.0	-0.3852	50.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684
55.0	-0.3852	55.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684
60.0	-0.3852	60.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684
65.0	-0.3852	65.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684
70.0	-0.3852	70.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684
75.0	-0.3852	75.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684
80.0	-0.3852	80.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684
85.0	-0.3852	85.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684
90.0	-0.3852	90.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684
95.0	-0.3852	95.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684
100.0	-0.3852	100.0	-0.3852	-0.3852	-0.5112	-0.5112	-0.5112	-0.5112	-0.5112	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684	101.1	-0.3684
***** MISC *****										---BOTTOM---									
NO.	CP	NO.	CP	NO.	CP	NO.	CP	NO.	CP	NO.	CP	NO.	CP	NO.	CP	NO.	CP	NO.	CP
1	-0.6655	1	-0.6655	1	-0.6655	1	-0.6655	1	-0.6655	38.2	-0.0628	38.2	-0.0628	38.2	-0.0628	38.2	-0.0628	38.2	-0.0628
2	-0.0369	2	-0.0369	2	-0.0369	2	-0.0369	2	-0.0369	43.4	-0.0373	43.4	-0.0373	43.4	-0.0373	43.4	-0.0373	43.4	-0.0373
3	-0.6655	3	-0.6655	3	-0.6655	3	-0.6655	3	-0.6655	50.4	-0.2028	50.4	-0.2028	50.4	-0.2028	50.4	-0.2028	50.4	-0.2028
4	-0.0369	4	-0.0369	4	-0.0369	4	-0.0369	4	-0.0369	56.1	0.0178	56.1	0.0178	56.1	0.0178	56.1	0.0178	56.1	0.0178
5	-0.6655	5	-0.6655	5	-0.6655	5	-0.6655	5	-0.6655	62.8	0.0178	62.8	0.0178	62.8	0.0178	62.8	0.0178	62.8	0.0178
6	-0.2485	6	-0.2485	6	-0.2485	6	-0.2485	6	-0.2485	69.7	0.0730	69.7	0.0730	69.7	0.0730	69.7	0.0730	69.7	0.0730
7	-0.4281	7	-0.4281	7	-0.4281	7	-0.4281	7	-0.4281	76.9	0.1282	76.9	0.1282	76.9	0.1282	76.9	0.1282	76.9	0.1282
8	-0.3812	8	-0.3812	8	-0.3812	8	-0.3812	8	-0.3812	83.4	0.1477	83.4	0.1477	83.4	0.1477	83.4	0.1477	83.4	0.1477
9	-0.3812	9	-0.3812	9	-0.3812	9	-0.3812	9	-0.3812	101.1	-0.5891	101.1	-0.5891	101.1	-0.5891	101.1	-0.5891	101.1	-0.5891
10	-0.4281	10	-0.4281	10	-0.4281	10	-0.4281	10	-0.4281										
11	-0.3812	11	-0.3812	11	-0.3812	11	-0.3812	11	-0.3812										
12	-0.3812	12	-0.3812	12	-0.3812	12	-0.3812	12	-0.3812										

TABLE A42. (Continued)

RUN: SEQ										PAGE 674									
281	3	CLARD	0.8725	CDAERD	0.5326	DCLC	0.0	WING	CANARD	PRESSURES	BASEPR	8.1904							
ALPHA		PTOT	2128.65	Q	VEL	YAW	H/C	CMUC	CMUJ	CMJT	HGT	87.2774	0.397797E+08						
BETA	4.02	CL	0.06	CD	CM	CHOLL	CH	CY	CMTR	CMTR	CLTR	0.074							
	-0.01	1.84			-1.17	0.01	-0.02	0.03	1.05	-0.58		1.01	0.49						
***** CANARD *****																			
XX/C	BP-3.375	CP	BP-10.125	XX/C	BP = 2	CP	BP = 6	CP	BP = 12	CP	BP = 16	CP	BP = 22	***** FUSELAGE *****					
0.0	-0.3029	-0.3546	-0.3546	0.0	-0.0249	-0.6048	-0.9873	-1.4746	-2.1995	-3.0893	-3.0893	-3.0893	-3.0893	-----TOP-----					
2.5	-0.3546	-0.3029	-0.3029	2.5	-0.3873	-0.9873	-1.4746	-2.1995	-3.0893	-3.0893	-3.0893	-3.0893	-3.0893	XLOC CP					
5.0	-0.3029	-0.3546	-0.3546	5.0	-0.6048	-0.7498	-1.2872	-1.6197	-1.6197	-1.6197	-1.6197	-1.6197	-1.6197	38.2 -0.2791					
10.0	-0.3029	-0.3546	-0.3546	10.0	-0.3873	-0.7498	-1.0397	-1.1122	-1.1122	-1.1122	-1.1122	-1.1122	-1.1122	43.4 -0.2791					
15.0	-0.3029	-0.3546	-0.3546	15.0	-0.6048	-0.9873	-0.9873	-0.9873	-0.9873	-0.9873	-0.9873	-0.9873	-0.9873	50.4 -0.2791					
20.0	-0.3546	-0.3029	-0.3029	20.0	-0.5323	-0.6048	-0.6048	-0.6048	-0.6048	-0.6048	-0.6048	-0.6048	-0.6048	56.1 -0.2791					
25.0	-0.3029	-0.3546	-0.3546	25.0	-0.6048	-0.9873	-0.9873	-0.9873	-0.9873	-0.9873	-0.9873	-0.9873	-0.9873	62.5 -0.3343					
30.0	-0.3029	-0.3546	-0.3546	30.0	-0.6866	-0.6866	-0.6866	-0.6866	-0.6866	-0.6866	-0.6866	-0.6866	-0.6866	69.7 -0.3343					
35.0	-0.3029	-0.3546	-0.3546	35.0	-0.9873	-0.9873	-0.9873	-0.9873	-0.9873	-0.9873	-0.9873	-0.9873	-0.9873	76.9 -0.3343					
40.0	-0.3546	-0.3029	-0.3029	40.0	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	83.4 -0.2791					
45.0	-0.3546	-0.3029	-0.3029	45.0	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	89.4 -0.3343					
50.0	-0.3546	-0.3029	-0.3029	50.0	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	95.4 -0.3898					
55.0	-0.3546	-0.3029	-0.3029	55.0	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	101.1 -0.3898					
60.0	-0.3546	-0.3029	-0.3029	60.0	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	101.1 -0.3898					
65.0	-0.3546	-0.3029	-0.3029	65.0	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	101.1 -0.3898					
70.0	-0.3546	-0.3029	-0.3029	70.0	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	101.1 -0.3898					
75.0	-0.3546	-0.3029	-0.3029	75.0	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	101.1 -0.3898					
80.0	-0.3546	-0.3029	-0.3029	80.0	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	-1.0397	101.1 -0.3898					
85.0	-0.3913	-0.3913	-0.3913	85.0	-1.1658	-2.7056	-2.6476	-1.7496	-1.8393	-1.8393	-1.8393	-1.8393	-1.8393	38.2 -0.1136					
90.0	-0.3913	-0.3913	-0.3913	90.0	-1.1658	-2.7056	-2.6476	-1.7496	-1.8393	-1.8393	-1.8393	-1.8393	-1.8393	43.4 -0.0884					
95.0	-0.4446	-0.4446	-0.4446	95.0	-0.4023	-2.1987	-1.7945	-1.7945	-1.7945	-1.7945	-1.7945	-1.7945	-1.7945	50.4 -0.2239					
100.0	-0.4446	-0.4446	-0.4446	100.0	-0.9117	-1.7945	-1.7945	-1.7945	-1.7945	-1.7945	-1.7945	-1.7945	-1.7945	56.1 -0.0584					
105.0	-0.4446	-0.4446	-0.4446	105.0	-1.9741	-1.9293	-1.6148	-1.6148	-1.6148	-1.6148	-1.6148	-1.6148	-1.6148	62.5 -0.0032					
110.0	-0.4446	-0.4446	-0.4446	110.0	-0.4061	0.3162	-0.0430	0.1368	-0.0430	0.1368	-0.0430	0.1368	-0.0430	69.7 0.1071					
115.0	-0.4446	-0.4446	-0.4446	115.0	0.5408	0.7653	-0.4472	0.4472	-0.4472	0.4472	-0.4472	0.4472	-0.4472	76.9 0.0519					
120.0	-0.4446	-0.4446	-0.4446	120.0	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612	83.4 0.1071					
125.0	-0.4446	-0.4446	-0.4446	125.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	89.4 0.1071					
130.0	-0.4446	-0.4446	-0.4446	130.0	-0.0579	-0.6866	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	95.4 -0.1688					
135.0	-0.4446	-0.4446	-0.4446	135.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	101.1 -0.7206					
140.0	-0.4446	-0.4446	-0.4446	140.0	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612						
145.0	-0.4446	-0.4446	-0.4446	145.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
150.0	-0.4446	-0.4446	-0.4446	150.0	-0.0579	-0.6866	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579						
155.0	-0.4446	-0.4446	-0.4446	155.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
160.0	-0.4446	-0.4446	-0.4446	160.0	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612						
165.0	-0.4446	-0.4446	-0.4446	165.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
170.0	-0.4446	-0.4446	-0.4446	170.0	-0.0579	-0.6866	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579						
175.0	-0.4446	-0.4446	-0.4446	175.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
180.0	-0.4446	-0.4446	-0.4446	180.0	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612						
185.0	-0.4446	-0.4446	-0.4446	185.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
190.0	-0.4446	-0.4446	-0.4446	190.0	-0.0579	-0.6866	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579						
195.0	-0.4446	-0.4446	-0.4446	195.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
200.0	-0.4446	-0.4446	-0.4446	200.0	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612						
205.0	-0.4446	-0.4446	-0.4446	205.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
210.0	-0.4446	-0.4446	-0.4446	210.0	-0.0579	-0.6866	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579						
215.0	-0.4446	-0.4446	-0.4446	215.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
220.0	-0.4446	-0.4446	-0.4446	220.0	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612						
225.0	-0.4446	-0.4446	-0.4446	225.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
230.0	-0.4446	-0.4446	-0.4446	230.0	-0.0579	-0.6866	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579						
235.0	-0.4446	-0.4446	-0.4446	235.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
240.0	-0.4446	-0.4446	-0.4446	240.0	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612						
245.0	-0.4446	-0.4446	-0.4446	245.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
250.0	-0.4446	-0.4446	-0.4446	250.0	-0.0579	-0.6866	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579						
255.0	-0.4446	-0.4446	-0.4446	255.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
260.0	-0.4446	-0.4446	-0.4446	260.0	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612						
265.0	-0.4446	-0.4446	-0.4446	265.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
270.0	-0.4446	-0.4446	-0.4446	270.0	-0.0579	-0.6866	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579						
275.0	-0.4446	-0.4446	-0.4446	275.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
280.0	-0.4446	-0.4446	-0.4446	280.0	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612						
285.0	-0.4446	-0.4446	-0.4446	285.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
290.0	-0.4446	-0.4446	-0.4446	290.0	-0.0579	-0.6866	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579						
295.0	-0.4446	-0.4446	-0.4446	295.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
300.0	-0.4446	-0.4446	-0.4446	300.0	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612						
305.0	-0.4446	-0.4446	-0.4446	305.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
310.0	-0.4446	-0.4446	-0.4446	310.0	-0.0579	-0.6866	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579						
315.0	-0.4446	-0.4446	-0.4446	315.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
320.0	-0.4446	-0.4446	-0.4446	320.0	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612						
325.0	-0.4446	-0.4446	-0.4446	325.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
330.0	-0.4446	-0.4446	-0.4446	330.0	-0.0579	-0.6866	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579	-0.0579						
335.0	-0.4446	-0.4446	-0.4446	335.0	0.1516	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579	0.1516	-0.0579						
340.0	-0.4446	-0.4446	-0.4446	340.0	0.3612	-0.6866	0.3612	0.3612	-0.6866	0.3612	0.36								

TABLE A42. (Concluded)

RUN: SEQ		PROPELLSIVE										WING / CANARD										PRESSURES		BASEPR = 8.1904		PAGE 876	
281		CLAERO = 1.3798										CRAERO = 0.7991										HGT		RN			
ALPHA		PTOT										Q										90.0912		0.397730E+06			
12.20		2133.40										VEL										CLTR		CDTR			
BETA		CL										CM										1.49		0.79			
-0.01		2.36										CROLL										1.49		0.79			
		CD										CN										1.49		0.79			
		0.48										CY										1.49		0.79			
		-1.31										0.03										1.49		0.79			
		-0.02										0.01										1.49		0.79			
		0.01										1.62										1.49		0.79			
		0.79										0.79										1.49		0.79			
		0.79										0.79										1.49		0.79			
		0.79										0.79										1.49		0.79			
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		0.79										0.79										1.49		0.79			
		0.79										0.79										1.49		0.79			
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		0.79										0.79										1.49		0.79			
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		0.79										0.79										1.49		0.79			
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		0.79										0.79										1.49		0.79			
		0.79										0.79										1.49		0.79			
		0.79										0.79										1.49		0.79			
		0.79										0.79										1.49		0.79			

TABLE A43. (Continued)

RUN: SEQ		PROPLULSIVE										WING / CANARD		PRESSURES		BASEPR = 8.1904		PAGE 68	
282 3		CDAERO = 0.6805										DCLC = 0.0		DMLC = 1.9312		HGT		BN	
ALPHA		PSTAT										VEL		CMUT		87.7968		0.295076E+06	
4.02		Q										YAW		2.148		CLTR		CDTR	
BETA		CM										CROLL		CNTR		1.10		0.51	
-0.01		-1.72										0.02		0.04		1.13			
		CD										CN		CV					
		CL										0.03		1.13					
		2.61										-0.28		-0.64					

TABLE A43. (Concluded)

RUN: SEQ										PROPULSIVE										WING / CANARD										PRESSURES										BASEPR = 8.1904										PAGE 688																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																									
282 5					CLARO = 1.2498					CDAERO = 0.8061					DCLC = 0.0					VEL					YAW					H/C					CMC					CMLN					CMUT					HGT					RN																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																				
ALPHA					PTOT					PSTAT					Q					2.60					46.98					0.01					2.74					0.0					1.940					89.7773					0.295104E+06																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																				
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TABLE A44. RUN 289, BC106V, DELF=45, CMU=0. (BN/B)W=0.25

RUN: SEQ		PROPLUISIVE										WING / CANARD		PRESSURES		PAGE 711			
289 2		CLAERO = 0.5316 CDAERO = 0.2390 DCCL = 0.0										BP = 2		BP = 12		BP = 18		BP = 22	
ALPHA		PTOT										XX/C		CP		CP		CP	
-0.06		2133.19										0.0		0.0542		0.1112		0.2937	
BETA		CD										0.0		0.0542		0.1112		0.2937	
0.06		0.53										-0.16		-0.0941		-0.1732		-0.2994	
		CL										0.00		0.00		0.00		0.00	
		CM										0.00		0.00		0.00		0.00	
		CROLL										-0.00		-0.00		-0.00		-0.00	
		CY										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.52		0.52		0.52		0.52	
		CMTR										0.17		0.17		0.17		0.17	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
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		CNTR										0.00		0.00		0.00		0.00	
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		CNTR										0.00		0.00		0.00		0.00	
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		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
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		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
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		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
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		CNTR										0.00		0.00		0.00		0.00	
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		CNTR										0.00		0.00		0.00		0.00	
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		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
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		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
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		CNTR										0.00		0.00		0.00		0.00	
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		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
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		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
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		CNTR										0.00		0.00		0.00		0.00	
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		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
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		CNTR										0.00		0.00		0.00		0.00	
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		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
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		CNTR										0.00		0.00		0.00		0.00	
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		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	
		CNTR										0.00		0.00		0.00		0.00	
		CMTR										0.00		0.00		0.00		0.00	
		CMT										0.00		0.00		0.00		0.00	

TABLE A44.

RUN: SEQ		PROPLUSIVE				WING / CANARD		PRESSURES		BASEPR = 8.1904		PAGE 713	
285	4	CLAFRO =	0.7639	CDAERO =	0.3084	DCLC =	0.0	OWLC =	0.0	HGT	RM	87.2514	0.100584E+07
ALPHA	4.15	PTOT	2103.04	VEL	160.84	YAW	H/C	CMC	CMUT	CLTR	CDTR	0.75	0.33
BETA	0.05	CL	0.76	CD	0.31	CM	0.16	0.00	0.00	0.77	0.14		
***** CANARD *****													
BP=3.375		BP=10.125	CP	CP	XX/C	CP	BP = 2	BP = 6	BP = 12	BP = 16	BP = 22	*****	
0.0	0.0844	-0.6127	0.0	0.1255	0.2391	-0.3859	-1.1700	-0.3859	-1.1700	-2.6587	XLOC	CP	
2.5	-0.7425	-1.0181	2.5	-0.2609	-0.0326	-0.7041	-1.0109	-0.7041	-1.0109	-1.5905	38.2	-0.2018	1 -0.3794
5.0	-0.9684	-0.6857	5.0	-0.0336	-0.1132	-0.5336	-0.8632	-0.5336	-0.8632	-1.1814	43.4	-0.1932	2 0.1463
10.0	0.6195	-0.6209	10.0	-0.2609	-0.2268	-0.4996	-0.6473	-0.4996	-0.6473	-0.8054	50.4	-0.1499	3 -0.4451
15.0	-0.4912	-0.5722	15.0	-0.1586	-0.2609	-0.4227	-0.5564	-0.4227	-0.5564	-0.6586	56.1	-0.1067	4 0.1791
25.0	-0.3856	-0.4344	24.0	0.2268	-0.3177	-0.4314	-0.4554	-0.4314	-0.4554	-0.5223	62.5	-0.0894	5 -0.4123
35.0	-0.3209	-0.3533	33.0	0.2480	-0.3137	-0.4123	-0.4451	-0.4123	-0.4451	-0.5223	69.7	-0.1326	6 0.0149
50.0	-0.3209	-0.3209	54.0	-0.3137	-0.3465	-0.4780	-0.1134	-0.4780	-0.1134	-0.4123	76.9	-0.1413	7 -0.3161
56.0	-0.3209	-0.3452	65.0	0.3682	-0.4526	-0.6170	-0.5851	-0.6170	-0.5851	-0.5564	83.4	-0.1236	8 -0.3020
65.0	-0.3776	-0.4425	78.5	0.1874	-0.6429	-1.0841	-0.9543	-1.0841	-0.9543	-0.8632	89.4	-0.2108	9 0.3020
76.0	-0.2804	-0.6127	79.5	-0.5678	-0.5444	-1.2116	-0.8780	-1.2116	-0.8780	-0.8632	95.4	-0.2481	10 -0.3020
79.0	-0.5398	-0.7283	80.5	-0.5444	-0.5678	-1.1940	-0.8604	-1.1940	-0.8604	-0.8632	101.1	-0.1932	11 -0.2950
80.5	-0.5386	-0.7200	81.3	0.5327	53.1121	-1.1062	-0.8604	-1.1062	-0.8604	-0.8632	101.1	-0.1932	12 -0.2950
81.0	-0.5152	-0.7024	82.0	-0.5386	-1.1121	-1.1413	-0.8838	-1.1413	-0.8838	-0.8632	101.1	-0.1932	
82.0	-0.5620	-0.7200	84.0	-0.5503	-0.5912	-1.0360	-0.9014	-1.0360	-0.9014	-0.8632	101.1	-0.1932	
84.0	-0.3045	-0.5327	87.0	-0.6029	-0.6088	-1.1706	-0.8780	-1.1706	-0.8780	-0.8632	101.1	-0.1932	
87.0	-0.5478	-0.7208	89.0	-0.6470	-0.6682	-1.1610	-0.9286	-1.1610	-0.9286	-0.8632	101.1	-0.1932	
89.0	-0.5478	-0.7208	93.0	-0.6330	-0.6682	-0.9639	-0.3161	-0.9639	-0.3161	-0.8632	101.1	-0.1932	
93.0	-0.5391	-0.7208	96.0	-0.6330	-0.6682	-0.8653	-0.9146	-0.8653	-0.9146	-0.8632	101.1	-0.1932	
96.0	-0.5391	-0.7208	100.0	-0.5837	-0.6470	-0.7245	-0.9146	-0.7245	-0.9146	-0.8632	101.1	-0.1932	
00.0	-0.7064	-0.7035	98.0	0.2612	0.3316	0.3598	0.3527	0.3598	0.3527	0.4781	89.4	0.1931	
00.0	-0.7035	-0.7035	84.0	0.4443	0.5851	-0.3020	0.5851	-0.3020	0.5851	0.4583	95.4	0.0923	
0.3431	0.3345	-0.7035	73.5	0.4420	-0.2480	0.5734	0.5405	0.5734	0.5405	0.4420	101.1	-0.3143	
0.6891	-0.7035	73.5	54.0	0.2448	0.2448	0.3108	0.3108	0.3108	0.3108	0.2120			
0.3431	0.3345	73.5	33.0	0.1134	-0.2480	0.1791	0.1791	0.1791	0.1791	0.1134			
0.6266	0.6632	0.5627	24.0	0.0459	0.0600	0.1141	0.1709	0.1141	0.1709	0.1028			
0.5708	0.33.0	0.2141	10.0	0.0118	0.0459	0.1596	0.2618	0.1596	0.2618	0.2448			
0.1249	0.1249	5.0	5.0	0.0005	-0.0109	0.2164	0.3187	0.2164	0.3187	0.3763			
0.0115	0.0115	2.5	2.5	-0.0677	-0.0338	0.2732	0.3982	0.2732	0.3982	0.4420			
0.3285	0.3285												

TABLE A44. (Concluded)

TABLE A45. RUN 290, BC1N6V, DELF=45, CMU=0.5, (BN/B)W=0.25

RUN:SEQ																BASEPR = 8.1904																PAGE 716																																																																																																																			
290 1																CLAERO = 0.4167 CDALC = 0.4210 DCLC = 0.2138 DWLC = 0.4139																HGT		RN																																																																																																																	
ALPHA 0.05																PTOT 2133.75																VEL 108.27																YAW -0.05																H/C 2.65																CMUJ 0.261																CMUJ 0.478																CMUT 0.739																																			
BETA 0.05																CL 1.04																CD 0.03																CM -0.06																CROLL -0.01																CN -0.00																CY 0.02																CNTR 0.62																CNTR 0.05																CLTR 0.62		CDTR 0.33	
***** CANARD *****																***** WING *****																***** FUSELAGE *****																MISC.***																																																																																																			
BP=3.375 BP=10.125																BP = 2 BP = 6 BP = 12 BP = 16 BP = 22																TOP----																																																																																																																			
X/C CP																X/C CP																X/C CP																NO. CP																																																																																																			
0.0 0.4845																0.0 -0.7215																-0.6216																-0.7464																0.3519																0.1272																38.2																1 -0.2981																																			
2.5 -0.4771																2.5 -0.2971																0.7763																-0.3970																-0.5967																-0.9212																43.4																2 -0.6590																																			
5.0 -0.4593																5.0 0.6265																0.5766																-0.3471																-0.4968																-0.7714																50.4																3 -0.5146																																			
10.0 0.0571																10.0 -0.3221																0.3269																-0.2721																-0.4469																-0.5967																56.1																4 -0.2289																																			
15.0 -0.5127																15.0 0.2770																0.1772																-0.3221																-0.4469																-0.4968																62.5																5 -0.4425																																			
20.0 -0.5127																20.0 0.0274																-0.0475																-0.4219																-0.4469																-0.4718																69.7																6 -0.1538																																			
25.0 -0.5483																25.0 -0.1538																-0.4425																-0.4425																-0.5868																-0.4425																76.9																7 -0.3910																																			
30.0 -0.7066																30.0 -0.4425																-0.4425																-0.8668																-0.8755																-0.5146																83.4																8 -0.3601																																			
35.0 -0.8333																35.0 -0.5951																-0.9561																-0.9561																-1.0511																-0.6711																89.4																9 -0.3446																																			
40.0 -1.1894																40.0 -0.8141																-2.2481																-0.9561																-0.9561																-1.0511																-1.1271																95.4																10 -0.3601																			
45.0 -0.3347																45.0 -0.8141																-27.8581																-0.8501																-0.8501																-1.2101																101.1																11 -0.3755																																			
50.0 -5.1805																50.0 -22.1375																115.4858																-0.8630																-1.0044																-1.0944																43.4																12 -0.3601																																			
55.0 -8.5370																55.0 -22.5234																-2.6627																-0.8758																-0.9530																-1.1458																43.4																2029																																			
60.0 -5.5035																60.0 -22.1759																-1.5443																-0.8758																-0.9518																-1.1330																50.4																0.0509																																			
65.0 -4.1281																65.0 -11.3136																-1.4929																-0.9273																-1.0173																56.1																0.0319																																																			
70.0 -0.7473																70.0 -1.5512																-1.4551																-1.0251																-1.1334																62.5																0.1201																																																			
75.0 -1.5571																75.0 -1.8912																-1.1179																-0.9787																-0.9310																69.7																0.4241																																																			
80.0 -1.5641																80.0 2.0217																-0.9478																-0.9787																-1.1024																76.9																0.3861																																																			
85.0 -0.9561																85.0 0.3514																-0.9787																-0.9787																-1.024																83.4																0.2721																																																			
90.0 -0.3481																90.0 -0.9787																-1.0714																-0.8859																0.3514																89.4																0.0630																																																			
95.0 0.3169																95.0 0.1348																0.0111																-0.3931																0.6762																95.4																0.0441																																																			
100.0 0.8209																100.0 -0.1538																-0.3703																0.3627																0.3514																101.1																0.3481																																																			
105.0 0.3169																105.0 -0.5868																-0.4425																-0.4425																-0.1538																0.0627																																																																			
110.0 0.6209																110.0 -0.5717																-0.6216																-0.5967																-0.4425																-0.4425																																																																			
115.0 0.7919																115.0 -0.5868																-0.3703																-0.6590																-0.4425																-0.4425																																																																			
120.0 0.5000																120.0 -0.5717																-0.6216																-0.5967																-0.4425																-0.4425																																																																			
125.0 0.3500																125.0 -0.6466																-0.5967																-0.6466																-0.4425																-0.4425																																																																			
130.0 0.2174																130.0 -0.6466																-0.5717																-0.6466																-0.4425																-0.4425																																																																			
135.0 0.0571																135.0 -0.5717																-0.5468																-0.5468																-0.2222																0.1349																																																																			
140.0 0.1105																140.0 -0.3598																																																																																																																																			

TABLE A45. (Continued)

PAGE 718

RUN: SEQ		CLARO =		PROPLUSIVE		WING / CANARD		PRESSURES		BASEPR = 8.1904	
290	3	PTOT	CL	CD	VEL	YAW	H/C	CMJC	CMUT	HGT	RN
ALPHA	4.08	2133.75			13.67	107.82	-0.05	2.86	0.265	87.0814	0.876836E+08
BETA	0.05	1.29	0.13	-0.03	0.00	0.00	-0.00	0.02	0.87	0.84	0.40
***** CANARD *****											
BP=3.375		BP=10.125		BP=2		BP=6		BP=12		BP=16	
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP
0.0	-1.0809	0.0	-0.7348	0.0	-0.6341	-0.9109	-0.5334	-2.1191	-0.5334	38.2	-0.3986
2.5	-1.2065	2.5	-0.3069	2.5	0.5992	-0.9884	-0.9844	-1.6156	-0.9844	43.4	-0.3966
5.0	-0.8116	5.0	0.5489	5.0	0.5237	-1.1627	-0.6341	-1.1627	-0.6341	50.4	-0.2242
10.0	0.2657	10.0	-0.3573	10.0	-0.2572	-1.1123	-0.6089	-0.8606	-0.6089	56.1	-0.0901
15.0	-0.7756	15.0	-0.1965	15.0	0.0958	-1.0368	-0.6089	-0.7086	-0.6089	62.5	-0.0326
20.0	-0.6679	20.0	0.0203	20.0	-0.1055	-0.9361	-0.6089	-0.5586	-0.6089	69.7	-0.0710
25.0	-0.6679	25.0	-0.8475	25.0	-0.0896	-0.1624	-0.6717	-0.4534	-0.6717	76.9	-0.1053
30.0	-0.8116	30.0	-0.8295	30.0	-0.3807	-0.3807	-0.5262	-0.5262	-0.5262	83.4	-0.1475
35.0	-0.9552	35.0	-0.6456	35.0	-0.5479	-0.5479	-0.6073	-0.7223	-0.6073	89.4	-0.2242
40.0	-1.1168	40.0	-0.4924	40.0	-2.6380	-0.9904	-1.1437	-1.4694	-0.9904	95.4	-0.2816
45.0	-1.6375	45.0	-1.2957	45.0	-31.4524	-0.9034	-0.9882	-1.3181	-0.9882	101.1	-0.2423
50.0	-3.7023	50.0	-22.9757	50.0	-1.4218	-1.0201	-0.9812	-0.3201	-0.9812	---BOTTOM---	
55.0	-6.2518	55.0	-23.1596	55.0	-1.9143	-0.8255	-1.0330	-1.5255	-0.8255	38.2	0.1590
60.0	-8.3041	60.0	-22.4185	60.0	-2.8216	-0.9812	-1.0070	-1.5255	-0.9812	43.4	0.2356
65.0	-20.0468	65.0	-22.5355	65.0	-2.8216	-0.9812	-1.0070	-1.5255	-0.9812	50.4	0.0632
70.0	-11.8554	70.0	-21.9782	70.0	-1.9143	-0.8255	-1.0459	-1.5255	-0.8255	56.1	0.0440
75.0	-8.3041	75.0	-12.5033	75.0	-1.7458	-1.0978	-1.0070	-0.3201	-1.0978	62.5	-0.2242
80.0	-2.9253	80.0	-0.3213	80.0	-1.5554	-1.0720	-1.2436	-0.3548	-1.2436	69.7	-0.3774
85.0	-0.7337	85.0	2.0779	85.0	-1.1857	-1.0409	-0.4171	-0.3548	-1.0409	76.9	-0.3853
90.0	-0.3943	90.0	0.2846	90.0	-1.0565	-1.0565	-1.0876	-0.3548	-1.0565	83.4	-0.1853
95.0	0.7337	95.0	-0.8382	95.0	-1.0720	-0.9785	-0.9629	-0.3158	-0.9785	89.4	-0.0057
100.0	0.4655	100.0	0.2378	100.0	0.0975	0.1286	0.4093	0.6120	0.1286	95.4	-0.0135
105.0	0.6379	105.0	0.2222	105.0	0.1754	0.2704	0.7892	0.4925	0.2704	101.1	-0.3966
110.0	0.4655	110.0	-0.1613	110.0	-0.3807	-0.3807	0.5853	0.0168	0.5853	101.1	-0.3966
115.0	0.6379	115.0	-0.3807	115.0	-0.2351	-0.2351	-0.0896	-0.1287	-0.0896	101.1	-0.3966
120.0	0.6187	120.0	-0.5990	120.0	-0.3807	-0.3807	-0.2351	-0.0168	-0.3807	101.1	-0.3966
125.0	0.7120	125.0	-0.5334	125.0	-0.6089	-0.6089	-0.4534	-0.0552	-0.6089	101.1	-0.3966
130.0	0.7505	130.0	-0.6844	130.0	-0.5082	-0.5082	-0.6341	-0.0215	-0.5082	101.1	-0.3966
135.0	0.3735	135.0	-1.2245	135.0	-0.5837	-0.5837	-0.6341	-0.0215	-0.5837	101.1	-0.3966
140.0	0.3376	140.0	0.8337	140.0	-0.5837	-0.5837	-0.6341	-0.0215	-0.5837	101.1	-0.3966
145.0	0.1939	145.0	0.2657	145.0	-0.5837	-0.5837	-0.6341	-0.0215	-0.5837	101.1	-0.3966
150.0	0.4094	150.0	0.5530	150.0	-0.5837	-0.5837	-0.6341	-0.0215	-0.5837	101.1	-0.3966

TABLE A45. (Concluded)

RUN: SEQ		CLAERO =		PROPLUISIVE		WING / CANARD		PRESSURES		BASEPR =		PAGE	
290	5	PTOT	PSTAT	Q	VEL	YAW	H/C	CMUC	CMUV	HGT	RM	720	
ALPHA	12.15	2133.68	2120.46	13.22	106.02	-0.04	2.72	0.279	0.514	88.9776	0.685757E+06		
BETA	0.04	2.05	0.59	-0.03	-0.00	-0.00	0.00	0.01	1.68	CLTR	CDTR		
										1.54	0.80		
***** CANARD *****													
BP=3.375		BP=10.125		BP=2		BP=6		BP=12		BP=16		BP=22	
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP
0.0	-8.0059	-3.0120	-0.0	-1.2132	-0.7976	-0.7716	-1.9427	-4.1788	-0.7716	-1.9427	-4.1788	-0.7716	-1.9427
2.5	-5.2213	-3.0863	2.5	-0.5633	0.1654	-0.9277	-1.4742	-3.1603	-0.9277	-1.4742	-3.1603	-0.9277	-1.4742
5.0	-1.6196	-3.0863	5.0	-0.4256	0.1384	-1.0318	-1.1679	-3.7124	-1.0318	-1.1679	-3.7124	-1.0318	-1.1679
10.0	0.4228	-3.2534	10.0	-0.6414	-0.0949	-1.1619	-0.9277	-3.0878	-1.1619	-0.9277	-3.0878	-1.1619	-0.9277
15.0	-1.4710	-3.4391	15.0	-0.0168	-0.2771	-1.2921	-0.8758	-2.0207	-1.2921	-0.8758	-2.0207	-1.2921	-0.8758
20.0	-1.1555	-4.1631	20.0	-0.1730	-0.4853	-1.2921	-0.8498	-0.9277	-1.2921	-0.8498	-0.9277	-1.2921	-0.8498
35.0	-1.0626	-3.2346	35.0	-0.2809	-0.4314	-1.2591	-0.9829	-0.7324	-1.2591	-0.9829	-0.7324	-1.2591	-0.9829
50.0	-1.1184	-1.2483	50.0	-0.5067	-0.6572	-1.1839	-0.9819	-0.9829	-1.1839	-0.9819	-0.9829	-1.1839	-0.9819
65.0	-1.6010	-1.3225	65.0	-0.8441	-1.2006	-1.2795	-1.1214	-0.9829	-1.2795	-1.1214	-0.9829	-1.2795	-1.1214
76.0	-0.5428	-3.6062	76.0	-0.3092	-3.8154	-1.5988	-1.4384	-1.5374	-1.5988	-1.4384	-1.5374	-1.5988	-1.4384
79.0	-0.9640	-6.3539	79.0	-23.8491	-46.0428	-1.4276	-1.2936	-1.3740	-1.4276	-1.2936	-1.3740	-1.4276	-1.2936
80.5	-9.3618	-21.8255	80.5	-22.9106	-5.8904	-1.7090	-1.2268	-0.5029	-1.7090	-1.2268	-0.5029	-1.7090	-1.2268
81.0	-8.1183	-13.0203	81.0	-23.3530	107.8493	-1.5618	-1.2668	-1.4008	-1.5618	-1.2668	-1.4008	-1.5618	-1.2668
82.0	-8.7244	-9.4419	82.0	-23.6078	-6.2606	-1.5432	-1.2936	-1.4544	-1.5432	-1.2936	-1.4544	-1.5432	-1.2936
84.0	-1.0390	-9.4419	84.0	-23.0316	-3.7461	-1.4678	-1.2936	-1.4142	-1.4678	-1.2936	-1.4142	-1.4678	-1.2936
87.0	-1.9235	-9.4419	87.0	-16.0224	-2.9822	-1.8029	-1.3338	-0.5430	-1.8029	-1.3338	-0.5430	-1.8029	-1.3338
89.0	-1.9335	-3.6965	89.0	-8.2900	-2.5170	-1.9526	-1.5979	-1.5172	-1.9526	-1.5979	-1.5172	-1.9526	-1.5979
93.0	-1.2601	-3.6965	93.0	0.1597	-1.0657	-1.5818	-1.4043	-1.5979	-1.5818	-1.4043	-1.5979	-1.5818	-1.4043
96.0	-0.5866	0.8199	96.0	-0.0821	-0.5820	-1.7430	-1.5011	-0.6143	-1.7430	-1.5011	-0.6143	-1.7430	-1.5011
100.0	0.5822	-0.4677	100.0	0.6596	0.4177	-0.0630	0.1597	0.1920	0.6596	0.1597	0.1920	0.6596	0.1597
96.0	0.6812	0.4831	96.0	0.3210	0.4177	-0.6465	0.4661	0.6596	0.3210	0.4661	0.6596	0.3210	0.4661
84.0	0.5322	-0.4677	84.0	0.2457	-0.5067	0.2457	0.3210	0.1705	0.2457	0.3210	0.1705	0.2457	0.3210
73.0	0.6812	0.4831	73.0	0.1705	0.1705	0.1705	0.1705	0.1705	0.1705	0.1705	0.1705	0.1705	0.1705
50.0	0.8397	0.6614	50.0	-0.1305	-0.5067	0.0200	0.1705	0.1705	0.0200	0.1705	0.1705	0.0200	0.1705
35.0	0.8125	0.5867	35.0	-0.2771	-0.3291	-0.0428	0.1654	0.1654	-0.2771	-0.0428	0.1654	0.1654	0.1654
25.0	0.5155	-1.5825	25.0	-0.8236	-0.6414	-0.3291	0.1654	0.1654	-0.8236	-0.6414	0.1654	0.1654	0.1654
10.0	0.4783	0.3855	10.0	-1.0578	-0.7195	-0.4593	0.1914	0.3962	-1.0578	-0.7195	0.1914	0.3962	0.3962
5.0	0.4412	0.4226	5.0	-1.0578	-0.7455	-0.4593	0.2174	0.3210	-1.0578	-0.7455	0.2174	0.3210	0.3210
2.5	0.6083	0.4412	2.5	-1.0578	-0.7455	-0.4593	0.2174	0.3210	-1.0578	-0.7455	0.2174	0.3210	0.3210
***** FUSELAGE *****													
XLOC		XLOC		XLOC		XLOC		XLOC		XLOC		XLOC	
CP	CP	CP	CP	CP	CP	CP	CP	CP	CP	CP	CP	CP	CP
38.2	-0.5866	38.2	-0.5866	38.2	-0.5866	38.2	-0.5866	38.2	-0.5866	38.2	-0.5866	38.2	-0.5866
43.4	-0.5074	43.4	-0.5074	43.4	-0.5074	43.4	-0.5074	43.4	-0.5074	43.4	-0.5074	43.4	-0.5074
50.4	-0.3290	50.4	-0.3290	50.4	-0.3290	50.4	-0.3290	50.4	-0.3290	50.4	-0.3290	50.4	-0.3290
56.1	-0.1903	56.1	-0.1903	56.1	-0.1903	56.1	-0.1903	56.1	-0.1903	56.1	-0.1903	56.1	-0.1903
62.5	-0.1112	62.5	-0.1112	62.5	-0.1112	62.5	-0.1112	62.5	-0.1112	62.5	-0.1112	62.5	-0.1112
69.7	-0.1803	69.7	-0.1803	69.7	-0.1803	69.7	-0.1803	69.7	-0.1803	69.7	-0.1803	69.7	-0.1803
76.9	-0.1708	76.9	-0.1708	76.9	-0.1708	76.9	-0.1708	76.9	-0.1708	76.9	-0.1708	76.9	-0.1708
83.4	-0.3092	83.4	-0.3092	83.4	-0.3092	83.4	-0.3092	83.4	-0.3092	83.4	-0.3092	83.4	-0.3092
89.4	-0.3489	89.4	-0.3489	89.4	-0.3489	89.4	-0.3489	89.4	-0.3489	89.4	-0.3489	89.4	-0.3489
101.1	-0.2894	101.1	-0.2894	101.1	-0.2894	101.1	-0.2894	101.1	-0.2894	101.1	-0.2894	101.1	-0.2894
***** MISC *****													
NO.		NO.		NO.		NO.		NO.		NO.		NO.	
CP	CP	CP	CP	CP	CP	CP	CP	CP	CP	CP	CP	CP	CP
1	-0.9581	1	-0.9581	1	-0.9581	1	-0.9581	1	-0.9581	1	-0.9581	1	-0.9581
2	0.0200	2	0.0200	2	0.0200	2	0.0200	2	0.0200	2	0.0200	2	0.0200
3	-0.8076	3	-0.8076	3	-0.8076	3	-0.8076	3	-0.8076	3	-0.8076	3	-0.8076
4	0.1708	4	0.1708	4	0.1708	4	0.1708	4	0.1708	4	0.1708	4	0.1708
5	-1.3343	5	-1.3343	5	-1.3343	5	-1.3343	5	-1.3343	5	-1.3343	5	-1.3343
6	0.0200	6	0.0200	6	0.0200	6	0.0200	6	0.0200	6	0.0200	6	0.0200
7	-0.6304	7	-0.6304	7	-0.6304	7	-0.6304	7	-0.6304	7	-0.6304	7	-0.6304
8	-0.6143	8	-0.6143	8	-0.6143	8	-0.6143	8	-0.6143	8	-0.6143	8	-0.6143
9	-0.6143	9	-0.6143	9	-0.6143	9	-0.6143	9	-0.6143	9	-0.6143	9	-0.6143
10	-0.5981	10	-0.5981	10	-0.5981	10	-0.5981	10	-0.5981	10	-0.5981	10	-0.5981
11	-0.5820	11	-0.5820	11	-0.5820	11	-0.5820	11	-0.5820	11	-0.5820	11	-0.5820
12	-0.5981	12	-0.5981	12	-0.5981	12	-0.5981	12	-0.5981	12	-0.5981	12	-0.5981

TABLE A46. (Continued)

PAGE 723

BASEPR = 8.1904
HGT RM
87.6989 0.465629E+06
CLTR
0.74 0.38

PROPLULSIVE WING / CANARD PRESSURES

CLARCO = 0.3103 COAERO = 0.5364 DCLC = 0.4821 DWLC = 0.9278

PTOT 2127.66 PSTAT 2127.66 Q VEL VAW H/C CMW CMUT

2134.11 2127.66 6.44 73.89 -0.05 2.68 0.562 1.032 1.534

BETA CL CD CROLL CH CNTR CMTR

0.05 1.72 -0.20 -0.09 -0.01 0.00 -0.00 0.77 0.16

***** CANARD *****										***** WING *****										***** FUSELAGE*****										***** MISCELLANEOUS *****											
BP=3.375 BP=10.125										BP = 2 BP = 6 BP = 12 BP = 16 BP = 22										-----TOP-----										-----BOTTOM-----											
CP										CP										XLOC CP										NO. CP											
291	0.0	-0.9501	-3.7321	0.0	-0.9298	-0.8228	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	38.2	-0.4297	43.4	-0.4297	50.4	-0.4297	56.1	-0.4297	62.5	-0.4297	69.7	-0.4297	76.9	-0.4297	83.4	-0.4297	89.4	-0.4297	95.4	-0.4297	101.1	-0.4297
ALPHA	2.5	-1.4075	-3.2367	2.5	-0.3955	0.8331	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	43.4	-0.4297	50.4	-0.4297	56.1	-0.4297	62.5	-0.4297	69.7	-0.4297	76.9	-0.4297	83.4	-0.4297	89.4	-0.4297	95.4	-0.4297	101.1	-0.4297		
BETA	4.05	-0.9501	-2.0553	5.0	0.6195	0.7263	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	50.4	-0.4297	56.1	-0.4297	62.5	-0.4297	69.7	-0.4297	76.9	-0.4297	83.4	-0.4297	89.4	-0.4297	95.4	-0.4297	101.1	-0.4297				
0.05	10.0	-0.9029	-1.2932	10.0	-0.3421	0.4058	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	56.1	-0.4297	62.5	-0.4297	69.7	-0.4297	76.9	-0.4297	83.4	-0.4297	89.4	-0.4297	95.4	-0.4297	101.1	-0.4297						
	15.0	-0.7977	-1.1407	15.0	0.2455	0.1921	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	62.5	-0.4297	69.7	-0.4297	76.9	-0.4297	83.4	-0.4297	89.4	-0.4297	95.4	-0.4297	101.1	-0.4297								
	25.0	-0.7215	-0.9121	25.0	0.0319	-0.0750	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	69.7	-0.4297	76.9	-0.4297	83.4	-0.4297	89.4	-0.4297	95.4	-0.4297	101.1	-0.4297										
	35.0	-0.9121	-0.9121	35.0	-0.2421	-0.2421	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	76.9	-0.4297	83.4	-0.4297	89.4	-0.4297	95.4	-0.4297	101.1	-0.4297												
	50.0	-0.9121	-0.9121	50.0	-0.3955	-0.3955	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	83.4	-0.4297	89.4	-0.4297	95.4	-0.4297																
	58.0	-0.9883	-1.3313	58.0	-0.7143	-1.4462	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	89.4	-0.4297	95.4	-0.4297																		
	65.0	-1.4456	-1.9029	65.0	-1.5275	-3.3573	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	95.4	-0.4297																				
	79.0	-0.3023	-4.5705	79.0	5.48.2114	-61.8567	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	80.5	-6.6284	-7.7716	80.5	-48.2655	219.3437	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	81.0	-13.2568	-33.0917	81.0	-48.6340	-4.5360	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	82.0	-8.1398	-18.9230	82.0	-48.7636	-2.4452	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	84.0	-5.9666	-12.7064	84.0	-15.5951	-1.9500	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	87.0	-0.8773	-3.8046	87.0	2.9463	-1.4228	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	89.0	-1.6475	-3.8046	89.0	3.7406	-1.2571	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	93.0	-2.0969	-3.8046	93.0	0.3646	-1.0917	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	96.0	-0.2671	-3.8046	96.0	-1.6874	-1.2571	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	100.0	-0.2671	-3.8046	100.0	-1.6874	-1.2571	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	98.0	-0.5658	-0.5462	98.0	0.0005	0.0005	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	84.0	1.2374	-0.9583	84.0	-0.2421	-0.3965	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	73.0	0.5858	0.5462	73.0	-0.7055	-0.7055	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	50.0	0.8308	0.5462	50.0	-0.7055	-0.7055	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	35.0	0.6886	0.5462	35.0	-0.7055	-0.7055	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	25.0	0.3455	-1.4075	25.0	-0.6093	-0.7160	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	10.0	0.3074	0.2312	10.0	-0.7160	-0.7160	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	5.0	0.2312	0.2693	5.0	-0.7160	-0.7160	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				
	2.5	0.4217	0.5361	2.5	-0.7160	-0.7160	-0.8331	-0.7694	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	-0.7887	101.1	-0.4297																				

TABLE A46. (Concluded)

RUN: SEC		PROPLULSIVE										WING / CANARD PRESSURES		BASEPR = 8.1904		PAGE 725	
291	5	CLARO =	0.9046	CDAERO =	0.8052	DCLC =	0.5439	DWLC =	1.0293					HGT	RN		
ALPHA	PTOT	PSTAT	0	VEL	YAW	H/C	CMUC	CMUW	CMUT					88.8068	0.453373E+06		
11.95	2134.25	2128.14	6.10	71.91	-0.04	2.72	0.591	1.083	1.674					CLTR	CDTR		
BETA	CL	CD	CM	CROLL	CN	CV	CNTR	CNTR	CNTR					1.37	0.70		
0.04	2.48	0.24	-0.05	-0.02	0.00	-0.00	1.49	0.21	0.21								
***** CANARD *****																	
BP=3.375		BP=10.125															
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP
0.0	-6.8032	0.0	-3.1433	0.0	-0.8612	0.0	-0.5793	0.0	-0.5793	0.0	-0.5793	0.0	-0.5793	0.0	-0.5793	0.0	-0.5793
2.5	-7.0042	2.5	-3.1834	2.5	-0.5793	2.5	-0.5793	2.5	-0.5793	2.5	-0.5793	2.5	-0.5793	2.5	-0.5793	2.5	-0.5793
5.0	-2.6607	5.0	-3.2237	5.0	0.4918	5.0	0.3791	5.0	0.3791	5.0	0.3791	5.0	0.3791	5.0	0.3791	5.0	0.3791
10.0	0.8786	10.0	-3.4247	10.0	-0.6357	10.0	-0.0156	10.0	-0.0156	10.0	-0.0156	10.0	-0.0156	10.0	-0.0156	10.0	-0.0156
15.0	-1.3736	15.0	-3.7063	15.0	-0.1535	15.0	-0.1847	15.0	-0.1847	15.0	-0.1847	15.0	-0.1847	15.0	-0.1847	15.0	-0.1847
20.0	-1.2128	20.0	-4.3097	20.0	-0.1283	20.0	-0.3539	20.0	-0.3539	20.0	-0.3539	20.0	-0.3539	20.0	-0.3539	20.0	-0.3539
25.0	-1.1323	25.0	-3.4650	25.0	-0.3047	25.0	-0.4677	25.0	-0.4677	25.0	-0.4677	25.0	-0.4677	25.0	-0.4677	25.0	-0.4677
30.0	-1.2932	30.0	-1.2932	30.0	-0.4677	30.0	-0.6307	30.0	-0.6307	30.0	-0.6307	30.0	-0.6307	30.0	-0.6307	30.0	-0.6307
35.0	-1.3335	35.0	-1.3335	35.0	-0.8889	35.0	-1.5754	35.0	-1.5754	35.0	-1.5754	35.0	-1.5754	35.0	-1.5754	35.0	-1.5754
40.0	-1.7758	40.0	-1.5345	40.0	-1.1464	40.0	-1.0644	40.0	-1.0644	40.0	-1.0644	40.0	-1.0644	40.0	-1.0644	40.0	-1.0644
45.0	-0.5291	45.0	-4.1889	45.0	-1.3457	45.0	-76.2274	45.0	-76.2274	45.0	-76.2274	45.0	-76.2274	45.0	-76.2274	45.0	-76.2274
50.0	-7.3259	50.0	-7.5673	50.0	-5.49.7207	50.0	-5.0676	50.0	-5.0676	50.0	-5.0676	50.0	-5.0676	50.0	-5.0676	50.0	-5.0676
55.0	-14.9041	55.0	-34.5369	55.0	81.3-50.9984	55.0	220.6077	55.0	220.6077	55.0	220.6077	55.0	220.6077	55.0	220.6077	55.0	220.6077
60.0	-9.1041	60.0	-20.3981	60.0	82.0-51.0558	60.0	-8.3750	60.0	-8.3750	60.0	-8.3750	60.0	-8.3750	60.0	-8.3750	60.0	-8.3750
65.0	-6.9073	65.0	-14.3008	65.0	84.0-49.5176	65.0	-3.7912	65.0	-3.7912	65.0	-3.7912	65.0	-3.7912	65.0	-3.7912	65.0	-3.7912
70.0	-1.4922	70.0	-20.3981	70.0	87.0-21.7905	70.0	-2.9202	70.0	-2.9202	70.0	-2.9202	70.0	-2.9202	70.0	-2.9202	70.0	-2.9202
75.0	-1.9330	75.0	-4.9226	75.0	89.0	0.1958	-2.5635	75.0	-2.5635	75.0	-2.5635	75.0	-2.5635	75.0	-2.5635	75.0	-2.5635
80.0	-2.4766	80.0	-1.5325	80.0	93.0	4.2476	-1.5156	80.0	-1.5156	80.0	-1.5156	80.0	-1.5156	80.0	-1.5156	80.0	-1.5156
85.0	-1.5027	85.0	0.8275	85.0	96.0	0.3705	-1.2712	85.0	-1.2712	85.0	-1.2712	85.0	-1.2712	85.0	-1.2712	85.0	-1.2712
90.0	1.2567	90.0	-1.1035	90.0	100.0	-1.6554	-1.4110	90.0	-1.4110	90.0	-1.4110	90.0	-1.4110	90.0	-1.4110	90.0	-1.4110
95.0	0.6559	95.0	0.4843	95.0	96.0	0.1958	0.0561	95.0	0.0561	95.0	0.0561	95.0	0.0561	95.0	0.0561	95.0	0.0561
100.0	1.2567	100.0	-1.1035	100.0	84.0	0.1558	0.1260	100.0	0.1260	100.0	0.1260	100.0	0.1260	100.0	0.1260	100.0	0.1260
105.0	0.6559	105.0	0.4843	105.0	73.5	-0.1417	-0.4677	105.0	-0.4677	105.0	-0.4677	105.0	-0.4677	105.0	-0.4677	105.0	-0.4677
110.0	0.7846	110.0	0.6988	110.0	54.0	-0.4677	-0.4677	110.0	-0.4677	110.0	-0.4677	110.0	-0.4677	110.0	-0.4677	110.0	-0.4677
115.0	0.8383	115.0	0.5970	115.0	33.0	-0.6307	-0.4677	115.0	-0.4677	115.0	-0.4677	115.0	-0.4677	115.0	-0.4677	115.0	-0.4677
120.0	0.5166	120.0	-1.6552	120.0	24.0	-0.5230	-0.6922	120.0	-0.6922	120.0	-0.6922	120.0	-0.6922	120.0	-0.6922	120.0	-0.6922
125.0	0.5166	125.0	0.3557	125.0	10.0	-0.5230	-0.6922	125.0	-0.6922	125.0	-0.6922	125.0	-0.6922	125.0	-0.6922	125.0	-0.6922
130.0	0.4362	130.0	0.3980	130.0	5.0	-0.6357	-0.6357	130.0	-0.6357	130.0	-0.6357	130.0	-0.6357	130.0	-0.6357	130.0	-0.6357
135.0	0.5970	135.0	0.4362	135.0	2.5	-0.5230	-0.6922	135.0	-0.6922	135.0	-0.6922	135.0	-0.6922	135.0	-0.6922	135.0	-0.6922
***** FUSELAGE *****																	
XLOC		CP															
38.2	-0.6314	38.2	-0.6314	38.2	-0.6314	38.2	-0.6314	38.2	-0.6314	38.2	-0.6314	38.2	-0.6314	38.2	-0.6314	38.2	-0.6314
43.4	-0.5456	43.4	-0.5456	43.4	-0.5456	43.4	-0.5456	43.4	-0.5456	43.4	-0.5456	43.4	-0.5456	43.4	-0.5456	43.4	-0.5456
50.4	-0.2882	50.4	-0.2882	50.4	-0.2882	50.4	-0.2882	50.4	-0.2882	50.4	-0.2882	50.4	-0.2882	50.4	-0.2882	50.4	-0.2882
56.1	-0.1165	56.1	-0.1165	56.1	-0.1165	56.1	-0.1165	56.1	-0.1165	56.1	-0.1165	56.1	-0.1165	56.1	-0.1165	56.1	-0.1165
62.5	-0.0307	62.5	-0.0307	62.5	-0.0307	62.5	-0.0307	62.5	-0.0307	62.5	-0.0307	62.5	-0.0307	62.5	-0.0307	62.5	-0.0307
69.7	-0.0736	69.7	-0.0736	69.7	-0.0736	69.7	-0.0736	69.7	-0.0736	69.7	-0.0736	69.7	-0.0736	69.7	-0.0736	69.7	-0.0736
76.9	-0.1594	76.9	-0.1594	76.9	-0.1594	76.9	-0.1594	76.9	-0.1594	76.9	-0.1594	76.9	-0.1594	76.9	-0.1594	76.9	-0.1594
83.4	-0.1894	83.4	-0.1894	83.4	-0.1894	83.4	-0.1894	83.4	-0.1894	83.4	-0.1894	83.4	-0.1894	83.4	-0.1894	83.4	-0.1894
89.4	-0.2452	89.4	-0.2452	89.4	-0.2452	89.4	-0.2452	89.4	-0.2452	89.4	-0.2452	89.4	-0.2452	89.4	-0.2452	89.4	-0.2452
95.4	-0.3311	95.4	-0.3311	95.4	-0.3311	95.4	-0.3311	95.4	-0.3311	95.4	-0.3311	95.4	-0.3311	95.4	-0.3311	95.4	-0.3311
101.1	-0.2882	101.1	-0.2882	101.1	-0.2882	101.1	-0.2882	101.1	-0.2882	101.1	-0.2882	101.1	-0.2882	101.1	-0.2882	101.1	-0.2882
***** MISC *****																	
NO.		CP															
1	-0.7937	1	-0.7937	1	-0.7937	1	-0.7937	1	-0.7937	1	-0.7937	1	-0.7937	1	-0.7937	1	-0.7937
2	-0.7937	2	-0.7937	2	-0.7937	2	-0.7937	2	-0.7937	2	-0.7937	2	-0.7937	2	-0.7937	2	-0.7937
3	-0.7937	3	-0.7937	3	-0.7937	3	-0.7937	3	-0.7937	3	-0.7937	3	-0.7937	3	-0.7937	3	-0.7937
4	0.0212	4	0.0212	4	0.0212	4	0.0212	4	0.0212	4	0.0212	4	0.0212	4	0.0212	4	0.0212
5	-0.7937	5	-0.7937	5	-0.7937	5	-0.7937	5	-0.7937	5	-0.7937	5	-0.7937	5	-0.7937	5	-0.7937
6	0.0212	6	0.0212	6	0.0212	6	0.0212	6	0.0212	6	0.0212	6	0.0212	6	0.0212	6	0.0212
7	-0.6075	7	-0.6075	7	-0.6075	7	-0.6075	7	-0.6075	7	-0.6075	7	-0.6075	7	-0.6075	7	-0.6075
8	-0.6075	8	-0.6075	8	-0.6075	8	-0.6075	8	-0.6075	8	-0.6075	8	-0.6075	8	-0.6075	8	-0.6075
9	-0.6075	9	-0.6075	9	-0.6075	9	-0.6075	9	-0.6075	9	-0.6075	9	-0.6075	9	-0.6075	9	-0.6075
10	-0.6075	10	-0.6075	10	-0.6075	10	-0.6075	10	-0.6075	10	-0.6075	10	-0.6075	10	-0.6075	10	-0.6075
11	-0.6425	11	-0.6425	11	-0.6425	11	-0.6425	11	-0.6425	11	-0.6425	11	-0.6425	11	-0.6425	11	-0.6425
12	-0.6425	12	-0.6425	12	-0.6425	12	-0.6425	12	-0.6425	12	-0.6425	12	-0.6425	12	-0.6425	12	-0.6425

TABLE A47. (Continued)

PAGE 728

RUN: SEQ		CLAERO = -0.0995		CDAERO = 0.7578		WING / CANARD PRESSURES		BASEPR = 8.1904	
292	3	PTOT	PSTAT	VEL	VAV	H/C	DCLC	CMUW	HGT
ALPHA		2134.46	2131.07	3.39	53.57	-0.05	2.67	2.045	87.4664
4.16		CL	CD	CM	CROLL	CN	CY	CNTR	CDTR
BETA		2.71	-0.71	-0.32	-0.03	0.01	-0.02	0.86	0.40
0.05									
***** CANARD *****									
BP=3.375 BP=10.125									
CP									
XX/C		-1.8932	-3.7031	0.0	-1.3315	-0.9256	-1.4330	-0.0123	-1.7374
0.0		-2.1828	-3.1962	2.5	-0.5197	0.7995	-0.1138	-0.7226	-1.9403
2.5		-1.0969	-2.8342	5.0	-0.6980	0.7995	-0.1138	-0.8241	-1.3315
5.0		-1.1472	-2.8342	10.0	-0.4182	0.4950	-0.4182	-0.6211	-1.1285
10.0		-1.0969	-1.8208	15.0	-0.3936	0.2921	-0.5197	-0.6211	-0.9256
15.0		-0.9521	-0.8211	20.0	-0.0892	-0.0123	-0.5197	-0.5197	-0.7226
25.0		-0.8211	-1.1693	35.0	-0.0797	-0.1710	-0.5197	-0.5197	-0.7578
50.0		-1.1693	-1.2418	55.0	-0.4644	-0.7578	-0.7578	-2.2347	-0.7578
56.0		-1.8208	-2.3276	65.0	-0.8513	-2.3960	-0.9285	-0.9285	-0.9285
65.0		-0.4454	-5.4003	75.5	-93.5783	-12.8612	-1.3147	-1.2968	-1.6326
76.0		-8.4082	-10.0000	80.5	-81.4377	-3.7529	-1.4000	-1.4000	-0.6178
79.0		-20.7357	-53.3938	81.3	-92.3252	400.4893	-1.2968	-1.4013	-1.6826
80.5		-12.2182	-30.2454	82.0	-92.2721	-7.2017	-1.1923	-1.4013	-1.6626
81.0		-8.5603	-19.8473	84.0	-88.7723	-3.7007	-1.1923	-1.2968	-0.4607
82.0		-0.8265	-0.8265	87.0	-24.6548	-3.0214	-1.2968	-1.5752	-0.7639
84.0		-1.5058	-1.5058	89.0	8.8812	-2.2040	-1.3237	-0.4436	-0.3807
87.0		-2.7822	-2.7822	93.0	6.5977	-1.7010	-1.2608	-0.4436	-0.3807
89.0		-1.4692	-1.4692	96.0	0.4995	-1.3866	-1.1980	-0.3868	-1.8896
93.0		0.6934	0.6934	100.0	-2.6440	-1.6281	-1.1980	-0.3868	-0.3807
96.0		-2.0097	-2.0097	98.0	-0.3179	-0.2590	-0.0594	0.3737	0.3807
100.0		0.4618	0.4618	84.0	-0.0664	-0.4644	-0.1224	0.8139	0.6881
96.0		0.4618	0.4618	73.5	-0.4644	-0.4644	0.1224	0.4157	0.4157
94.0		0.21610	0.21610	54.0	-1.0512	-1.3445	-1.0512	-0.1710	0.1224
73.0		0.6934	0.6934	33.0	-1.3445	-0.4644	-1.3445	-0.7578	-0.1710
50.0		0.7129	0.4957	24.0	-1.0271	-1.2300	-1.1285	-0.7226	-0.3167
35.0		0.2785	-1.6760	10.0	-0.9256	-1.0271	-1.2300	-0.6211	-0.1710
25.0		0.3508	0.2061	5.0	-0.8251	-1.0271	-1.2300	-0.7226	0.1224
10.0		0.2061	0.2061	2.5	-1.0271	-0.9256	-1.0271	-0.5197	0.1224
5.0		0.4233	0.4957						
***** FUSELAGE *****									
BP=22									
CP									
XX/C		38.2	-0.6196	38.2	-0.6196	38.2	-0.6196	38.2	-0.6196
0.0		43.4	-0.5423	43.4	-0.5423	43.4	-0.5423	43.4	-0.5423
2.5		50.4	-0.3106	50.4	-0.3106	50.4	-0.3106	50.4	-0.3106
5.0		56.1	-0.1561	56.1	-0.1561	56.1	-0.1561	56.1	-0.1561
10.0		62.5	-0.1561	62.5	-0.1561	62.5	-0.1561	62.5	-0.1561
15.0		69.7	-0.0789	69.7	-0.0789	69.7	-0.0789	69.7	-0.0789
25.0		76.9	-0.1561	76.9	-0.1561	76.9	-0.1561	76.9	-0.1561
35.0		83.4	-0.3106	83.4	-0.3106	83.4	-0.3106	83.4	-0.3106
50.0		95.4	-0.3876	95.4	-0.3876	95.4	-0.3876	95.4	-0.3876
56.0		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
65.0		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
76.0		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
83.4		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
89.0		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
95.4		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.1	-0.3876	101.1	-0.3876	101.1	-0.3876	101.1	-0.3876
101.1		101.							

TABLE A47. (Concluded)

RUN:SEQ		CLAERO = 0.1906		PROPULSIVE		WING / CANARD		PRESSURES		BASEPR = 8.1904		PAGE 730	
292	5	PTOT	PSTAT	Q	VEL	YAW	H/C	CMAC	CMJW	HGT	RM		
ALPHA	12.13	2134.60	2131.32	3.28	52.67	-0.04	2.74	1.177	2.140	89.4884	0.332585E+06		
BETA	0.04	CL	CD	CM	CROLL	CN	CV	CNTR	CNTR	CLTR	CDTR		
		3.31	-0.26	-0.17	-0.02	0.00	-0.04	1.32	0.33	1.22	0.61		
***** CANARD *****													
BP=3.375 BP=10.125		BP = 2		BP = 6		BP = 12		BP = 16		BP = 22		***** FUSELAGE *****	
XX/C		XX/C		XX/C		XX/C		XX/C		XX/C		***** TOP *****	
CP		CP		CP		CP		CP		CP		XLOC CP	
0.0	-6.7051	0.0	-1.4075	0.0	-0.7778	-1.5125	-0.9877	-4.3460	38.2	-0.6712	1	-0.5108	1
2.5	-3.4108	2.5	-0.5680	0.4815	-1.5125	-0.8827	-3.1916	43.4	-0.6712	2	-1.4210	2	
5.0	-3.6356	5.0	0.5865	0.4815	-1.5125	-0.8827	-1.8274	50.4	-0.3517	3	-1.1176	3	
10.0	-3.7102	10.0	-0.5680	0.1667	-1.5125	-0.7778	-1.1976	56.1	-0.1120	4	0.0961	4	
15.0	-4.1595	15.0	0.2717	0.1667	-1.4075	-0.8827	-0.9877	62.5	-0.1120	5	-0.8142	5	
20.0	-4.7586	20.0	-0.0432	-0.2531	-1.1976	-0.7778	-0.7778	69.7	-0.0322	6	0.0981	6	
25.0	-4.1649	25.0	-0.2073	-0.2073	-1.4210	-1.1176	-0.5108	76.9	-0.1120	7	-0.4892	7	
30.0	-1.4843	30.0	-0.5108	-0.5108	-1.1176	-1.7244	-0.8142	83.4	-0.1120	8	-0.5543	8	
35.0	-1.5392	35.0	-0.9109	-2.1889	-1.0707	-1.2304	-0.9908	89.4	-0.1919	9	-0.5543	9	
40.0	-2.0633	40.0	-2.1889	-4.6653	-1.3902	-1.7096	-1.7096	95.4	-0.2718	10	-0.4892	10	
45.0	-2.0911	45.0	-79.5-97.7861	-123.4592	-1.8581	-1.4257	-1.4797	101.1	-0.2718	11	-0.4892	11	
50.0	-4.9081	50.0	-80.5-95.1392	-7.1543	-1.4797	-1.5338	-0.5059	101.1	-0.2718	12	-0.5543	12	
55.0	-9.3255	55.0	-81.3-98.9231	404.7815	-1.6959	-1.3716	-1.3716	38.2	0.2873				
60.0	-22.2867	60.0	-82.0-96.0022	-8.6138	-1.4257	-1.4257	-1.4257	43.4	0.2873				
65.0	-31.7446	65.0	-84.0-92.8155	-4.8846	-1.3716	-1.5338	-1.5338	50.4	-0.0322				
70.0	-21.3140	70.0	-87.0-23.8002	-3.5334	-1.6419	-1.4257	-0.3988	56.1	-0.2718				
75.0	-1.2635	75.0	-89.0	8.6790	-2.5698	-1.5946	-1.5946	62.5	-0.8310				
80.0	-1.9121	80.0	93.0	6.4032	-1.8547	-1.5296	-0.6193	69.7	-0.9908				
85.0	-3.0677	85.0	96.0	0.4212	-1.7246	-1.3895	-1.3345	76.9	-0.9109				
90.0	-1.7096	90.0	100.0	-2.5048	-1.9197	-1.1394	-1.2044	83.4	-0.5913				
95.0	-0.1120	95.0	96.0	-0.2841	-0.1641	0.2911	0.4862	89.4	-0.1919				
100.0	2.2045	100.0	84.0	0.0310	0.0310	-0.5543	0.8113	95.4	-0.3517				
96.0	0.6068	96.0	73.5	0.0961	-0.5108	0.0961	0.7029	101.1	-1.0707				
2.2045	0.6068	2.2045	54.0	-0.8142	-0.8142	-0.1108	0.0961						
0.6068	0.6068	0.6068	33.0	-1.4210	-0.5108	-1.1176	-0.5108						
0.8585	0.8585	0.8585	24.0	-1.0927	-1.1976	-1.1976	-0.5880						
0.4074	-1.9884	0.4074	10.0	-1.0927	-0.8827	-1.1976	-0.7778						
0.4074	0.4074	0.4074	5.0	-0.8827	-1.0927	-1.1976	-0.9877						
0.3325	0.3325	0.3325	2.5	-0.8827	-0.9877	-1.1976	-0.8827						
0.5571	0.5571	0.5571											

TABLE 48. (Concluded)

RUN: SEQ		CLAEED = 1.3521		CDAEED = 0.9399		WING / CANARD		PRESSURES		BASEPR = 8.1805		PAGE 735	
296 6		PSTAT		VEL		YAW		CMJC		HGT		BN	
ALPHA		2141.98		13.22		105.76		-0.05		89.5966		0.867901E+06	
BETA		CL		CM		CROLL		CN		CLTR		CDTR	
0.05		2.11		-0.37		0.02		0.01		1.57		0.90	
BP=3.375		BP=10.125		BP=2		BP=6		BP=12		BP=16		BP=22	
XX/C		CP		XX/C		CP		CP		CP		CP	
0.0	-7.8076	-2.5196	0.0	1.8907	0.6935	-2.8202	-5.0325	-2.2216	-2.2216	38.2	-0.4802	1	-0.8757
2.5	-3.5957	-2.4824	2.5	-0.5819	0.0686	-1.5188	-5.1826	-2.4818	-2.4818	43.4	-0.4406	2	0.3285
5.0	-1.8516	-2.4024	5.0	0.3031	-0.2435	-1.2065	-3.8092	-2.4038	-2.4038	50.4	-0.2820	3	0.8757
10.0	-0.1446	-2.5567	10.0	-0.5558	-0.5819	-1.1264	-1.1844	-2.5078	-2.5078	56.1	-0.1829	4	0.3285
15.0	-1.2208	-2.5937	15.0	-0.5038	-0.6339	-1.0764	-1.0243	-2.5599	-2.5599	62.5	-0.1631	5	-2.2303
20.0	-0.5224	-2.9463	20.0	-0.4517	-0.7119	-1.0243	-0.8681	-2.5078	-2.5078	68.7	-0.2226	6	0.1027
25.0	-0.8887	-2.7607	25.0	-0.4994	-0.6499	-0.9509	-0.8757	-2.2303	-2.2303	76.9	-0.2622	7	-0.6390
30.0	-0.8125	-0.9053	30.0	-0.4974	-1.1934	-1.2132	-1.0349	-1.0547	-1.0547	83.4	-0.2424	8	-0.6390
35.0	-0.8497	-0.5528	35.0	-0.2926	-4.7002	-1.8472	-1.6689	-1.5897	-1.5897	89.4	-0.3415	9	-0.6229
40.0	-1.0352	-1.3955	40.0	-0.6499	-0.8003	-1.0262	-1.6198	-1.7537	-1.7537	95.4	-0.4207	10	-0.6552
45.0	-0.6270	-1.1651	45.0	-0.6566	-39.9720	-1.7939	-1.6198	-1.7537	-1.7537	101.1	-0.3415	11	-0.6390
50.0	-2.3711	-1.7024	50.0	-0.5257	-3.6023	-1.7805	-1.7403	-0.6552	-0.6552	--80170M--	--	12	-0.6068
55.0	-3.7383	1.7024	55.0	-0.2800	119.6249	-1.7135	-1.7135	-1.7135	-1.7135	38.2	0.1737		
60.0	-3.3478	0.6843	60.0	-0.2574	-5.2232	-1.7571	-1.6331	-1.6509	-1.6509	43.4	0.1938		
65.0	-3.0263	-4.9553	65.0	-0.2495	-3.9105	-1.6198	-1.6465	-1.7269	-1.7269	50.4	-0.0442		
70.0	-1.6868	-4.9553	70.0	-0.1638	-2.9058	-1.8475	-1.7001	-0.6285	-0.6285	56.1	0.0848		
75.0	-3.0665	-1.6689	75.0	-0.6122	-2.9001	-1.9614	-1.7518	-1.7840	-1.7840	62.5	-0.0641		
80.0	-2.9765	0.7483	80.0	-0.6833	-2.3646	-1.8808	-0.6713	-0.6390	-0.6390	68.7	-0.0442		
85.0	-2.9170	-0.4802	85.0	-0.8326	-2.1388	-1.8163	-1.7840	-1.8002	-1.8002	76.9	0.0648		
90.0	-3.3361	0.3718	90.0	-1.1390	-1.9260	-1.6389	-1.7195	-0.6068	-0.6068	83.4	0.1539		
95.0	0.7881	-0.4802	95.0	1.1348	0.7478	0.3285	0.2479	0.3608	0.3608	89.4	0.2529		
100.0	0.0945	-0.4802	100.0	1.7798	1.5219	-0.6390	0.6994	0.3285	0.3285	95.4	-0.0442		
105.0	0.7681	0.3718	105.0	1.1563	-0.4994	0.7048	0.9543	0.3285	0.3285	101.1	-0.9586		
110.0	0.0945	0.3718	110.0	0.3285	0.3285	0.3285	0.3285	0.1778	0.1778				
115.0	0.7681	0.3718	115.0	0.1027	-0.5746	0.3285	0.3285	0.1027	0.1027				
120.0	0.7059	0.5791	120.0	-0.0413	0.0688	0.3285	0.3285	0.2510	0.2510				
125.0	0.3378	-1.0538	125.0	-0.3215	0.0092	0.3812	0.5113	0.4037	0.4037				
130.0	0.3378	0.3378	130.0	-0.6859	-0.2955	0.4072	0.5373	0.4790	0.4790				
135.0	0.3378	0.3750	135.0	-1.2067	-0.7380	0.3812	0.3291	0.2532	0.2532				
140.0	0.6162	0.5420	140.0										

TABLE A49. RUN 297. BC1W6V, DELF-45, CMU=1.0, (BN/S)W=0.25, (BN/S)C=0.5

RUN: SEQ										PROPLUSTRIVE										WING / CANARD										PRESSURES										BASEPR = 8.1908										PAGE 738																																																																																									
297 ALPHA										CLAERO = 0.1632 CDAERO = 0.6370 DCLC = 0.6665 DWLC = 0.9392										HGT										HGT										87.7528 0.431959E+06																																																																																																			
-0.05										PTOT										Q VEL YAW H/C										CMUW										CMUT																																																																																																			
BETA										2142.10										5.54 68.42										0.05 2.68										0.814 1.108										1.922																																																																																									
0.05										CL										CD										CROLL										CN										CY										CMTR										CDTR										0.64 0.45																																																											
										1.79										-0.39										-0.44										0.01										-0.01										-0.04										-0.18																																																																					

TABLE A49. (Concluded)

RUN: SEQ		PROPLULSIVE										WING / CANARD PRESSURES										BASEPR = 8.1905				PAGE 740			
297		CLAERO = 0.9190										DCLC = 0.7383										HGT RN							
ALPHA		PSTAT										YAW H/C										89.2687				0.439947E+06			
12.02		2136.12										5.76										CLTR				CDTR			
BETA		CD										CM										1.43				0.88			
0.05		2.70										CROLL										1.43				0.88			
		0.32										CN										1.56				-0.07			
		0.00										CV										1.56				-0.07			
		0.02										0.02										0.02				0.02			
		0.05										0.05										0.05				0.05			
		0.10										0.10										0.10				0.10			
		0.15										0.15										0.15				0.15			
		0.20										0.20										0.20				0.20			
		0.25										0.25										0.25				0.25			
		0.30										0.30										0.30				0.30			
		0.35										0.35										0.35				0.35			
		0.40										0.40										0.40				0.40			
		0.45										0.45										0.45				0.45			
		0.50										0.50										0.50				0.50			
		0.55										0.55										0.55				0.55			
		0.60										0.60										0.60				0.60			
		0.65										0.65										0.65				0.65			
		0.70										0.70										0.70				0.70			
		0.75										0.75										0.75				0.75			
		0.80										0.80										0.80				0.80			
		0.85										0.85										0.85				0.85			
		0.90										0.90										0.90				0.90			
		0.95										0.95										0.95				0.95			
		1.00										1.00										1.00				1.00			
		1.05										1.05										1.05				1.05			
		1.10										1.10										1.10				1.10			
		1.15										1.15										1.15				1.15			
		1.20										1.20										1.20				1.20			
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		9.70																											

TABLE A50. RUN 298. SC1WV, DELF=45, CMU=2.0, (BM/S)V=0.25, (BM/S)C=0.5

RUN: SEQ										PAGE 741									
298	1	CLAERO	-0.2258	CD AERO	-0.8233	DCLC	-1.2037	DWLC	-1.7253	BASEPR	-8.1905								
ALPHA	PTOT	PSTAT	0	VEL	YAW	W/C	CMUC	CMUW	CMUT	HOT	RN								
0.10	2142.10	2138.93	3.16	51.77	-0.06	2.69	1.468	1.390	3.456	87.8940	0.328344E+06								
BETA	CL	CD	CK	CROLL	CN	CV	CMTR	CMTR	CMTR	CLTR	CDTR								
0.08	2.70	-1.01	-0.66	0.02	-0.01	-0.08	0.65	-0.21	0.46	0.65	0.46								
..... CANARD										 FUSELAGE									
BP=3.37% BP=10.125										-----TOP-----									
XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP	XX/C	CP
0.0	0.3135	-0.2293	0.0	-0.7289	-0.5114	0.5763	0.5763	0.5763	0.5763	38.2	-0.1478	1	-0.2467	38.2	-0.1478	1	-0.2467	38.2	-0.1478
2.5	-0.3068	-1.0422	2.5	-0.2939	0.9026	-0.1851	-0.2939	-0.1851	-0.2939	43.4	-0.2308	2	0.0679	43.4	-0.2308	2	0.0679	43.4	-0.2308
5.0	-0.4619	-1.0046	5.0	-0.6850	0.5763	-0.1851	-0.6850	-0.1851	-0.6850	50.4	-0.0680	3	-0.5612	50.4	-0.0680	3	-0.5612	50.4	-0.0680
10.0	-0.2293	-0.9271	10.0	-0.1851	0.3588	-0.2939	-0.1851	-0.2939	-0.1851	56.1	0.1006	4	0.0679	56.1	0.1006	4	0.0679	56.1	0.1006
15.0	-0.6170	-0.8496	15.0	0.3688	0.1412	-0.2939	0.3688	0.1412	-0.2939	62.3	0.1006	5	-0.2467	62.3	0.1006	5	-0.2467	62.3	0.1006
25.0	-0.5395	-0.6945	25.0	0.1412	-0.0763	-0.1851	0.1412	-0.0763	-0.1851	69.7	0.0178	6	0.0679	69.7	0.0178	6	0.0679	69.7	0.0178
35.0	-0.6170	-0.6170	35.0	0.0679	0.0679	-0.2467	0.0679	-0.2467	-0.2467	76.9	0.1006	7	-0.4039	76.9	0.1006	7	-0.4039	76.9	0.1006
50.0	-0.6170	-0.6170	50.0	-0.2467	-0.2467	-0.5612	-0.2467	-0.5612	-0.5612	82.4	-0.1478	8	-0.2691	82.4	-0.1478	8	-0.2691	82.4	-0.1478
65.0	-1.3924	-0.6170	65.0	-0.7274	-2.0521	-0.9102	-0.7274	-2.0521	-0.9102	88.4	-0.1478	9	-0.3265	88.4	-0.1478	9	-0.3265	88.4	-0.1478
76.0	-0.3843	3.3376	76.0	0.5146	-4.1222	-1.1414	0.5146	-4.1222	-1.1414	101.1	-0.1478	10	-0.3265	101.1	-0.1478	10	-0.3265	101.1	-0.1478
78.0	-6.9784	-4.0289	78.0		-102.2755	-0.8920		-102.2755	-0.8920	101.1	-0.1478	11	-0.3265	101.1	-0.1478	11	-0.3265	101.1	-0.1478
80.5	-110.6728	3.3626	80.5		-8.4903	-1.0039		-8.4903	-1.0039	101.1	-0.1478	12	-0.3265	101.1	-0.1478	12	-0.3265	101.1	-0.1478
81.0	-107.9295	1.0114	81.0		467.8423	-0.8920		467.8423	-0.8920	101.1	-0.1478	13	-0.3265	101.1	-0.1478	13	-0.3265	101.1	-0.1478
82.0	-105.1944	-1.7877	82.0		-8.4573	-1.1719		-8.4573	-1.1719	101.1	-0.1478	14	-0.3265	101.1	-0.1478	14	-0.3265	101.1	-0.1478
84.0	-57.2106		84.0	-89.5673	-4.1949	-0.9480	-89.5673	-4.1949	-0.9480	101.1	-0.1478	15	-0.3265	101.1	-0.1478	15	-0.3265	101.1	-0.1478
87.0	-59.6186		87.0	-7.5538	-2.6826	-0.8920	-7.5538	-2.6826	-0.8920	101.1	-0.1478	16	-0.3265	101.1	-0.1478	16	-0.3265	101.1	-0.1478
89.0	-1.3898		89.0	9.7051	-3.0213	-1.1452	9.7051	-3.0213	-1.1452	101.1	-0.1478	17	-0.3265	101.1	-0.1478	17	-0.3265	101.1	-0.1478
93.0	15.1699		93.0	3.3027	-1.6170	-1.0778	3.3027	-1.6170	-1.0778	101.1	-0.1478	18	-0.3265	101.1	-0.1478	18	-0.3265	101.1	-0.1478
96.0	8.9559		96.0	-0.4713	-1.4148	-1.0104	-0.4713	-1.4148	-1.0104	101.1	-0.1478	19	-0.3265	101.1	-0.1478	19	-0.3265	101.1	-0.1478
100.0	3.2470		100.0	-3.1671	-1.6170	-0.8082	-3.1671	-1.6170	-0.8082	101.1	-0.1478	20	-0.3265	101.1	-0.1478	20	-0.3265	101.1	-0.1478
96.0	0.4318		96.0	0.2028	0.4722	0.3374	0.2028	0.4722	0.3374	101.1	-0.1478	21	-0.3265	101.1	-0.1478	21	-0.3265	101.1	-0.1478
84.0	3.2470		84.0	0.4722	0.6744	-0.3385	0.4722	0.6744	-0.3385	101.1	-0.1478	22	-0.3265	101.1	-0.1478	22	-0.3265	101.1	-0.1478
73.0	0.4318		73.0	0.3823	-0.2487	0.6968	0.3823	-0.2487	0.6968	101.1	-0.1478	23	-0.3265	101.1	-0.1478	23	-0.3265	101.1	-0.1478
50.0	0.9285		50.0	0.0879	0.3823	0.3823	0.0879	0.3823	0.3823	101.1	-0.1478	24	-0.3265	101.1	-0.1478	24	-0.3265	101.1	-0.1478
35.0	0.8237		35.0	-0.5612	0.0679	0.0679	-0.5612	0.0679	0.0679	101.1	-0.1478	25	-0.3265	101.1	-0.1478	25	-0.3265	101.1	-0.1478
25.0	0.0034		25.0	-0.7289	-0.8377	-0.0763	-0.7289	-0.8377	-0.0763	101.1	-0.1478	26	-0.3265	101.1	-0.1478	26	-0.3265	101.1	-0.1478
10.0	0.0809		10.0	-0.5114	-1.0552	-0.4026	-0.5114	-1.0552	-0.4026	101.1	-0.1478	27	-0.3265	101.1	-0.1478	27	-0.3265	101.1	-0.1478
5.0	0.0034		5.0	-0.4026	-0.7289	-0.1851	-0.4026	-0.7289	-0.1851	101.1	-0.1478	28	-0.3265	101.1	-0.1478	28	-0.3265	101.1	-0.1478
2.5	-0.0742		2.5	-0.4026	-0.8377	-0.1851	-0.4026	-0.8377	-0.1851	101.1	-0.1478	29	-0.3265	101.1	-0.1478	29	-0.3265	101.1	-0.1478
0.0	0.3135		0.0	-0.4026	-0.8377	-0.1851	-0.4026	-0.8377	-0.1851	101.1	-0.1478	30	-0.3265	101.1	-0.1478	30	-0.3265	101.1	-0.1478

C-5

TABLE A30. (Continued)

RUN:SEQ																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																											
298	3	CLAERO = -0.0367				CDRO = 0.6375				DCLC = 1.2544				PRESSURES				BASEPR = 8.1905				PAGE 749																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																					
ALPHA		PTOT		PSTAT		Q		VEL		YAW		H/C		CMUC		CMUW		HGT		BN		87.4363		0.325022E+06																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																			
3.97		2142.03		2138.86		3.17		51.80		-0.08		2.37		1.464		1.985		3.448				CLTR		CDTR																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																			
BETA		CL		CD		CM		CROLL		CN		CV		CCTR		CMTT		O.85		O.84																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																							
0.08		3.00		-0.79		-0.63		0.02		-0.02		-0.11		0.69		-0.17																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																											
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%X/C		CP		%X/C		CP		BP = 2		BP = 6		BP = 12		BP = 16		BP = 22		XLOC		CP		38.2		-0.3449		1.1953		1		-0.5926		3		0.0363		3		-0.5926		4		0.0363		5		0.5926		6		0.0323		7		-0.3008		8		-0.2333		9		-0.1699		10		-0.2333		11		-0.3006		12		-0.3008																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																	
0.0		-0.7259		0.0		-0.8429		-0.8429		0.0001		-0.4341		-1.1953		-1.5215		-0.8891		80.4		-0.0126		56.1		0.1517		62.5		0.0690		89.7		0.1517		76.9		-0.0136		83.4		-0.0136		89.4		-0.0690		95.4		-0.2333		101.1		-0.3006		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449		38.2		-0.3449	

TABLE A50. (Concluded)

A4.0 TABULATED DOWNWASH DATA

Table A51 presents the tabulation of downwash measurements behind the wing of the propulsive wing/canard. Downwash data are presented for the full span and 1/2 span blowing nozzles. The downwash of the short (1/4) span was not measured.

TABLE A51. TABULATED DOWNMASH DATA

RUN	POINT	V _∞	VPROBE	ε	CONFIG*	δ _F	VARIABLE	C _{μw}	C _L	C _{LTR}
57	11	157.16	97.52	1.92	BW6V	0	α=0	0	0.142	
57	12	157.86	99.79	1.95			2	0	0.232	
57	13	158.52	100.07	2.95			4	0	0.322	
57	15	158.95	96.66	4.67			8	0	0.532	
57	17	159.05	98.66	9.52			12	0	0.752	
59	2	164.34	102.56	4.04	BW6V	0	γ=0	0.5	0.369	0.265
59	3	163.83	103.37	5.14			2	0.5	0.495	0.377
59	6	163.33	103.37	5.89			4	0.5	0.617	0.483
59	8	163.68	106.57	9.08			8	0.5	0.862	0.704
59	10	164.63	107.09	14.76			12	0.5	1.143	0.962
61	4	101.174	66.06	5.50	BW6V	0	α=0	1.0	0.580	0.296
61	5	100.682	69.36	6.22			2	1.0	0.732	0.412
61	6	101.144	68.14	7.45			4	1.0	0.887	0.533
61	9	101.103	68.55	11.32			8	1.0	1.144	0.723
61	12	100.587	74.05	16.35			12	1.0	1.501	0.100
62	2	70.399	46.98	8.89	BW6V	0	α=0	2.0	0.898	0.320
62	3	70.369	49.51	8.64			2	2.0	1.075	0.427
62	4	70.377	48.73	10.44			4	2.0	1.266	0.551
62	6	70.358	49.61	12.94			8	2.0	1.650	0.800
62	8	71.666	53.94	18.28			12	2.0	2.029	1.098
64	3	159.158	111.19	4.11	BW6V	15	α=0	0	0.470	
64	4	159.230	111.44	5.20			2	0	0.560	
64	5	159.581	112.44	6.59			4	0	0.653	
64	7	157.348	114.17	9.60			8	0	0.845	
64	9	159.087	117.55	15.60			12	0	1.083	

*CONFIG. code on Table 3

TABLE A51. TABULATED DOWNWASH DATA (Continued)

RUN	POINT	V _∞	V _{PROBE}	ε	CONFIG.	δ _F	VARIABLE	C _{μW}	C _L	C _{LTR}
65	4	152.700	114.11	7.98	BW6V	15	α=0	0.5	0.923	0.687
65	5	152.700	115.72	9.93			2	0.5	0.988	0.740
65	6	153.322	116.33	11.45			4	0.5	1.053	0.792
65	8	153.308	119.76	15.62			8	0.5	1.186	0.902
65	10	152.031	123.60	21.09			12	0.5	1.355	1.042
66	2	105.835	83.27	10.88	BW6V	15	α=2	1.0	1.433	0.910
66	3	105.357	81.80	8.82			0	1.0	1.308	0.806
66	5	105.756	83.32	14.52			4	1.0	1.584	1.034
66	7	105.716	85.93	17.00			8	1.0	1.892	1.294
66	10	104.784	87.75	22.70			12	1.0	2.279	1.622
67	2	76.092	63.51	9.91	BW6V	15	α=0	2.0	1.860	0.901
67	3	76.076	62.95	11.48			2	2.0	2.041	1.029
67	4	76.675	63.04	13.25			4	2.0	2.179	1.136
67	6	76.555	63.77	17.01			8	2.0	2.255	1.417
67	8	76.022	66.61	21.80			12	2.0	3.018	1.768
69	3	157.198	110.18	2.57	BC1W6V	15	α=0	0	0.489	
69	4	157.884	109.93	1.25			2	0	0.592	
69	6	158.280	115.66	-0.31			4	0	0.700	
69	8	158.358	143.29	27.10			8	0	0.938	
69	10	157.539	139.48	30.16			12	0	1.221	
70	2	151.288	115.73	6.20	BC1W6V	15	α=0	0.5	1.099	0.792
70	3	151.608	114.91	6.90			2	0.5	1.246	0.922
70	4	151.906	125.83	8.31			4	0.5	1.381	1.042
70	6	156.534	134.22	8.59			8	0.5	1.656	
70	9	155.363	136.49	14.52			12	0.5	2.038	1.649

TABLE A51. TABULATED DOWNWASH DATA (Continued)

RUN	POINT	V_{∞}	VPROBE	ϵ	CONFIG.	δ_F	VARIABLE	$C_{\mu W}$	C_L	$C_{L_{TR}}$
71	2	110.406	85.05	8.12	BC1W6V	15	$\alpha=0$	1.0	1.420	0.833
71	3	110.384	87.34	10.07			2	1.0	1.594	0.972
71	5	110.775	85.71	11.48			4	1.0	1.769	1.116
71	7	109.895	102.83	9.20			8	1.0	2.183	1.455
71	9	109.027	114.91	14.29			12	1.0	2.638	1.838
72	3	78.716	62.31	9.61	BC1W6V	15	$\alpha=0$	2.0	2.062	0.883
72	5	78.669	61.64	11.72			2	2.0	2.229	1.045
72	6	78.665	52.22	11.32			4	2.0	2.471	1.221
72	9	78.623	70.24	12.99			8	2.0	1.577	2.948
72	12	77.443	76.28	13.09			12	2.0	2.019	3.547
75	10	149.540	113.19	4.23	BC1W6V	45	$\alpha=0$	0	2.371	
75	11	148.960	117.31	2.33			2	0	2.535	
75	12	148.311	112.20	2.47			4	0	2.688	
76	2	148.624	116.45	8.06	BC1W6V	45	$\alpha=0$	0.5	1.578	1.049
76	3	150.850	123.54	9.55			2	0.5	1.641	1.118
76	4	150.576	123.08	12.15			4	0.5	1.756	1.221
76	7	149.156	132.45	15.70			8	0.5	2.079	1.523
76	10	149.540	141.47	18.59			12	0.5	2.371	1.805
77	2	105.958	85.68	8.35	BC1W6V	45	$\alpha=0$	1.0	2.330	1.273
77	3	105.509	84.81	10.09			2	1.0	2.469	1.386
77	4	105.962	85.04	13.51			4	1.0	2.585	1.495
77	6	104.656	92.92	17.84			8	1.0	2.960	1.822
77	8	102.856	100.85	19.22			12	1.0	3.459	2.256
79	3	74.745	59.82	9.13	BC1W6V	45	$\alpha=0$	1.0	3.456	1.298
79	9	74.750	60.62	14.47			8	1.0	4.110	1.870
79	11	74.139	71.08	18.58			12	1.0	4.614	2.304

TABLE A51. TABULATED DOWNWASH DATA (Continued)

RUN	POINT	V_{∞}	VPRODE	ϵ	CONFIG.	δ_F	VARIABLE	C_{μ_w}	C_L	$C_{L_{TR}}$
85	2	158.756	114.66	5.13	BC2W6V	45	$\alpha=0$	0	0.514	
85	4	158.864	113.93	6.36			2	0	0.601	
85	7	159.301	118.97	10.30			8	0	0.917	
85	9	159.381	117.55	14.50			12	0	1.139	
86	1	150.652	120.53	7.48	BC2W6V	45	$\alpha=0$	0.5	1.543	1.037
86	2	150.023	119.40	8.39			2	0.5	1.615	1.034
86	3	151.610	124.14	11.63			4	0.5	1.675	1.147
86	4	153.514	121.23	10.24			4	0.5	1.657	1.149
86	5	152.911	125.90	15.44			8	0.5	1.945	1.436
86	6	150.731	143.52	20.68			12	0.5	2.222	1.727
86	7	151.082	144.70	21.91			12	0.5	2.218	1.677
87	1	104.471	87.42	8.74	BC2W6V	45	$\alpha=0$	1.0	2.649	1.608
87	2	104.412	84.46	9.64			2	1.0	2.761	1.702
87	4	103.928	84.77	10.80			4	1.0	2.857	1.774
87	5	103.467	85.80	12.51			8	1.0	2.982	1.863
87	6	101.585	95.25	18.98			12	1.0	3.367	2.165
88	1	74.305	62.35	6.65	BC2W6V	45	$\alpha=0$	2.0	3.950	1.918
88	2	72.376	59.71	8.43			2	2.0	4.217	2.029
88	4	74.898	60.09	9.39			4	2.0	4.140	2.037
88	5	74.229	58.58	13.68			8	2.0	4.301	2.106
88	7	73.583	63.99	17.54			12	2.0	4.617	2.337
89	2	149.841	122.26	11.31	BC2W6V	45	$h=14.3$	0.5	1.861	1.365
89	3	149.817	124.14	11.71			16.4	0.5	1.827	1.310
89	5	151.079	123.17	9.25			32.7	0.5	1.607	1.102
89	6	150.171	115.52	9.14			65.6	0.5	1.529	1.018
89	7	150.609	117.29	9.05			87.0	0.5	1.504	0.995

TABLE A51. TABULATED DOWNWASH DATA (Continued)

RUN	POINT	V_{∞}	VPROBE	ϵ	CONFIG.	δ_F	VARIABLE	$C_{\mu W}$	C_L	C_{LTR}
90	1	75.349	60.62	11.70	BC2M6V	45	$h=14.5$	2.0	4.157	2.149
90	2	75.318	59.75	12.98			16.4	2.0	4.111	2.102
90	3	76.441	66.96	8.30			32.7	2.0	3.812	1.863
90	4	79.283	57.25	8.05			65.4	2.0	3.573	1.757
90	5	74.694	54.92	8.87			87.0	2.0	3.852	1.804
92	2	157.717	113.93	4.71	BC2M6V	45	$h=14.2$	0	0.741	
92	3	158.016	115.63	4.42			16.4	0	0.702	
92	4	156.860	108.91	6.25			32.7	0	0.602	
92	5	158.314	113.75	6.83			65.4	0	0.543	
92	6	158.591	111.70	6.52			87.0	0	0.524	
97	2	159.243	113.73	8.32	BC2M5V	45	$\alpha=0$	0	0.577	
97	3	159.412	111.22	8.98			0	0	0.576	
97	4	159.822	111.86	10.71			2	0	0.663	
97	5	159.596	112.61	11.95			4	0	0.750	
97	6	159.982	115.65	14.55			8	0	0.891	
97	7	160.046	113.36	19.59			12	0	1.076	
98	1	143.023	124.91	8.24	BC2M5V	45	$\alpha=0$	0.5	1.834	1.242
98	3	143.766	126.32	11.04			2	0.5	1.905	1.304
98	4	144.800	137.69	11.24			4	0.5	1.987	1.385
98	5	144.834	148.34	17.71			8	0.5	2.217	1.599
98	6	144.523	157.68	23.03			12	0.5	2.393	1.758
99	2	99.412	90.60	8.01	BC2M5V	45	$\alpha=0$	1.0	3.088	1.855
99	4	101.778	92.31	10.50			2	1.0	3.111	1.914
99	6	99.834	93.63	11.33			4	1.0	3.295	2.034
99	7	100.766	104.14	13.56			8	1.0	3.485	2.212
99	8	98.838	108.76	18.55			12	1.0	3.761	2.413

TABLE A51. TABULATED DOWNWASH DATA (Continued)

RUN	POINT	V_{∞}	V_{PROBE}	ϵ	CONFIG.	δ_F	VARIABLE	C_{μ_w}	C_L	$C_{L_{TR}}$
100	2	73.145	60.78	6.89	BC2W5V	45	$\alpha=0$	2.0	4.332	2.042
100	3	71.161	59.04	8.42			2	2.0	4.587	2.127
100	4	72.457	59.41	7.27			4	2.0	4.581	2.174
100	5	72.481	63.81	11.02			6	2.0	4.720	2.281
100	6	71.798	66.82	9.69			8	2.0	4.885	2.370
100	7	73.106	74.45	16.28			12	2.0	5.062	2.586
108	3	159.033	109.16	3.64	PC3W6V	45	$\alpha=0$	0	0.544	
108	4	159.396	109.93	3.59			2	0	0.647	
108	6	160.087	94.61	8.76			8	0	0.962	
108	9	159.846	110.55	28.23			12	0	1.199	
109	4	152.576	118.25	8.19	BC3W6V	45	$\alpha=0$	0.5	1.408	0.935
109	5	152.565	120.10	9.96			2	0.5	1.496	1.019
109	7	152.273	120.74	12.35			4	0.5	1.586	1.094
109	12	148.460	136.04	16.83			12	0.5	2.128	1.576
110	2	103.301	82.34	8.79	BC3W6V	45	$\alpha=0$	1.0	2.368	1.364
110	3	103.727	81.30	11.06			2	1.0	2.523	1.512
110	5	105.510	86.35	13.44			4	1.0	2.646	1.657
110	6	104.616	93.96	13.20			8	1.0	2.990	1.950
110	7	105.019	100.78	21.72			12	1.0	3.286	2.202
111	2	75.707	58.21	10.64			$\alpha=0$	2.0	3.374	1.466
111	3	75.061	57.32	10.18	BC3W6V	45	2	2.0	3.575	1.599
111	5	75.036	58.32	10.97			4	2.0	3.786	1.778
111	8	75.015	65.95	14.93			8	2.0	4.345	2.282
111	10	75.630	76.21	19.86			12	2.0	4.704	2.625

TABLE A51. TABULATED DOWNWASH DATA (Continued)

RUN	POINT	V_{∞}	VPROBE	ϵ	CONFIG.	δ_F	VARIABLE	C_{H_W}	C_L	$C_{L_{TR}}$
142	2	160.726	112.19	6.28	BW6V	45	$\alpha=0$	0	0.528	
142	3	161.723	113.92	6.50			2	0	0.615	
142	4	162.090	113.92	7.89			4	0	0.704	
142	5	161.542	112.19	12.00			8	0	0.883	
142	6	161.597	119.95	19.34			12	0	1.088	
143	1	129.910	121.41	8.88	BW6V	45	$\alpha=0$	0.5	1.462	1.080
143	2	129.570	122.13	11.28			2	0.5	1.490	1.100
143	3	131.750	124.91	11.69			4	0.5	1.498	1.116
143	4	131.710	131.11	16.01			8	0.5	1.570	1.179
143	5	133.756	136.07	20.08			12	0.5	1.629	1.242
144	1	88.261	88.95	9.64	BW6V	45	$\alpha=0$	1.0	2.564	1.751
144	2	87.153	87.79	13.27			2	1.0	2.763	1.915
144	3	88.759	91.27	12.53			4	1.0	2.851	2.021
144	4	87.540	91.12	17.89			8	1.0	3.243	2.372
144	5	87.569	92.75	20.71			12	1.0	3.405	2.512
145	1	65.763	61.99	12.76	BW6V	45	$\alpha=0$	2.0	3.439	1.991
145	2	64.344	63.04	10.53			2	2.0	3.652	2.105
145	3	63.569	63.77	12.30			4	2.0	3.834	2.225
145	4	65.081	66.08	15.28			8	2.0	4.122	2.538
145	5	64.329	67.74	19.23			12	2.0	4.423	2.777
146	1	63.788	53.70	9.76	BW6V	45	$\alpha=0$	3.0	4.499	2.276
146	2	64.528	55.10	11.01			2	3.0	4.588	2.380
146	3	64.522	56.92	11.43			4	3.0	4.773	2.533
146	4	63.755	56.73	16.58			8	3.0	5.238	2.891
146	5	63.762	57.72	19.26			12	3.0	5.477	3.088

TABLE A51. TABULATED DOWMASH DATA (Continued)

RUN	POINT	V_{∞}	V_{PROBE}	ϵ	CONFIG.	δ_F	VARIABLE	$C_{\mu W}$	C_L	$C_{L_{TR}}$
147	1	54.752	45.49	9.02	BW6V	45	$\alpha = 0$	4.0	5.497	2.465
147	2	54.749	46.32	10.53			2	4.0	5.672	2.595
147	3	55.620	46.72	10.97			4	4.0	5.689	2.669
147	4	56.480	49.45	14.12			8	4.0	5.935	2.939
147	5	55.616	50.38	17.89			12	4.0	6.420	3.271
148	1	67.401	57.52	9.48	BW6V	45	$\alpha = 0$	2.0	3.496	2.083
148	2	67.391	58.29	12.74			2	2.0	3.663	2.227
148	3	67.383	54.24	14.57			4	2.0	3.800	2.343
148	4	68.104	58.47	16.12			8	2.0	4.197	2.659
148	5	67.376	61.29	18.26			12	2.0	4.534	2.932
149	1	67.389	54.24	10.68	BW6V	45	$\alpha = 0$	1.0	2.490	1.912
149	2	67.383	54.93	12.19			2	1.0	2.624	2.034
149	3	68.093	55.75	13.92			4	1.0	2.685	2.101
149	4	67.370	57.87	18.10			8	1.0	3.031	2.419
149	5	67.370	59.96	21.27			12	1.0	3.358	2.670
153	1	76.777	46.24	13.54	BW6V	45	$h = 14.7$	2.0	2.154	0.638
153	2	76.154	50.32	8.79			16.8	2.0	2.513	0.973
153	3	76.095	58.95	12.36			32.7	2.0	3.530	1.989
153	4	76.729	58.21	7.73			65.5	2.0	3.465	1.946
153	5	76.123	58.99	7.50			87.7	2.0	3.468	1.923
154	1	155.226	115.49	9.92	BW6V	45	$h = 15.3$	0.5	0.984	0.600
154	2	154.628	115.90	10.02			16.5	0.5	0.961	0.581
154	3	153.611	122.99	9.27			32.7	0.5	0.831	0.455
154	4	151.573	119.20	7.96			65.4	0.5	0.815	0.429
154	5	151.350	118.52	8.23			86.9	0.5	0.816	0.425

TABLE A51. TABULATED DOWNWASH DATA (Continued)

RUN	POINT	V_{∞}	VPROBE	ϵ	CONFIG.	δ_F	VARIABLE	C_{H_W}	C_L	$C_{L_{TR}}$
155	1	160.556	110.94	4.49	BW6V	45	h=14.9	0	0.723	
155	2	160.883	110.44	4.86			16.5	0	0.701	
155	3	160.013	109.42	4.84			33.3	0	0.606	
155	4	160.313	108.91	6.11			65.7	0	0.552	
155	5	160.362	109.16	5.35			87.1	0	0.530	
156	1	161.623	110.69	5.37	BW6V	45	h=14.9	0	0.727	
156	2	161.651	111.45	4.94			16.5	0	0.706	
156	3	161.067	109.42	5.86			32.6	0	0.609	
156	4	161.779	113.61	7.22			65.5	0	0.550	
156	5	160.204	110.69	6.42			87.3	0	0.526	
157	1	154.846	113.29	11.23	BW6V	45	h=15.5	0.5	0.998	0.626
157	2	154.213	114.61	12.22			16.4	0.5	0.982	0.607
157	4	154.248	124.48	10.06			32.6	0.5	0.828	0.447
157	5	152.819	121.66	8.83			65.6	0.5	0.789	0.395
157	6	154.085	121.11	8.89			87.3	0.5	0.764	0.377
158	1	106.073	78.39	11.69	BW6V	45	h=15.6	1.0	2.078	1.269
158	2	106.456	79.66	12.92			16.4	1.0	2.052	1.248
158	3	107.147	89.87	10.34			32.6	1.0	1.883	1.088
158	4	107.154	85.91	8.45			65.6	1.0	1.814	1.018
158	6	106.308	85.54	10.89			87.0	1.0	1.810	0.999
159	1	78.740	56.33	8.93	BW6V	45	h=14.9	2.0	2.428	0.949
159	2	77.613	50.67	11.09			16.4	2.0	2.536	1.007
159	3	76.241	64.61	11.38			32.9	2.0	3.668	2.095
159	4	77.458	62.63	10.30			65.5	2.0	3.559	2.029
159	5	76.856	61.93	11.53			86.9	2.0	3.558	2.002

TABLE A51. TABULATED DOWNMASH DATA

RUN	POINT	V_{∞}	VPRODE	ϵ	CONFIG.	δ_F	VARIABLE	$C_{\mu W}$	C_L	$C_{L_{TR}}$
160	1	76.226	64.45	16.38	BW6V	45	$h=30.4$	2.0	3.899	2.269
160	2	76.817	62.80	15.63			32.6	2.0	3.850	2.245
160	3	76.817	64.63	12.61			65.5	2.0	3.575	2.039
160	4	78.000	64.45	14.27			87.2	2.0	3.600	2.040
161	1	104.795	86.85	16.69	BW6V	45	$h=30.4$	1.0	2.140	1.269
161	2	107.436	90.46	15.88			32.4	1.0	2.024	1.192
161	3	108.308	88.48	12.67			65.5	1.0	1.894	1.078
161	4	107.033	87.48	13.92			87.1	1.0	1.900	1.065
162	1	151.796	124.64	16.64	BW6V	45	$h=30.4$	0.5	0.916	0.520
162	2	152.435	126.17	15.18			32.8	0.5	0.892	0.499
162	3	153.404	122.49	13.17			65.8	0.5	0.814	0.425
162	4	153.291	123.13	12.45			87.0	0.5	0.806	0.417
163	1	169.088	111.45	8.22	BW6V	45	$h=29.4$	0	0.808	
163	2	160.708	111.20	7.87			32.9	0	0.797	
163	3	160.120	110.44	8.24			65.3	0	0.729	
163	4	161.011	111.20	8.20			87.1	0	0.702	
171	2	157.605	118.97	- 2.67	BC1V	45	$\alpha=0$	0	0.201	
171	3	157.701	116.84	- 2.54			2	0	0.239	
171	4	157.488	110.94	3.41			4	0	0.279	
171	5	157.872	105.00	23.62			8	0	0.348	
171	6	157.985	115.87	13.51			12	0	0.374	
172	1	150.558	108.39	- 2.14	BC1V	45	$\alpha=0$	0.25	0.487	
172	2	149.074	111.70	- 2.00			2	0.25	0.531	
172	3	149.454	119.68	- 3.09			4	0.25	0.562	
172	5	149.817	142.64	23.99			8	0.25	0.663	
172	6	149.540	139.61	17.36			12	0.25	0.837	

TABLE A51. TABULATED DOWNWASH DATA (Continued)

RUN	POINT	V_{∞}	VPROBE	ϵ	CONFIG.	δ_F	VARIABLE	C_{H_C}	C_L	$C_{L_{TR}}$
173	1	102.061	72.13	- 0.59	BC1V	45	$\alpha=0$	0.5	0.724	0.435
173	2	102.521	73.29	- 1.58			2	0.5	0.769	0.491
173	3	102.890	75.54	- 1.37			4	0.5	0.827	0.558
173	4	102.964	92.69	- 1.06			8	0.5	0.926	0.674
173	5	102.506	81.93	4.54			12	0.5	1.025	0.788
174	1	74.926	52.36	1.99	BC1V	45	$\alpha=0$	1.0	0.971	0.430
174	2	70.393	50.73	- 0.42			2	1.0	1.083	0.486
174	3	70.370	50.17	- 0.31			4	1.0	1.141	0.560
174	4	72.956	53.42	1.85			8	1.0	1.182	0.692
176	2	158.081	112.20	- 2.23	BC1V	45	$\alpha=0$	0	1.115	1.092
176	3	158.123	107.61	- 2.45			2	0	1.466	1.444
176	4	158.495	107.61	8.77			4	0	1.778	1.755
176	5	158.571	111.70	14.37			8	0	0.252	0.249
176	6	158.355	114.66	9.13			12	0	0.343	0.341
177	1	143.431	106.04	- 2.24	BC1V	45	$\alpha=0$	0.25	0.427	0.303
177	2	146.725	110.69	- 3.44			2	0.25	0.465	0.344
177	3	146.081	123.86	- 3.53			4	0.25	0.519	0.394
177	4	148.665	147.57	- 0.85			8	0.25	0.576	0.452
177	5	148.378	137.84	30.28			12	0.25	0.754	0.622
178	1	102.817	73.29	- 0.62	BC1V	45	$\alpha=0$	0.5	0.596	0.355
178	2	102.788	73.67	- 1.15			2	0.5	0.640	0.392
178	3	102.308	73.29	- 0.78			2	0.5	0.642	0.301
178	4	102.746	77.01	- 0.38			4	0.5	0.694	0.440
178	5	103.651	99.16	2.11			8	0.5	0.810	0.548
178	6	106.320	77.01	11.82			12	0.5	0.938	0.679

TABLE A51. TABULATED DOWNWASH DATA

RUN	POINT	V_{∞}	VPROBE	ϵ	CONFIG.	δ_F	VARIABLE	$C_{\mu C}$	C_L	C_{LTR}
179	1	74.097	50.73	1.17	BC1V	45	$\alpha=0$	1.0	0.819	0.352
179	2	72.814	48.47	2.49			2	1.0	0.898	0.401
179	3	69.533	50.73	1.58			4	1.0	1.014	0.456
179	4	70.187	56.96	3.18			8	1.0	1.114	0.542
179	5	70.181	71.35	5.59			12	1.0	1.280	0.687
181	3	157.599	111.70	- 0.15	BV	0	$\alpha=0$	0	-0.000	-0.038
181	4	158.035	115.63	2.39			2	0	-0.000	-0.033
181	5	157.780	118.97	- 0.46			4	0	0.104	-0.027
181	6	157.831	121.99	- 0.55			8	0	0.022	-0.015
181	7	157.583	125.85	- 2.04			12	0	0.039	0.002
187	2	156.237	128.68	6.93	BM6V	45	$\alpha=0$	$C_{\mu W}$	0.546	
187	3	156.939	128.33	7.93			2	0	0.636	
187	4	157.007	127.43	9.66			4	0	0.720	
187	5	157.097	125.92	12.41			8	0	0.911	
187	6	156.262	124.39	20.65			12	0		
188	1	155.868	130.67	7.01	BM6V	45	$\alpha=0$	$b_W=1/2$	0.885	0.627
188	2	153.483	129.06	8.02			2	0.5	0.964	0.692
188	3	154.131	130.34	9.23			4	0.5	1.013	0.738
188	4	158.090	133.78	14.00			8	0.5	1.080	0.810
188	5	155.132	149.57	21.90			12	0.5	1.200	0.912
189	1	107.023	99.72	7.41	BM6V	45	$\alpha=0$	$b_W=1/2$	1.527	0.977
189	2	109.171	101.22	9.55			2	1.0	1.587	1.047
189	3	107.427	96.56	15.39			8	1.0	1.872	1.244
189	4	110.382	108.82	20.90			12	1.0	1.970	1.400

TABLE A51. TABULATED DOWNWASH DATA (Continued)

RUN	POINT	V_{∞}	VPROBE	ϵ	CONF'G.	δ_F	VARIABLE	C_{LW}	C_L	C_{LTR}
190	1	77.350	73.37	6.26	BN6V	45	$\alpha=0$	$b_N=1/2$	2.142	1.088
190	2	77.745	72.82	9.14			2	2.0	2.279	1.186
190	3	77.927	73.85	8.95			4	2.0	2.330	1.250
190	4	77.337	77.30	15.95			8	2.0	2.627	1.495
190	5	76.732	77.76	17.96			12	2.0	2.800	1.619
216	2	128.442	104.65	7.59	BC1W6V	45	$\alpha=0$	0	0.526	0.433
216	3	128.477	107.87	5.19			2	0	0.650	0.556
216	4	128.864	113.07	5.50			4	0	0.759	0.665
216	5	128.888	89.89	19.02			8	0	0.996	0.901
216	7	128.566	113.07	34.54			12	0	1.226	1.131
217	1	80.186	73.71	9.82	BC1W6V	45	$\alpha=0$	$b_N=1/2$	2.023	0.932
217	3	80.167	73.72	8.94			2	1.0	2.003	0.892
217	4	80.155	73.08	9.27			4	1.0	2.076	0.943
217	5	79.563	79.67	11.81			8	1.0	2.434	1.246
217	6	78.405	93.10	14.33			12	1.0	2.893	1.632
218	1	57.454	39.95	5.14	BC1W6V	45	$\alpha=0$	$b_N=1/2$	3.292	1.160
218	2	55.827	38.61	9.49			2	2.0	3.510	1.200
218	3	56.622	36.68	10.17			4	2.0	3.412	1.122
218	4	58.215	36.10	11.88			8	2.0	3.434	1.188
218	5	56.610	40.97	12.82			12	2.0	4.018	1.571

TABLE A51. TABULATED DOWNMASH DATA (Continued)

RUN	POINT	V _∞	VPROBE	ε	CONFIG.	δ _F	VARIABLE	C _{μ_w}	C _L	C _{LTR}
227	1	60.963	52.89	5.46	BW6V	45	h=14.3	b _W =1/2	2.104	0.655
227	2	61.674	56.64	7.13			16.4	2.0	2.770	1.321
227	3	65.085	48.35	9.85			32.6	2.0	2.668	1.369
227	4	60.253	43.83	5.70			65.6	2.0	2.765	1.250
227	5	59.489	40.03	10.87			86.7	2.0	2.817	1.266
228	1	83.702	68.75	9.39	BW6V	45	h=14.4	b _W =1/2	1.913	1.176
228	2	84.223	68.79	11.78			16.3	1.0	2.034	1.261
228	3	90.182	68.27	8.28			32.6	1.0	1.824	1.144
228	5	87.728	63.91	8.15			65.5	1.0	1.801	1.084
229	1	116.119	94.92	9.84	BW6V	45	h=14.8	b _W =1/2	1.582	1.239
229	2	111.035	84.76	9.21			16.3	0.5	1.659	1.281
229	3	114.876	89.20	6.46			32.7	0.5	1.478	1.126
229	5	112.610	87.10	6.46			64.7	0.5	1.428	1.062
229	6	115.743	87.65	7.00			87.2	0.5	1.385	1.039
230	1	128.458	93.75	8.65	BW6V	45	h=14.8	0	0.762	0.816
230	2	128.446	94.15	8.69			16.3	0	0.742	0.796
230	3	128.089	94.56	7.23			32.7	0	0.641	0.696
230	4	126.983	95.67	7.80			65.3	0	0.582	0.638
230	5	126.668	94.74	6.73			86.9	0	0.565	0.622
231	1	127.604	92.52	14.25	BW6V	45	α=8	0	1.006	1.063
231	2	127.545	93.42	13.30			h=43.7	0	0.949	1.006
231	3	127.024	95.50	12.64			64.8	0	0.928	0.986
							86.8			

TABLE A51. TABULATED DOWNWASH DATA (Concluded)

RUN	POINT	V_{∞}	VPROBE	ϵ	CONFIG.	δ_F	VARIABLE	$C_{\mu W}$	C_L	C_{LTR}
232	2	114.951	97.45	17.04	BM6V	45	$\alpha=8$ $h=44.5$ 65.4 87.1	0.5	1.785 1.726 1.686	1.405 1.344 1.302
232	4	114.968	91.63	14.18						
232	5	115.076	88.92	14.92						
233	1	77.974	67.83	15.47	BM6V	45	$\alpha=8$ $h=44.5$ 65.5 87.0 44.5 65.2 86.7	1.0	2.618 2.546 2.532 3.462 3.298 3.251	1.791 1.745 1.721 1.953 1.833 1.792
233	2	78.993	63.06	14.52						
233	3	78.434	61.75	17.31						
233	4	57.364	51.41	15.53						
233	7	56.113	45.47	14.96						
233	9	58.091	45.13	16.78						

A5.0 TABULATED RUN INDEX

Table A52 presents the Run Index for NASA-LaRC Test 290.

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TABLE A52. (Continued)

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DATE

NASA-LARC TEST 240 14.5 x 21.35 inch FULL-SPAN PULSIVE WING																								
Run No	Configuration	25°	30°	35°	40°	45°	50°	55°	60°	Sc	S _{FE}	S _{FE}	S _{FE}	Sc	Sc	Sc	Sc	Sc	Sc	Q	α	β	Remarks	Notes
80	BWC	1	1	6	1	0°	45°	45°												6.7	0°	0°		
81	BWC	1	1	6	1	0°	45°	45°												23	0°	0°		
82	BWC	1	1	6	1	0°	45°	45°												30	0°	0°		
83	BWC	1	1	6	2	0°	45°	45°												0	0°	0°		
84	BWC	1	1	6	2	0°	45°	45°												0	0°	0°		
85	BWC	1	1	6	2	0°	45°	45°												0	0°	0°		
86	BWC	1	1	6	2	0°	45°	45°												0	0°	0°		
87	BWC	1	1	6	2	0°	45°	45°												0	0°	0°		
88	BWC	1	1	6	2	0°	45°	45°												0	0°	0°		
89	BWC	1	1	6	2	0°	45°	45°												0	0°	0°		
89	BWC	1	1	6	2	0°	45°	45°												0	0°	0°		
90	BWC	1	1	6	2	0°	45°	45°												0	0°	0°		
91																				0	0°	0°		
92	BWC	1	1	6	2	0°	45°	45°												0	0°	0°		
93	BWC	1	1	5	2	0°	45°	45°												0	0°	0°		
94	BWC	1	1	5	2	0°	45°	45°												0	0°	0°		
95	BWC	1	1	5	2	0°	45°	45°												0	0°	0°		
96	BWC	1	1	5	2	0°	45°	45°												0	0°	0°		
97	BWC	1	1	5	2	0°	45°	45°												0	0°	0°		
98	BWC	1	1	5	2	0°	45°	45°												0	0°	0°		
98	BWC	1	1	5	2	0°	45°	45°												0	0°	0°		
115, 2, 0, 2, 3																								

TABLE A52. (Continued)

PREPARED BY										NASA - LARC													
CHECKED BY										TEST 250													
DATE										14.51 31.75 VOR													
										FULL-SPAN													
										PROFULSIVE													
										WING													
BAR NO	CONFIGURATION	29 25 30	29 25 30	29 25 30	29 25 30	29 25 30	SC	SF ₁₀	SF ₄₅	SF ₉₀	SEV DATA	DOWN	W _L	M _{PR}	C _M _W	C _M _C	Q	α	β	REMARKS	111	111	
118	BWC	1	1	6	1	10°	45°	45°			Y		∞	1.0	0	0	30	B	0°			1/2	
119	BWC	1	1	6	1	10°	45°	45°			Y		∞	2.5	.5	.21	27.5	B	0°			1/2	
120	BWC	1	1	6	1	10°	45°	45°			Y		∞	2.5	1.0	.43	13.9	B	0°			1/2	
121	BWC																					1/2	
122	BWC	1	1	6	1	10°	45°	15°					∞	1.0	-	-	0	0°	0°		RUN ABORTED - 1 Fully MDP		1/2
123	BWC										Y										N.G.		1/2
124	BWC	1	1	6	1	10°	45°	45°			Y		∞	2.5	2.0	.88	6.7	B	0°			1/2	
125	BWC	1	1	6	1	10°	45°	45°					A	2.5	2.0	.87	7.0	0°	0°			1/2	
126	BWC	1	1	6	1	10°	45°	45°					A	2.5	1.0	.44	14	0°	0°			1/2	
127	BWC	1	1	6	1	10°	45°	45°					A	2.5	.5	.22	28.5	0°	0°			1/2	
128	BWC	1	1	6	1	10°	45°	45°			Y		A	1.0	0	0	30	0°	0°			1/2	
129											Y										RUN N.G.		1/2
130	BWC	1	1	6	1	0°	45°	45°					∞	2.4	1.0	.44	12.8	B	0°			1/2	
131	BWC	1	1	6	1	0°	45°	45°					∞	2.5	3.0	1.28	4.5	B	0°			1/2	
132	BWC	1	1	6	1	0°	45°	45°					∞	2.5	4.0	1.74	3.4	B	0°			1/2	
133	BWC	1	1	6	1	0°	45°	45°					∞	2.5	2.0	.07	6.9	2°	A			1/2	
134	BWC	1	1	6	1	0°	45°	45°					∞	2.5	.5	.21	28	2°	A			1/2	
135	BWC	1	1	6	1	0°	45°	45°					∞	1.0	0	0	30	2°	A			1/2	
136	BWC	1	1	6	1	0°	45°	45°					B	1.0	0	0	30	2°	0.8			1/2	
137	BWC	1	1	6	1	0°	45°	45°					B	2.5	.5	.22	2.8	2°	0.8			1/2	
																						1-0.8 → F.O.B	
																						1-80 → F.A.O	

ORIGINAL PAGE IS
OF POOR QUALITY

TABLE A52. (Continued)

PREPARED BY			CHECKED BY			DATE			NASA - LARC TEST 230 14.81 21.75 MPH FULL-SPAN Pulsative Wing									
Run	Configuration	29 28	27 26	25 24	23 22	21 20	19 18	17 16	15 14	13 12	11 10	9 8	7 6	5 4	3 2	1 0	Remarks	Wing
138	BWC	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1		1/2
139	BWC	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1		1/2
140	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	WT TARE	1/2
141	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	Static Run	1/2
142	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1		1/2
143	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	100004 INIA PH	1/2
144	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1		1/2
145	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1		1/2
146	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	High CM	1/2
147	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	" "	1/2
148	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	Control Q. Vary NPA	1/2
149	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	" "	1/2
150	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	" "	1/2
151	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	PM > 10K INIB	1/2
152	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	PM > 10K INIB	1/2
153	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1		1/2
154	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	PM > 10K INIB	1/2
155	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1		1/2
156	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1		1/2
157	BW	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	PM > 10K INIB	1/2

TABLE A52. (Continued)

PREPARED BY		CHECKED BY		DATE	
NASA - LARC					
TEST 230					
14.51 21.25 VETA					
FULL - 8PM					
P33 FULL-SIVE					
WING					

Run No	CONFIGURATION	20% 1/2	20% 1/4	20% 3/8	20% 1/2	20% 3/4	20% 1	20% 1 1/4	20% 1 1/2	20% 1 3/4	20% 2	20% 2 1/4	20% 2 1/2	20% 2 3/4	20% 3	20% 3 1/4	20% 3 1/2	20% 3 3/4	20% 4	20% 4 1/4	20% 4 1/2	20% 4 3/4	20% 5	20% 5 1/4	20% 5 1/2	20% 5 3/4	20% 6	20% 6 1/4	20% 6 1/2	20% 6 3/4	20% 7	20% 7 1/4	20% 7 1/2	20% 7 3/4	20% 8	20% 8 1/4	20% 8 1/2	20% 8 3/4	20% 9	20% 9 1/4	20% 9 1/2	20% 9 3/4	20% 10	20% 10 1/4	20% 10 1/2	20% 10 3/4	20% 11	20% 11 1/4	20% 11 1/2	20% 11 3/4	20% 12	20% 12 1/4	20% 12 1/2	20% 12 3/4	20% 13	20% 13 1/4	20% 13 1/2	20% 13 3/4	20% 14	20% 14 1/4	20% 14 1/2	20% 14 3/4	20% 15	20% 15 1/4	20% 15 1/2	20% 15 3/4	20% 16	20% 16 1/4	20% 16 1/2	20% 16 3/4	20% 17	20% 17 1/4	20% 17 1/2	20% 17 3/4	20% 18	20% 18 1/4	20% 18 1/2	20% 18 3/4	20% 19	20% 19 1/4	20% 19 1/2	20% 19 3/4	20% 20	20% 20 1/4	20% 20 1/2	20% 20 3/4	20% 21	20% 21 1/4	20% 21 1/2	20% 21 3/4	20% 22	20% 22 1/4	20% 22 1/2	20% 22 3/4	20% 23	20% 23 1/4	20% 23 1/2	20% 23 3/4	20% 24	20% 24 1/4	20% 24 1/2	20% 24 3/4	20% 25	20% 25 1/4	20% 25 1/2	20% 25 3/4	20% 26	20% 26 1/4	20% 26 1/2	20% 26 3/4	20% 27	20% 27 1/4	20% 27 1/2	20% 27 3/4	20% 28	20% 28 1/4	20% 28 1/2	20% 28 3/4	20% 29	20% 29 1/4	20% 29 1/2	20% 29 3/4	20% 30	20% 30 1/4	20% 30 1/2	20% 30 3/4	20% 31	20% 31 1/4	20% 31 1/2	20% 31 3/4	20% 32	20% 32 1/4	20% 32 1/2	20% 32 3/4	20% 33	20% 33 1/4	20% 33 1/2	20% 33 3/4	20% 34	20% 34 1/4	20% 34 1/2	20% 34 3/4	20% 35	20% 35 1/4	20% 35 1/2	20% 35 3/4	20% 36	20% 36 1/4	20% 36 1/2	20% 36 3/4	20% 37	20% 37 1/4	20% 37 1/2	20% 37 3/4	20% 38	20% 38 1/4	20% 38 1/2	20% 38 3/4	20% 39	20% 39 1/4	20% 39 1/2	20% 39 3/4	20% 40	20% 40 1/4	20% 40 1/2	20% 40 3/4	20% 41	20% 41 1/4	20% 41 1/2	20% 41 3/4	20% 42	20% 42 1/4	20% 42 1/2	20% 42 3/4	20% 43	20% 43 1/4	20% 43 1/2	20% 43 3/4	20% 44	20% 44 1/4	20% 44 1/2	20% 44 3/4	20% 45	20% 45 1/4	20% 45 1/2	20% 45 3/4	20% 46	20% 46 1/4	20% 46 1/2	20% 46 3/4	20% 47	20% 47 1/4	20% 47 1/2	20% 47 3/4	20% 48	20% 48 1/4	20% 48 1/2	20% 48 3/4	20% 49	20% 49 1/4	20% 49 1/2	20% 49 3/4	20% 50	20% 50 1/4	20% 50 1/2	20% 50 3/4	20% 51	20% 51 1/4	20% 51 1/2	20% 51 3/4	20% 52	20% 52 1/4	20% 52 1/2	20% 52 3/4	20% 53	20% 53 1/4	20% 53 1/2	20% 53 3/4	20% 54	20% 54 1/4	20% 54 1/2	20% 54 3/4	20% 55	20% 55 1/4	20% 55 1/2	20% 55 3/4	20% 56	20% 56 1/4	20% 56 1/2	20% 56 3/4	20% 57	20% 57 1/4	20% 57 1/2	20% 57 3/4	20% 58	20% 58 1/4	20% 58 1/2	20% 58 3/4	20% 59	20% 59 1/4	20% 59 1/2	20% 59 3/4	20% 60	20% 60 1/4	20% 60 1/2	20% 60 3/4	20% 61	20% 61 1/4	20% 61 1/2	20% 61 3/4	20% 62	20% 62 1/4	20% 62 1/2	20% 62 3/4	20% 63	20% 63 1/4	20% 63 1/2	20% 63 3/4	20% 64	20% 64 1/4	20% 64 1/2	20% 64 3/4	20% 65	20% 65 1/4	20% 65 1/2	20% 65 3/4	20% 66	20% 66 1/4	20% 66 1/2	20% 66 3/4	20% 67	20% 67 1/4	20% 67 1/2	20% 67 3/4	20% 68	20% 68 1/4	20% 68 1/2	20% 68 3/4	20% 69	20% 69 1/4	20% 69 1/2	20% 69 3/4	20% 70	20% 70 1/4	20% 70 1/2	20% 70 3/4	20% 71	20% 71 1/4	20% 71 1/2	20% 71 3/4	20% 72	20% 72 1/4	20% 72 1/2	20% 72 3/4	20% 73	20% 73 1/4	20% 73 1/2	20% 73 3/4	20% 74	20% 74 1/4	20% 74 1/2	20% 74 3/4	20% 75	20% 75 1/4	20% 75 1/2	20% 75 3/4	20% 76	20% 76 1/4	20% 76 1/2	20% 76 3/4	20% 77	20% 77 1/4	20% 77 1/2	20% 77 3/4	20% 78	20% 78 1/4	20% 78 1/2	20% 78 3/4	20% 79	20% 79 1/4	20% 79 1/2	20% 79 3/4	20% 80	20% 80 1/4	20% 80 1/2	20% 80 3/4	20% 81	20% 81 1/4	20% 81 1/2	20% 81 3/4	20% 82	20% 82 1/4	20% 82 1/2	20% 82 3/4	20% 83	20% 83 1/4	20% 83 1/2	20% 83 3/4	20% 84	20% 84 1/4	20% 84 1/2	20% 84 3/4	20% 85	20% 85 1/4	20% 85 1/2	20% 85 3/4	20% 86	20% 86 1/4	20% 86 1/2	20% 86 3/4	20% 87	20% 87 1/4	20% 87 1/2	20% 87 3/4	20% 88	20% 88 1/4	20% 88 1/2	20% 88 3/4	20% 89	20% 89 1/4	20% 89 1/2	20% 89 3/4	20% 90	20% 90 1/4	20% 90 1/2	20% 90 3/4	20% 91	20% 91 1/4	20% 91 1/2	20% 91 3/4	20% 92	20% 92 1/4	20% 92 1/2	20% 92 3/4	20% 93	20% 93 1/4	20% 93 1/2	20% 93 3/4	20% 94	20% 94 1/4	20% 94 1/2	20% 94 3/4	20% 95	20% 95 1/4	20% 95 1/2	20% 95 3/4	20% 96	20% 96 1/4	20% 96 1/2	20% 96 3/4	20% 97	20% 97 1/4	20% 97 1/2	20% 97 3/4	20% 98	20% 98 1/4	20% 98 1/2	20% 98 3/4	20% 99	20% 99 1/4	20% 99 1/2	20% 99 3/4	20% 100	20% 100 1/4	20% 100 1/2	20% 100 3/4

REMARKS	α	β	C _m	C _m _w	N _{pp}	W _E	SCV	DOWN	S _{F_w}	S _{F_E}	S _C	20% 1/2	20% 1/4	20% 3/8	20% 1/2	20% 3/4	20% 1	20% 1 1/4	20% 1 1/2	20% 1 3/4	20% 2	20% 2 1/4	20% 2 1/2	20% 2 3/4	20% 3	20% 3 1/4	20% 3 1/2	20% 3 3/4	20% 4	20% 4 1/4	20% 4 1/2	20% 4 3/4	20% 5	20% 5 1/4	20% 5 1/2	20% 5 3/4	20% 6	20% 6 1/4	20% 6 1/2	20% 6 3/4	20% 7	20% 7 1/4	20% 7 1/2	20% 7 3/4	20% 8	20% 8 1/4	20% 8 1/2	20% 8 3/4	20% 9	20% 9 1/4	20% 9 1/2	20% 9 3/4	20% 10	20% 10 1/4	20% 10 1/2	20% 10 3/4	20% 11	20% 11 1/4	20% 11 1/2	20% 11 3/4	20% 12	20% 12 1/4	20% 12 1/2	20% 12 3/4	20% 13	20% 13 1/4	20% 13 1/2	20% 13 3/4	20% 14	20% 14 1/4	20% 14 1/2	20% 14 3/4	20% 15	20% 15 1/4	20% 15 1/2	20% 15 3/4	20% 16	20% 16 1/4	20% 16 1/2	20% 16 3/4	20% 17	20% 17 1/4	20% 17 1/2	20% 17 3/4	20% 18	20% 18 1/4	20% 18 1/2	20% 18 3/4	20% 19	20% 19 1/4	20% 19 1/2	20% 19 3/4	20% 20	20% 20 1/4	20% 20 1/2	20% 20 3/4	20% 21	20% 21 1/4	20% 21 1/2	20% 21 3/4	20% 22	20% 22 1/4	20% 22 1/2	20% 22 3/4	20% 23	20% 23 1/4	20% 23 1/2	20% 23 3/4	20% 24	20% 24 1/4	20% 24 1/2	20% 24 3/4	20% 25	20% 25 1/4	20% 25 1/2	20% 25 3/4	20% 26	20% 26 1/4	20% 26 1/2	20% 26 3/4	20% 27	20% 27 1/4	20% 27 1/2	20% 27 3/4	20% 28	20% 28 1/4	20% 28 1/2	20% 28 3/4	20% 29	20% 29 1/4	20% 29 1/2	20% 29 3/4	20% 30	20% 30 1/4	20% 30 1/2	20% 30 3/4	20% 31	20% 31 1/4	20% 31 1/2	20% 31 3/4	20% 32	20% 32 1/4	20% 32 1/2	20% 32 3/4	20% 33	20% 33 1/4	20% 33 1/2	20% 33 3/4	20% 34	20% 34 1/4	20% 34 1/2	20% 34 3/4	20% 35	20% 35 1/4	20% 35 1/2	20% 35 3/4	20% 36	20% 36 1/4	20% 36 1/2	20% 36 3/4	20% 37	20% 37 1/4	20% 37 1/2	20% 37 3/4	20% 38	20% 38 1/4	20% 38 1/2	20% 38 3/4	20% 39	20% 39 1/4	20% 39 1/2	20% 39 3/4	20% 40	20% 40 1/4	20% 40 1/2	20% 40 3/4	20% 41	20% 41 1/4	20% 41 1/2	20% 41 3/4	20% 42	20% 42 1/4	20% 42 1/2	20% 42 3/4	20% 43	20% 43 1/4	20% 43 1/2	20% 43 3/4	20% 44	20% 44 1/4	20% 44 1/2	20% 44 3/4	20% 45	20% 45 1/4	20% 45 1/2	20% 45 3/4	20% 46	20% 46 1/4	20% 46 1/2	20% 46 3/4	20% 47	20% 47 1/4	20% 47 1/2	20% 47 3/4	20% 48	20% 48 1/4	20% 48 1/2	20% 48 3/4	20% 49	20% 49 1/4	20% 49 1/2	20% 49 3/4	20% 50	20% 50 1/4	20% 50 1/2	20% 50 3/4	20% 51	20% 51 1/4	20% 51 1/2	20% 51 3/4	20% 52	20% 52 1/4	20% 52 1/2	20% 52 3/4	20% 53	20% 53 1/4	20% 53 1/2	20% 53 3/4	20% 54	20% 54 1/4	20% 54 1/2	20% 54 3/4	20% 55	20% 55 1/4	20% 55 1/2	20% 55 3/4	20% 56	20% 56 1/4	20% 56 1/2	20% 56 3/4	20% 57	20% 57 1/4	20% 57 1/2	20% 57 3/4	20% 58	20% 58 1/4	20% 58 1/2	20% 58 3/4	20% 59	20% 59 1/4	20% 59 1/2	20% 59 3/4	20% 60	20% 60 1/4	20% 60 1/2	20% 60 3/4	20% 61	20% 61 1/4	20% 61 1/2	20% 61 3/4	20% 62	20% 62 1/4	20% 62 1/2	20% 62 3/4	20% 63	20% 63 1/4	20% 63 1/2	20% 63 3/4	20% 64	20% 64 1/4	20% 64 1/2	20% 64 3/4	20% 65	20% 65 1/4	20% 65 1/2	20% 65 3/4	20% 66	20% 66 1/4	20% 66 1/2	20% 66 3/4	20% 67	20% 67 1/4	20% 67 1/2	20% 67 3/4	20% 68	20% 68 1/4	20% 68 1/2	20% 68 3/4	20% 69	20% 69 1/4	20% 69 1/2	20% 69 3/4	20% 70	20% 70 1/4	20% 70 1/2	20% 70 3/4	20% 71	20% 71 1/4	20% 71 1/2	20% 71 3/4	20% 72	20% 72 1/4	20% 72 1/2	20% 72 3/4	20% 73	20% 73 1/4	20% 73 1/2	20% 73 3/4	20% 74	20% 74 1/4	20% 74 1/2	20% 74 3/4	20% 75	20% 75 1/4	20% 75 1/2	20% 75 3/4	20% 76	20% 76 1/4	20% 76 1/2	20% 76 3/4	20% 77	20% 77 1/4	20% 77 1/2	20% 77 3/4	20% 78	20% 78 1/4	20% 78 1/2	20% 78 3/4	20% 79	20% 79 1/4	20% 79 1/2	20% 79 3/4	20% 80	20% 80 1/4	20% 80 1/2	20% 80 3/4	20% 81	20% 81 1/4	20% 81 1/2	20% 81 3/4	20% 82	20% 82 1/4	20% 82 1/2	20% 82 3/4	20% 83	20% 83 1/4	20% 83 1/2	20% 83 3/4	20% 84	20% 84 1/4	20% 84 1/2	20% 84 3/4	20% 85	20% 85 1/4	20% 85 1/2	20% 85 3/4	20% 86	20% 86 1/4	20% 86 1/2	20% 86 3/4	20% 87	20% 87 1/4	20% 87 1/2	20% 87 3/4	20% 88	20% 88 1/4	20% 88 1/2	20% 88 3/4	20% 89	20% 89 1/4	20% 89 1/2	20% 89 3/4	20% 90	20% 90 1/4	20% 90 1/2	20% 90 3/4	20% 91	20% 91 1/4	20% 91 1/2	20% 91 3/4	20% 92	20% 92 1/4	20% 92 1/2	20% 92 3/4	20% 93	20% 93 1/4	20% 93 1/2	20% 93 3/4	20% 94	20% 94 1/4	20% 94 1/2	20% 94 3/4	20% 95	20% 95 1/4	20% 95 1/2	20% 95 3/4	20% 96	20% 96 1/4	20% 96 1/2	20% 96 3/4	20% 97	20% 97 1/4	20% 97 1/2	20% 97 3/4	20% 98	20% 98 1/4	20% 98 1/2	20% 98 3/4	20% 99	20% 99 1/4	20% 99 1/2	20% 99 3/4	20% 100	20% 100 1/4	20% 100 1/2	20% 100 3/4

PM > 10K INLB	0°	0°	0	0	2.5	A	Y		-	45°	-	6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

TABLE A52. (Continued)

PREPARED BY		CHECKED BY		DATE															
NASA-LARC TEST 230 14.5X31.75 VPM FULL-SPAN PROFUSIVE WING																			
RUN NO	CONFIGURATION	29 28 27 26 25 24 23 22 21 20 19 18 17 16 15 14 13 12 11 10 9 8 7 6 5 4 3 2 1	S_c	S_{F_w}	S_{F_c}	Scv Dmax	DOWN	M_c	M_{PR}	C_{M_w}	C_{M_c}	Q	α	β	REMARKS	$\frac{1}{2} S_{max}$	$\frac{1}{2} S_{min}$		
178	BC	-	1	-	0°	-	45°	Y	∞	2.5	0	.5	12.5	B	0°		1:50	3/4	
179	BC	-	1	-	0°	-	45°	Y	∞	2.5	0	1.0	6.0	B	0°		2:10	3/4	
180	B	-	-	-	-	-	-	-	∞	1.0	-	-	0	0°	0°	WT TARE	2:55	3/4	
181	B	-	-	-	-	-	-	Y	∞	1.0	0	0	3.0	B	0°		3:15	3/4	
182	BW	1/2	-	6	-	-	45°	-	∞	VMR	∞	0	0	0°	0°	PTING 1/2 PDL CALIB		3/4	
183	BW	1/2	-	6	-	-	45°	-	∞	E	∞	0	0	0°	0°	WT TARE + STATIC RUN		3/4	
184	BW	1/2	-	6	-	-	45°	-	∞	E	∞	0	0	0°	0°	STATIC RUN		3/4	
185	BW	1/2	-	6	-	-	45°	-	∞	VMR	∞	0	0	0°	0°	PTING 1/2 PDL CALIB		3/4	
186	BW	1/2	-	6	-	-	45°	-	∞	F	∞	0	0	0°	0°	STATIC RUN		3/4	
187	BW	1/2	-	6	-	-	45°	-	∞	1.0	0	0	3.0	B	0°		11:20	3/4	
188	BW	1/2	-	6	-	-	45°	-	∞	2.5	.5	0	28.7	B	0°		11:35	3/4	
189	BW	1/2	-	6	-	-	45°	-	∞	2.5	1	0	14.9	B	0°		11:35	3/4	
190	BW	1/2	-	6	-	-	45°	-	∞	2.5	2	0	7.5	B	0°		11:40	3/4	
191	BW	1/2	-	6	-	-	45°	-	∞	1.0	0	0	3.0	0°	B		11:40	3/4	
192	BW	1/2	-	6	-	-	45°	-	∞	2.5	.5	0	30.5	0°	B		11:40	3/4	
193	BW	1/2	-	6	-	-	45°	-	∞	2.5	2	0	7.6	0°	B		11:40	3/4	
194	BW	1/2	-	6	-	-	45°	-	∞	1.0	-	-	0	0°	0°	WT TARE (w/ 40 lb WTS)		3/4	
195	BW	1/2	-	6	-	-	45°	-	∞	G	∞	0	0	0°	0°	STATIC RUN		3/4	
196	BW	1/2	-	6	-	-	45°	-	∞	1.0	-	-	0	0°	0°	WT TARE (w/o 40 lb WTS)	1:45	3/4	
197	BW	1/2	-	6	-	-	45°	-	∞	G	∞	0	0	0°	0°	STATIC RUN		3/4	
198																		1:50 → + 11.0	
199																			
200																			
201																			

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OF POOR QUALITY

TABLE A52. (Continued)

PREPARED BY CHECKED BY DATE			NASA-LARC TEST 230 1A-21 21.75 VEH FULL-SPAN Pulsive WING										REMARKS		TIME	DATE
Run	Configuration	1/2	2/3	3/4	4/5	5/6	6/7	7/8	8/9	9/10	10/11	11/12	12/13	13/14	14/15	15/16
198	BW	1/2	-	-	-	-	-	-	-	-	-	-	-	DAL INTERFERENCE CUE RUN	3/4	
199	EW	1/2	-	-	-	-	-	-	-	-	-	-	-	"	3/4	
200	BW	1/2	-	-	-	-	-	-	-	-	-	-	-	"	3/4	
201	BWC	1/2	1	6	1	0°	45°	45°						WT TARE	3/4	
202	BWC	1/2	1	6	1	0°	45°	45°						STATIC RUN	3/4	
203	BWC	1/2	1	6	1	0°	45°	45°						"	3/4	
204														No Data w/ Tare??	3/4	
205	B													Sting Press Tare Run	3/4	
206														Model loading run w/ Jack	3/4	
207														"	3/4	
208														"	3/4	
209														"	3/4	
210														"	3/4	
211	P													"	3/4	
212	BWC	1/2	1	6	1	0°	45°	45°						STING PRESS TARE RUN	3/4	
213	BWC	1/2	1	6	1	0°	45°	45°						STATIC THROUST RUN N.G.	3/4	
214	BWC	1/2	1	6	1	0°	45°	45°						"	3/4	
215	BWC	1/2	1	6	1	0°	45°	45°						"	3/4	
216	BWC	1/2	1	6	1	0°	45°	45°						"	3/4	
217	BWC	1/2	1	6	1	0°	45°	45°						"	3/4	

PREPARED BY	
CHECKED BY	
DATE	

A-386

TABLE A52. (Continued)

SUB NO	CONFIGURATION	29% LEADING EDGE	20% TRAILING EDGE	27% TRAILING EDGE	30% TRAILING EDGE	33% TRAILING EDGE	SFC	SFW	SFE	SCV DOWN	NORM DOWN	M/E	M/R	C _m W	C _m C	Q	α	β	REMARKS	TIME
237	BWC	1/2	1	6	1	0°	0°	0°	0°			∞	1.0	-	-	0	0°	0°	WT TAKE	24
238	BWC	1/2	1	6	1	0°	0°	0°	0°			∞	1.0	-	-	0	0°	0°	WT TAKE	24
239	BWC	1/2	1	6	1	0°	0°	0°	0°			∞	VARY ∞	∞	∞	0	0°	0°	STATIC RUN	24
240	BWC	1/2	1	6	1	0°	0°	0°	0°	Y		∞	1.0	0	0	30 A	0°	0°		24
241	BWC	1/2	1	6	1	0°	0°	0°	0°	Y		∞	2.0	.5	.31	21.1 B	0°	0°		24
242	BWC	1/2	1	6	1	0°	0°	0°	0°			∞	2.0	1.0	.66	10.4 B	0°	0°		24
243	B																		CHANGE TO TENT STING	24
244																			STING-PRESS TAKE RUN	24
245																			? POSSIBLY XDCER CALIB	24
246																			? POSSIBLY HGT & α CALIB	24
247	B																		? PLEN PRESS "	24
248	BWC	1/2	1	6	1	0°	0°	0°	0°			∞	VARY ∞	∞	∞	0	0°	0°	STING-PRESS TAKE RUN	24
249	BWC	1/2	1	6	1	0°	0°	0°	0°			∞	1.0	-	-	0	0°	0°	STATIC RUN	24
250	BWC	1/2	1	6	1	0°	0°	0°	0°			∞	2.0	.5	.28	17.5 B	0°	0°	WT TAKE	24
251	BWC	1/2	1	6	1	0°	0°	0°	0°			∞	2.4	1.0	.54	12 B	0°	0°		24
252	BWC	1/2	1	6	1	0°	0°	0°	0°			∞	2.4	2.0	1.1	6 B	0°	0°		24
253	BW	1/2	-	6	-	-	-	0°	-			∞	VARY ∞	∞	-	0	0°	0°	Wing PITCH as Prev Calib	24
254	BW	1/2	-	6	-	-	-	0°	-			∞	1.0	-	-	0	0°	0°	WT TAKE	24
255	BW	1/2	-	6	-	-	-	0°	-			∞	2.4	∞	0	0	0°	0°	STATIC RUN	24

TABLE A52. (Concluded)

[illegible]

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16. Abstract A full span model of a wing/canard concept representing a fighter configuration has been tested at STOL conditions in the NASA Langley 4 x 7 meter tunnel. The results of this test are presented, and comparisons are made to previous data of the same configuration tested as a semispan model. The potential of the propulsive wing/canard to develop very high lift coefficients was investigated with several nozzle spans (nozzle aspect ratios). Although longitudinal trim was not accomplished with the blowing distributions and configurations tested, the propulsive wing/canard appears to offer an approach to managing the large negative pitching moments associated with trailing edge flap blowing. Also presented are data showing the effects of large flap deflections and relative wing/canard positions. Presented in the appendix to the report are limited lateral-directional and ground effects data, as well as wing downwash measurements.		
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